Brisbane City Council BCC

CLAYTON UTZ-(BCC - COLIN JENSEN - 5TH STATEMENT) #1698022, SM #1697201, ZIP#1698033 File 540236/1 Volume 1 OF 6 ORIGINAL

Queensland Floods Commission of Inquiry Inquiry

Fifth Statement of Colin David Jensen - 31 August 2011

Volume 1 of 6

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Our reference /80117397

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10/11/11

Exhibit Number:

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Fifth Statement of Colin David Jensen

- I, Colin David Jensen, Chief Executive Officer, of 266 George Street, Brisbane, in the State of Queensland, state on oath as follows:
- A. Attachment "CDJ-30" is a copy of a notice from the Commissioner of the Queensland Floods Commission of Inquiry (Commission) dated 10 August 2011 requiring me to provide certain information to the Commission in the form of a statement by 1 September 2011 (Notice). This Statement is provided in response to the Notice.
- B. For the purposes of responding to the Notice and preparing this Statement I have, in my position as Chief Executive Officer of the Brisbane City Council (Council), had access to:
 - (a) the business records of Council; and
 - (b) Council officers,

to obtain information to provide a response to the Notice. Unless otherwise stated, the matters set out in this Statement are based on my own knowledge or the information derived from the above sources. This Statement responds in detail to specific matters raised by the Notice. I have necessarily relied on Council officers to assist me in preparing this statement. While I am familiar with the matters dealt with in this statement, I am Chief Executive Officer of a large organisation and therefore I am not necessarily familiar with all of the detail.

- C. I set out below my responses to each of the questions set out in the Notice.
- D. The documents from the above sources and attached to this Statement have been collated by Council officers under my instruction.
- 1. Whether all documents requested by the Requirement dated 1 March 2011 have been provided to the Commission
- 1.1 From the information provided to me by Council officers, I believe the Requirement dated
 1 March 2011 has been complied with in all material respects. If the Commission believes
 otherwise and identifies the documents, I will ensure that the documents are made available to the
 Commission.



- The details of any draft flood studies obtained or made available to the Council since March
 2011
- 2.1 Council has commissioned several flood studies which are currently in progress and at varying stages of completion. To my knowledge, the flood studies contained in Table A below were obtained in the ordinary course of Council's business and not in response to, or for the purposes of assessment of, the January 2011 Flood Event.
- 2.2 In respect of some studies, preliminary technical reports have been drafted, whilst other studies are still at hydraulic/hydrologic modelling stage and an accompanying technical report has yet to be completed.
- 2.3 Those studies "in progress" or "completed to preliminary report stage" since March 2011 are listed in Table A and copies of the studies appear (in the order set out in Table A) at Attachment "CDJ-31" to this Statement (Studies).
- 2.4 In accordance with Council's standard practice, the Studies:
 - (a) that are "completed to preliminary report stage":
 - (i) have not yet been reviewed by independent peer reviewers or by officers within Council's Water Resources Branch;
 - (ii) are likely to be revised and amended further before becoming final for review and endorsement by the Council's Chair of Environment and Sustainability;
 and
 - (iii) will then proceed to approval by the appropriate level of Council,
 - (b) that are "in progress" are still at early draft stages and are yet to be reviewed by senior engineers. It is anticipated that significant technical work still needs to be undertaken and major amendments could be made before reaching preliminary report stage.

Table A

Flood Study	Status	BCC File Name	Exhibit CDJ-31 Barcode Reference
Bulimba Creek Flood	Preliminary Draft	Bulimba Creek Flood Study Preliminary	BCC.079.0950
Study		Draft.pdf	BCC.079.1050

Taigum Channel Flood Study	Work In progress – preliminary documentation yet to reviewed by Senior Engineers	W041720- PR001Ahz_Taigum Drain Flood Study_In Progress.pdf	BCC.079.0271
Carseldine Channel Flooding Investigation	Preliminary Draft	W3051461- PR001Etl_Carseldine_Ch annel_Report_Preliminar y Draft.pdf	BCC.079.0117
Albany Creek Flood Study	Work In progress – preliminary documentation yet to reviewed by Senior Engineers	Albany Creek Study_Part 1 of 2_ In Progress.pdf Albany Creek Study_Part 2 of 2_ In Progress.pdf	BCC.079.0394 BCC.079.0451
Perrin Creek Flooding Investigation	Work In progress – preliminary documentation yet to reviewed by Senior Engineers	W3060314- RE002hz_Perrin_Creek_I nvestigation_In Progress.pdf	BCC.079.0187
Stable Swamp Creek	Work In progress – preliminary documentation yet to reviewed by Senior Engineers	StableSwampFloodStudy _ReportA_Calibration_In Progress.pdf StableSwampFloodStudy _ReportB_Design_Event _Modelling_In Progress.pdf StableSwampFloodStudy _ReportC_MitigationRep ort_In Progress.pdf	BCC.079.0505 BCC.079.0598 BCC.0790.754

- Any changes to the Council's land planning processes, policies or other statutory instruments in response to flooding that occurred during the period 1 December 2010 to 31 January 2011, including drafts, considerations and adopted documents of Council
- 3.1 Council, as a matter of course, continually reviews and revises its land planning policies and processes. Since the January 2011 Flood Event, a number of specific initiatives have been undertaken by Council in response to flooding, including the following (which have been completed):
 - (a) the report by the Joint Flood Taskforce dated 8 March 2011 (JFTF Report);

(b) the report by the Flood Response Review Board released 24 May 2011 (FRRB Report);

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- (c) Council's Flood Action Plan (Action Plan):
 - (i) was originally developed, and sets out the actions Council proposes to take, in response to the recommendations in the FRRB Report. The original Action Plan was released to the public on 24 June 2011;
 - (ii) was updated to take into account the findings and recommendations in the Commission's Interim Report and was released to the public on 16 August 2011; and
 - (iii) will be further updated to take into account the findings and recommendations in the Commission's Final Report proposed to be released in February 2012.
- 3.2 The above Reports and Action Plan outline a large number of measures Council has taken or intends to take in response to the January 2011 Flood Event, and include recommended changes to planning processes, policies and other statutory instruments.
- 3.3 Attached to this Statement are copies of:
 - (a) the report of the JFTF Attachment "CDJ-32";
 - (b) the FRRB report Attachment "CDJ-33" and
 - (c) the Action Plan (as amended to incorporate recommendations from the Commission's Interim Report) Attachment "CDJ-34".
- 3.4 Changes to Council's land planning processes, policies and other statutory instruments in response to flooding fall into two categories:
 - (a) responses which were undertaken solely or mainly in response to the January 2011 Flood Event; and
 - (b) responses which comprise changes to processes or plans which were already underway or planned, and which Council is also now taking into account in its response to the January 2011 Flood Event.

Category 1 - New planning initiatives in response to the January 2011 Flood Event

3.5 In light of the January 2011 Flood Event, Council requested the JFTF in early February 2011 to determine (within 30 days) what interim standards should be used to enable new development and

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	e (within 30 days) what		e (within 30 days) what interim standards should be used to enable new

redevelopment to proceed with confidence and certainty until the Commission issues its final report. The JFTF Report recommended that Council put in place interim flood levels and standards for the purposes of development assessment.

Temporary Local Planning Instrument

- 3.6 The interim measure taken by Council was the creation of the *Temporary Local Planning Instrument 01/11 Brisbane Interim Flood Response* which was endorsed by Full Council on 10 May 2011 and was effective from 16 May 2011 (**TLPI**). Attachment "**CDJ-35**" is a copy of the TLPI.
- 3.7 The TLPI applies to the land affected by the January 2011 Brisbane River flooding as well as by waterway or creek flooding.
- 3.8 The TLPI is effective for up to 12 months and prevails over the current Brisbane City Plan 2000 when an inconsistency arises. It is my understanding that a TLPI may only be approved in the first instance as a matter of statute for up to 12 months. That is the explanation for the expiry date on the current TLPI. It is also my understanding that an extension of the period of validity of the TLPI may be granted on application to the State. It is likely, in my opinion, that an extension will be required and/or will be highly desirable from the perspective of a full and proper consideration of the final response of Council to the January 2011 Flood Event and the Commission's final recommendations.
- 3.9 In response to a letter from the Minister for Local Government and Planning dated 27 April 2011 (see TLPI Chronology below), Council has begun to draft a full City Plan amendment to reflect the changes effected by the TLPI.
- 3.10 Members of the public can access information as to whether the TLPI covers their property by accessing the TLPI maps on the Council website.
- 3.11 In summary, the new planning provisions introduced by the TLPI:
 - introduce the concept of an Interim Residential Flood Level (IRFL) which requires building levels to be increased;
 - (b) allow building heights to increase in response to the IRFL;
 - (c) require the location of essential services (electricity supply, telecommunications, fire services, etc) to be either higher than the IRFL or sufficiently waterproofed;



- (d) state that filling and retaining walls must not create local drainage problems or cause amenity issues; and
- (e) determine instances where resilient building materials will have to be used in developments.
- 3.12 A chronology of events leading up to the adoption of the TLPI is set out below. Attached and marked "CDJ-36" is a bundle of documents which reflect the process followed in developing the TLPI and the decisions made in respect of it.

TLPI Chronology

Draft Joint Flood Taskforce (JFTF) report presented to Establishment and Coordination Committee (E&C).		
cil officers met with Queensland State Government officers to iate TLPI timelines and process.		
City Planning, Water Resources and Development Assessment staff met to scope TLPI content.		
ntation of draft TLPI content to Council's Planning Guidance nittee.		
workshop with State colleagues.		
City Planning, Water Resources and Development Assessment staff hold workshop to finalise TLPI content.		
Draft TLPI presented to Town Planning Sub-Committee (TPSC).		
Draft TLPI presented to E&C Strategy.		
Councillor briefings take place prior to full Council consideration.		
11 Full Council endorses TLPI.		
delivered to Queensland Government.		
nsland Reconstruction Authority (QRA) briefed on draft TLPI.		
from Queensland Government requiring a number of modifications draft TLPI.		
nt workshop with Building Codes Queensland (BCQ) on TLPI flood nce provisions.		
ril 2011 Further meeting with Queensland Government to negotiate requested modifications.		

Date	Event		
15 April 2011	TLPI presented to external Development Industry Forum.		
18 April 2011	Response to request for modifications delivered to Queensland Government.		
19 April 2011	Lord Mayor briefed on the proposed TLPI.		
20 April 2011	Independent Design Advisory Panel (IDAP) briefed on Resilient Building Design requirements of TLPI.		
27 April 2011	Letter received from Minister – permission to adopt TLPI.		
3 May 2011	E&C formal resolves to adopt TLPI.		
7/8 May 2011	Water Resources & Information Services Branch worked over the weekend to extract flood level database from flood mapping to inform Flood Wise Property Report (FWPR).		
10 May 2011	Full Council endorses TLPI.		
16 May 2011	TLPI goes live.		

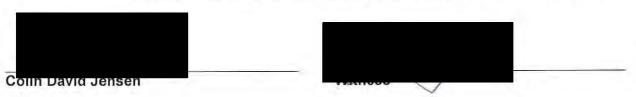
Updated FloodWise Property Report system

- 3.13 Following the January 2011 Flood Event, Council liaised closely with the Queensland Reconstruction Authority (QRA) and the Department of Environment and Resource Management in determining and refining the estimated extent of the January 2011 Flood Event, which was used to partly define the extent of the TLPI coverage.
- 3.14 The estimated flood depth was then modelled by Council engineers in order to provide a best estimate of the January 2011 Brisbane River flood level. The January 2011 Brisbane River flood level information was combined with existing information about flood levels and risk at each affected property and made publicly available via an update to Council's FloodWise Property Report. Attachment "CDJ-37" is an example of an updated FloodWise Property Report.

Changes to development assessment planning processes and services.

- Following the January 2011 Flood Event, Council sought to assist building owners, consultants, and builders by:
 - (a) providing free pre-lodgement meetings (for development applications), a telephone hotline, a flood enquiries email address, on-site meetings and published fact sheets to

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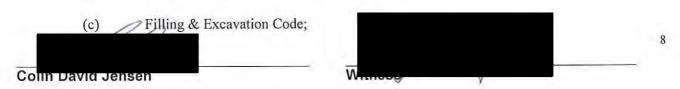
give advice on the options relating to individual buildings affected by the January 2011 Flood Event;

- (b) applying a facilitative approach for development that was "building work for the restoration to its original condition of any building that has been accidentally damaged or destroyed". The effect of this approach is that the development is exempt and does not require a development application to be made to Council for approval;
- (c) for those instances requiring a development application, providing a reduction in application fees and a fast-tracking assessment and decision; and
- (d) adopting a risk-tolerant approach to allow many low impact businesses affected by flooding of their premises to temporarily relocate to the business owner's home and be treated as a temporary home business.

<u>Category 2 - Existing or scheduled planning initiatives incorporating response to the January 2011</u> Flood Event

Status of the New City Plan - new Flood Code

- 3.16 Council has begun, as a matter of ordinary Council business, the necessary groundwork to prepare a new planning scheme (also known as the City Plan) for Brisbane. The nature of the development of the City Plan requires consultation which will not commence until mid 2012. Therefore, drafting of the City Plan is scheduled to commence after consideration of the Commission's final report. It is intended that the new City Plan will contain the following aspects relevant to flooding:
 - upgraded Strategic Plan principles for managing risk to people and property from flooding;
 - (b) reviewed and updated provisions to manage flood hazard from river, creek, overland flow, and storm tide; and
 - (c) updated provisions for managing cumulative impacts from filling and development.
- 3.17 At this stage, it is intended that the flood hazard provisions being developed for the new City Plan will include amendments to provisions in the following City Plan 2000 Codes:
 - (a) House Code;
 - (b) Compensatory Earthworks Planning Scheme Policy;



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	(a)	Flood Wise Property Reports on the Council internet site; Flood Flag Maps on the Council internet				
4.2	Counci	I provides information about flood risk for specific properties through the following means:				
Public	y available	e information				
4.1	to the in	o Council's Initial Submission dated 1 April 2011 at paragraphs 2.3, 5.4 and 5.7 which refers a formation Council makes available to members of the public regarding flood information c. This information is still current as at the date of this Statement.				
	(c)	prospective developers and their representatives.				
	(b)	insurance companies;				
	(a)	members of the public;				
4.		formation about flood risk for specific properties is made available and any processes for ing this information applicable to each of the following:				
		is released in February 2012. It is my understanding that the prime purpose of the Flood to consolidate the various assessment criteria that relate to flooding into a single Code.				
3.20	The nev	The new Flood Code for inclusion in the City Plan will be finalised after the Commission's Final				
3.19	With regard to Brisbane River flooding, the preparation of these provisions will be informed by the recommendations and direction of the Joint Flood Taskforce, the Flood Response Review Board, and the Commission.					
3.18	In addit	tion to these updates, a new Flood Code will be prepared for inclusion in the new City Plan.				
	(j)	Subdivision & Development Guidelines.				
	(i)	Child Care Facility Code; and				
	(h)	Park Planning & Design Code;				
	(g)	Waterway Code;				
	(f)	Structure Planning Code;				
	(e)	Subdivision Code;				
	(d)	Stormwater Management Code (where relevant to flood hazard);				

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- (c) Flood study reports available through Council libraries;
- (d) Flood models available to the industry;
- (e) Council's Brisbane River Flood Forecast Reporting System which allows the Council Contact Centre to provide property specific information regarding flood levels to Brisbane residents; and
- (f) the Early Warning Alert Service transmitted by SMS, email or landline to Brisbane residents.

FloodWise Property Report

- 4.3 As set out above, the flood information provided in the FloodWise Property Report has been updated since the January 2011 Flood Event. In general terms, information is sourced from Council flood studies and models undertaken for the river, and major creeks and waterways. It is designed so residents and professionals can assess the estimated flood risk of a property and make informed decisions when buying, renting, building or renovating, as well as adhere to Council building regulations.
- 4.4 Depending on the flood risks associated with a property, the report may include the following:
 - (a) January 2011 River flood levels;
 - (b) estimated flood levels for the 20%, 5%, 2% and 1% AEP events;
 - (c) source of flooding including river, creek, defined overland flow or storm tide;
 - (d) minimum and maximum ground levels;
 - (e) minimum habitable floor level for building and development; and
 - (f) whether a property is located within a waterway corridor or is a large allotment, that is, over 1000 square metres.

Flood Flag Maps

4.5 Flood Flag Maps show all known sources of flooding in Brisbane, including creek, river, stormtide and overland flow flooding. Flood Flag Maps build on existing information from hydraulic modelling and use computer generated mapping to show areas that may flood in a period of intense rainfall or extreme storm events. Flood Flag Maps show flooding that has between a 1% - 2% chance of occurring each year.

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Flood Studies

4.6 A number of flood study reports are publically available through Council libraries. Council engineers also provide technical responses to resident's queries regarding flood risk received via the Contact Centre or Council's email.

Flood Models

4.7 By request, flood models are available to industry. Under the current arrangements, all requests are directed to City Projects Office, Flood Management Team. A data agreement form ("Request for BCC Computer Model") is completed. The model is provided subject to the terms and conditions as outlined in the request form. The models generally provide broadscale flood information rather than information on specific properties, and is generally used and modified by experienced flood modelling professionals for specific projects.

Early Warning Alert Service

- 4.8 Council has an Early Warning Alert Service which provides early notifications for residents, who have registered for this service, potentially impacted by:
 - (a) creek flooding; and/or
 - (b) severe storm events.
- 4.9 Information is provided via SMS, email and/or phone message to landline. This system is registration-based and free to residents of Brisbane.
- 4.10 Council uses information derived from its FloodWise software system to provide data for the Early Warning Alert Service relevant to creek flooding.
- 4.11 The FloodWise software system is a graphical display of real-time on-line information derived from data collected by telemetry that monitors creek and river water level recorders and rainfall gauges across Brisbane. FloodWise:
 - (a) records water level data at various sites across Brisbane;
 - (b) cross-references this data with road heights and levels at which communities may become flooded or isolated;
 - (c) through the website, indicates the flood status of the roads;



- (d) as roads are threatened or become closed due to rising flood levels, SMS and email notifications are automatically issued to registered users;
- (e) is aimed at providing threat-specific information regarding flash flooding events; and
- (f) provides information to assist Council response operations during weather-related events.

Specific Information provided during a flood event

- 4.12 The sources of information set out in 4.2 above are available to members of the public at all times.
- 4.13 In addition, during a flood event, Council makes use of its "Bender" model to determine local flood height information. Mr Ken Morris, Director of Council's Flood Information Centre describes the model, its inputs and outputs in his second statement dated 3 May 2011 (at paragraph 3). The Bender model is "live" in the sense that it can be run by reference to changing BoM predictions as they are updated and received. Council also prepares in advance "static" inundation maps for specific river flows. One example is the 12,000 cumecs map provided to the public prior to the peak of the flood event.
- 4.14 Council made use of the Bender modelling approach in the January 2011 Flood Event to communicate with residents as follows:
 - (a) First, Council made property-specific information available to residents on each occasion that the Bender model and associated Brisbane River Flood Forecast System was revised by reference to revised BoM predicted River levels. It made that information available through Council's Contact Centre, usually within 20 minutes or so of receiving revised levels from BoM. A person calling the Contact Centre and specifying their address was told the predicted depth on the highest and lowest points of their property and when the peak level was forecast to occur;
 - (b) Second, Council used Bender to produce lists of streets and suburbs likely to be inundated. These lists were updated and broadcast to the public from time to time. This information was distributed by Council through various channels including social networking services, television, radio and print media, Council's website, Community Service Announcements, doorknocking of residences and premises, posters, letter box drops and pamphlets placed on cars; and
 - (c) Third, Council made use of Bender output (and of maps of flood inundation previously prepared) to publicise by reference to a map of the City likely areas of inundation.

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Insurance Companies

- 4.15 Over the past 3 years, Council (as a result of the Lord Mayor's Flood Taskforce, details of which may be found at www.brisbane.qld.gov.au) has been working with the Insurance Council of Australia (ICA) to provide Council's flood risk data to ICA.
- 4.16 Council has supplied detailed flood levels and ground level survey data to assist with the ICA's National Flood Information Database (NFID) project. The data was requested in October 2010 and was provided to ICA by Council in December 2010.
- 4.17 The aim was to provide information to assist the insurance market with its underwriting process in pricing flood risk and offering flood cover to policy holders. This information was already publically available on-line and free of charge through Council's Floodwise Property Reports (which exist for each individual property that is subject to flooding) and Flood Flag Maps (which exist for every Brisbane suburb that is subject to flooding).
- 4.18 During the January 2011 Flood Event, predicted flood maps were requested and provided to the ICA via the Local Disaster Coordination Centre and the office of the Chief Executive Officer.
- 4.19 In addition to the publicly available information set out above, Council has (and will when requested) provide access to its MIKE 11 2003/2004 model.
- 4.20 By way of example, Council, in response to a recent request, is currently facilitating access to its MIKE 11 2003/2004 model for the ICA and member insurers on Council's standard terms and conditions.
- Whether and to what extent Council's infrastructure (for example, sewers, roads, stormwater) was affected by flooding that occurred during the period 1 December 2010 to 31 January 2011, citing specific examples where possible
- 5.1 The effect of the flooding on Council's infrastructure assets can be described in two ways;
 - (a) loss of the asset (for example, Riverwalk); or
 - (b) assets which were temporarily out of service or partially damaged (for example, silt build-up in stormwater drains which have been, or are in the process of being, cleaned out by Council).
- Attachment "CDJ-38" is a copy of Council's Damage Assessment Matrix (Matrix) as at 19 August 2011. The Matrix is a register of the estimated cost to restore essential public assets, and shows that the estimated restoration cost to Council infrastructure damaged as a result of the January 2011

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Flood Event is approximately \$400 million. This compares with the value of Council's infrastructure at around \$24 billion.

- 5.3 The restoration cost was mitigated by Council acting in accordance with its Business Continuity Plans (BCPs). Examples of the actions taken to mitigate the effects of the January 2011 Flood Event include:
 - (a) removing traffic signal control equipment during the flood event;
 - (b) removing parking meters during the flood event;
 - (c) educting storm water pipes;
 - (d) relocating computer archives from West End;
 - (e) pre-positioning of sandbags to protect infrastructure;
 - (f) relocating CityCats and City Ferries;
 - (g) relocating Council cars from Basement 2 of Brisbane Square; and
 - (h) relocating library books from Fairfield Library.
- 5.4 A copy of the BCP's referred to above are located at Attachment "CDJ-39".
- While Council has its own engineers who undertook preliminary damage assessment and estimates, a decision was made to also engage independent consultants to prepare reports on the damage to Council infrastructure.
- Council has obtained a report from Cardno (Qld) Pty Ltd (Cardno) dated April 2011, advising Council on how Council's infrastructure (the categories of which are set out in the report and listed in paragraph 5.7 below) was damaged during the January 2011 Flood Event and providing recommendations as to how such damage can be mitigated in the future (Cardno Report).

 Attachment "CDJ-40" is a copy of the Cardno Report. The Cardno Report is a final draft, but it has not yet been finalised. Council is currently collating comments in relation to the Cardno Report and it will be finalised.
- 5.7 The Cardno Report addresses the following categories of Council infrastructure:
 - (a) Roads, footpaths and kerbs;

(b) Traffic signals;

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- (c) Stormwater drainage and enclosed pipes;
- (d) Riverwalls and earthen slopes;
- (e) Parks (park infrastructure and landscaping);
- (f) Trees (park and street);
- (g) Community leased assets (sports clubs and fields);
- (h) Ferry terminals; and
- (i) Pontoons.
- Council has also obtained a report from Arup Pty Ltd (Arup) in relation to damage to the New Farm Riverwalk (Arup Report). Council is now consulting with the public regarding the alternative concept designs for its replacement. Attachment "CDJ-41" is a copy of the Arup Report.

6. For 5, details of the reconstruction of this infrastructure including costs and programs

- 6.1 The reconstruction of Council infrastructure is well-advanced which is demonstrated by the documents contained in Attachment "CDJ-42", being a bundle of Sub Committee Reports to the Lord Mayor's Recovery Task Group in August 2011.
- 6.2 In addition to restoring Council infrastructure, Council has provided funding to a number of community groups for the repair of community infrastructure which is not owned by Council but provides benefits to residents. Attachment "CDJ-43" comprises:
 - (a) Community Facility Flood Recovery List as at 15 February 2011, being an estimate of the cost of repair of the community facilities at that date;
 - (b) Community Facility Flood Recovery List as at 16 August 2011, being an estimate of the cost of repair of the community facilities at that date; and
 - (c) a schedule of grants provided to community facilities by Council.

7. Funding arrangements for repairs to damaged Council infrastructure

7.1 The repairs required to Council Infrastructure and assets damaged during the January 2011 Flood Event are proposed to be funded from various sources including:



(b) Australian and Queensland Government Funding administered through the Queensland Reconstruction Authority.

Council's Budget

- 7.2 Immediately following the January 2011 Flood Event, Council officers identified flood damage to Council assets and compiled an indicative estimate of the flood damage. This initial estimate was completed by the end of January 2011. The damage estimate was jointly reviewed by the members of the Establishment and Co-ordination Committee and the members of the Executive Management Team in mid February 2011 to consider flood funding strategies. The funding strategies considered primarily focused on the cessation or deferral of both operating activities and capital projects across the following 5 year period.
- 7.3 The deferral or cessation of projects and activities as part of the flood funding strategy was implemented immediately. This flood funding strategy was predicated on the assumption that deferred and deleted projects would be considered for reinstatement as part of the budget process as grant funding becomes available.
- 7.4 The flood funding strategy has been maintained in the subsequent budget process for the 2011/12 Budget.
- 7.5 Attachment "CDJ-44" is a bundle of documents relating to Council's budget initiatives. This bundle comprises:
 - (a) a presentation entitled "Flood Special Budget Review" dated 11 February 2011;
 - (b) a memorandum entitled "2010-11 Third Budget Review" dated 25 March 2011;
 - (c) a presentation entitled "2010-11 Third Budget Review" dated 1 April 2011;
 - (d) a memorandum entitled "2010-11 Third Budget Review" dated 7 April 2011;
 - (e) a presentation entitled "2010-11 Third Budget Review" dated 13 April 2011; and
 - (f) a submission to the Establishment and Co-ordination Committee entitled "2010-11 Budget - Third Review "Flood Mini-Budget" dated 27 April 2011.
 - 7.6 In addition to funding the repair of its own infrastructure, the former Lord Mayor set up a relief fund to support Brisbane's recovery after the January floods, known as the Lord Mayor's Community Disaster Relief Appeal Fund (Relief Fund). This Relief Fund has Deductible Gift



7.7 As at 18 August 2011, the Relief Fund had received total donations of \$1,090,934. Council had distributed \$785,000 of those funds to 19 clubs and community organisations, leaving a balance of \$308,795 yet to be distributed. It is my understanding, that the Board and Management of the Relief Fund is meeting on 6 September 2011 and they intend to disburse these remaining funds in accordance with the eligibility criteria. I understand that previous donors to the Relief Fund are considering further contributions. Attachment "CDJ-45" is a schedule of the amounts of grants distributed.

Australian and Queensland Government funding through the Queensland Reconstruction Authority (QRA)

- 7.8 Following the Queensland Government activation of the Australian Government's National Disaster and Relief Recovery Arrangements (NDRRA) for the January 2011 Flood Event, Council provided an estimate of damage to QRA. As this estimate was in excess of the trigger point, Council is entitled to apply for grants under the NDRRA. Council has incurred expenditure within the categories of:
 - (a) Counter Disaster Operations (CDO);
 - (b) Emergent Works (EW); and
 - (c) Restoration of Essential Public Assets (REPA).
- 7.9 Claims under the CDO and EW which have been approved by the QRA have been offset against the advance provided in 2010/11 of \$85m. The balance of the advance not offset will be utilised for REPA claims which will be lodged on a monthly basis for each project following project approval by QRA.
- 7.10 Attachment "CDJ-46" is a summary of the Claims Submitted by Council to the QRA (arranged by NDRRA Classification) as well as the current status of those claims as at 25 August 2011.
- 7.11 Attachment "CDJ-47" is a bundle of documents relating to Council's interaction with the QRA.

 This bundle comprises the following documents:

Document Description		Date	CDJ-49 Barcode reference
Email	(QRA) to C Jensen (enclosing letter)	24.02.11	BCC.091.0004
Draft Business Case		March 2011	BCC.091.0020

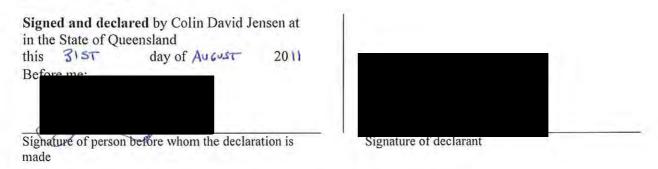
Letter QRA to BCC	11.03.11	BCC.091.0010
Letter BCC to QRA (enclosing Attachments A - C)	11.03.11	BCC.100.5681
Letter BCC to QRA	16.03.11	BCC.100.5694
Letter QRA to BCC (enclosing Recipient Created Tax Invoice)	23.03.11	BCC.100.5724
Letter QRA to BCC (enclosing Recipient Created Tax Invoice)	23.03.11	BCC.091.0017
Letter QRA to BCC	01.04.11	BCC.091.0008
Letter BCC to QRA	25.05.11	BCC.091.0015
Letter QRA to BCC	03.06.11	BCC.091.0028
Letter QRA to BCC	03.06.11	BCC.091.0030
Letter QRA to BCC	08.06.11	BCC.091.0029
Letter BCC to QRA	10.06.11	BCC.100.5866
Letter QRA to BCC	20.06.11	BCC.100.5727
Extract from BCC 2010/11 Annual Financial Statements	June 2011	BCC.091.0003
Letter QRA to BCC (enclosing Assessed Submissions Schedule)	16.08.11	BCC.091.0031

- 8. Any policies or other documents which require property owners to have an evacuation plan and/or route in the case of flooding
- 8.1 I am aware that Mr Martin Reason, Acting Planning Manager of City Planning & Economic Development has received a Requirement to Provide Information which also requests that he consider the subject matter of this question from the Commission. In those circumstances, and given Mr Reason holds expertise in the area of planning, I consider he is more qualified to provide information regarding the planning policies or documents referred to in this question.
- 8.2 In general terms, I am aware that Council's planning approvals routinely require compliance with all (largely State-based) legislative and regulatory requirements regarding building safety and evacuation. I am not aware of any such requirements in relation to flooding at this time.



I make this statement conscientiously believing the same to be true, and by virtue of the provisions of the Oaths Act 1867 (Qld).

Dated 31 August 2011



Full name and qualification of person before whom the declaration is made

Our ref: Doc 1675963

10 August 2011

Mr Colin Jensen Chief Executive Officer Brisbane City Council C/- Clayton Utz

Attn:

REQUIREMENT TO PROVIDE STATEMENT TO COMMISSION OF INQUIRY

I, Justice Catherine E Holmes, Commissioner of Inquiry, pursuant to section 5(1)(d) of the Commissions of Inquiry Act 1950 (Qld), require Mr Colin Jensen to provide a written statement, under oath or affirmation, to the Queensland Floods Commission of Inquiry, in which the said Mr Jensen:

- provides all information in his possession and identifies the source or sources of that information;
- makes commentary and provides opinions he is qualified to give as to the appropriateness of particular actions or decisions and the basis of that commentary or opinion;

in respect of the following:

- 1. whether all documents requested by the Requirement dated 1 March 2011 have been provided to the Commission;
- 2. the details of any draft flood studies obtained or made available to the Council since March 2011;
- 3. any changes to the Council's land planning processes, policies or other statutory instruments in response to flooding that occurred during the period 1 December 2010 to 31 January 2011, including drafts, considerations and adopted documents of Council;
- 4. how information about flood risk for specific properties is made available and any processes for obtaining this information applicable to each of the following:
 - a. members of the public;
 - b. insurance companies;
 - c. prospective developers and their representatives;
- whether and to what extent Council's infrastructure (for example, sewers, roads, stormwater) was affected by flooding that occurred during the period 1 December 2010 to 31 January 2011, citing specific examples where possible;
- 6. for 5, details of the reconstruction of this infrastructure including costs and programs;
- 7. funding arrangements for repairs to damaged Council infrastructure;

8. any policies or other documents which require property owners to have an evacuation plan and/or route in the case of flooding.

Mr Jensen may also address other topics relevant to the Terms of Reference of the Commission in the statement, if he wishes.

The statement is to be provided to the Queensland Floods Commission of Inquiry by 5pm, 1 September 2011.

The statement can be provided by post, email or by arranging delivery to the Commission by emailing info@floodcommission.qld.gov.au.

Commissioner

Justice C E Holmes

1. Holmes

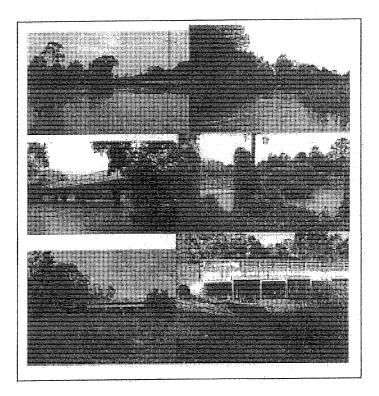


Bulimba Creek Flood Study

June 2011

Prepared for Water Resources

Prepared by: Water and Environment City Design



Prepared by

Flood Management
Water & Environment
City Design

for

Brisbane City Council Water Resources

Approved for Information

Julie McLellan Manager, Water Resources

Bulimba Creek Flood Study

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Dedicated to a better Brisbane



Bulimba Creek Flood Study Executive Summary

June 2011

Prepared for Water Resources

Prepared by Water and Environment City Design

Executive Summary

Introduction

Bulimba Creek is one of Brisbane's major creek systems. Its catchment covers an area of 125 km² and includes a number of Brisbane's southern and eastern suburbs. Bulimba is the second largest of Brisbane's creeks with only Oxley Creek being larger with an area of 258 km². The creek originates at an elevation of approximately 70m AHD (Australian Height Datum) in Stretton, northwest of the Gateway Motorway. It then flows through the suburbs of Runcorn, Sunnybank, Macgregor, Eight Mile Plains, Wishart, Mansfield, Carindale, Carina and Tingalpa before discharging into the Brisbane River at Murarrie. The majority of the main channel remains in a relatively natural state.

The tributaries of Bulimba Creek are only partly retained in their natural condition with many sections being heavily modified. The main tributaries and their respective catchment areas are listed below. A catchment location map of Bulimba Creek and its main tributaries is shown in Figure 1.

	i i i	
Tributary		Catchment\
	1 1 1	Area(km²)
Mimosa Creek	1 17 7 7	6.8
Bulimba Creek East Arm		14.8
Newnham Road Tributary (no formal	name)	3.8
Spring Creek		5.0
Salvin Creek		5.4
Phillips Creek	ar Artistan	4.2
Tingalpa Channel (no formal name)		13.2
Hemmant Channel (no formal name)		6.9
Lindum Creek		4.8

The Bulimba Creek Catchment is long and narrow, with a steeper gradient in its upper reaches and flatter/wider flood plains in the lower reaches. The lower reaches of the Creek meander extensively and are tidally influenced.

Most of the catchment is residentially developed with some industrial and commercial zones though some rural and bushland areas also exist. There are frequent transport crossings of the main waterway including road and rail bridges, pedestrian/bikeway bridges and causeways.

Records of flood levels along Bulimba Creek have been collected since the 1960s. A major flood study was prepared in the early 1990s to estimate flood discharges and likely flood levels and extents. Since this time more comprehensive records of additional flooding and catchment rainfall have been collected to be used in developing and calibrating more refined flood models.

Much of the Bulimba Creek flood plain has been developed in recent years and consequently has benefitted from modern knowledge and standards around flooding. However there are some areas adjacent to Bulimba Creek waterway and its tributaries that were developed before current standards were in place and consequently may be flood liable. Potential options to reduce flooding have been looked at in previous flood studies and are reconsidered in this report.

Study Objectives

The present flood study was undertaken to:

- 1. Review and update the existing hydrology and hydraulic models
- 2. Calibrate and verify hydrology and hydraulic models so that these are capable of regenerating recorded flood levels to an acceptable accuracy
- 3. Undertake design event modelling and provide flood levels and flood discharges for design events with Average Recurrence Intervals (ARI) of 2, 5, 10, 20, 50 and 100 years.
- 4. Identify the areas subject to flooding and review potential flood mitigation options as recommended in previous flood studies
- 5. Collate results/findings of flood modelling undertaken previously on selected tributaries: Newnham Road Tributary, Phillips and Salvin Creeks. (Lindum Creek, Spring Creek, Hemmant Channel and Tingalpa Channel are not included in this repor)

Study Elements

The Bulimba Creek Flood Study 2009 was carried out in several stages, which form separate reports within this document:

Report A: Model Calibration

Report B: Design Event Modelling

Report C: Flood Mitigation Assessment

Report D: Newnham Road Tributary Flood Investigation

Report E: Phillips Creek Flood Investigation

Report F: Salvin Creek Flood Investigation

Appendix A: Catchment Details

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Report A - Model Calibration

The Bulimba Creek Flood Study Model Calibration Report describes:

- the development of a hydrological model using the WBNM computer package for the Bulimba Creek Catchment to estimate flood discharges, and the calibration of this model against available hydrographical information
- the development and calibration of a hydraulic model using the MIKE11 computer package for Bulimba Creek, East Arm of Bulimba Creek and Mimosa Creek to reproduce recorded flood heights and estimated flood discharges to an acceptable accuracy.

Hydrological and hydraulic model calibration involve simulating recorded rainfall data for historical rainfall events through the developed hydrology and hydraulic models. Selection of model parameters for the catchment was undertaken such that the models could reproduce the recorded flood level information for the historical events to an acceptable accuracy.

Model calibration was undertaken using recorded rainfall data for March 1992, January 1994 and March 2001 storms. Model verification was made using November 2004 and May 1996 storm events. Appendices B, C, D and E summarise the details of the historical rainfall events, results of the model calibration and verification, and boundary conditions adopted for the MIKE11 hydraulic model respectively.

Report B - Design Event Modelling

The models described in the Calibration Report were used to derive a range of design flood information (i.e. flood levels, flows, velocities) for the 2, 5, 10, 20, 50 and 100 year ARI event for the selected Bulimba Creek waterways.

The Design Event Modelling Report summarises the procedure adopted in modelling design events and in predicting flood levels and discharges. Duration Independent Storm temporal patterns were used in the hydrology model WBNM to obtain the rainfall-runoff for the catchment in each design event. Hydraulic modelling was performed assuming ultimate catchment development conditions and considering the existence of waterway corridors. It assumes that revegetation of the creek overbank, for 15m on each side (known as a Minimum Riparian Corridor: MRC¹), would occur in the future and development would take place up to the Waterway Corridor extent.

Results of the Design Event Analysis are tabled in **Appendix I** while Flood Inundation plots are included in **Appendix J**. Hydraulic Structure Reference Sheets (HSRS) are included in **Appendix K**. HSRS describes the details of the structures modelled in the MIKE11 model including their hydraulic properties.

¹ Minimum Riparian Corridor (MRC): Land and Vegetation within and directly adjacent to the waterway is defined as the riparian corridor. MRC is the width that needed for the waterway to preserve its ecological and hydrological standards in maintaining the waterway health. It provides habitat to terrestrial and aquatic organisms, traps sediments and nutrients to improve water quality, helps to increase bank stability.

Report C - Flood Mitigation Assessment

Flood Mitigation Options

When examining the flooding areas of Bulimba Creek it can be seen how successful modern town planning has been in keeping recent development away from the creek corridors and above the Defined Flood² level. However, there are areas subdivided in an earlier age when standards were different. When the standards change, it is impractical to re-develop the city and these areas exist as liable to flooding.

Flood liable areas adjacent to Bulimba Creek and its tributaries were identified using the results of the design event analysis. Flood mitigation options recommended in previous flood studies were examined and possible future mitigation measures were considered.

The Bulimba Creek Flood Study, 1992 (BCFS) included investigation into critical flooding areas of Bulimba Creek and recommended seven potential flood mitigation options out of twenty-one options initially identified. These recommendations were made on the basis of conceptual benefit /cost analysis only.

The BCFS recommended the following flood mitigation options:

- 1. Upgrading of Cleveland Rail bridge crossing
- 2. Construction of an overflow channel (above the tidal influence area) just downstream of the Gateway Arterial.
- 3. Construction of flood protection levees in Altandi Street at Sunnybank
- 4. Deweeding of Mimosa Creek from downstream of Klump Road to the confluence with Bulimba Creek
- 5. Construction of flood protection levees and associated pumping stations around Fursden Road, Wood Avenue, Grey Street, Billan Street and part of Caravan Park.
- 6. Construction of a detention basin in Toohey Forest Park on Mimosa Creek.
- 7. Construction of detention basin in Mt Gravatt Park on Mimosa Creek.

However, only the first five options were finally included in BCFS as the preferred flood mitigation options.

Findings

The majority of the flood affected properties are located in the Mimosa Creek Catchment in Macgregor and is due partly to the back up of flood water from Bulimba Creek. There also exist clusters of flood affected dwellings adjacent to Bulimba Creek in the vicinity of:

- · Altandi and Coultis Street in Sunnybank Hills
- Fursden Road, Wood Avenue, Gray and Billan Streets in Carina
- Boundary and Hamilton Streets in Tingalpa.

The above flood liable locations were identified in the BCFS as were the recommended mitigation measures listed above.

Defined Flood Event (DFE): The flood event adopted by Local government for the management of development in the particular locality. Generally 1 in 100 year Average Recurrence Interval (ARI) flood event has been accepted as the preferred DFE

Out of the proposed mitigation measures, the Cleveland Rail Bridge widening was undertaken in 1993/94 and de-weeding was carried out on Mimosa Creek to facilitate faster discharge of floodwaters.

The other listed options however, were not recommended and not implemented for the following reasons.

- 1. Levees are usually only effective in situations where the timing difference between flood peaks from the major waterway and the local catchment (i.e. the catchment that drains to the levee on the protected side) are significant. This allows flood waters from the local catchment to leave the levee-protected area before the major waterway flood arrives. As the Bulimba Creek Catchment is relatively small with only a minor difference in the timing of creek and local flood peaks, a levee in this situation runs the risk of causing greater flooding due to local flows not being able to escape prior to the main flood arriving. Consequently, levees are not an effective flood mitigation measure for Bulimba Creek.
 - Levees may promote an unrealistic expectation of flood immunity to residents if the system fails through blockage to the drainage or malfunctioning of the dewatering system. Furthermore, levees cannot be designed to eliminate all flood events and failure would result in significant property damage and an unacceptable risk to life.
- 2. Proposed detention basins to mitigate flooding in Mimosa Creek in Toohey Forest Park and Mt Gravatt Park displayed incompatibility with environmental rules and community expectations. These detention basins were also considered to increase the flood risk on the community living immediately downstream with the potential for dam break type scenarios to occur. Therefore detention basins were not recommended in the 1992 study and are still not identified as a viable option.
- 3. Construction of an additional overflow (high level) channel downstream of the Gateway Arterial crossing would not be very effective in the proposed location due to the lack of hydraulic gradient in this part of Bulimba Creek. Additionally, such a scheme has the potential to increase flooding downstream as it lowers the natural retention of the flood. This channel would also require regular maintenance including vegetation management, and erosion and sediment control. The necessity of undertaking an archaeological survey had also been identified in the 1992 study.

As with many areas across Brisbane, a long-term, strategic approach would be more effective in delivering flood mitigation for Bulimba Creek. Many buildings are nearing the end of their life-cycle and redevelopment of these areas should be undertaken using current flood planning standards. Future flood mitigation measures would be mostly based on non-structural measures with appropriate land use planning controls, flood-proofed construction techniques and community awareness campaigns helping to minimise flooding and damages during a flood.

Report D - Newnham Road Tributary Flood Investigation

The Newnham Road Tributary Flood Study involved the hydraulic analysis of the waterway from its confluence with Bulimba Creek upstream to adjacent Kentish Street (see Figure 1.2), using the HEC-RAS software for steady flow conditions. The purpose of this study is to determine flood levels for the open section of the waterway, which is approximately 1.9km in length.

The HEC-RAS model developed for this study updated an existing HEC-RAS model developed in 2003. Cross section information was based on ground survey data from both a BCC survey of 2001 and private development survey of 2002. Additional information was obtained from Airborne Laser Scanning (ALS) data (2002) and field measurements.

Flow data was obtained from the Bulimba Creek hydrologic model (WBNM), with modification to inflow location points as necessary to account for the coarseness of that model. Calibration of the HEC-RAS hydraulic model was not undertaken due to the lack of recorded flood information. The creek contains a number of physical structures including 11 crossings, 3 drop-structures and a Stormwater Quality Improvement Device (SQID).

Design event modelling was undertaken for the 2, 5, 10, 20, 50 and 100 year ARI events with the inclusion of a Minimum Riparian Corridor (MRC). Peak flood levels for all design events are included in Appendix I-2.

Report E - Phillips Creek Flood Investigation

The study involved the establishment of a HEC-RAS hydraulic model to determine flood levels and flooding characteristics for the reach of Phillips Creek from Birdwood Road down to Creek Road, (see Figure 1.3) a length of approximately 1.6km.

The section of Phillips Creek immediately upstream of Creek Road was re-aligned in 1984 and 1988 in connection with property development. Within this reach, the creek passes through road crossings at Anzac Road and Gallipoli Road.

Downstream of Creek Road the waterway has been piped underneath the Carindale Shopping Centre and Old Cleveland Road. The waterway passes through a Stormwater Quality Improvement Device (SQID) downstream of Old Cleveland Road and then into Bulimba Creek. Modelling of this complex section of waterway downstream of Creek Road was not included in the investigation.

Cross-section data for the study was based on the ground survey of December 2006 and BCC Airborne Laser Scanning (ALS) data (2002).

Design event modelling was undertaken for the 2, 5, 10, 20, 50 and 100 year ARI events. The Rational Method was used to determine the peak flow data used in the steady state HEC-RAS model. A waterway corridor and Minimum Riparian Corridor (MRC) were incorporated into the HEC-RAS modelling. Peak flood levels and discharges for all design events are tabulated in **Appendix I-2**.

Report F - Salvin Creek Flood Investigation

The flood investigation undertaken involved the establishment of a HEC-RAS model for the Salvin Creek main branch and Glengariff tributary (Refer Figure 1.4).

Salvin Creek comprises a main reach which flows from Cavendish Road down to the confluence with Bulimba Creek, and a tributary (Glengariff Tributary) which flows from the Pine Mountain quarry and joins the main reach approximately halfway along its course near Glengariff Street.

A HEC-RAS model was initially developed in 2003 with cross section information based on ground survey of 2001 and 2003. In 2004, additional cross sections were extracted from the ALS data of 2002 to extend the Main Reach from Glenheaton Court to the Bulimba Creek confluence. It was further refined and updated in 2007 and 2009.

Calibration of the HEC-RAS hydraulic model was not undertaken due to the unavailability of recorded information. Design event modelling was undertaken for the 2, 5, 10, 20, 50 and 100 year ARI events. The Bulimba Creek WBNM hydrology model provided the flow inputs to the steady state HEC-RAS model.

Peak flood levels and discharges for all design events are tabulated in Appendix I-2.



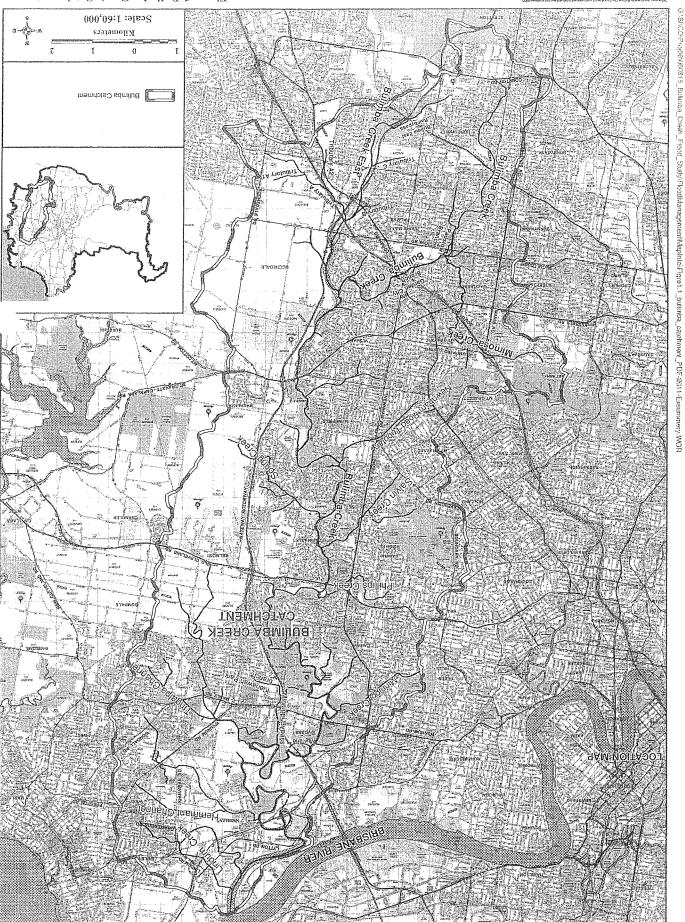


Figure 1-Bulimba Creek Catchment Location Map





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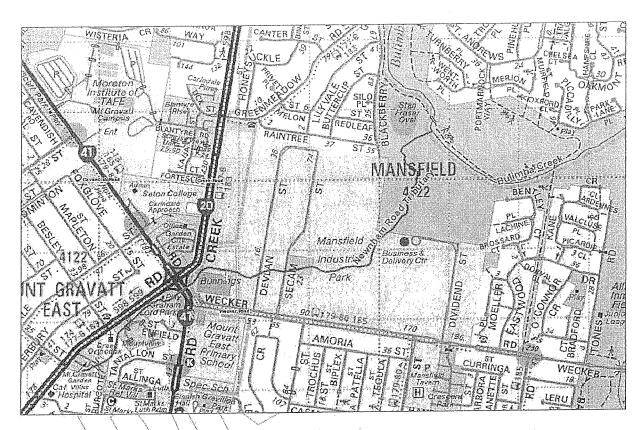


Figure 1.2: Newnham Road Tributary Location Map

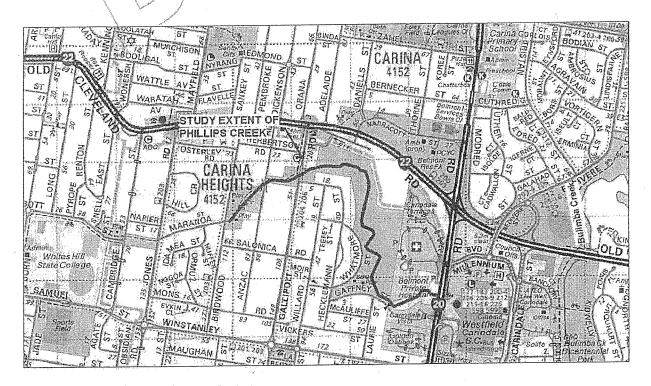


Figure 1.3: Phillips Creek Location Map

Figure 1.4: Salvin Creek Location Map

Bulimba Creek Flood Study - Executive Summary

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Bulimba Creek Flood Study Report A – Model Calibration

June 2011

Prepared for Water Resources

Prepared by
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City Design



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Approved Julie McLellan (Manager, Water Resources)

Bulimba Creek Flood Study - Report A: Model Calibration

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1.0 Introduction

The aim of the *Bulimba Creek Flood Study 2009* has been to review, update and extend the available hydrology and hydraulic models for the creek allowing revised flood discharges and flood levels to be estimated and flooding issues to be detailed.

The Bulimba Creek Flood Study - Report A: Model Calibration describes the development of the current hydrological model using the Watershed Bounded Network Model (WBNM) software, its calibration against available hydrographical information and its application in estimating flood discharges. It also describes the development of the MIKE11 hydraulic model and its calibration. These calibrated models have been used to derive peak flood discharges and levels for a range of design flood events from the 2 year Average Recurrence Interval (ARI) to 100 year ARI, for the Bulimba Creek catchment. These results are included in Report B: Design Event Modelling.

2.0 Catchment Description

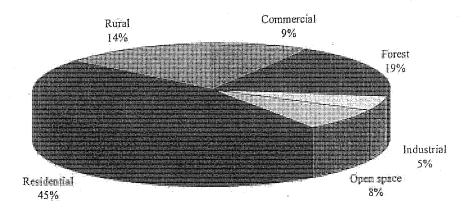
Bulimba Creek is a tributary of the Brisbane River and has a catchment area of 125km². It flows through Brisbane's Southern and Eastern suburbs and merges with the Brisbane River downstream of the Gateway Bridge at Murarrie. Tributaries to Bulimba Creek include (listed from upper to lower catchment) Mimosa Creek, Bulimba Creek East, Newnham Creek, Spring Creek, Salvin Creek, Phillips Creek, Tingalpa and Hemmant channels and Lindum Creek. The location of the Bulimba Creek Catchment is shown in Figure 2.1. The catchment areas serviced by each tributary are listed in Table 2.1.

Table 2.1: Catchment Areas of Selected Tributaries

Item	Tributary	Area(Km²)
1	Mimosa Creek	6.8
2	Bulimba Creek East Arm	14.8
3	Newnham Creek	3.8
4	Spring Creek	5.0
5	Salvin Creek	5.4
6	Phillips Creek	4.2
7	Tingalpa Channel (no formal name)	13.2
8	Hemmant Channel (no formal name)	6.9
9	Lindum Creek	4.8

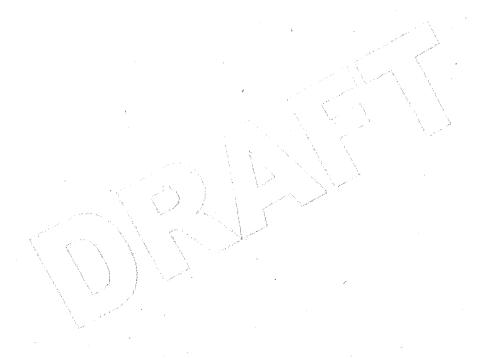
The main branch of Bulimba Creek, the East Arm, and the Mimosa Creek tributary are moderately steep in their upper reaches. The main branch flattens out in the lower sections and meanders as it nears the confluence with Brisbane River. The lower portion of Bulimba Creek is tidal and consists of wetlands and wide floodplains.

Most of the catchment is residentially developed with some rural, bushland, commercial and industrial zoning. Waterway corridors exist along all waterways within the catchment with a significant amount of open space and park along the main creek corridor. Figure 2.2 shows the break-up of present land use types.



There are a number of highly modified sections of creek (i.e. having been channelised or diverted). These areas are located between Compton Road and Beenleigh Road on the main branch and in the vicinity of the Beenleigh rail line and the Gateway Motorway on the Bulimba East Arm.

Numerous hydraulic structures exist across Bulimba Creek and its tributaries, including road, pedestrian, bikeway, rail and motorway crossings, services crossings, and flow control structures. The majority of hydraulic structures are included in the hydraulic model.



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Figure 2.1 Location Map of Bulimba Creek

Kilometers Scale: 1:60,000

Arterial Roads Sub-Arterial Roads

3.0 Previous Studies on Bulimba Creek

A number of studies have been commissioned and completed for Bulimba Creek and its tributaries. These studies provide valuable information on the creek's topography, hydraulics and flood mitigation potential. A brief summary of these reports is provided below.

3.1 Gateway Arterial Road: Lower Bulimba Creek Hydraulic Study (1985)

In 1985 Gutteridge Haskins & Davey (GHD) Pty Ltd undertook a hydraulic study to assess the impact of the Gateway Motorway project. The study was prepared by GHD for Crooks Michell Peacock Stewart Pty Ltd, Queensland on behalf of Main Roads Department (QMRD), Brisbane, Qld.

As a part of the study, cross-sections were surveyed in the lower reaches of Bulimba Creek. These cross sections were available for use in hydraulic models prepared by the Brisbane City Council.

3.2 Bulimba Creek Flood Study (1992)

Brisbane City Council commissioned Connell Wagner to undertake the Bulimba Creek Flood Study in 1992. Key outcomes of the study were the development of a calibrated hydrologic model (RORB) and hydraulic model (RUBICON) for the catchment. Mimosa Creek and the uppermost reaches of the main branch and East Arm tributary were modelled in separate HEC-2 models. A range of flood mitigation options were investigated and costed.

Survey data for the study was obtained from Council ground surveys taken between 1980 and 1991, and the GHD study on Gateway Arterial Road: Lower Bulimba Creek Hydraulic Study (1985).

The RORB model was calibrated against a Water Resources Commission gauge at Wecker Road using data obtained between 1971 and 1990. The RUBICON model was calibrated against recorded flood levels from six major events that occurred between 1971 and 1984 at several locations throughout the catchment.

3.3 Master Drainage Plan and Flood Study: Hemmant-Wynnum West Area (1997)

Brisbane City Council commissioned the Master Drainage Plan and Flood Study: Hemmant-Wynnum West Area (1997) to assess flooding and water quality concerns and review flood regulation lines within the portion of the Bulimba Creek catchment serviced by the Hemmant channel. A detailed RAFTS hydrology model was developed while hydraulic modelling for that study was performed using MIKE11. Flood mitigation strategies were investigated as part of the study.

3.4 Bulimba Creek: Catchment Management Plan (1998)

The Bulimba Creek Catchment Management Plan was developed by Council. It included a hydrological analysis of the catchment and considered a range of flow detention devices within the catchment. Initially, a RORB hydrological model was created using parameters derived from the 1992 Bulimba Creek Flood Study. The RORB model was later converted to the Unified River Basin Simulation Model (URBS) hydrology model format.

3.5 Bulimba Creek (East) Catchment: Stormwater Management Plan (2001)

Council undertook the Bulimba Creek (East) Catchment Stormwater Management Plan (SMP) to evaluate flooding, drainage, water quality and environmental conditions within the Bulimba Creek East catchment. The hydrology model used for this study was developed using WBNM, and hydraulic modelling was completed using MIKE11. An important element of the SMP was the definition of updated flood inundation and flood regulation lines which accounted for the construction of the Gateway Motorway through that part of the catchment. Other key outcomes of the study were a water quality analysis and a preliminary revegetation strategy.

3.6 Gumdale to Tingalpa Stormwater Management Plan (1998)

The Gumdale to Tingalpa Stormwater Management Plan was prepared in 1998 to evaluate flooding, drainage, water quality and environmental conditions within that part of the catchment. The hydrology model was developed using RAFTS software while hydraulic modelling was completed using MIKE11. Key outcomes of the study were defining flood inundation and flood regulation lines and a broad revegetation strategy.

4.0 Available Data

4.1 Hydrologic Data

4.1.1 Rainfall Data

A number of pluviograph stations exist within and adjacent to the Bulimba Creek catchment. Details of these stations are summarised in **Table 4.1** and their locations are shown on **Figure 4.1**. Most of the pluviograph stations have only been installed in recent years and widespread data is only available for floods that were associated with May 1996, March 2001 and November 2004 rainfall events. These storms were concentrated in the upper part of the catchment. The selection of rainfall events for model calibration and verification is discussed further in **Section 6 Model Calibration**.

Table 4.1: Pluviograph Information

Station			Rainfall data availability					
ID	Location	Operation Period	16/03/92 Event	19/01/94 Event	01/05/96 Event	09/03/01 Eyent	07/11/04 Event	
BMR138	Griffith University, Mt Gravatt	Feb 1989 to current	*	*	*	*	*	
P_R029	Perrin Creek, Balmoral Works Depot, Morningside	Nov 1991 to Oct 2005	*		*	*	*	
W_R521	Wynnum Creek, Pine Street Works Depot, Wynnum	Jan 1994 to Feb 2001	-	*	*		÷	
BMR527	Doughboy Parade, Hemmant	Jan 1994 to current		*	*	*	#	
BMR706	Old Cleveland Road, Carindale	Jan 1994 to current	2000 - 10	*	本	*	*	
NMR548	Joachim Street, Holland Park	Feb 1994 to current		*				
NMR833	Cnr Cavendish & Boundary Roads, Coorparoo	Feb 1994 to Dec 2004			*	*	*	
BMR709	School Road, Rochedale	Feb 1994 to Jan 2000			**************************************			
BMR830	Merion Place, Carindale	Feb 1994 to current			*	*	*	
BMR803	Greenwood Street, Wishart	Feb 1994 to current			*		*	
NMR596	Norman Creek, Tarana St at Camp Hill	Mar 1998 to current				本	*	
LTR141	Lota Creek, Rickertt Road, Ransome	Jun 1999 to current					*	
OXRI14	Oxley Creek, Calamvale Telstra, Calamvale	Feb 1989 to current	*	*		*	*	
S_R205	Scrubby Creek-Gowan Road, Calamvale (Logan CC)	Feb 1999 to current					*	
LTR755	Lota Creek, Harman Rec Reserve, Manly	Nov 1999 to current					*	
BMR836	Bulimba Creek, Gagarra Street, Eight Mile Plains	Jan 2000 to current		: '			‡	
W_R837	Wynnum Bowls Club, Wynnum	Oct 2001 to current					*	
SLR210	Millers Road, Underwood (Logan CC)						*	

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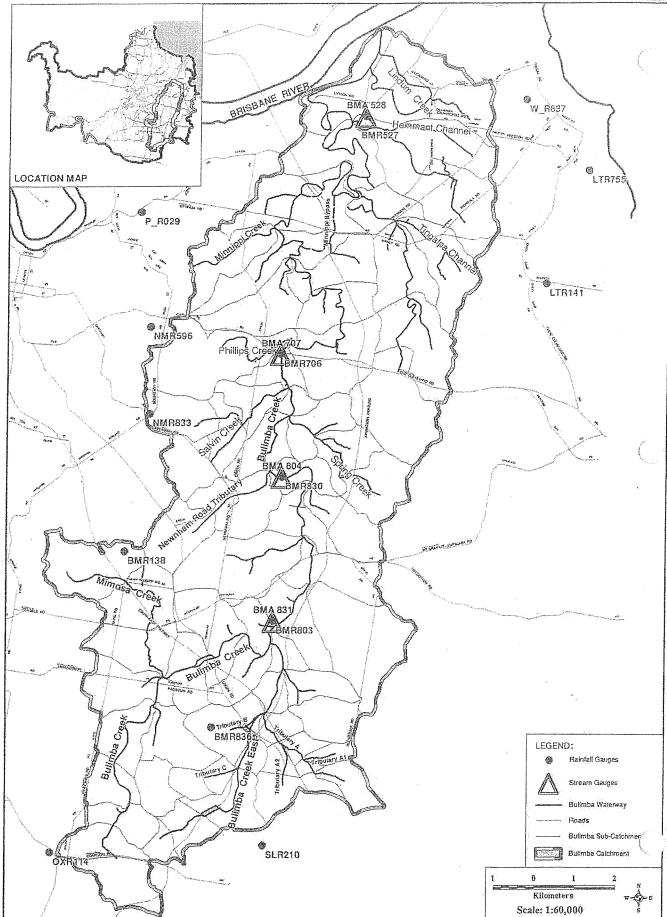


Figure 4.1: Rainfall Gauges (Pluviograph) and Stream Gauge Locations in Bulimba Catchment

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Locations in Bulimba Catchment

4.1.2 Stream Height Data

Continuous Stream Height Gauges

The stream height of Bulimba Creek has been measured since 1971. The earliest records came from a continuous stream height gauge located approximately 1km downstream of the Wecker Road, Mansfield crossing. The Water Resources Commission (WRC) operated this gauge until 1996. In 1994, Council installed another gauge on the opposite side (i.e. in the right bank) of Bulimba Creek at Merion Place, Carindale. The records from these two gauges provide the longest continuous stream height record for Bulimba Creek. Since 1994, Council has installed a number of other continuous stream height gauges in the Bulimba Creek catchment. Details of the locations of all these gauges are provided in Table 4.2 and their locations are shown on Figure 4.2.

Table 4.2: Stream Gauge Information

Station ID	Location	Operating Period
WRC	Wecker Road Gauge, Mansfield	July 1971 to 1996
BMA831	Merion Place, Carindale	February 1994 to current
BMA528	Doughboy Parade, Hemmant	January 1994 to current
BMA707	Old Cleveland Road, Carindale	January 1994 to current
BMA804	Greenwood Street, Wishart	February 1994 to current

The Department of Natural Resources and Water (DNRW) provided stream height data for the Wecker Road gauge for the period prior to 1994. The levels were taken from gauge zero, which equates to 5.165m Australian Height Datum (AHD). Out of the available stream height gauging stations, only the Wecker Road/Merion Place gauging stations provide recorded data for all events considered for model calibration and validation. Table 4.3 lists the recorded peak flood levels at the stream gauges for flood events since 1992. These records were used in the calibration and verification stage of both the hydrologic and hydraulic models.

Table 4.3: Recorded Flood Levels (m AHD) at Stream Gauges

		Recorded Flood levels in mAHD					
Gauging Station	MIKE11 Chainage	Са	llibration Eve	Verification Events			
	(m)	March 1992	January 1994	March 2001	May 1996	November 2004	
BMA804 - Greenwood Street, Wishart	8570			NR	22.49	22.77	
WRC Gauge – Wecker Road	13965	10.65	10.08				
BMA831 - Merion Place, Carindale	13965			11.99	11.32	11.58	
BMA707 - Old Cleveland Road, Carindale	17870		4.87	6.83	6.05	6.03	
BMA528 – Doughboy Parade, Hemmant	34440			1.75	NR	NR	

NR - No Record

Maximum Stream Height Gauges

Council also operates gauges that record only the maximum height of flooding at selected locations. These are called Maximum Height Gauges (MHGs) and have been installed at a number of places in Bulimba Creek. Maximum Height Gauge readings are available for flooding events since 1976.

Currently, there are twenty-six MHGs on the main branch of Bulimba Creek, five gauges on the East branch and one gauge on Mimosa Creek. Table 4.4 provides details of the MHG locations and recorded data are listed in Table D1 in Appendix D. Figure 4.2 shows the location of the MHGs with new and old gauge identification numbers. The availability of MHG data for each storm event was adopted as one of the criteria in selecting calibration events.

Table 4.4: Maximum Height Gauges Locations

MHG	Name	M11 Model	AMTD(M)	Location Information
New	Old	Chainage(M)	Antibum	
Bulimba	Upstream	1 Extension		
Closed	вмов	175	39700	Compton Road D/S
Bulimba	Creek M	ain Branch		
340	1	1800	37165	Beenleigh Road U/S
330	2	2470	36495	Daw Road
320	3	3765	35200	Kimmax Street
310	4	4260	34705	Padstow Road U/S
300	5	4780	34185	Bleasby Road
290	6	5615	33350	Pacific Motorway U/S
280	6A	5985	32980	Logan Road D/S
270	7	7420	31545	Kavanagh Road
260	- 8	8555	30410	Greenwood Street
250	9	10575	28390	Mt Gravatt-Capalaba Road U/S
240	10	12320	26645	Wecker Road D/S
230	11	14845	24120	Dewdrop Street
220	12	15600	23365	Pine Mountain Road D/S
210	13	17370	21595	Winstanley Street D/S
200	14	17810	21155	Old Cleveland Road U/S
190	15	18025	20940	Old Cleveland Road D/S
180	16	19165	19800	Scrub Road Footbridge U/S
170	17	22305	16660	Fursden Road
160	18	23165	15800	Wood Avenue
Closed	19	25515	13450	Wynnum Road U/S 1
Closed	20	25565	13400	Wynnum Road U/S 2
150	21	25865	13100	Wynnum Road U/S 3
Closed	23	25915	13050	Verdun Street
140	22	26015	12950	Wynnum Road D/S
130	24	26640	12325	Murarrie Road U/S

MHG	Name	M11 Model	AMTD(M)	Location Information		
New	Old	Chainage(M)	MILLE (I'K)			
120	25	26780	12185	Murarrie Road D/S		
110	26	31165	7800	Fleming Road		
100	27	32110	6855	Gross Avenue		
Bulimba	Creek Ea	st Branch				
430	8C	2700	3580	Underwood Road U/S		
420	8B/E	3725	2555	Logan Road U/S		
410	8A	4600	1680	Miles Platting Road U/S		
Closed	8D	5000	1280	Gateway Arterial on ramp		
400	8F	5045	1235	Daydream Place		
Mimosa	Creek					
500	BM4A	2718	56170	Parkway St D/S		

4.2 Topographic data

4.2.1 Existing data

Topographic data used for this study was taken from the hydrology and hydraulic studies undertaken prior to 2000. Data for the study was obtained primarily from three other previous studies as stated below (for further details refer to Section 3). The topographic data retrieved from these three studies were supplemented by Airborne Laser Scanning (ALS) survey information available in the BCC GIS database.

- Gateway Arterial Road: Lower Bulimba Creek Hydraulic Study (1985) provided some surveyed cross section data of the lower reaches of Bulimba Creek (downstream of Old Cleveland Road). That cross section information was adopted in the Bulimba Creek Flood Study (1992).
- Bulimba Creek Flood Study (1992) included surveyed cross sectional data of Bulimba Creek obtained by Council between 1980 and 1991. This cross section data was extracted from the RUBICON hydraulic model. One constraint in the use of this existing model data is that the extent of modifications to the original survey data is unknown.
- Bulimba Creek (East Arm) Hydraulic Analysis (1999) contained a MIKE11 model of the east branch of Bulimba Creek, modelled between Persse Road, Runcorn and Miles Platting Road, Rochedale. Topographic data was taken from the Bulimba Creek Flood Study (1992) with some new survey data collected for the study.

The floodplain in the lower reaches of Bulimba Creek, especially downstream of the Gateway Arterial, is very flat. Consequently there is insufficient data to determine accurately the level at which floodwaters break out of the main creek and flow across the floodplain and the resulting flood depths on the floodplain. Therefore, cross-sections extracted from the ALS data were used in combination with existing cross-section information to obtain relevant ground levels.

4.2.2 Aerial photography and ALS surveys

Aerial images taken between 2001 and 2007 are available in the Council's GIS database. These images were helpful in defining existing development within the catchment. In conjunction with site inspections, aerial photographs were used to determine the hydraulic roughness parameters and stages of development as related to hydrologic and hydraulic model details. Aerial images were also helpful in the identification of hydraulic structure locations and their details.

ALS survey data was also used to verify cross section information sourced from previous modelling work. This was done by extracting ALS cross sections and comparing them with modelled data. In several instances significant differences were identified prompting modification of the sections based on ALS data.

4.2.3 New Survey Data

New survey data was acquired at several locations along the creek. Additional cross sections were surveyed to enable the model of Bulimba Creek main branch to be extended up to Compton Road and also to introduce topographic changes in the vicinity of the concrete weir located adjacent Brandon Road.

The Council had conducted cross section surveys for the construction of two new hydraulic structures in 2005/2006 on the Bulimba creek. In addition there were a few cross sections surveyed by the consultant Cardno in conjunction with the Eastern Bus-way Project. These details were also used in this study.

Specifically, new survey data was available in the following locations:

- Bulimba Creek main branch crossing at Logan Road (upstream and downstream, 2005/06)
- Craig Street footbridge over Bulimba Creek (2006)
- in the vicinity of Old Cleveland Road bridge (upstream & downstream) on Bulimba Creek (2006)
- upstream & downstream of the concrete weir located downstream of Brandon Road (2006)
- between Nemies Road and Compton Road (2006).

4.3 Hydraulic structures

As-constructed drawings and design plans of existing bridges and culverts on Bulimba Creek and its tributaries were obtained from Council records, Department of Main Roads and Queensland Railways. These plans provided additional topographic and structure information, which was included in the hydraulic model. The total number of hydraulic structures modelled in the MIKE11 model is sixty. These crossing structures include:

- 18 road bridges
- 8 foot/bikeway bridges
- 2 railway bridges
- 31 sets of road culverts
- 1 concrete weir

5.0 Hydrologic and Hydraulic Modelling

5.1 Introduction

Hydrology and hydraulic models were developed for the Bulimba Creek catchment in the present study. The hydrology model simulates the rainfall-runoff in the catchment and derives the outflows from each sub-catchment. The hydraulic model analyses the movement of floodwaters through the creek branches and hydraulic structures to identify the general flow behaviour and resulting flood depths.

The WBNM (2003 version 1.03, June 2005) hydrologic model was selected to model the Bulimba Creek catchment and further information on the model including model theory is available at the web site http://www.uow.edu.au/eng/cme/research/wbnm.html.

The MIKE11 (DHI version 2005) hydraulic model was used to assess the hydraulic behaviour of Bulimba Creek. This model can simulate steady flow as well as unsteady flow behaviour in creeks. Further information on the model is available at the web site http://www.dbigroup.com.

5.2 Hydrologic model set up-

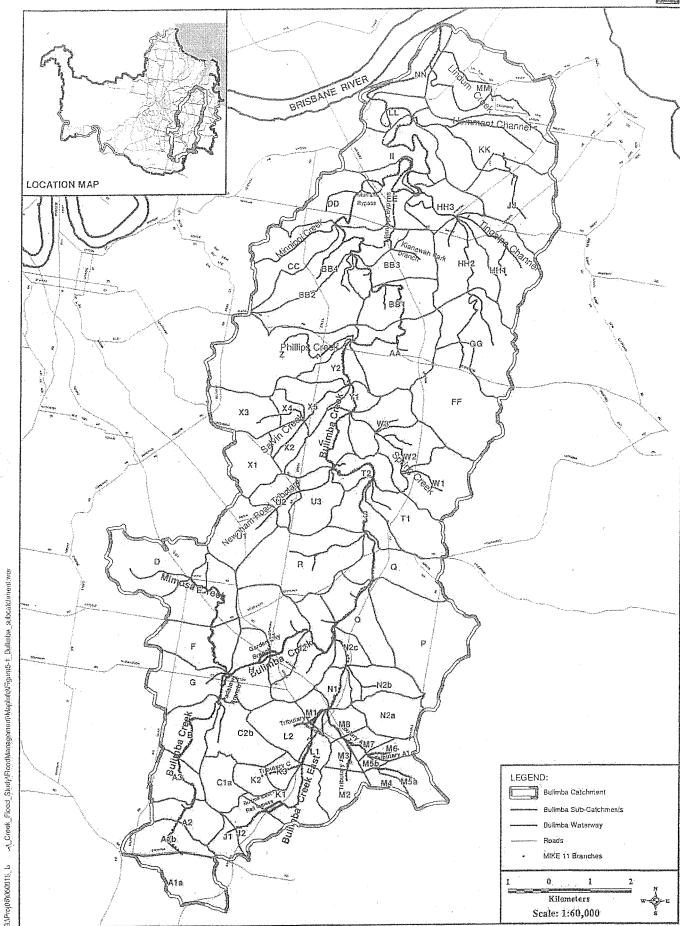
A WBNM hydrologic model was developed for the full Bulimba Creek catchment. The subcatchment layout adopted in the RORB hydrology model of the 1992 Bulimba Creek Flood Study formed the basis for the development of the new sub-catchment layout for the WBNM hydrologic model.

The Bulimba Creek catchment was divided into 76 smaller catchments for use with the WBNM hydrologic model. The natural topography of the catchment, location of hydraulic structures along the creek and major roads running through the catchment influenced the identification of subcatchment boundaries. Of the 76 sub-catchment areas, the main branch of Bulimba Creek contains 53, the East branch contains 20 and Mimosa Creek contains the remaining 3. Subcatchment areas, their centroid and outlet coordinates were determined with the help of Councils GIS data. The Bulimba Creek subcatchment layout adopted in the WBNM model is shown in Figure 5.1.

Land use information from Brisbane City Plan (2000), was used to determine existing fractions of imperviousness for each subcatchment (together with aerial photography). The impervious fraction values of sub-catchments were determined in accordance with **Table 4.05.1** of the *Queensland Urban Drainage Manual* (DNRW, 2007). The impervious fractions adopted for each category of land development is listed in **Table 5.1**.

Computed details of subcatchment areas, centroid and outlet coordinates of subcatchments for the WBNM hydrology model are provided in Table A1 (Appendix A). The relative proportions of development in each subcatchment for the existing and ultimate land use also provided in Table A2 (Appendix A).

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Figure 5.1: Sub-catchment Layout Adopted in the Hydrologic Model (WBNM) for Bulimba Creek

Table 5.1: Adopted Fraction Impervious Vs Development Category

Land development type	Fraction impervious
Roads	1.00
Commercial and Industrial	0.90
Medium Density Residential (excluding Roads)	0.70
Low –Medium Density Residential (excluding Roads)	0.55
Low Density Residential	0.40
Rural residential	0.20
Open Space, Parks, etc.	0:00

In a WBNM model rainfall losses may be modelled as loss rate (initial and continuing loss), runoff proportion, Horton Loss equation, or time varying loss. Numerous hydrologic investigations within Brisbane catchments have found that the initial/continuing loss model as the most appropriate for our climatic conditions, land use and topography. This method was therefore adopted for the current study.

5.3 Hydraulic model set up (Bulimba Main Branch, East Arm and Mimosa Creek)

5.3.1 Overview

The hydraulic model for this flood study was developed using the one-dimensional software MIKE11 (2005 version). The Bulimba Creek system was modelled as three main branches; namely Bulimba main branch, Bulimba East Arm and Mimosa Creek. Tributaries of Bulimba Creek that meet the main channel downstream of the Logan Road crossings, except the East Arm, were not included in the MIKE11 hydraulic model for a variety of reasons. Some had no surveyed cross section data (e.g. Spring Creek) whilst others had been modelled previously in conjunction with other major studies (i.e. Tingalpa Channel, Hemmant Channel). Three of the tributaries (Newnham, Salvin and Phillips Creeks) have previously been modelled using alternate modelling software. Detailed assessments of these three creeks are included in Reports D, E and F of this flood study.

5.3.2 Main Branch

The main branch of Bulimba Creek had previously been modelled from Nemies Road, Runcorn to the confluence with Brisbane River. In the current study, the main branch of the MIKE11 hydraulic model was extended up to Compton Road. Figure 5.2 shows the Bulimba Creek model schematic layout. Detailed information of the branches that were included in the MIKE11 model is provided in Table 5.2. Inflow points used to input the estimated catchment runoff hydrographs for each branch are shown in Figure 5.3.

New surveyed cross sections were used;

- between Nemies Road and Compton Road along the upstream-extended section of Bulimba Creek
- in the vicinity of the Brandon Road weir, where five new surveyed cross sections were included
- in Bulimba Creek and Garden City Branch at the Logan Road culverts
- to the north and south of Old Cleveland Road and also at Craig Street footbridge.

The Murarrie and Minnippi bypass branches were modelled as regular branches by introducing some cross sections extracted from ALS data.

In the lower reaches of Bulimba Creek where it meanders extensively (Figure 5.1), cross sections that were obtained from the GHD model (refer Section 3.1) intersect the creek at more than one location (e.g. 46GHD, 46BGHD and 46CGHD). At these locations, the cross-sections were divided into a number of segments representing the main channel and a portion of the floodplain. Links between the various segments of the full cross sections (e.g. 46GHD_AB, 46GHD_BC etc) were then introduced, as link channels in the network file, to allow cross flow between segments when floodwaters exceed the bank-full capacity of the creek. Cross section model chainages and their sources are provided in Table A2 (Appendix A). The cross section layout used in MIKE11 model is shown in Figures B-1 to B-9 in Appendix B.

5.3.3 East Arm

As discussed in Section 4.2, the MIKE11 (version 1999B) model developed in the Stormwater Management Plan (SMP) for the Bulimba Creek (East) Catchment (BCC, 2001), was incorporated into the Bulimba Creek current MIKE11 model. This model extended from Persse Road to Miles Platting Road. In the finalisation of the current MIKE11 model, the Bulimba East catchment SMP model data was checked against existing topographic data and coordinates were updated to match aerial photography maps.

The downstream extent of the SMP study model for Bulimba Creek East was located just downstream of Miles Platting Road. The East Arm branch was extended to the confluence with Bulimba Creek with this model update by adding cross sections sourced from the RUBICON model (1992) and ALS data.

5.3.4 Mimosa Creek

The Mimosa Creek branch is also represented in the MIKE11 model, extending from its confluence with the Bulimba main branch, near Padstow Road, upstream to Klumpp Road in Mount Gravatt. Cross section information for the MIKE 11 model was extracted from the HEC-2 model, which was originally developed for the 1992 Bulimba Creek Flood Study (refer Section 3.2).

5.3.5 Hydraulic Structures

A list of the structures (bridges & culverts) modelled in the MIKE11 model is provided in Table A3 (Appendix A). Modelling information for bridges and culverts was taken from the Council's GIS database and construction drawings as described in Section 4.3. In modelling the bridges in the MIKE11 model, bridge geometry was represented as irregular shaped culverts and weir combinations, with a Manning's roughness (n) equivalent to the creek channel roughness at that location.

The hydraulic structure details included in the SMP study MIKE11 model for Bulimba Creek East Arm at Beenleigh Road were updated to match with the HEC-RAS model developed in 2004. That HEC-RAS model was developed to assess the hydraulic impact of the Beenleigh-East Rail upgrade project (BCC, 2004). There were also a few irregularities in relation to the structure lengths and upstream and downstream cross section locations for a few structures. These details were corrected in the MIKE11 model.

5.3.6 Model Parameters

Manning's roughness values were originally determined from site inspections and aerial photographs and adopted in the MIKE11 model. These values were slightly adjusted during the model calibration process.



Table 5.2: Bulimba Creek MIKE11 Model Branch Details

Branch and the state of the sta	Description	Branch length (m)	Cross section ID
Bulimba - Main branch	Bulimba Creek - Main branch extends from Nemies Road, Runcorn to the Brisbane River confluence at Murarrie.	38965	ВМ
Bulimba - Upstream extension	Bulimba Creek - Main Branch from Compton Road crossing to Nemies Road in Runcom.	935	BM*
Mimosa Creek	Extends from Klumpp Road in Mt Gravatt to the confluence with Bulimba Creek at Macgregor.	3880	MI
Padstow	Bulimba Creek splits upstream of Padstow Road in Sunnybank and merges after crossing Padstow Road (before the Mimosa Creek merges with the main creek).	375	ВМ
Garden_City	Bulimba Creek flow splits just upstream of the Pacific Motorway near Garden City and merges with main creek just downstream of Logan Road	658	BM.
Minnippi bypass	Overland flow path from Minnippi Parklands flowing underneath the Gateway Arterial and joining Bulimba Creek further downstream of Wymum Road in Tingalpa.	2004	BM
Murarrie bypass	Overland flow path that passes through the Brisbane Polo Grounds and crossing Murarrie Road and the Gateway Arterial.	650	MÜ
Bulimba_East_Arm	East Branch of Bulimba Creek, that starts from Persse Road Runcorn and extends to the confluence with the Main Branch at Rochedale.	6280	BE
Tributary A (Trib_A)	East arm tributary modeled from Underwood Road and joins East arm just upstream of the Pacific Motorway	3021	Maca care cang
Tributary A_1 (Trib_ A_1)	Minor tributaries of East Arm - Tributary A, modeled from Rochedale Road to its meeting point with Tributary A, located downstream of School Road	750	para amplica
Tributary A ₂ (Trib_A ₂)	Minor tributaries of East Arm - Tributary A, modeled from Underwood Road to its meeting point with Tributary A upstream of Pacific Motorway	1042	******
Tributary B (Trib_B)	Tributary of East Arm, modeled from Bordeaux Street to its merging with Tributary A, downstream of Logan Road.	492	en les an
Tributary C (Trib_C)	Tributary of East arm modeled downstream of Warrigal Road and join East arm upstream of Underwood Road.	1120	
Clev_Rail	Overland flow path that splits up lower reaches of Bulimba Creek at Hemmant recreation reserve. It crosses Port of Brisbane Motorway and meets the main creek at Hemmant. after crossing the Cleveland Railway.	Link channel	w side *
Kianawah Park branch	Canal that joins Minnippi by pass downstream ME culverts	1006	
Bulimba East rail bypass	Flow split up at Beenleigh Road Rail and Gateway crossing	520	
45GHD_us1, 45GHD_us2, 45GHD_ds, 46GHD_ds	Overland flow paths in lower reaches of Bulimba Creek downstream of the Gateway Motorway and besides cross section 45GHD and 46GHD	Link channel	

Bulimba Creek Flood Study - Report A: Model Calibration

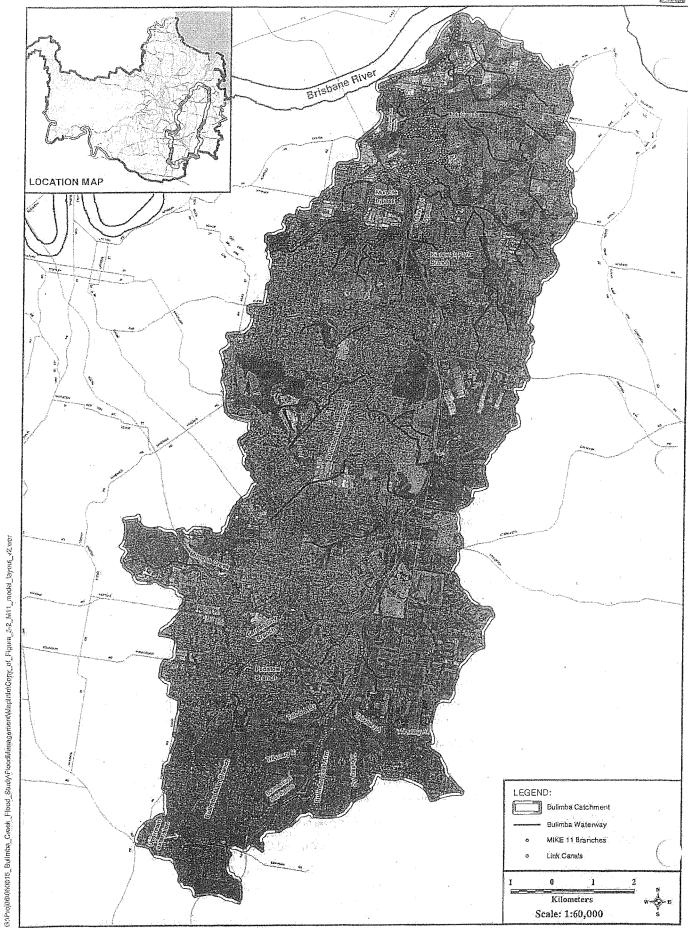


Figure 5.2: Bulimba Creek- MIKE11 Model Layout



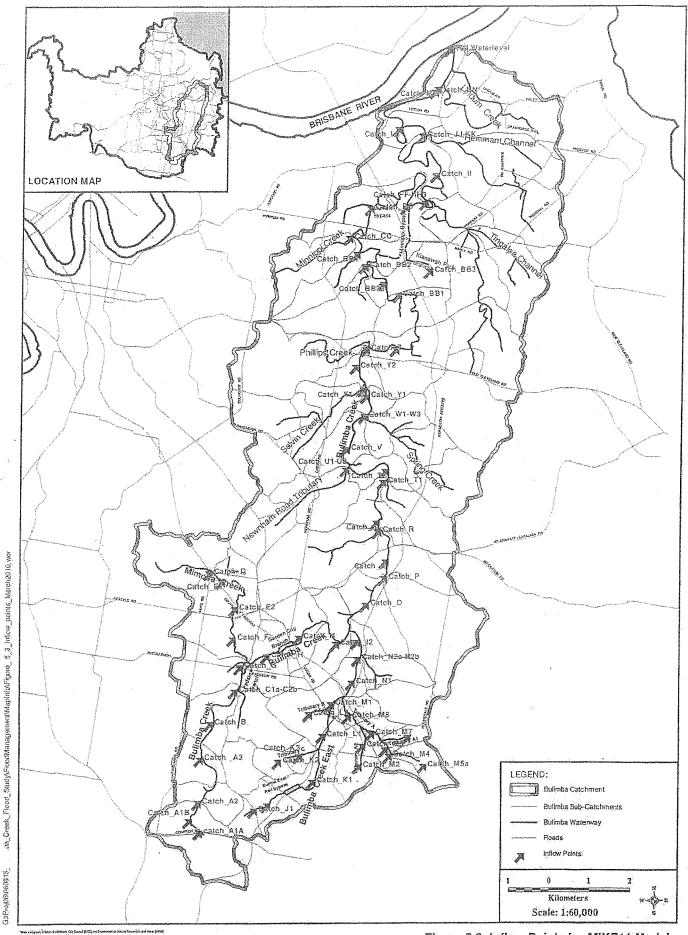


Figure 5.3: Inflow Points for MIKE11 Model

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6.0 Model Calibration

6.1 Selection of Calibration and Verification Events

Significant rainfall events have been recorded in the Bulimba Creek catchment in 1992, 1994, 1996, 2001 and 2004. Pluviograph data, stream gauge and MHG levels were available for these events for the selection of model calibration and verification purposes. Availability of pluviograph data for each of these events are listed in Table 4.1 (Section 4.1.1).

All these events were short duration storms with the exception of the 1996 event where rainfall continued for nearly seven days resulting in multiple flood peaks. Only a few pluviograph records were available for the events that occurred in the early nineties. There was more pluviograph station data coverage for recent rainfall events. All available rainfall records were reviewed to identify the events suitable for calibration.

The events selected for calibration and verification are shown in Table 4.3. These events cover the periods listed below and provide sufficient information. The cumulative depths of recorded rainfall in these events are plotted in Figures C1 - C5 (Appendix C).

Calibration Events

- a 16-17 March 1992 (modelled for 30 hours from 16/03/1992 00:00:00am)
- 19-20 January 1994 (modelled for 45 hours from 19/01/1994 02:00:00 am)
- 9-10 March 2001 (modelled for 24 hours from 09/03/2001 12:00:00 noon)

Verification Events

- 30 April to 07 May 1996 (modelled for 192 hours from 30/04/1996 00:00:00am)
- 7 November 2004 (modelled for 24 hours from 07/11/2004 00:00:00am)

The availability of rainfall and stream height gauging data for each event is summarised in the Table 6.1 below.

The availability of recorded rainfall (pluviograph) readings, peak water level data and MHG records were used as a basis for this selection of flood events for model calibration and verification. Out of the three events selected for calibration, two events possess MHG data for the full length of the Bulimba Creek system, and continuous water level records at two gauging stations during the events. One of the verification events possesses MHG readings for the full length of Bulimba Creek.

Table D1 (Appendix D1) lists the MHG readings recorded for these events.

The required tolerance between recorded and calculated flood levels for an acceptable level of calibration and verification is:

- Continuous stream gauge recorded flood levels: 150mm (+ or -)
- Maximum height gauge records: 300mm (+ or -).

Table 6.1: Rainfall & Stream Height Data used for Calibration & Verification Events

Pluviograph Station Name	C	Calibration Eve	nts	Verificatio	n Events
	March 1992	January 1994	March 2001	May 1996	Novembe 2004
BMR138	X	- X	×	\boxtimes	×
Griffith University, Mt Gravatt					-
P_R029	×	No data	×	×	×
Balmoral Depot, Morningside OXR114	D		×	No data	×
Calamvale Telstra, Calamvale	⊠	스		140 data	<i>♪</i> <u> </u>
Coorpargo – (Older station)		×			
Cavendish/Boundary Roads			1		
BMR527		×			. X
Doughboy Pde, Hemmant			1 1		1
BMR706			×		
Carindale shopping centre WRSR521					
Pine St works depot, Wynnwn	na proportion and a	$\boxtimes \setminus$	No data		No data
NMR833- Coorparoo					
Cavendish/Boundary Roads		[]		×	X
BMR830			×	×	×
Merion Place, Carindale	1 1				
BMR836		<u> </u>	\boxtimes		\boxtimes
Gagarra Street, Eight Mile Plains				<u> </u>	
NMR596	1 / 1 / 1	ī	×	** * :	⊠
Tarana St Park, Camp Hill			<u> </u>	:	
BMR803		:			X
Bulimba Creek -Greenwood St,					
Wishart W R837				***	
Wynnum Bowls Club, Wynnum					
LTR141					×
Rickertt Road, Ransome					
SLR210					
Millers Road, Underwood					
Stream Gauge Data Used for Ca	libration and V	erification Eve	nts	100	
Stream Height Gauge	C	alibration Even	its	Verificatio	n Events
- 5 5		January		May 1996	November
	March 1992	1994	March 2001	111ay 1330	2004
Wecker Rd DPI Gauge	×	☒			
Merion Place - BMA831			X		N N
Old Cleveland Rd - BMA707		×	. 🗵	図	×
Doughboy Parade - BMA528			×		
Greenwood St - BMA804				×	⊠
	22 Readings	12 Readings	31 Readings	31 Readings	20 Reading
Maximum Height Gauges	Whole	upper	Whole	Whole catchment	upper catchment
(Refer Table D1-Appendix D)	catchment	catchinent up to OCR	catchment	Colemnent	Scrub Road

up to OCR

6.2 Methodology

6.2.1 Hydrologic Model Calibration

The WBNM hydrological model for the Bulimba Creek catchment was developed using available topographical data as described in Section 4.2. Model parameters were reviewed as recommended in the WBNM manual (2005). Muskingum parameters adopted in the flow path block of the existing WBNM model had been determined by undertaking a Muskingum analysis. This analysis was reviewed in the consistency-checking phase of the hydraulic model development and is discussed in Section 6.5. Muskingum parameters adopted for the model are listed in Table 6.2.

Table 6.2: Muskingum Parameters

	Muskingum	Muskingum Parameters	
Branch	K (hours)	X	
Bulimba Creek: Compton Road to East arm confluence	3.20	0.45	
Bulimba Creek: East arm confluence to Wecker Road	1.50	0.44	
Bulimba Creek: Wecker Road to Old Cleveland Road	2.10	0.38	
Bulimba Creek: Old Cleveland Road to Brisbane River confluence	12.50	0.34	
Bulimba Creek East Arm	2.35	0.31	
Mimosa Creek	1.40	0.45	

The Muskingum K (channel lag) parameter for each reach was used to obtain an average stream velocity to enable the lag time for each WBNM subcatchment to be calculated. The calculated channel lag time and Muskingum parameter-x for each subcatchment were then input into the WBNM model.

Rainfall Distribution

The rainfall data from various pluviograph stations were assigned to the subcatchments in the WBNM model using a Thiessen polygon distribution. These distributions are shown in Figure C6-C10 (Appendix C).

Rainfall Losses: Initial and continuing

Initial and continuing losses¹ for each rainfall event were determined. Initial loss values were adjusted to achieve the best fit of the start of the rising limb of the discharge hydrograph. Continuous loss values were selected to match the shape and timing of the peak of the hydrograph. Adopted loss rates for calibration events and verification events are listed in Table 6.3: Initial and Continuous Losses.

¹ Initial loss occurs prior to surface runoff commencing while continuous loss occurs during throughout the event. Both are dependent on a variety of catchment characteristics including soil infiltration properties.

Table 6.3: Initial and Continuous Losses

	Initial l	Continuous loss	
Storm Event	Pervious	Impervious	rate (mm/h)
March 1992	20:	10	0.0
January 1994	55	50	1.0
May 1996	20	10	1.0
March 2001	80	70	1.2
November 2004	50	30	1.2

Calibration

Having run the hydrologic model (WBNM) with one of the calibration events, peak flood levels were compared with those recorded at stream gauging stations. Discharge hydrograph obtained from the WBNM model result file for each gauge location was converted to a stage hydrograph using the rating curve in obtaining the corresponding peak flood level. The model parameters were adjusted and the model was re-run with the same recorded event until the model had produced recorded flood levels within acceptable tolerances.

This procedure was repeated with other calibration events with further adjustments to model parameters. The calibration of the model was achieved by fine-tuning of model parameters until that could reproduce results representing general flow behaviour observed in the catchment. The calibrated hydrologic model results were then confirmed by modelling selected verification events. Further adjustments were made at the consistency checking phase (Section 6.5) with the hydraulic model.

6.2.2 Hydraulic Model Calibration

Discharge hydrographs obtained from the hydrologic model for calibrated events were used to run the hydraulic model with preliminary model parameters, which included roughness values that were based on the site inspections and aerial photography. Modelled flood levels at the gauged locations were then compared with recorded flood levels to check that they fell within the specified tolerances listed in **Section 6.1**. Alterations were made to the roughness values as required.

During the calibration and verification process, recorded flood hydrographs at continuous stream gauging stations for each event were compared with the modelled stage hydrograph as shown in **Figures D1-D16 in Appendix D**. In addition to the comparison with recorded flood levels, the shape and timing of the peak of the hydrograph was also examined to ensure a reasonable match. Roughness values adopted in the MIKE11 model are listed in **Table 6.4**.

Downstream Model Boundary

Adopted tide data for each calibration event at the Bulimba Creek confluence with the Brisbane River at Pinkenba were determined using the relevant editions of Queensland Tide Tables. These details are plotted in Figures E1–E5 in Appendix E: Downstream Boundary Levels Adopted for Calibration and Verification Events.

Table 6.4: Manning's Roughness (n) Values used in the MIKE11 Model

Waterway	Manning's 'n'	
Bulimba Creek		
Nemies Road to Brandon Road weir	0.085	
Brandon Road weir to Logan Road	0.09-0.10	
Logan Road to Greenwood Street	0.08-0.09	
Greenwood Street to Wecker Road	0.065-0.07	
Wecker Road to Greenmeadow Street	0.07-0.075	
Greenmeadow Street to Old Cleveland Road	0.06-0.065	
Old Cleveland Road to Scrub Road	0.05=0.06	
Scrub Road to Minnippi Parklands	0.04_0.05	
Minnippi Parklands to Boundary Road	0.035	
Boundary Road to confluence with Brisbane River	0.03	
Mimosa Creek		
Klumpp Road to Hoad Street	0.07-0.08	
Hoad Street to Pacific Motorway	0.08-0.10	
Pacific Motorway to Sheraton Street	0.07-0.075	
Sheraton Street to Bulimba Creek confluence	0.09	
Bulimba Creek East Arm		
Persse Road to Beenleigh Road crossing	0.095-0.09	
Beenleigh Road to Railway Bridge crossing	0.055	
North of Railway bridge to Gateway Motorway crossing	0.090-0.095	
North of Gateway Motorway crossing to Logan Road	0.09-0.08	
North of Logan Road to Pacific Motorway crossing	0.08-0.07	
North of Pacific Motorway to Bulimba Creek confluence	0.08-0.09	
Other branches		
Garden City branch	0.09	
Padstow branch	0.08-0.09	
Bulimba -East Rail bypass	0.10	
Tributary A in Bulimba East Arm	0.08	
Tributary A1 in Bulimba East Arm	0.08	
Tributary A2 in Bulimba East Arm	0.08	
Tributary B in Bulimba East Arm	0.06-0.08	
Tributary B1 in Bulimba East Arm	0.08	
Murarrie bypass branch	0.045	
Minnippi bypass branch	0.09	

Rating Curves

As listed in Section 4.2, survey data used in the hydraulic models were generally 10-20 years old and surveyed cross sections were not available at stream gauge or MHG locations; therefore interpolated cross sections were used at these locations. This involved estimating the actual gauge location from available topographical data and interpolating cross sections from the old survey data.

Rating curves were developed for the gauging stations at Greenwood Street, Merion Place, Wecker Road and Old Cleveland Road, using flood levels and discharge results (obtained from the hydraulic model) and existing or interpolated cross sections. These rating curves were used to convert the discharge hydrographs calculated by the WBNM model into stage hydrographs. A rating curve was not derived for the Doughboy Parade gauging station as this gauge is tidal.

The Greenwood Street and Merion Place gauges are located in relatively steep reaches of Bulimba Creek and these sites are generally independent of downstream water levels. The Old Cleveland Road gauge is located further downstream in a flatter reach, just above the extent of tidal influence. A rock bar just downstream of the gauge increases the creek invert level from approximately 0.0 to 1.5m AHD, thereby limiting the upstream end of the tidal prism. The gauge is not subject to tidal influence.

6.3 Calibration Results

Good agreement between recorded and calculated flood levels was achieved for the three calibration events considered. Recorded and modelled flood levels at continuous stream gauge locations for these events are listed in Table 6.5 below. Recorded flood levels for all five events considered at Merion Place gauging station and prior to that, Weeker Road provided good calibration for all events with the exception of the May 1996 (verification) event. The Old Cleveland Road gauging station recorded levels for all events except March 1992 event. This station gave good calibration with MIKE11 results for the March 2001 and November 2004 events while the other two events provided 300mm tolerances. Greenwood Street gauging station recorded data for the May 1996 and November 2004 events, the latter providing a good match with the modelled results. Details of calibration and verification results for each event are discussed in detail below.

A comparison of recorded MHG levels with peak flood levels calculated by the MIKE11 hydraulic model is provided in **Table D1** (Appendix D1). The calculated peak flood levels were generally within 300mm of the recorded level across the five calibration and verification events considered.

Table 6.5: Calibration and Verification Results at Continuous Gauging Sites

Event	Merion Place		Old Cleveland Road		Greenwood Street	
	Rec.	MIKE11	Rec.	MIKE11	Rec.	MIKE11
March 1992	10.65	10.60	NR	5.59	NR.	21.78
January 1994	10.08	9.94	4.87	5.13	NR	21.38
May 1996	11.32	11.06	6.12	5.75	22.49	22.10
March 2001	11.99	11.97	6.83	6.78	NR	22.87
November 2004	11.58	11.52	6.03	6.05	22.77	22.63

Results in **bold** indicate results that match specified tolerances

NR: not recorded

6.3.1 March 1992 Event

Rainfall data were available from four pluviograph stations. Two of these stations are located within the Bulimba Creek catchment (as shown in Figure C06, Appendix C). Stream gauge records were only available at Wecker Road gauging station for this event. MHG records were available at seventeen sites in Bulimba Creek as listed in Table D1 (Appendix D1) while only at one site in Mimosa Creek.

The best calibration was achieved in the March 1992 event, with almost all calculated flood peaks falling within 300mm of recorded MHG readings (except at two locations) and within 150mm at Wecker Road stream gauge.

Peak flood discharge profiles obtained from the WBNM hydrological model for this event were converted into water levels using the derived rating curves at gauging stations. The derived peak level also matched well with that of the recorded peak at the Wecker Road gauging station. Timing of the stage hydrograph was also acceptable. Table 6.5 shows the recorded and modelled flood levels for calibration events at stream gauging stations. Figure D1:March 1992 Event (Appendix D2) displays stage hydrographs at Wecker Road gauging station for modelled and recorded results for that event while Figure D2 (Appendix D2) shows the peak water level profile along Bulimba Creek.

6.3.2 January 1994 event

Rainfall data was available from seven pluviograph stations (as shown in Figure C07, Appendix C). Continuous stream gauge records were available at Wecker Road and Old Cleveland Road gauging stations. MHG readings were available at ten sites in Bulimba Creek extending up to Old Cleveland Road and one in Mimosa Creek.

The Wecker Road gauge levels matched the modelled flood levels of both MIKE11 and WBNM, while the modelled flood level for the Old Cleveland Road gauge was 260mm higher than that recorded (refer Table 6.4). Modelled flood levels were within the acceptable tolerances of the recorded MHG levels (including the Mimosa Creek MHG) with the exception of two sites. Figure D3 and D4 (Appendix D2) show stage hydrographs at Wecker Road and Old Cleveland Road gauging stations while Figure D5 (Appendix D2) shows the peak water level along Bulimba Creek for January 1994 event. The modelled flood peak occurs slightly earlier than that of the recorded.

6.3.3 March 2001 Event

Rainfall data was available from nine pluviograph stations (as shown in Figure C09, Appendix C). Stream gauge records were available at Merion Place and Old Cleveland Road gauging stations. MHG readings were available at seventeen sites in Bulimba Creek, three sites in Bulimba East Arm and at one site in Mimosa Creek.

MIKE11 and WBNM results were within the specified tolerances of the recorded levels at both stream gauge stations. Out of the twenty two MHG site readings available, eighteen were well within the 300mm tolerances (including the three Bulimba Creek East arm and Mimosa Creek MHG readings). Figure D6 and D7 (Appendix D2) show stage hydrographs at Merion Place and Old Cleveland Road gauging stations while Figure D8 (Appendix D2) shows the peak flood level along Bulimba Creek.

6.4 Model Verification

Model verification provides a means of checking the calibrated model parameters. Verification events were selected in a similar way to calibration events. Two rainfall events were selected for verification: November 2004 and May 1996. Model verification also displayed satisfactory results between the calculated and recorded flood levels for the two events as discussed below.

6.4.1 November 2004 Event

This rainfall event mainly covered the upper part of the catchment. Stream gauge records were available at the three gauging stations in Bulimba Creek. Rainfall records were available from fifteen pluviograph stations (as shown in Figure C10, Appendix C). MHG readings were available at fourteen MHGs in Bulimba Creek, four in Bulimba East arm and one in Mimosa Creek.

Merion Place gauging station gave a good match for both MIKE11 and WBNM results. At the Old Cleveland Road and Greenwood Street gauging stations, MIKE11 model results were within acceptable tolerances of recorded results. WBNM model results were slightly higher than the specified limits. Of all the MHG readings, twelve in Bulimba Creek, three in Bulimba Creek East arm and the Mimosa Creek MHG were within the acceptable tolerances. Figure D9 - D11 (Appendix D2) show stage hydrographs at Merion Place, Greenwood Street and Old Cleveland Road gauging stations while Figure D12 (Appendix D2) shows the peak water level along Bulimba Creek. There is a slight delay in the modelled peak flood level at all three gauging stations compared to recorded peak flood levels.

6.4.2 May 1996 Event

This is the only long duration event of the five considered events for calibration/verification of the Bulimba Creek models. Rainfall records were available from ten pluviograph stations (as shown in Figure C08, Appendix C): Stream gauge records were available at the three sites in Bulimba Creek; modelled results were slightly lower than the specified limits. WBNM model results at Old Cleveland Road gauge matched well with recorded results. MHG readings were available at most of the MHG sites and seventeen were within the specified limits in Bulimba Creek. Two MHG readings were available at Bulimba Creek East Arm with modelled results falling within the acceptable limits. The Mimosa Creek MHG also gave acceptable results, Figure D13 - D15 (Appendix D2) show stage hydrographs at Merion Place, Greenwood Street and Old Cleveland Road gauging stations while Figure D16 (Appendix D2) shows the peak flood level along Bulimba Creek.

6.5 Hydrology and Hydraulic Model Consistency Checking

To check the reliability of estimated flood discharge characteristics from the hydrologic and hydraulic models, consistency checks are required at selected locations. Peak values, timing and shape of discharge hydrographs obtained from hydrology and hydraulic models are compared in this process. Model parameters adopted in relation to channel routing (i.e. Muskingum parameters) in the hydrology model may be adjusted in the consistency checking.

Channel routing can be performed in a number of ways in WBNM, including non-linear routing, time delay and Muskingum routing. Muskingum routing provides the highest level of consistency between hydraulic and hydrologic models and was therefore chosen for the Bulimba Creek WBNM model. The MIKE11 model that accompanies this investigation contains detailed topographical data for the channels, which link the subcatchments within the Bulimba Creek main channel. By analysing the hydrograph routing presence in the hydraulic model, it is possible to derive the Muskingum parameters X and K, which can be used within the hydrologic model to provide consistent channel routing characteristics.

To determine the Muskingum parameters used in the WBNM model, the MIKE11 hydraulic model was divided into five reaches, based on the channel slope and creek roughness. These reaches were:

- Bulimba Creek East Branch Persse Rd to Bulimba Creek confluence
- Bulimba Creek Nemies Road to Bulimba Creek East confluence
- Bulimba Creek Bulimba Creek East confluence to Wecker Road
- Bulimba Creek Wecker Road to Old Cleveland Road
- Bulimba Creek Old Cleveland Road to mouth.

A parabolic hydrograph was routed through the MIKE11 model along each of these reaches. The flow hydrograph at the upstream and downstream limits of each reach was analysed to determine the Muskingum parameters (K and X) for that reach. These parameters were then input into the WBNM model for the relevant sub-catchments. Hydrographs produced by the WBNM model were then compared with those of the MIKE11 model focussing on the peak flow rate and timing of peaks at the above locations. This procedure was repeated by adjusting K and X to achieve a reasonable match of peaks and timing between both models. In this way, a consistent amount of channel routing was employed in both models, thus providing consistency between the models.

The Muskingum analysis was repeated several times during the model calibration process to ensure both models were using a consistent amount of channel routing. The final set of parameters adopted for the WBNM model is listed in Table 6.2: Muskingam Parameters. Plots of Muskingum weighted flow against storage for determination of X and K for the five reaches listed above are provided in Figures F1 - F5 in Appendix F.

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Bulimba Creek Flood Study Report B - Design Event Modelling

June 2011

Prepared for Water Resources

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Bulimba Creek Flood Study - Report B: Design Event Modelling

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1.0 Introduction

The calibrated hydrology and hydraulic models discussed in the *Bulimba Creek Flood Study – Report A: Model Calibration* were used to derive design flood levels, discharges and velocities for Bulimba Creek, Mimosa Creek and Bulimba Creek-East Arm including its tributaries. The *Bulimba Creek Flood Study – Report B: Design Event Modelling* follows on from the Calibration Report, presenting the methodology and results of the design event analyses.

Design events modelled for Bulimba Creek include the 2, 5, 10, 20, 50 and 100 year average recurrence interval (ARI) storm events and the results are presented in **Appendix I**. Hydraulic structure reference sheets are also included as Appendix K.

2.0 Model Data

2.1 Design Rainfall

2.1.1 Duration Independent Storms (DIS)

To derive design storm events for Bulimba Creek catchment, the duration-independent storm (DIS) event was employed. This method of DIS analysis was developed by Morris (1996) and involves the use of a single temporal pattern for all design storm durations. The synthetic events contain the maximum likely rainfall for any given design storm duration (up to 24 hours).

The DIS is generated for a given recurrence interval using the intensity-frequency-duration (IFD) curves presented for Brisbane in the Australian Rainfall & Runoff (Pilgrim (ed) 1987). For each ARI event a synthetic single storm temporal pattern is built by combining the worst burst of rainfall extracted from points on the IFD chart. The derived temporal pattern for each ARI event is then applied to the catchment using the hydrology model (WBNM) developed in the calibration phase and peak discharges are extracted at nominated locations. A flood frequency analysis is then undertaken for the catchment using the recorded rainfall data for the region to derive the peak discharges for each ARI event at the nominated locations. A factor, which is to be applied in the hydrology model, is then derived for each ARI event by comparing the peak discharges in the flood frequency analysis curve. The methodology adopted is discussed further in Section 3.1 and 3.2.

2.2 Tail Water Conditions

The mean high water springs (MHWS) water level was used as the constant downstream tidal boundary at Hemmant for the design event modelling. A constant tide level of 1.00m AHD was adopted for all design events.

2.3 Topographic Data and Structure Details

As described in the calibration report, existing cross section data and some recently surveyed cross sections were included in the MIKE11 hydraulic model. Existing cross section data was taken from the RUBICON model developed for the Bulimba Creek Flood Study in 1992. New survey data was available for Bulimba Creek main branch in the vicinity of:

- Brandon Road weir
- Logan Road culverts
- Craig Street footbridge
- Old Cleveland Road Bridge

New cross sections were extracted from the Airborne Laser Scanning (ALS) survey data when ground survey was not available. These sections were mainly used in the Murarrie bypass, Minnippi bypass and Kianawah Park branch in the MIKE11 model. Cross section data for Mimosa Creek was extracted from the HEC-2 model developed in 1992 for the Bulimba Creek Flood Study. A few of these cross sections were extended as required using ALS data and included in the MIKE11 hydraulic model.

Details of structures for inclusion in the MIKE11 model were obtained from the 'as constructed' drawings. Bridges were modelled as irregular shaped culverts with the Manning's roughness coefficient equivalent to the creek bed roughness at that location. Hydraulic Structure Reference Sheets which provide structure geometry details and flood information were prepared for the modelled structures.

2.4 Land Use

Ultimate catchment development conditions within Bulimba Creek Catchment as set out in *Brisbane City Plan (BCC 2000)* were assumed in estimating design flood levels. Land use planning maps for Brisbane City including the Rochedale Master Plan, were used to calculate the percentage of impervious surface areas within individual sub catchments for use in the hydrology model. Impervious fractions for particular land development categories were obtained from Table 4.05.1 in the *Queensland Urban Drainage Manual* (QUDM), second edition, 2007.

3.0 Hydrologic Modelling

3.1 Design Event Model Setup

Design event modelling was based on ultimate development conditions within the catchment. Changes to the extent and degree of development in the catchment are quantified using the percentage of impervious surface area associated with each sub-catchment. The hydrologic model (WBNM) was modified using impervious fractions that represent ultimate catchment development. The impervious fractions adopted in the hydrologic model are listed in Table A1 of Appendix A.

As mentioned in Section 2.1.1, the DIS methodology requires that a factor be applied to the DIS temporal pattern to ensure consistency between the calculated peak flood discharge for each design event (i.e. 2 to 100 year ARI) and that derived through a Flood Frequency Analysis (FFA) which uses an annual maximum flow series derived from historic rainfall. A complex procedure was adopted to determine these factors for each design ARI event. This procedure is discussed below.

3.2 Flood Frequency Analysis

Recorded rainfall data (pluviograph) are available for the Brisbane CBD from 1911 onwards. Eleven rainfall events were extracted from each year (from 1911, for 91 years) with each event covering a 72 hour period, containing the most intense burst of rainfall for nominated durations of 30 minutes, 1, 2, 3, 4, 6, 12, 18, 24, 36 and 48 hours. These selected eleven events from each year were analysed using the calibrated Bulimba Creek WBNM hydrologic model with existing catchment urbanisation to estimate peak flood discharges for each event in each sub-catchment.

Following the extraction of peak discharges, the annual peak discharge for each sub-catchment for each data year was tabulated. Flood frequency analysis on the annual maximum series was then undertaken at a number of selected locations within the Bulimba Creek Catchment.

The selected locations (Figure 5.1 in Report A) were:

- Nemies Road (subcatchment A1)
- Turnmill Street (subcatchment F)
- Padstow Road downstream (subcatchment G)
- Greenwood Street (subcatchment O)
- Old Cleveland Road (subcatchment Y2)

The estimated peak discharges were plotted to produce frequency distributions using Weibull plotting positions. The line of best fit was determined for each plot and corresponding peak discharges were estimated for the 2, 5, 10, 20, 50 and 100 year ARI events. Flood frequency analysis plots are included in Figures G1 - G5 (Appendix G). The estimated flood discharges for each ARI event from the flood frequency analyses at the five locations listed above are shown in Table 3.1.

Table 3.1: Flood discharges obtained from flood frequency analysis

	Flood Discharge (m³/sec): Flood Frequency Analysis									
ARI (years)	Nemies Road (A1)	Turnmill Street (F)	Padstow Road (G)	Greenwood Street (O)	Old Cleveland Road (Y2)					
100	87.1	125	188.1	558.4	601.8					
50	77.6	111	168.8	499.8	537.0					
20	65.2	93	143.1	422.2	453.3					
10	55.9	80	123.3	362.3	390.8					
5	46.5	· , 67 ,·	102.8	302:3	328,4					
2	33.3	49	73.2	215.6	241.4					

3.3 Derivation of Duration Independent Storms

Duration Independent Storms (DIS) were developed for given ARI events using intensity-frequency-duration (IFD) curves for Brisbane based on Australian Rainfall & Runoff (Pilgrim (ed) 1987). Initially, the DISs were analysed with the calibrated WBNM hydrology model for each ARI event, and peak discharges were extracted at the five locations, where flood frequency analysis were undertaken (refer Section 3.2).

The analyses found that peak discharges produced by the DIS events were higher than those of the flood frequency analysis discharges. DIS events were subsequently factored until the peak discharges at the selected locations were found to be comparable to those derived from the flood frequency analysis. Factored Duration Independent Storms (FDIS) were then used in estimating design event discharges at all locations. DIS factors adopted for each ARI event, estimated peak discharges using un-factored DISs (UDIS) and FDIS and the percentage difference between FDIS and FFA are listed in Table 3.2:

3.3.1 Factored DIS Discharges

The comparison of discharges obtained from the flood frequency analysis (Table 3.1) and factored DIS discharges (Table 3.2) for each ARI event shows good agreement at Nemies Road, Turnmill Street, Greenwood Street and Old Cleveland Road. Therefore, the results in Table 3.1 indicate that the factored DIS temporal patterns may be used in the WBNM hydrology model to estimate design flow hydrographs. Hydrology model discharges obtained for these factored storms at the five subcatchment locations are also included in flood frequency analysis plots in Figures G1 - G5 (Appendix G).

3.3.2 Design Event Hydrographs

The run-off hydrographs obtained from the hydrology model using the factored DIS with the ultimate catchment development condition were used as inflow hydrographs to the MIKE11 hydraulic model as described in the next chapter. Peak flow discharges obtained from the WBNM hydrology model for design events 2, 5, 10, 20, 50 and 100 year ARI at sub-catchment outlets are included in **Table H1** in **Appendix H**.

Table 3.2: Factored DIS discharges & Comparison with FFA Discharges

	Compa	HISOH OF DISCI	narge(m³/sec):		•	Community and an extra constant of
ARI (years)	100	50	20	10	5	2
Factor applied (%)	85	85	86	87	84	80
	Nemies Road			en in de la companya	visionin salahan <u>Salah Kabatasan Sa</u>	ra Gerva 🚣
UDIS	102.7	90.8	75.8	64.7	56.2	42.8
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FDIS	611.7	539.8	454.2	390.1	326.3	233.1
FFA	601.8	537.0	453.3	390.8	328.4	241.4
Difference(%)*	-1.65	-0.52	-0.20	0.18	0.64	3.44

4.0 Hydraulic Modelling

4.1 Design Event Model Setup

The MIKE11 model developed in the calibration stage was adopted for design event modelling, with appropriate modifications, to represent the design event modelling situation. The modelling scenario adopted is based on the existence of waterway corridors with riparian vegetation and is described in detail in the sections 4.2 and 4.3 below. Cross sections in the MIKE11 model were altered to include:

- Minimum (vegetated) Riparian Corridor (MRC) widths
- Waterway Corridors: the effective flood storage and flow conveyance widths were altered to match the waterway corridor limits

Design inflows for each event were obtained from the hydrology model for the ultimate catchment development condition and applied to the MIKE 11 model as node boundaries and point discharges.

4.2 Waterway Corridors

Waterway corridors are an integral part of the Council's Planning Scheme for Brisbane and are described in the Brisbane City Plan (2000) as:

"The corridors along a waterway indicated on the Planning Scheme maps. These corridors are defined by:

- A flood regulation line (FRL)
- A local plan environmental corridor or a waterway corridor (WC)
- · A waterway corridor defined in a stormwater management plan
- A waterway corridor defined in a waterway management plan.

If more than one of these is available for a particular waterway, the largest applies.

If there is no FRL described in a local plan, SMP or WMP, a 30m distance measured on each side from the centre line of the waterway," would apply (BCC 2000, vol. 1, ch.3, p.75).

These corridors identify zones where water flow, water quality, ecology and open space, and recreational and amenity values are to be preserved and/or managed in an ecologically sustainable manner.

The presence of waterway corridors¹ has been incorporated in the MIKE11 model by superimposing the corridor extents over each model cross section and incorporating vertical walls to exclude the conveyance and/or storage characteristics of the watercourse beyond the limits of the waterway corridor. Essentially, this practice assumes that filling and development will ultimately occur beyond the boundary of the waterway corridors.

¹ The location of the majority of waterway corridors along major creeks coincides with that of flood regulation lines. Where the waterway corridor is wider than the FRL, modelling has been based on the width of the FRL only.

4.3 Minimum Riparian Corridor

Vegetation, which exists along the banks of a watercourse, is known as riparian vegetation. It is a key contributor to waterway health acting as a buffer between the waterway and the adjacent lands. A well-vegetated riparian zone can improve water quality by filtering overland flow and reducing erosion along creek banks. Shady trees protect vulnerable organisms from extremes of temperature; root systems and woody debris become habitat for fauna; and organic matter sustains aquatic food webs. Vegetation also provides habitat and forage for fauna and adds to a waterway's recreational value.

This study calculates anticipated flood levels assuming a minimum vegetated riparian corridor width along the entire creek system. The hydraulic investigation does not in any way imply that Council is planning to establish a minimum riparian vegetated corridor width in the creek catchment. The minimum riparian vegetated corridor is modelled solely in recognition that at some specified time in the future, revegetation may occur, either through natural regeneration or as a result of human planting programs. The results of this modelling are intended to ensure that the habitable floor levels of developments within the flood plain take account of possible future revegetation.

Minimum riparian corridors have been applied to main branches of all reaches modelled in the hydraulic model. The minimum riparian corridor was simulated as dense vegetation by applying a 'Manning's n' value of 0.15, extending from the top of the low flow banks for a minimum width of 15m on both sides of the creek. Where there was no obvious low flow channel, the vegetation was applied at the anticipated 2 year ARI flood level on the basis that this size event is generally contained within the bed and banks of the creek. Where the existing Manning's n value of the cross section in the vicinity of the MRC was higher than 0.15, the existing value was not altered.

4.4 Results

4.4.1 Flood Levels

Modelled design event flood levels along the Bulimba Creek, Mimosa Creek and Bulimba Creek-East Arm and a few of its tributaries were obtained using the MIKE11 hydraulic model. In addition flood levels are reported for the Garden City, Padstow, Kianawah Park, Minnippi and Murarrie bypass branches on Bulimba Creek. Flood information for three other main tributaries: Newnham Road Tributary, Philips Creek and Salvin Creek are derived from three separate flood studies and are included as Reports D, E and F. Estimated peak flood levels for ultimate catchment development conditions, with the presence of minimum riparian corridors and waterway corridors/flood regulation lines, are included in Table I1 of Appendix I. Corresponding peak flood discharges for the design events are tabulated in Table I2 of Appendix I.

Flood Inundation Extents have been included in Appendix J for the 2, 5, 10, 20, 50 and 100 year ARI events.

Minimum Energy (ME) culverts under the Gateway Motorway south of Wynnum Road were modelled in the Minnippi bypass branch in the MIKEII hydraulic model. Flow through these culverts during

large flood events may result in higher tail water levels to the Kianawah Park branch, which joins the Minnippi bypass branch immediately downstream of the Gateway Motorway. Therefore flood levels in Kianawah Park branch may be affected by backwater in the Minnippi bypass branch.

4.4.2 Hydraulic Structure Reference Sheets

The hydraulic structures (bridges and culverts) modelled in the hydraulic model, and their details are presented in Appendix K. These sheets describe the modelled structure geometry and its associated hydraulic characteristics assuming ultimate catchment development conditions. The geometry details of the bridges and culverts were taken from the records of Brisbane City Council, Department of Main Roads and Queensland Rail engineering drawings.

In each hydraulic structure reference sheet, a table displays the hydraulic characteristics of the structure as derived from the MIKE11 hydraulic model for the 2 year to 100 year ARI event. These details include peak flow rate, peak flood level upstream of the structure and afflux and peak flow velocity through the structure for each ARI event. A recent photograph of the structures is also included with most sheets.

5.0 References

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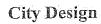


Bulimba Creek Flood Study Report C – Flood Mitigation Assessment

June 2011

Prepared for Water Resources

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Table 2: Flood Mitigation options recommended in 1992 Flood Study

1.0 Introduction

Bulimba Creek waterway, its Eastern Branch and Mimosa Creek were modelled using the MIKE11 hydraulic model as described in Reports A & B of this flood study. This model was developed to derive design flood levels and inundation maps for the 2, 5, 10, 20, 50 and 100 year ARI events. Separate HEC-RAS (steady state) models were also developed for three other tributaries of Bulimba Creek namely, Newnham Road Tributary, Salvin and Philips Creek Catchments. Design event modelling results including inundation maps were examined to identify flood liable areas in the Bulimba Creek Catchment.

When examining the flood liable areas of Bulimba Creek it can be seen how successful modern town planning has been in keeping the recent development away from the Creek corridors and above the defined flood line. However there are areas subdivided in an earlier age when standards were different. It is not possible to re-subdivide the city when these standards change and therefore some areas still exist as flood liable.

The Bulimba Creek Flood Mitigation Assessment report comments on the possible flood mitigation measures that could be applied to the Bulimba Creek Catchment and some of its tributaries. This study specifically reconsiders the validity of the mitigation proposals recommended in the previous Bulimba Creek Flood Study (BCC, 1992) and comments on their applicability.

2.0 Flooding in Bulimba Creek

2.1 Assessment of Key Flooding Areas in Bulimba Creek

Inundation maps and peak flood levels derived from this Flood Study have been used to identify areas where significant flood damage could occur. The results of this assessment are presented in Table 2.1. The identified areas were then cross referenced with the flood mitigation recommendations from the Bulimba Creek Flood Study, 1992 (BCFS).

Table 2.1: Possible flood affected areas in Bulimba Creek

Item	Flood Affected Area	Tributary/Creek	Number of Properties Flooded in a "100 year" ARI event
1	Kianawah Park south of Wynnum Road - Tingalpa	Bulimba Creek	Between 20 and 50
2	Hamilton Street and Boundary Streets North of Wynnum Road - Tingalpa	Bulimba Creek	Between 20 and 50
3	Fursden Road and surroundings in Carina	Bulimba Creek	Between 50 and 100
4	Altandî / Naldi Street in Sunny Bank	Bulimba Creek	Less than 20
5	Springfield Street	Mimosa Creek	Between 50 and 100
6	Upstream of Kessels Road	Mimosa Creek	Between 50 and 100
7	Brandon Road weir (435m downstream from Brandon Road culvert crossing)	Bulimba Creek	Less than 10

2.2 Possible Reasons for Flooding

The advancement of reliable flood estimation methods has enabled flood risk to properties and the community to be reduced through effective floodplain management strategies. As a result "Development Standards" based on design flood levels requiring floor levels to be above the 100 year flood were first introduced in the 1980's. Developments that were either constructed prior to that time or been approved but not constructed were not subject to these standards and may have been built to lower levels.

Formal Subdivision and Development Guidelines were not adopted within the Brisbane City limits until 1997. Significant development occurred in Bulimba Creek Catchment after this time with most having being built above the defined flood levels using flood information from the BCFS. Thus, the appropriate design flood immunity has been provided with most of these developments. This has been a good example of Council's town planning controls providing an effective pro-active flood mitigation measure. However, there still exist flood liable areas where development had occurred prior to the introduction of flood control planning measures.

3.0 Potential Flood Mitigation Measures

3.1 Background

Flood mitigation activities are aimed at reducing flood impacts on the community and the environment. The mitigation measures are generally categorised as non-structural or structural.

Non-structural measures rely on non-constructed activities including flood warning systems, education schemes, planning controls and vegetation maintenance.

Structural initiatives involve constructed modification to the creek/eatchment that aims to lower flood levels. These techniques include:

- · Increasing the size of the creek channel
- Increasing the channel "smoothness" or reducing roughness.
- Increasing the channel flow capacity by minimising constrictions.

These methods improve the flood conveyance capacity and lower flood levels.

An alternative is to increase the flood storage capacity (volume) of the floodplain as this tends to attenuate the peak flow rate in the creek and thus reduce flood levels.

However, in lowering flood levels, care is required to ensure that flooding is not simply transferred to another location. For example, lowering flood levels by improving flood capacity in an upstream portion of a creek reduces flood storage. This may cause increased flooding downstream. Alternatively increasing flood storage by adding a detention basin will increase flood levels upstream of the basin with the potential to cause the problem that is sought to be avoided.

3.1.1 Non-Structural Measures

Non-Structural activities aim to minimise flood damage by reducing flood risk. The following actions are non-structural mitigation measures:

- Flood forecasting and warning systems: Such systems would help to identify impending storms and keep the community ready to take appropriate action and precautionary measures to reduce their flood damage. The Bureau of Meteorology operates flood forecasting on large river systems. There is no such flood warning system developed for any creek at this time. The "flash flooding" nature of Bulimba Creek (i.e. short time between rainfall and resultant flood) makes this service not viable at present.
- Flood Education by awareness campaigns: Flood education would help to raise community awareness of possible problems, future impacts and actions that should be taken in a flood situation to help an individual reduce their own flood damage. As a first step individuals can get information from a property-based "Be FloodWise Property Report". This is provided by the Brisbane City Council at no cost to residents.

Bulimba Creek Flood Study - Report C: Flood Mitigation Assessment

The Bureau of Meteorology web site (http://www.bom.gov.au/) defines "flash flooding" as that results from relatively short intense bursts of rainfall i.e. Thunderstorms. It can deposit exceptional amounts of water over a small area within that short period. Flooding occurs when soil absorption, runoff and drainage system cannot adequately disperse that intense rainfall. It is difficult to provide effective warning systems because of their rapid onset.

- Land use controls: These include adopting appropriate zoning controls, policies and guidelines to keep new development above the relevant flood levels.
- Purchase of Flood Affected Properties: Purchase of properties with low flood immunity removes the damage altogether. A voluntary Home Purchase Scheme has been operational in Brisbane since 2006 to purchase properties with low flood immunity.
- Creek Channel Maintenance: Creek channel maintenance involves removal or trimming plant growth that may cause partial blockage to flood flows. Growth of exotic vines and other vegetation may lower the flood carrying capacity of a creek and may cause increased flooding.

3.1.2 Structural Mitigation Options

These options adopt constructed alterations to the creek to directly reduce the depth of floodwater. Possible structural flood mitigation options are listed below.

a. Improvements to Creek Channel to increase flow capacity

The creek flow capacity can be increased by widening, realigning (removal of bends) or deepening the waterway and by clearing channel bed and bank obstructions. Such improvements tend to increase the flow velocity and result in carrying the flow at a lower flood level.

However consideration needs to be given to two aspects of such a solution:

- The lower flood depth also reduces flood storage and thus may have the effect of increased flood flows and levels downstream
- The higher velocities may cause erosion problems. The creek's stable regime may be disrupted. If this is likely then the design must include measures to re-stabilise the channel. In the past this was achieved by extensive (and expensive) maintenance plans and rock and concrete bank stabilization measures. Current environmental requirements render such measures unfavourable and natural channels are preferred.

During major flooding events in natural creek systems, the majority of flow is carried by the floodplain. Therefore to reduce flooding using works in the main channel, extensive modifications are required. This involves destruction of riparian habitats raising significant environmental concerns. Thus main channel widening is now rarely carried out.

b. Improvements to Creek Floodplains to Increase Flow Capacity

This is an expensive option unless the land is in public ownership as the costs associated with the acquisition of land are likely to be high. Publicly owned land, provided it is extensive enough to carry out a suitable scheme, may offer viable flood mitigation options.

c. Improvements at Bridge Crossings

Some older bridge crossings were designed without the current consideration of potential flood impacts. Some of these bridges may be altered to reduce the flood impact. These works may include improving flow alignment of the approaching water and reshaping of wing walls and pier leading edges. Replacing the entire bridge generally only occurs if there is a need to realign or otherwise upgrade the road as the cost of replacement most likely far outweighs the flood benefits derived.

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d. Floodplain Bypass

Flood bypass canals may have been built or occur naturally within a creek system and may help to reduce flooding by providing additional waterway area. These flow paths increase the area available to store and convey floodwaters, and facilitate fast release of flood waters from the area of concern, thereby lowering flood levels.

A bypass floodway may help in the case of a meandered creek where it takes longer to drain floodwaters to the mouth. Opportunities for the construction of a bypass floodway depend on the site topography, geotechnical properties of soil, hydraulic characteristics, environmental and ecological considerations of the site, availability of land and future maintenance requirements.

A concern associated with this option is the likelihood of transferring the flood problem from one area to another as a result of the bypass. If there are already flooded areas near the downstream end of the bypass the acceleration of the flow tends to increase flood levels.

Bulimba Creek has a low flood gradient in the area downstream of Wynnum Road that has been proposed as a channel bypass area in the previous BCFS. A lack of hydraulic grade would make the channel ineffective in transferring large volumes of flood water.

e. Detention Basins

A detention basin is a small scale reservoir which provides temporary storage of flood waters. These systems attenuate floods by storing flood waters in the basin thereby reducing peak flows and flood levels. They are normally located in an upstream location of the catchment and regulate the release of flow downstream.

Detention basins have inherent disadvantages requiring substantial land for flood storage, which results in inundating land that was not previously flooded. There is also the potential, in long duration or multiple peak rainfall events, for the basin to be filled to its full capacity in the early parts of the storm. The basin is then rendered ineffective for flood mitigation purposes for the remainder of the storm event. Detention basins may change the existing environmental system of the creek both upstream and downstream of the basin location.

f. Levees

Levees are constructed barrier walls which exclude part of a floodplain from a flood event in protecting properties within the excluded area. Levee heights and formation levels are determined on a variety of factors which include; physical limitations of the site, availability of funds, the condition of the development that requires flood immunity and environmental considerations.

Levees may also promote an unrealistic expectation of flood immunity to residents if the associated drainage system fails to operate effectively in a flooding event. There are two main problems with levees particularly on small creek systems like Bulimba creek:

Rainfall that collects on the protected side of the levee is unable to escape as the natural flow
path to the main watercourse is obstructed and accumulates behind the levee. There is a
reliance on the functioning of any drainage system through the levee to operate effectively
during a flood event. The drainage system may however be compromised by blockage or the
malfunctioning of any dewatering pumps if present (eg: due to unforseen circumstances like
power failure).

2. Levees cannot be designed to eliminate all flood events. There is always the possibility of overtopping once flooding exceeds the design capacity of the levee. A flood event that can overtop the levee may occur or the levee could collapse or otherwise breach due to inadvertent tampering. When this occurs flooding of the isolated area would be much faster than if the levee did not exist. Behind a levee such flooding would be unexpected and that would result in an unacceptable risk to life and significant property damage. Loss of life has a much higher probability in such a situation and therefore levees are not a recommended mitigation measure.

g. Flood Proofing to Existing Structures

Flood proofing involves raising existing structures above the designated flood level or replacing the flood affected walls and flooring with flood tolerant materials. This will not stop flooding but will reduce flood damage to the building structure and those contents that are raised above flood level. This method is available to the home owner at the home owner's expense.

3.1.3 Flood Mitigation Justification

All flood mitigation schemes undergo a process to evaluate the cost effectiveness of the scheme. The cost of the scheme, including the initial construction cost and any ongoing maintenance cost, is compared to the savings that could be gained in reducing both direct and indirect flood damage cost in all future floods expected during the life of the mitigation scheme. In addition, environmental consequences are assessed. A mitigation project that is viable on economic grounds, where reduction in flood damage is greater than the cost of the scheme, can fail the test if environmental damages are unacceptable.

3.2 Flood Mitigation Measures Recommended by Previous Studies

Flood mitigation measures were investigated in the BCFS. This study initially identified twenty-one flood mitigation options and preliminary benefit /cost analyses were undertaken to select seven potentially feasible options. These seven measures are described in Table 2 below. In the BCFS these options were assessed against a set of environmental rules² to determine their acceptability. Subsequently two options involving the construction of detention basins in environmentally sensitive areas were abandoned. The remaining five options were recommended of these, two have been completed. The other three, after further consideration, were ruled out on environmental amenity and safety grounds.

² Connell Wagner, 1992: Section G lists these rules and implications on flood mitigation.

Table 2: Flood Mitigation options recommended in 1992 Flood Study

Item	Mitigation Option	Status
1	Cleveland Rail bridge crossing upgrade to a larger opening.	Completed in 1994.
2	Flood protection levees near Altandi and Coultis Streets Sunnybank.	Not adopted as levees are now not considered as a viable mitigation measure in Brisbane to reduce residential flooding (See 3.1.2.f)
3	Construction of detention basin in Toohey Forest Park on Mimosa Creek. It requires constructing 150m long bund to a maximum height of 6m on Mimosa Creek, north of the Griffith university's eastern access road. This would inundate 6.5 to 7 ha of forest for periods of one day.	Not adopted. Incompatible with environment and community requirements.
4	De-weeding of Mimosa Creek from east of Klump Road to the confluence with Bulimba Creek. The aim is to increase flood carrying capacity without widespread clearing, excavation and channelization of the Creek.	Completed in 2008
5	Construction of flood protection bunds and associated pumping stations around Fursden Road. Levees were recommended in Billan Street, Wood Avenue, lower lying areas of Fursden Road and adjacent Caravan park off Creek Road. (Bunds of 2.5m maximum height with gentle side slopes). Flood gates and pumping stations are proposed for draining local stormwater.	Not adopted. (Refer 3.1.2.f & Item 2 above).
6	Construction of detention basin in Mt Gravatt Park. That involved constructing a bund to a maximum height of 7m adjacent to Clair Waux College and Hoad Street with a spillway. During a flood about 7 ha of land would be inundated up to a day.	Not adopted. Incompatible with environmental and community requirements.
7	Construct an overflow channel (above the tidal influence) just downstream of the Gateway Arterial. Construction of 200m wide, 350m long channel to bypass meandered section of Bulimba Creek was recommended to benefit properties at Fleming Road to north of Wynnum Road and around Greenslade Street in Tingalpa. (UBD ref. map 162: D6 to C5).	Not adopted. It is not recommended as an effective option as discussed in 3.1.2.d. Requirement for an archeological survey and vegetation management issues were identified in BCFS. It would also increase the tidal prism at Highest Astronomical Tide levels.

4.0 Conclusion

Structural and non-structural flood mitigation opportunities in Bulimba Creek catchment have been assessed. The BCFS had investigated some favourable flood mitigation schemes for Bulimba Creek Catchment and recommended seven mitigation options. Introduction of detention basins for flood mitigation in Bulimba Creek was rejected due to the incompatibility with environmental and community requirements.

Of the remaining five recommended options, possible mitigation schemes (item 1 and 4) have already been undertaken as discussed in **Table 2**. Schemes which did not proceed were mainly due to environmental, amenity or safety concerns.

Introduction of bypass canals as flood mitigation measures were not recommended as it is foreseeable that this would transfer the problems downstream to where flooding already exists. Construction of levees has inherent safety risks. More effective non-structural options for Bulimba Creek are available as discussed.

Non-structural methods of flood mitigation for the remaining flood affected properties in Bulimba Creek are ongoing. Rebuilding or redevelopment of these properties will ultimately lead to reduced flood impacts.

Town Planning and building controls are the primary mechanism to effectively reduce flood impacts in the Bulimba Creek Catchment.

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Bulimba Creek Flood Study Report D - Newnham Road Tributary Flood Investigation

June 2011

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Bulimba Creek Flood Study - Report D: Newnham Road Tributary Flood Investigation

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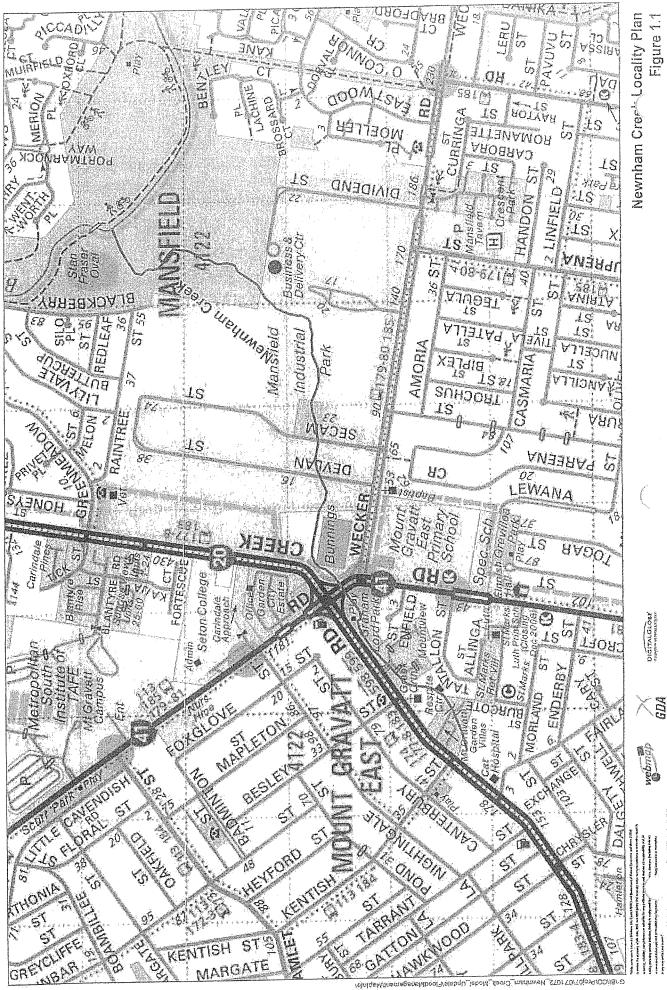
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Figure 2.1: Newnham Creek Catchment Minor Inflow Points (Showing HEC-RAS Chainage)

1.0 Introduction

Newnham Road Tributary (Newnham Creek) is a small tributary of Bulimba Creek located in Mansfield on Brisbane's south side. The Newnham Road Tributary Flood Study involves the hydraulic analysis of the waterway from its confluence with Bulimba Creek to upstream at 215 Creek Road. The study involves the establishment of a HEC-RAS hydraulic model to determine flood levels for the open section of the waterway. The flooding results from this study will be used as the basis for flood level advice to the public. Flooding events considered are the 2, 5, 10, 20, 50 and 100 year ARI events.

Figure 1.1 indicates the locality of the creek and the extents of the open waterway for which the model has been created.



2.0 Catchment Hydrology

2.1 Catchment Description

The Newnham Road tributary catchment forms part of the greater Bulimba Creek Catchment and includes areas within the suburbs of Mansfield and Mt Gravatt East. The contributing catchment area of Newnham Creek to the confluence with Bulimba Creek is approximately 3.8 km². A portion of the catchment in the Mt Gravatt area is forested, whereas the remaining areas are urban residential and commercial, with some industrial sectors at the lower end.

2.2 Creek Characteristics

The open-channel section of Newnham Creek is approximately 1.9km in length. Upstream of the open channel sections is piped drainage. This piped drainage services the surrounding residential and commercial areas.

Newnham Road tributary contains 11 crossings, three drop-structures and a Stormwater Quality Improvement Device (SQID). A description of the location of each of these structures is given in Table 3.1

At the 215 Creek Road development the waterway is an engineered rock-lined channel. After the development it becomes a trapezoidal concrete-lined channel until downstream of 285 Creek Road where an unlined channel begins. The unlined channel continues to Bunnings Warehouse where it becomes a concrete-lined channel for the length of the Bunnings Warehouse bridges, before reverting back to an unlined channel after the downstream bridge. This unlined channel continues until the confluence with Bulimba Creek and is generally not maintained with large areas of tall reeds and heavy vegetation. The trapezoidal concrete-lined channel section features three hydraulic drop-structures.

The main channel base width varies from approximately 3m (in the concrete-lined channel) to 10m (in the rock-lined and natural channel areas) and the depth varies from approximately 2 to 4m in both channels. The average bed slope of the creek within the study area is approximately 1.0 % (1 in 100).

2.3 Discharge Calculations

The discharges used in the HEC-RAS model were obtained from a combination of flow data adopted in the previous HEC-RAS model developed by Brisbane City Council in 2001 and the 215, Creek Road Development HEC-RAS model. These discharges represent the expected Ultimate Conditions of the catchment.

The previous BCC model had only one flow change location for the entire length of creek. From review of the layout of the contributing stormwater drainage network it was apparent that there were a number of significant inflow locations along the length of the drain and that the previous BCC model was excessively conservative. Additional flow change locations were added to the current model to further distribute the flow along the length of creek being modelled (refer to Figure 2.1).

The design peak discharges adopted are shown in Table 2.1.

Table 2.1: Adopted Peak Discharge

HEC-RAS	Discharge (m³/s)								
Chainage (m)	2 year ARI	5 year ARI	10 year ARI	20 year ARI	50 year ARI	100 year ARI			
1880	26.2	35.0	38.7	42.0	48.3	60.6			
1790	31.3	42.6	48.2	52.0	58.4	68.7			
1753	31.3	43.7	52.1	61.6	69.6	80.7			
1591	31.3	44.7	55.9	63.6	80,8	92.6			
1366	35.3	50.4	63.0	71.8	91.1	104.5			
918	39.2	56.1	70.2	79.9	101.4	11(6.3			
621	43.2	61.8	77.3	88.0	111.7	128.2			



Figure 2.1: Newnham Creek Catchment Minor Inflow Points (Showing HEC-RAS Chainage)

3.0 Hydraulic Modelling

3.1 General

The hydraulic analysis was undertaken using the HEC-RAS (Version 3.1.3) hydraulic modelling software for steady flow conditions. Section 3.2 details the setup and assumptions used in the modelling. The modelling results are presented in Section 3.3.

3.2 HEC-RAS Model Setup

3.2.1 Cross Sections

The HEC-RAS model for the 1.9 km study reach was comprised of 77 cross-sections, as shown in Figure 3.1. The cross-sectional data used in the model was obtained from the following sources:

- Extracted from the existing BCC and 215 Creek Road models;
- Extracted from DTMs (Digital Terrain Models) made using BCC Airborne Laser Scanning (ALS) data, with modification made to the in-channel dimensions
- Measurements taken during site visits to the area
- Design drawings of the concrete-lined trapezoidal channel and SQID structure

Cross sections were interpolated within HEC-RAS at locations where the channel shape varied linearly between cross sections. The source data used in each cross section is detailed in the HEC-RAS model.

3.2.2 Minimum Vegetated Riparian Corridor

The vegetation along a waterway is called riparian vegetation. It is a key contributor to waterway health, acting as a buffer between the waterway and adjacent lands. A well vegetated riparian zone can improve water quality by filtering overland flow and reducing erosion along creek banks. Shady trees protect vulnerable organisms from extremes of temperature; root systems and woody debris become habitat for fauna; and organic matter sustains aquatic food webs. Vegetation also provides habitat and forage for fauna and adds to a waterway's recreational value. However, many hydrological/hydraulic studies have shown that increasing vegetation densities within a floodplain increases anticipated flood levels. To date this perspective has discouraged the revegetation of riparian vegetation, especially in areas known to be 'potentially flood sensitive' under existing vegetation densities. However, the Waterway Management Plan (BCC, 2003c) process allows the hydrological and ecological impacts of riparian revegetation to be assessed and managed in an integrated manner.

This study calculates anticipated flood levels assuming a Minimum Vegetated Riparian Corridor (MRC) width along the entire creek system. This hydraulic investigation does not in any way imply that Council is planning to establish a width in the Newnham Creek Catchment. The MRC is modelled solely in recognition that at some unspecified time in the future, revegetation may occur, either through natural regeneration or as a result of human planting programs. The results of this modelling

are intended to ensure that the habitable floor levels of developments within the floodplain take account of possible future revegetation. This type of forward planning is supported by Guidelines for Flood Regulation Line and Minimum Fill Level Assessment (BCC, 1994).

A MRC was incorporated into the HEC-RAS modelling. A Manning's 'n' value of 0.15 was used to represent the MRC, which typically incorporates the main channel plus a distance of 15m either side of the top of bank. The MRC is only modelled downstream of the SQID on Secam Street. This is due to the remainder of the channel being largely concrete-lined with industrial and residential developments adjacent the channel.

3.2.3 Manning's 'n'

For areas outside the MRC, the Manning's 'n' values were obtained with reference to a site inspection, aerial photography and hydraulic roughness literature as per BCC Natural Channel Design Guidelines (BCC, 2003). The Manning's 'n' values used were as follows:

- In-channel Areas:
 - Concrete-lined Channels, n = 0.015
 - Natural Channel, n = 0.040
 - Engineered Channel with Rock Protection, n = 0.040
 - Channel Area Immediately Downstream of Drop Structures, n = 0.06
- Overbank Areas:
 - Combined Grassed/Paved Regions, n = 0.025
 - Concrete Areas, n = 0.015
 - Road Areas, n = 0.016
 - Shrubs and Scattered Trees Light Density, n = 0.045
 - Shrubs and Scattered Trees Light to Medium Density, n = 0.06

The Manning's 'n' values downstream of the hydraulic drop structures were increased from 0.015 to 0.06 to simulate the turbulent and unstable water profile that is expected to occur from this structure. The Manning's 'n' values return to 0.015 for the concrete-lined channel shortly after hydraulic drop structures.

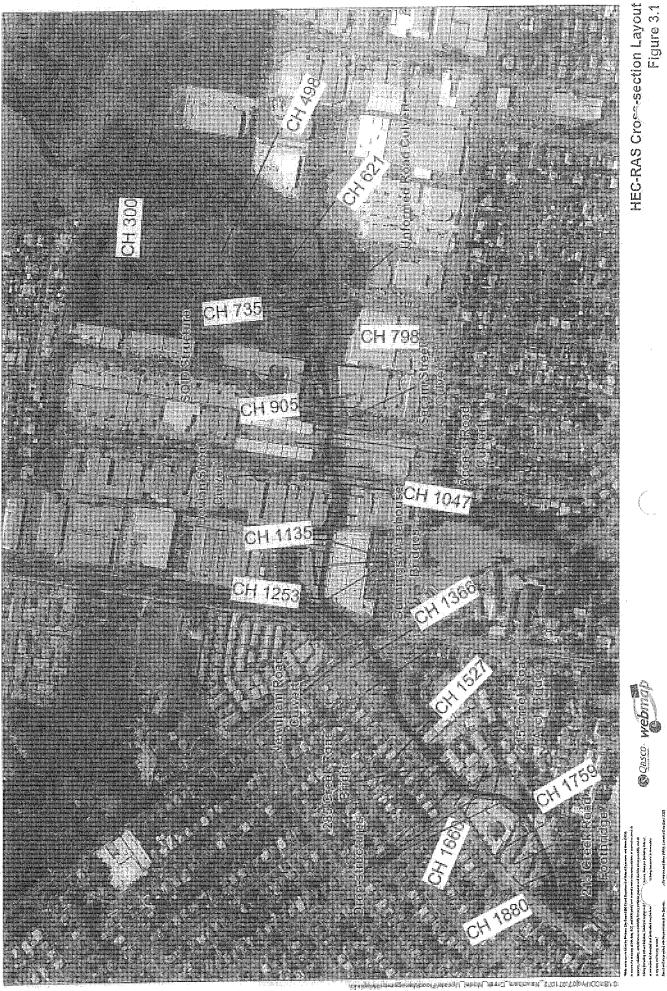
3.2.4 Hydraulic Structures

Within the model there are 15 hydraulic structures (6 bridges, 5 culverts, 3 drop-structures and 1 SQID). The configuration of each of the structures is given below in Table 3.1.

Table 3.1: Hydraulic Structure Details

HEC-RAS Chainage (m)	Structure	Configuration
749.0	Unformed Road structure	5 x Ø1650 mm piped culvert. Sizes and invert levels were assumed due to lack of survey and design information.
871.0	Secam Street SQID	Cross-sections from 'as constructed' drawings. Refer to plan W10273/2.
934.0	Secam Street structure	3 / 2400 x 2400 mm RCBCs.
959.0	Access Road structure	5 x Ø1800 mm piped culvert.
1029.0	Devlan Street structure	5 x Ø1800 mm piped culvert
1248.0 1160.0 1130.0	3 Bunnings Warehouse structures	3 x 10m Bridges. Sizes and invert levels were based on hand measurements.
1345.0	Newnham Road structure	4 x Ø1800 mm piped culvert.
1583,0	285 Creek Road structure	1 x 20m Bridge.
1752.9 1690.0 1643.0	3 drop-structures between 215 Creek Road and 285 Creek Road;	Cross-sections from 'design' drawings. Refer to plans W8357/5, W8357/10 and W8357/11.
1785.4	215 Creek Road structure	1 x 20m Arch Bridge. Sizes and invert levels were based on hand measurements.
1831.0	215 Creek Road structure	1 x 10m Footbridge. Sizes and invert levels were based on hand measurements.

The cross-sections at Chainages 1253 and 1243 have been aligned parallel and positioned upstream and downstream of the crossing. As the alignment of the crossing is not perpendicular to the flow direction, the "skew" option was used in the HEC-RAS model to reduce the cross-sectional area. For hydraulic structures containing handrails, full blockage of the handrail was assumed in the model.



3.2.5 Boundary Conditions

Peak discharge was used as the upstream boundary condition at Chainage 1880. A number of "flow change" locations were added to represent the increase in discharge in the downstream direction due to lateral inflows over the 1.9 km length of creek.

At the downstream boundary a "known water level" was used for each ARI event. The adopted values are shown in Table 3.2, these flood levels were extracted from the MIKE11 model after its calibration and verification against historic events.

Table 3.2: Downstream Tailwater Level

Design ARI	Flood level (m AHD)
2 year	10.09 (2 year ARI event in Bulimba Creek)
5 year	10.09 (2 year ARI event in Bulimba Creek)
10 year	10:56 (5 year ARI event in Bulimba Creek)
20 year	10.83 (10 year ARI event in Bulimba Creek)
50 year	11.09 (20 year ARI event in Bulimba Creek)
100 year	11.42 (50 year ARI event in Bulimba Creek)

3.3 Modelling Results

3.3.1 General

The HEC-RAS model was run for the 2, 5, 10, 20, 50 and 100 year ARI events. The complete tabulated results are shown in **Appendix I-2** and the flood level and velocity results are discussed separately in **Sections 3.3.2** and 3.3.3 respectively.

From the results, it is apparent that the bank full discharge of the main channel is quite variable and ranges from less than 2 year ARI to the 100 year ARI. The reach predominantly contains sub-critical flows for the full range of ARI events modelled. However, super critical flow is present at the drop structures in the concrete-lined trapezoidal channel.

The results show that during the 2 year and 5 year ARI events, hydraulic jumps occur at drop-structures 1 and 2. This may not happen in reality but the hydraulic jumps have minimal effect on the calculated flood levels.

3.3.2 Flood levels

The flood level results for the six ARI events modelled are shown in Table 3.3. The bracketed figures represent the head loss at the hydraulic structure. The respective flood inundation plots for each ARI event are shown in Appendix J.

Table 3.3: Flood Level Results

red bie di				Level (m AH)	I	
HEC-RAS Chainage	2 year ARI	5 year ARI	10 year ARI	20 year ARI	50 year ARI	100 year ARI
1880.0	24.1	24.4	24.4	24.5	24.6	24.9
1873.0	24.1	24.3	24.4	24.5	24.6	24.8
1866.0	24.0	24.2	24.3	24.3	24.5	24.8
1860.0	23.7	24.0	24.2	24.3	24.5	24.8
1854.0	23.7	24.0	24.2	24.3	24.5	24.8
1847.0	23.7	24.0	24.2	24.3	24.5	24.8
1841.0	23.6	24.0	24.2	24.3	24.5	24.8
1834.0	23.6	24.0	24.1	24.3	24.4	24.7
215 Creek Road Footbridge	(0.0)	(-0.1)	(0.0)	(-0.1)	(0.0)	(-0.1)
1828.0	23.6	23.9	24.1	24.2	24.4	24.6
1821.0	23.6	23.9	24.1	24.2	24.3	24.6
1815.0	23.6	23.9	24.1	24.2	24.3	24.6
1808.0	23.6	23.9	24.1	24.2	24.3	24.6
1802.0	23(6	23.9	24.1	24.2	24.3	24.6
1795.0	23.5	23.9	24.1	24.2	24.3	24.6
1790.0	23,4	(23,6	>23.8	23.8	24.0	24.2
1789.0	23.1	23.3	23.4	23.5	23.7	24.1
1788.8	22.8	23.3	23.5	23.8	24.0	24.3
15 Creek Road Arch Bridge	(-0.1)	(-0.2)	(-0.2)	(-0.2)	(=0.2)	(-0.3)
1782.0	22.7	23.1	23.3	23.6	23.8	24.0
1777.0	22.7	23.2	23.4	23.6	23.8	24.1
1771.0	22.7	23.2	23.4	23,6	23,8	24.1
1765.0	22.7	23.1	23.4	23.6	23.8	24.1
1759.0	22.7	23.1	23.4	23.6	23.8	24.1
1753.0	22.4	22.8	23.0	23.1	23.2	23.4
Drop Structure 1						
1752.9	22.6	23.0	23.1	23.3	23.4	23.6
1690.1	21.9	22.5	22.7	22.8	23.0	23.1
Drop Structure 2		1				
1690.0	20.1	20.4	20.7	20,9	21.1	21.3
1660.0	21.4	21.8	22.3	22.5	22.7	22.9
1643.1	20.7	21.2	22.1	22.2	22.5	22.6
Drop Structure 3					-	·T
1643.0	20.8	21.4	22.3	22,4	22.6	22.7
1625.6	20.4	21.3	22.2	22.3	22.6	22.7
1591.0	20,1	21.2	22.2	22.3	22.5	22.6
285 Creek Road Access Bridge	(-0.4)	(-1.2)	(-0.5)	(-0.4)	(-1.3)	(-0.9)
1576.0	19.7	20.0	20.7	20.9	21.2	21.7
1526.6	19.6	20.1	20.4	20.6	20.8	21.0
. 1411.0	19.3	19.9	20.1	20.2	20.4	20.6
1366.0	19.2	19.8	20.1	20.2	20.5	20.6
Newnham Road	(-1.2)	(-1.5)	(-1.5)	(-1.4)	(-0.8)	(-0.5)

	Flood Water Level (m AHD)								
HEC-RAS Chainage	2 year ARI	5 year ARI	10 year ARI	20 year ARI	50 year ARI	100 year ARI			
Culvert									
1317.0	18.0	18.3	18.6	18.8	19.7	20.1			
1282.0	17.8	18.3	18.6	18.9	19.7	20.0			
1253.0	17.9	18.4	18.7	18.9	19.7	20.1			
Bunnings Warehouse Bridge (U/S)	(-0.2)	(-0.2)	(-0.2)	(-0.2)	(-0.4)	(-0.4)			
1243.0	17.7	18.2	18.5	18.7	19.3	> 19.7			
1219.0	17.7	18.2	18.5	18.7	19.2	19.7			
1190.0	17.7	18.2	18.5	18.7	19.2	19.8			
1164.0	17.8	18.2	18.5	18.7	19.3	19.8			
Bunnings Warehouse Bridge (Middle)	(0.1)	(0.0)	(0.0)	(0.0)	(-0.1)	(-0.3)			
1156.0	17.7	18.2	18.5	18.7	19.3	19.5			
1147.0	17.7	18.1	18.4	18.5	19.0	19.3			
1135.0	17.7	18.2	18.4	18.6	19.1	19.3			
Bunnings Warehouse Bridge (D/S)	(0.0)	(0.0)	(0.0)	(0.0)	(-0.3)	(-0.3)			
1127.0	17.7	<18.2	18.4	18.6	18.8	19.0			
1125.0	17.7	18.1	18.4	18.6	18.8	19.1			
1099.0	17.1	17.9	18.1	18.2	18.4	18.5			
1066.0	17.0	17.9	18.1	18.2	18.4	18.5			
1047.0	17.0	17.9	18.1	18.2	18.5	18.6			
Devlan Street Culvert	(-0.7)	(-1.1)	(-1.0)	(-1.0)	(-1.1)	(-1.1)			
1013.0	16.3	16.8	17.1	17.2	17.4	17.5			
982.0	16.2	16.8	17.0	17.1	17.3	17.4			
Access Road Culvert	(-0.5)	(-0.5)	(-0.5)	(-0.4)	(-0.4)	(-0.4)			
948.0	15.7	16.3	16.5	16.7	16.9	17.0			
Secam Street Culvert	(-0.3)	(-0.6)	(-0.6)	(-0.7)	(-0.6)	(-0.6)			
918.0	15.4	15.7	15.9	16.0	16.3	16.4			
905.0	15.4	15.7	15.9	16.1	16.3	16.5			
904.9	15.4	15.8	16.0	16.1	16.3	16.5			
879.0	15.4	15.7	15.9	16.1	16.3	16.4			
SQID Inline Weir	(-0.1)	(0.0)	(0.0)	(-0.1)	(-0.1)	(0.0)			
870.0	15.3	15.7	15.9	16.0	16.2	16.4			
845.0	15.3	15.7	15.8	16.0	16.2	16.3			
798.0	15.1	15.5	15.6	15.7	15.9	16.0			
759.0	15,0	15.3	15.5	15.5	15.7	15.8			
Unformed Road Culvert	(-1.1)	.(-1.1)	(-1.1)	(-1.0)	(-1.1)	(-1.1)			
735.0	13.9	14.2	14.4	14.5	14.6	14.7			
621.0	12.7	12.9	13.1	13.2	13.4	13.5			
498.0	12.0	12,3	12.4	12.5	12.7	12.8			
300.0	10.1	10.1	10.6	10.8	11.1	11.4			

Inundation and flood immunity levels for each of the structures are given below in Table 3.4.

Table 3.4: Structure Inundation and Flood Immunity Levels

		Flood	Inundation Over Deck Level (m)						
Structure Name	Deck Level (m) AHD	Immunity (ARI)	2 year ARI	5 year ARI	10 year ARI	20 year ARI	50 year ARI	100 year ARI	
Unformed Road Culvert	15.00	2-уг	0.00	0.31	0.45	0.53	0.67	0.75	
Secam Street Culvert	16.00	2-уг	-0.32	0.30	0.54	0.67	0.89	1.02	
Access Road Culvert	16,20	< 2-yr	0.04	0.59	0.80	0.91	1.11	1.23	
Devlan Street Culvert	17.48	2-уг	-0.51	0.38	0.63	0.75	0.97	1.09	
Bunnings D/S Bridge	18.74	20-yr	-1.04	-0.57	-0.33	-0.19	0.32	0.59	
Bunnings Middle Bridge	18.99	20-уг	-1.24	-0.75	(-0.47	-0.29	0.31	0.80	
Bunnings U/S Bridge	19.70	20-уг	-1.82	-1.30	-0,98	-0.76	0.04	0.38	
Newnham Road Culvert	19.51 (south entrance)	2-ут	-1.22	0.32	0.56	0.68	0.97	1.12	
285 Creek Road Bridge	22.00	5 -уг	1.86	0:75	0.18	0.30	0.52	0,64	
215 Creek Road Arch Bridge	24.40	>100-yr	-1.57	-I:11	-0.86	-0.61	-0.39	-0.07	
215 Creek Road Footbridge	24:80	>100-yr	-1.18	-0.84	-0.67	-0.55	-0.38	-0.06	

Note: The figures in Italics indicate the flood water level below the deck level

There are four locations where in theory a hydraulic jump occurs within the trapezoidal concrete-lined channel. As expected, three of these locations are at the hydraulic drop structures. The fourth location is at the downstream end of the concrete-lined channel where the channel type changes from concrete-lined to the less efficient natural channel. The modelling shows that the hydraulic jumps will generally be 'flooded' out due to the turbulence of the water across the jump. This will result in a more stable water level profile. The longitudinal profile from the hydraulic model is shown in Figure 3.2.

3.3.3 Inundation Mapping

The flood immunity at various locations can be observed from the flood inundation plots presented in **Appendix J**, It should be noted that the elevation data used as the basis for the inundation mapping is dated to 2002. It does not necessarily accurately depict the present day surface elevations at the upstream development (215 Creek Road) where construction was completed after 2002. Therefore inundation lines corresponding to that location is represented by a dashed line on the flood inundation plots.

The flood inundation plots show that the 215 Creek Road development experiences inundation during the 50 year and 100 year ARI events. Creek Road is inundated during the 10, 20, 50 and 100 year ARI events, with similar results at the Newnham Road intersection. The Bunnings Warehouse main carpark is flooded during the 100 year ARI event while the rear goods storage area shows inundation during the 50 and 100 year ARI events. Further downstream, Secam and Devlan Streets show inundation during events larger than a 2 year ARI. Downstream of the SQID all flooding is confined to open space reserve and no properties are affected.

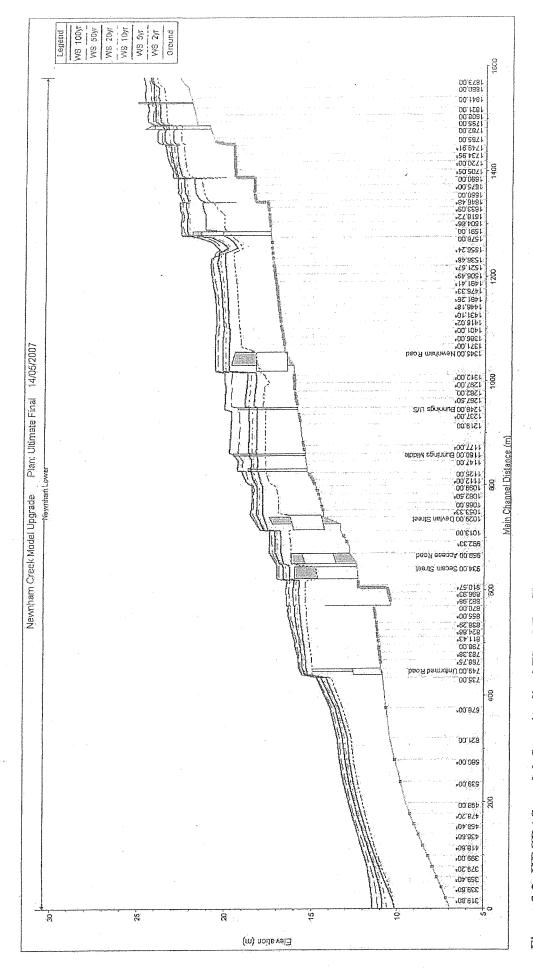


Figure 3.2: HECRAS model-Longitudinal Flood Profile

3.3.4 Velocities

Table 3.5 indicates the peak average velocities within the main channel for the length of creek modelled.

Table 3.5: Velocity Results

HEC-RAS Chainage						
(m)	2 year ARI	5 year ARI	10 year ARI	20 year ARI	50 year ARI	100 year ARI
1880.0	2.1	2.1	2.2	2.2	2.1	1.9
1873.0	1.9	2.0	2.1	2.1	2,1	2.0
1866.0	2.2	2.3	2.4	2.4	2.3	2.1
1860.0	2.9	2,8	2.7	2:5	2.4	2.1
1854.0	2.7	2.6	2.3	2.2	2,1	1.9
1847.0	2,4	2.2	2.0	1.8	1.7	1.5
1841.0	2.2	1.9	1/7	1.6	1.5	1.4
1834.0	2.0	2.0	1.9>	1.9	1.9	1.7
215 Creek Road Footbi	ridge					
1828.0	1.8	_/1.9	1.8	1.8	1.8	1.8
1821.0	1.8	1.9	1.9	2.0	2.0	2.0
1815.0	1.7	1.8	1.8	1.8	1.8	1.8
1808.0	\ 1.6 \	1.6	1.6	1.6	1.5	1.4
1802.0	1.5	1.4	1.4	1.5	1.4	1.3
1795.0	1.5/	1.5	1.5	1.5	1.6	1.5
1790.0	Ž.3	2.5	2.7	2,7	2.9	3.0
1789.0	3.2	3.5	3.6	3.7	3.7	3.4
1788.8	1.8	1.9	1.9	1.9	1.9	2.0
215 Creek Road Arch I	Bridge					
1782.0	1.9	2.1	2.1	2.1	2.2	2.3
1777.0	1.5	1.5	1.5	1.4	1.4	1.5
1771.0	1.5	1.4	1.4	1.3	1.3	1.4
1765.0	1.4	1.4	1.4	1.3	1.3	1.4
1759.0	1.4	1.4	1.4	1.3	1.3	1.3
1753.0	2.5	2.8	3.0	3.3	3.5	3.8
Drop Structure 1						
1752.9	1.7	1.9	2.1	2.4	2.5	2.7
1690.1	3.7	3.5	3.6	3.8	3.9	4.1
Drop Structure 2						
1690.0	6.8	6.9	6.9	6.9	6.9	7.0
1660.0	1.7	1.8	1.6	1.7	1.6	1.6
1643.1	3.7	3.7	2.5	2.8	2.7	3.0
Drop Structure 3						
1643.0	2.2	1.9	1.3	1.4	1.4	1.5
1625.6	2.8	1.9	1.1	1.2	1,2	1.2
1591.0	3.0	2.3	1.6	1.8	1.9	2.1
285 Creek Road Access	Bridge					
1576.0	4.2	4.8	3.8	3.8	4,1	3.3
1526.6	2.1	2.1	2.0	1.9	1.7	1.7
1411.0	1.4	1.5	1.7	1.8	1.9	1.9

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HEC-RAS Chainage	Average Velocity (m/s)								
(m)	2 year ARI	5 year ARI	10 year ARI	20 year ARI	50 year ARI	100 year ARI			
1366.0	1.6	0.8	0.7	0.7	0.6	0.6			
Newnham Road Culve	rt								
1317.0	2.8	3.4	3.5	3.6	3.0	2.5			
1282.0	2.2	2.4	2.6	2.7	2.4	2.5			
1253.0	1.5	1.6	1.7	1.8	1.7	1.7			
Bunnings Warehouse I	Bridge (U/S)								
1243.0	2.1	2.3	2.5	2.6	2.7	^{در} * 2.7			
1219.0	1.9	2.2	2.5	2.6	2.8	2.5			
1190.0	1.8	2.1	2.4	2.5	2.6	2:3			
1164.0	1.6	1.9	2.2	2.3	2.2	2.0			
Bunnings Warehouse I	Bridge (Midd	le)							
1156.0	7. 1.7.	1.9	2.2	2.3	2.3	2.3			
1147.0	1.9	2.2	2.5	2.7	2.9	2.9			
1135.0	1.6	1.9	2.2	2.4	2,6	2.6			
Bunnings Warehouse I	Bridge (D/S)								
1127.0	1.6	1.9	2.2	2.4	2.8	3.0			
1125.0	1.8	2.0	2.2	2.3	2.6	2.7			
1099.0	3:0	₹2.5	>2.8	3.0	3.4	3.8			
1066.0	1.9\	1.5	1.7	1.8	2.1	2.3			
1047.0	1.0	0.9	1.0	1.0	1.0	1.1			
Devlan Street Culvert					Y	T -			
1013.0	0.9	1.0	1.2	1.3	1.5	1.6			
982.0	1.3	1.3	1.4	1.5	1.6	1.7			
Access Road Culvert					1	T			
948.0	0.8	0.8	0.9	0.9	1.0	1.0			
Secam Street Culvert						T 6.			
918.0	1.1	1.4	1.6	1.7	1.9	2.1			
905.0	0.6	0.7	0.9	0.9	1.1	1.2			
904.9	0.3	0.4	0.5	0.6	0.7	0.8			
879.0	0.6	0.8	0.9	1.0	1.2	1.3			
SQID Inline Weir									
870.0	1.2	1.4	1.6	1.7	I.9	2.1			
845.0	0.6	0.7	0.8	0.9	1.0	1.1			
798.0	0.7	0.8	0.8	0.9	1.0	1.1			
759.0	0.7	0.7	0.8	0.9	1.0	1.1			
Unformed Road Culve	rt		r-		T	1.4			
735.0	1.0	1.1	1.2	1.2	1.3	1.4			
621.0	0.4	0.5	0.5	0.5	0.6	0.6			
498.0	0.9	0.9	1.0	1.0	1.1	1.1			
300.0	0.6	0.9	0.7	0.6	0.6	0.6			

The velocities are quite varied along the length of the study reach. This is predominantly because of the many different channel types and the presence of numerous hydraulic structures; such as weirs, drop structures, bridges and culverts.

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The engineered rock-lined channel within the residential development at 215 Creek Road (Ch.1880 to Ch.1759) contains velocities ranging from approximately 1.3 m/s to 2.3 m/s. A 0.7 m drop in the channel invert level, upstream of the Arch Bridge, causes a spike in velocities. At this location the velocities reach up to 3.7 m/s. The flow is predominantly sub-critical within this reach of the creek.

Within the trapezoidal concrete-lined channel (Ch.1753 to Ch.1527), there are numerous spikes in the velocity profile due to the presence of the hydraulic drop structures at the Chainages 1752.9, 1690 and 1643. As a result, the velocities range from approximately 1.4m/s to 7.0m/s.

Within the short length of natural channel between the concrete-lined channels (Ch.1527 to Ch.1282), the velocities are generally back to below 2m/s, apart from immediately downstream of the Newnham Road Culvert. The flow is almost entirely sub-critical within this length of creek.

The next section of Newnham Creek consists of a concrete-lined channel (Ch.1282 to Ch.1127). The velocities in this section are slightly higher than those in the natural channel segment, ranging from approximately 1.5m/s to 2.9m/s. The flow in this section is sub-critical.

The final section consists of natural channel and is the longest reach of the creek (Ch.1125 to Ch.300). The velocities here are lower, ranging from approximately 0.5m/s to 1.4m/s. There is a spike in velocities at the SQID structure, with increases up to 2.3m/s. All flow in this section is sub-critical.

4.0 Conclusion

BCC City Design Flood Management have undertaken hydraulic modelling of Newnham Creek using HEC-RAS (Version 3.1.3) for steady flow conditions. The hydraulic modelling assumed the presence of Minimum Riparian Corridor (MRC) from immediately downstream of the Secam Street Stormwater Quality Improvement Device (SQID) to the confluence with Bulimba Creek.

The new model was created using the previous BCC HEC-RAS model combined with the 215 Creek Road Development model (containing field survey taken in 2002) and updated with Airborne Laser Scanning (ALS) data and hand measurements taken during site visits. The extents of the model were from immediately upstream of the 215 Creek Road residential development to the confluence with Bulimba Creek. The model incorporated 15 hydraulic structures (6 bridges, 5 culverts, 3 drop-structures and 1 SQID device).

The results of the hydraulic modelling indicate that:

- The Access Road has a very low flooding immunity, overtopping in the 2 year ARI event;
- Secam Street, Devlan Street, Newmann Road and the Unformed Road have low flooding immunity, all being overtopped in the 5 year ARI event;
- The 285 Creek Road Access Bridge has average flooding immunity, being only overtopped in the 10 year ARI event;
- The Up Stream (U/S), Middle and Down Stream (D/S) Bunnings Warehouse Bridges (Ch. 1248, 1160 and 1131 respectively) have high flooding immunity, with the deck only overtopped in the 50 year ARI event;
- The 215 Creek Road Footbridge and Arch Bridge have flood immunities greater than 100 year ARI.

The flood inundation plots show that:

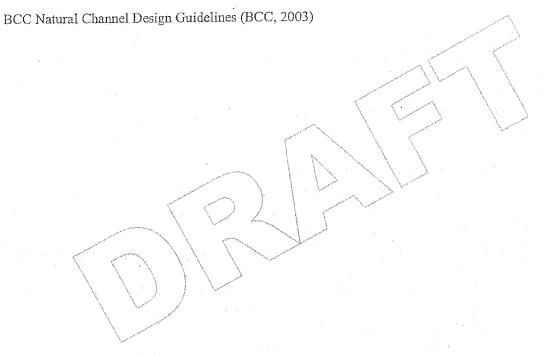
- The 215 Creek Road development exhibits inundation during the 50 year and 100 year ARI events;
- Creek Road is inundated during the 10, 20, 50 and 100 year ARI events, with similar results at the Newnham Road intersection;
- The Bunnings Warehouse main carpark is flooded during the 100 year ARI event while the rear storage area shows inundation during the 50 and 100 year ARI events;
- Secam and Devlan Streets show inundation during events larger than a 2 year ARI; and
- Downstream of the SQID all flooding is confined to open space reserve and no properties are affected.

The velocities are quite varied along the length of the study reach in all events. This is predominantly because of the effects of hydraulic drop-structures, concrete-lined and natural channels and the MRC. The minimum velocity, which is in the vicinity of 0.4 m/s, occurs in the SQID structure. The maximum velocity, which is in the vicinity of 7.0 m/s, occurs in the trapezoidal concrete-lined channel in the 100 year ARI event at the hydraulic drop structure located at Ch. 1690.

5.0 References

Waterway Management Plan (BCC, 2003c)

Guidelines for Flood Regulation Line and Minimum Fill Level Assessment (BCC, 1994).



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Bulimba Creek Flood Study Report E - Phillips Creek Flood Investigations

June 2011

Prepared for Water Resources

Prepared by
Water & Environment
City Design

City Design

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Approved

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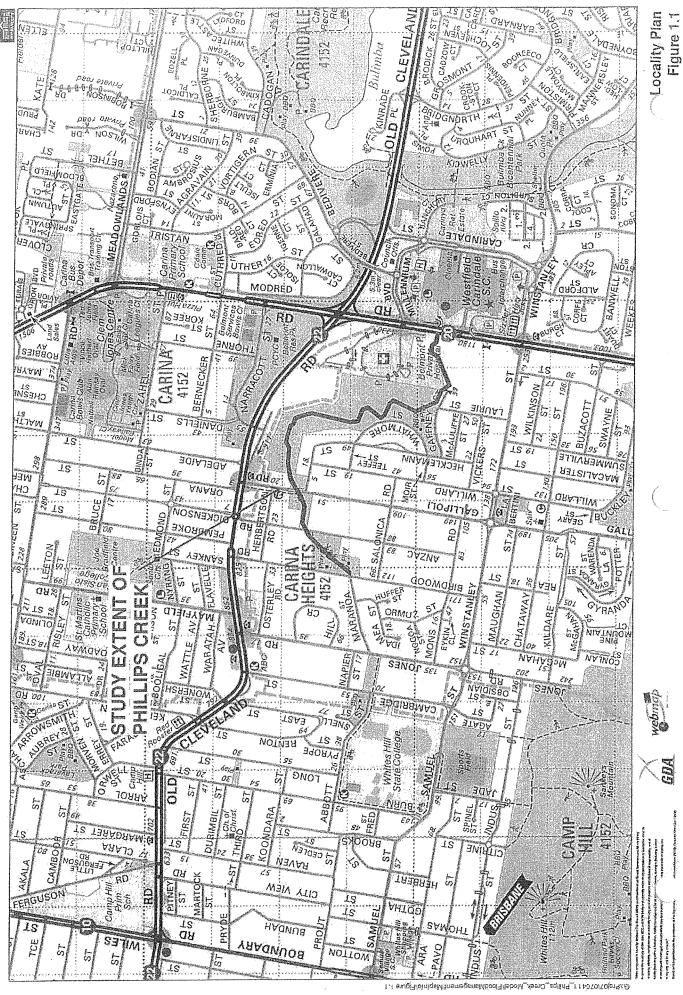
1.0 Introduction

The investigation involves the hydraulic analysis of the waterway section of Phillips Creek between Birdwood Road and Creek Road. The study involves the establishment of a HEC-RAS hydraulic model to determine flood levels and flooding characteristics. Flooding events from the 2 year ARI to the 100 year ARI have been considered.

Historically, there has not been a hydraulic model for Phillips Creek. However, early in 2007 a HEC-RAS model was created to assess the flooding impacts of two bikeway bridges in the vicinity of Creek Road. The hydraulic model used in this investigation extended from Creek Road to Gallipoli Road.

For this investigation, the HEC-RAS model was extended further from Gallipoli Road to Birdwood Road. Upstream of Birdwood Road the old creek channel is piped. Figure 1.1 indicates the locality of the creek and the extent of the waterway for which the model has been created.

J.



2.0 Catchment Hydrology

2.1 Catchment Description

The Phillips Creek Catchment forms part of the greater Bulimba Creek Catchment and includes areas within the suburbs of Camp Hill and Carina. The contributing catchment area to Creek Road is approximately 3.6km^2 and is indicated in Figure 2.1. The catchment falls from an elevation of 110m AHD at Whites Hill Reserve to approximately 5.7m AHD at the upstream side of Creek Road. The catchment is effectively developed and a significant portion of the upper catchment is forested, whereas the middle and lower sections are predominantly urban residential, with some green space adjacent the waterway.

2.2 Creek Characteristics

Hydraulic modelling of Phillips Creek has been undertaken using HEC-RAS (Version 3.1.3) for steady flow conditions, to a total length of approximately 1.6 kms as a part of this investigation. The main channel width varies from approximately 10 to 20m and the depth varies from approximately 2 to 4m. The average bed slope of the creek within the study area is 0.6 % (1 in 167).

The analysed section of the Philips Creek waterway extended immediately downstream of Birdwood Road to the upstream side of Creek Road. Within this reach, the creek passes through two road crossings. The first crossing is at Anzac Road and the second at Gallipoli Road. Further downstream there are two proposed bikeway bridges, one across Phillips Creek and the other across a tributary channel. The creek forms part of a large valley and there are no distinctive floodplains associated with the creek.

Upstream of Gallipoli Road, the creek is in a somewhat natural condition and flows through open space parkland with private properties at close proximity on both sides. The over-banks are characterised by maintained grassed areas with scattered large trees.

Downstream of Gallipoli Road, the creek is heavily vegetated with weeds, shrubs and established trees. The low flow channel meanders within the overall creek cross-section within this reach of the creek.

The section of Phillips Creek immediately upstream of Creek Road within the Belmont Specialist Centre property was re-aligned in 1984, as part of a development approval. The creek was effectively straightened and was considerably shortened, increasing the gradient of the creek. The creek was further re-aligned in 1998, again as part of development within this property.

Downstream of Creek Road the waterway has been piped underneath the Carindale Shopping Centre and Old Cleveland Road. Downstream of Old Cleveland Road the waterway passes through a Stormwater Quality Improvement Device (SQID) then on to Bulimba Creek. Modelling of this complex section of waterway downstream of Creek Road was outside the scope of this investigation.

2.3 Discharge Calculations

The Rational Method was used to determine the peak discharge at three locations along the 1.6 km creek length. The peak discharge was used as input into the steady state HEC-RAS model. As calibration data is not available for this creek it wasn't deemed necessary to undertake more rigorous analysis involving hydrologic modelling. Calculations were undertaken for the 2, 5, 10, 20, 50 and 100 year ARI events and were based on "Ultimate" catchment conditions according to the current City Plan (2000). The calculations assumed an impervious area percentage of approximately 35%.

The input parameters and results of the Rational Method calculations are shown in Table 2.1. Further details of these calculations are presented in Appendix L.

Table 2.1: Adopted Peak Discharge

				Discharge (m³/s)						
Location	Catchment Area (ha)	t _c (mins)	2 year ARI	5 year ARI	10 year ARI	20 year ARI	50 year ARI	100 year ARI		
At Anzac Road	275.0	38.7	30.5	44.1	53.5	65.4	85.1	99.4		
At Gallipóli Road	283.8	40.0	30.6	45.2	54.3	66.0	86.4	101.0		
At Creek Road	361.4	51.0	34.1	49.9	60.2	73.8	96.8	113.0		

3.0 Hydraulic Modelling

3.1 General

The hydraulic analysis was undertaken using the HEC-RAS (Version 3.1.3) hydraulic modelling software. Steady flow conditions were used as it was considered that flood storage effects and attenuation due to hydraulic structures would be minimal. Also, this methodology was consistent with previous modelling undertaken for the bikeway bridges.

There are no hydrometric records for Phillips Creek; therefore the model was unable to be verified against historical storm events.

Section 3.2 details the set-up and assumptions used in the modelling. The modelling results are presented in Section 3.3.

3.2 HEC-RAS Model Set-up

3.2.1 Cross Sections

The HEC-RAS model for the 1.6 km length of creek was comprised of 21 cross-sections, as shown in Figure 3.1.

The cross-section data for the modelling was obtained from the following sources:

- From Chainages 4 to 966, the cross-sectional data was primarily obtained from December 2006 field survey spot levels
- From Chainages 119 and 125, the cross-sectional data was obtained from a DTM (Digital Terrain Model) of the December 2006 field survey.
- From Chainages 1066 to 1580, the cross-sectional data was obtained from a combination of December 2006 field survey spot levels and BCC Airborne Laser Scanning (ALS) data.

The HEC-RAS model extents are from immediately downstream of Birdwood Road (Chainage 1580) to immediately upstream of Creek Road (Chainage 4).

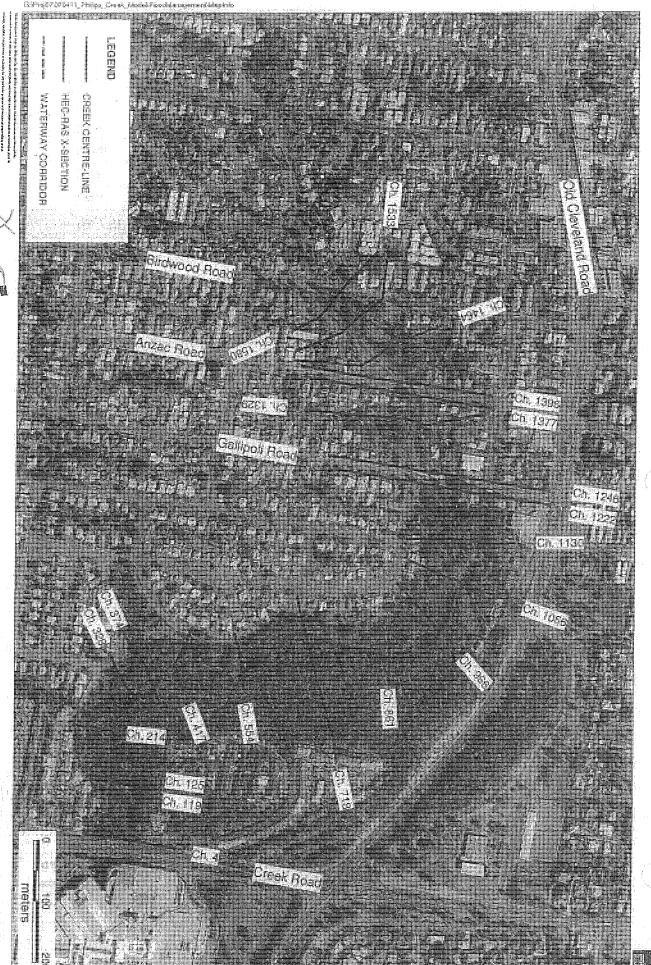
3.2.2 Waterway Corridor

A waterway corridor was incorporated into the HEC-RAS modelling. The waterway corridor was taken from the most recent regulatory information from City Plan (2000) and is also indicated in Figure 3.1.

3.2.3 Manning's 'n'

A Manning's 'n' value of 0.15 was used to represent the Minimum Riparian Corridor (MRC), which typically represents a distance of 15m either side of the bank of the main channel.

For areas outside the MRC, the Manning's 'n' values were obtained with reference to a site inspection, aerial photography and hydraulic roughness literature. A Manning's 'n' value of 0.05 was generally



HEC-RAS Cross-section Layout Figure 3.1 used for the main channel. Upstream of Gallipoli Road, Manning's 'n' values between 0.03 to 0.06 were used to represent the over-bank areas. Downstream of Gallipoli Road a value of 0.08 was used to represent the over-bank areas.

3.2.4 Hydraulic Structures

Within the study area, there are three crossings over Phillips Creek:

- At Anzac Road (Chainage 1387) the structure consists of a 510 1800 mm piped culvert.
- At Gallipoli Road (Chainage 1234) the structure also consists of a 5 / Ø 1800 mm piped culvert.
- At Chainage 122 there is a proposed low-level bikeway bridge, which has been included in the model

The cross-sections at Chainages 119, 125, 1222, 1246, 1377 and 1396 have been aligned parallel and positioned upstream / downstream of the crossings. As the alignment of all three crossings is not perpendicular to the flow direction, the skew option was used in HEC-RAS model to reduce the cross-sectional area. All hydraulic structures were modelled assuming full blockage of the handrail and the Energy Equation results were adopted.

3.2.5 Boundary Conditions

At Chainage 1580 of the HEC-RAS model the upstream boundary condition was represented by the peak discharge. To represent lateral inflows along the 1.6km length of creek, the flow was increased in the downstream direction at these locations.

At the downstream boundary a known water level was used for each ARI event. The adopted values are shown in Table 3.1 and were obtained from the *Draft Design Report for the Phillips Creek Sewer Stabilisation Works* (2001), which investigated a section of the creek upstream of Creek Road. The 20 year ARI event flood level was not available, so it was interpolated at this location. As the creek has a reasonable longitudinal bed slope, any accuracy limitations with selection of the tail water level will only influence flood levels locally upstream of Creek Road.

Table 3.1: Downstream Tail water Level

Design ARI	Flood level (m AHD)
2 year	8.4
5 year	9.2
10 year	9.5
20 year	9.8
50 year	10.2
100 year	10.6

3.3 Modelling Results

3.3.1 General

The HEC-RAS model was run for the 2 year to 100 year ARI events. The complete tabulated results are shown in Appendix I-2 and the flood level and velocity results are discussed separately in Sections 3.3.2 and 3.3.3 respectively. Section 3.3.4 shows a comparison between the current 100 year ARI level used for flood planning purposes and the results of this study.

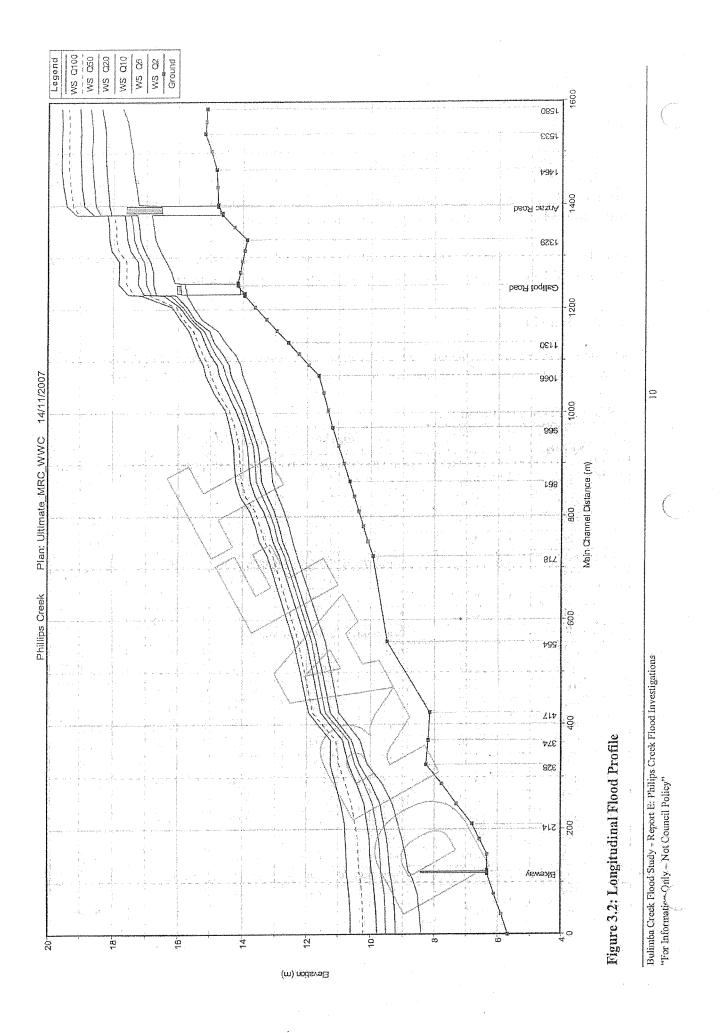
From the results, it is apparent that the bank full discharge of the main channel of the creek is less than the 2 year ARI and the flow is sub-critical for the full range of ARI eyents modelled.

3.3.2 Flood levels

The flood level results for the six ARI events modelled are shown in Table 3.2 and graphically in Figure 3.2. The respective flood inundation plot for each ARI event is shown in Appendix J.

Table 3.2: Flood Level Results

Table 5.2. Flood 2.c	TO RECORDED					
Chainage			Floodwater L	evel (m AHD)		
Chaine	2 year ARI	5 year ARI	10 year ARI	20 year ARI	50 year ARI	100 year AR
1580 \	17.71	18.34	18.70	19.03	19.38	19.59
1533	17.50	18.24	18.64	18.99	19.36	19.57
1464	17.38	18.22	18.64	19.00	19,37	19.59
1396	17.23	18.12	18.54	18.89	19,24	19.44
Anzac Rd Culvert		Minimun	n level for over	topping ~ 17.60	D m AHD	
1377	16.83	17.27	17.46	17.66	17.97	18.17
1329	16.70	17.17	17.37	17.58	17.91	18.12
1246	16.12	16.77	17.00	17.24	17.60	17.83
Gallipoli Rd Culvert		Minimun	n level for over	topping ~ 16.03	5 m AHD	
1222	15.74	16.06	16.24	16.46	16.87	17.14
1130	14.54	14.90	15,04	15.19	15.40	15.53
1066	13.99	14.35	14.52	14.72	14.99	15.15
966	13.44	13.72	13.86	14.00	14.24	14.39
861	13.08	13.41	13.58	13.76	14,04	14.22
718	12.30	12.56	12.69	12.84	13.07	13.21
554	11.42	11.69	11.84	12.00	12.25	12.40
417	10.98	11.25	11.40	11.56	11.80	11.93
374	10.34	10.59	10.71	10.88	11.08	11.24
328	10.09	10.35	10.49	10.68	10.99	11.24
214	9.13	9.59	9.82	10.09	10.46	10.81
125	8.79	9.40	9.67	9.96	10.36	10.74
Proposed Bridge		Minimur	n level for over	topping ~ 8.25	m AHD	
119	8.72	9.36	9.64	9.94	10.34	10.72
4	8.40	9.20	9.50	9.80	10.20	10.60
						



From these results, it is apparent that:

- Both Anzac Road and Gallipoli Road culvert crossings have very low flooding immunity.
- Anzac Road has flood immunity of between 2 year to 5 year ARI and Gallipoli Road has flood immunity of approximately 2 year ARI.
- Anzac Road is inundated by approximately 0.50m in the 5 year ARI event and 1.85m in the 100 year ARI event.
- Gallipoli Road is inundated by approximately 0.7m in the 5 year ARI event and 1.80m in the 100 year ARI event.

The proposed low-level bikeway bridge at Chainage 122 is inundated by all ARI events modelled. In the 2 year ARI event the bridge is inundated by approximately 0.55m and in the 100 year ARI event by approximately 2.5m.

3.3.3 Velocities

Table 3.3 indicates the peak average velocities within the main channel for the length of creek modelled.

Table 3.3: Velocity Results

Chainage	Main Channel Peak Average Velocity (m/s)					
	2 year ARI	5 year ARI	10 year ARI	20 year ARI	50 year ARI	100 year ARI
1580	1.8	1.8	1.9	2.0	2.2	2.4
1533	1.5	1.4	1.4	1.5	1.6	1.8
1464	1.1	0.9	0.8	0.9	0.9	·- [1,0]
1396	1.3	1.2	1.2	1.3	1.5	1.6
Anzac Rd Culvert				100		
1377	1.1	1.3	1.4	1.6	1.8	1.9
1329	1.2	1.2	1.2	1.2	1.3	1.3
1246	1.7	1.4	1.3	1.3	1.3	1.3
Gallipoli Rd Culvert						
1222	1.4	1.7	1.9	2.1	2.2.	2.2
1130	* 1.8	1.7	1.7	1.7	1.8	1.9
1066	1.4	1.6	1.8	1.8	1.8	1.9
966	1.5	1.8	2.0	2.2	2,3	2.4
861	0.9	1.0	1.1	1.1	1.3	1.3
718	1.9	2.2	2.4	2.6	2.9	3.1
554	1.8	2.0	2.1	2.1	2.3	2.4
417	1.4	1.6	1,7	1.9	2.1	2.2
374	2.9	3.1	3,3	3.4	3.6	3.6
328	1.7	1.8	1.8	1.8	1.9	1.8
214	1.6	1,7	1.8	1.9	2,0	2.0
125	1.5	1,3	1.3	1.3	1.4	1.4
Proposed Bridge			,	,		
119	1.6	1.3	1.3	1.4	1.4	1.4
4	1.0	1.0	1.0	1.1	1.2	1.2

There is a wide range of velocities along the length of the study reach. The minimum velocity, which is in the vicinity of 0.83m/s, occurs at Chainage 1464 in the 10 year ARI event. The maximum velocity, which is in the vicinity of 3.63m/s, occurs at Chainage 374 in the 100 year ARI event.

During an inspection of the site it was observed that downstream of Gallipoli Road there were a number of locations where erosion was occurring on the outside of bends within the main channel. Whilst bank erosion is a natural occurrence in creek systems, the degree of bank erosion would suggest that the creek has still to reach equilibrium conditions. One of these locations is in the vicinity of Chainage 966 and another is in the vicinity of Chainage 214. Excessively high velocities are not reflected in the HEC-RAS results at these locations. This is most likely because the modelling doesn't consider the current conditions, but rather considers the future flood planning scenario (MRC and waterway corridor) where velocities would be lower than existing.

3.3.4 Comparison with Current Flood Planning Level

As there is no existing hydraulic model for the creek, the current 100 year ARI levels used for flood planning purposes are based on the highest recorded flood level plus 0.7m. A comparison between this level and the Ultimate 100 year ARI level determined as part of this study is shown in Figures 3.3 and 3.4.

From Figure 3.3 it is apparent that the current level used for 100 year ARI flood planning purposes is significantly above the Ultimate 100 year ARI level; at some locations the difference is up to 1.1m. This difference is most likely very conservative as the current level used for 100 year ARI flood planning purposes incorporates a significant degree of interpolation between recorded debris marks. However, in terms of flood inundation extents, there is very little difference. This is because areas adjacent the creek are relatively steep and therefore a vertical change in flood level does not translate to a significant increase in lateral flooding extents.

Recorded flood levels measured from debris marks. No Maximum Height Gauges are present within the catchment.

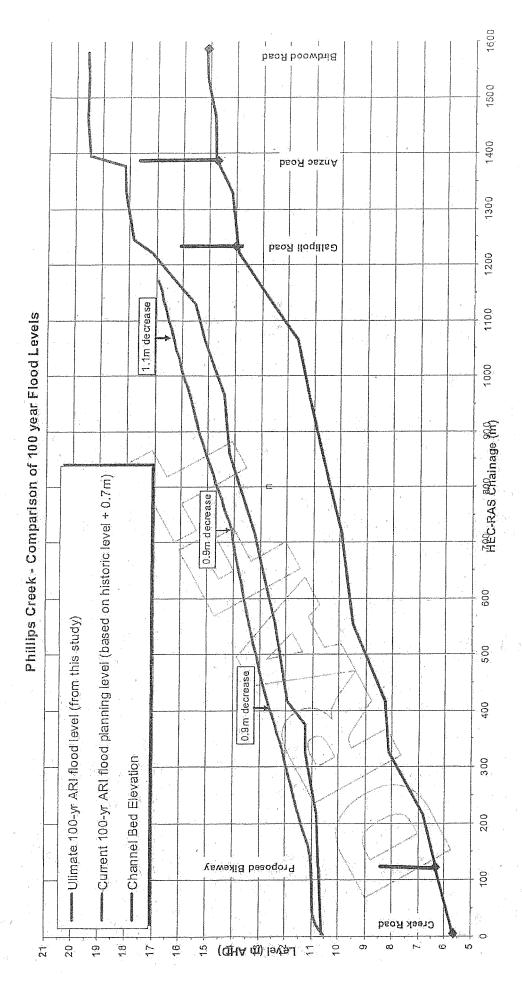


Figure 3.3: Comparison of 100 year ARI Flood Levels

Bulimba Creek Flood Study - Report E: Philips Creek Flood Investigations "For Information Only - Not Council Policy"

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4.0 Conclusion

Hydraulic modelling of Phillips Creek has been undertaken using HEC-RAS (Version 3.1.3) for steady flow conditions. The hydraulic modelling assumed the presence of both a waterway corridor and Minimum Riparian Corridor (MRC). The model was created predominantly from field survey undertaken in December 2006. Hydrologic calculations were undertaken using the Rational Method, assuming ultimate catchment development to the current Brisbane City Plan (2000). The model extended from immediately downstream of Birdwood Road to immediately upstream of Creek Road, approximately 1.6 km. The location was shown in Figure 1.1.

The model incorporated road crossings at Anzac Road and Gallipoli Road together with a proposed bikeway crossing located near Creek Road. The results of the hydraulic modelling indicate that both road crossings have very low flooding immunity. At Anzac Road the flood immunity is between 2 year to 5 year ARI and at Gallipoli Road the flood immunity is approximately 2 year ARI. The proposed low-level bikeway bridge is inundated by all ARI events modelled. There are a number of properties with low flood immunity in the immediate vicinity of the Anzac and Gallipoli Road crossings, as shown in the flood inundation maps in Appendix J.

The current 100 year ARI flood level used for flood planning purposes is significantly higher than the 100 year ARI flood level determined in this study. At some locations the difference is up to 1.1m. The flood levels currently used for flood planning purposes are derived from interpolation between records from the highest recorded creek flooding. While the flood level difference may seem large, there is very little difference in flood inundation extents as areas adjacent the creek are relatively steep, and a vertical change in flood level does not translate to a significant increase in lateral flood extents.

5.0 References

BCC 2000, Brisbane City Plan 2000, Brisbane City Council, Brisbane

Draft Design Report for the Phillips Creek Sewer Stabilisation Works (2001)

Appendix L: Rational Method Calculations

Creek Road Catchment				
Catchment Area	361 ha			
Impervious Fraction	0.35			
Overland Flow Length	200m			
Piped Flow Length	3000m			
Open Channel Flow Length	1600m			
Overland Flow Time	20 mins			
Piped Flow Time	17 mins			
Open Channel Flow Time	13 mins			
Total Time	51 mins			

Creek Road Catchment				
ARI (yrs)	C	I (mm/hr)	Q (m ³ /s)	
2	0.65	52	34.1	
5	0.73	68	49.9	
10	0.77	778	60.2	
20	0.81	191	73.8	
50	0.88	109	\96.8	
100 \	0.92	<u></u>	113.0	

Anzac Road Catchme	nt
Catchment Area	275 ha
Impervious Fraction	0.35
Overland Flow Length	200m
Piped Flow Length	√3000m
Open Channel Flow Length	200m
Overland Flow Time	20 mins
Piped Flow Time	17 mins
Open Channel Flow Time	2 mins
Total Time	39 mins

Anzac Road Catchment				
ARI (yrs) C		I (mm/hr)	$Q (m^3/s)$	
2	0.65	61	30.5	
5	0.73	79	44.1	
10	0.77	91	53.5	
20	0.81	106	65.4	
50	0.88	126	85.1	
100	0.92	141	99.4	

Gallipoli Road Catchment				
Catchment Area	286 ha			
Impervious Fraction	0.35			
Overland Flow Length	200m			
Piped Flow Length	3000m			
Open Channel Flow Length	350m			
Overland Flow Time	20 mins			
Piped Flow Time	17 mins			
Open Channel Flow Time	3 mins			
Total Time	40 mins			

Gallipoli Road Catchment				
ARI (yrs)	C	I (mm/hr)	Q (m ³ /s)	
2	0.65	59	30.6	
5	0.73	78	45.2	
10	0.77	89	54.3	
20	0.81	103	66.0	
50	0.88	123	86.4	
100	0.92	138	101.0	

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Bulimba Creek Flood Study Report F - Salvin Creek Flood Investigation

June 2011

Prepared for Brisbane City Council Water Resources

Prepared by
Water & Environment
City Design



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1.0 Introduction

Salvin Creek is a small tributary of Bulimba Creek located in Brisbane's southern suburbs as indicated in Figure 1.1. The creek catchment comprises an area of 5.4 km². The Salvin Tributary junction with Bulimba Creek is in the vicinity of Meadowbank Street in Carindale. The Creek consists of two main branches:

- The main reach merges with Bulimba Creek near Meadowbank Street, Carindale and extends upstream to Cavendish Road, Mt Gravatt East.
- The Glengariff reach separates from the main reach just upstream of Creek Road near Glengariff Street, Mt Gravatt East and extends upstream to the quarry located within Whites Hill Reserve, north of Pine Mountain Road.

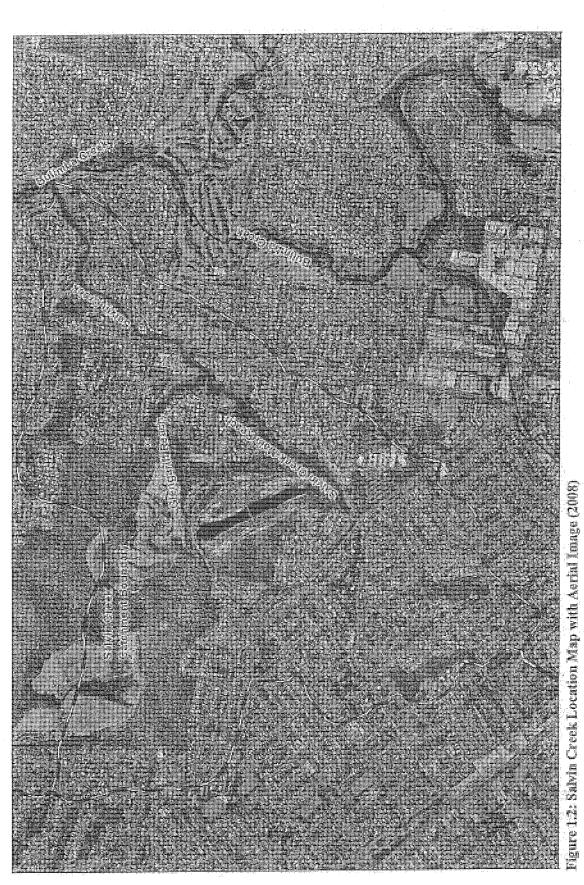
Salvin Creek flows with a steep gradient and crosses Tristania Street and Pine Mountain Road in Mt Gravatt East, and Creek Road and Donnington Street (2 crossings) in Carindale.

The Salvin Creek Flood Investigation includes the hydraulic analysis of both the main and Glengariff reaches. The study involves the establishment of a HEC-RAS hydraulic model to determine flood levels for the 2, 5, 10, 20, 50 and 100 year ARI design events for the waterway. The flood levels derived from this study will be used as the basis in updating the Council's design flood level records.

Figures 1.1 and 1.2 indicate the locality of the creek and the extent of the open waterway for which the hydraulic model has been created.

Figure 1.1: Salvin Creek Location Map

Bulimba Creek Flood Study - Report F: Salvin Creek Flood Investigation



Bulimba Creek Flood Study - Report F: Salvin Creek Flood Investigation

2.0 Catchment Hydrology

2.1 Catchment Description

The Salvin Creek Catchment forms part of the Bulimba Creek Catchment and is located within the suburbs of Mt Gravatt East, Holland Park, Carina Heights and Carindale. The contributing catchment area of Salvin Creek up to the confluence with Bulimba Creek is approximately 5.4 km², of which almost 2.0 km² feeds the Glengariff Tributary. A portion of the catchment within the Glengariff tributary is forested as part of the Whites Hill Reserve in Carina Heights. The remaining parts of catchment are occupied by the urban residential and commercial developments. Figure 1.1B shows the extent of the Salvin Creek Catchment.

2.2 Creek Characteristics

The main reach of Salvin Creek begins immediately west of Cavendish Road, Mt Gravatt East. At this point, catchment runoff exits as pipe drainage from the road crossing at an elevation of approximately 40 m AHD and flows for nearly 2.7 km to reach Bulimba Creek.

The Glengariff tributary originates in the Whites Hill Reserve at an elevation of about 70 m AHD. The bed gradient of the Glengariff tributary is steeper than the main reach of the Salvin Creek. The average bed slope of the creek within the study area is approximately 1.0 % (1 in 100). The length of this reach considered for modelling is nearly 1 km.

The Creek has been divided into upper and lower reaches for the purpose of modelling in the HEC-RAS hydraulic (steady flow) model. The Upper reach is defined as that part of the creek located between Cavendish Road and its junction with the Glengariff tributary, and has a length of about 1.2 km. The remainder of the main reach up to Bulimba Creek is named as the Lower reach and it occupies a length of about 1.5 km.

2.3 Discharge Calculations

The WBNM hydrologic model developed for the entire Bulimba Creek Catchment was used to derive design event flows for Salvin Creek Catchment. Details of the extracted flow rates are listed in **Table 2.1** below.

Within the WBNM model the Salvin Creek Catchment contains five sub-catchments; two of these are located in the Glengariff reach, two in the Upperr reach and the last in the Lower reach. Flow rates generated by the WBNM hydrologic model for 2, 5, 10, 20, 50 and 100 year ARI events were extracted and adopted in the HEC-RAS model.

In reviewing the layout of contributing stormwater drainage network within the Salvin Creek Catchment, it was apparent that there were more than two main inflow locations along the length of the upper and lower reaches. Therefore additional flow change locations were added to the Lower reach of the model to further distribute the flow along the length of creek being modelled.

Table 2.1: Adopted Peak Discharge used in HEC-RAS Model

HEC-RAS	Inflow	WBNM	Ultii	nate Devel	opment Ca	tchment Di	scharge (m	³/sec)
Chainage (m)	location (cross section)	sub catchment ID	2 year ARI	5 year ARI	10 year ARI	20 year ARI	50 year ARI	100 year ARI
Upper	Reach							
2130	SC110	X1	16.9	23.9	30	35.5	\ 43.1	49.3
1930	SC100	X2	24.1	34.5	43.3	51.6	62.5	71.6
Glengarif	f Reach							
910	SC1040	Х3	12.8	19.1	24.5	29.3	36.1	41.6
510	SC1020	X4-	17.1	25.5	\32.6	38.8	48.1	55.5
Lower Reach								
910	SC1040	20%-X5 Z	47.3	69.1	86.3	104.6	127.6	147.1
486	SC1020	60% X5	65.4	92.1	111.2	129.5	153.2	171.7



Figure 2.1: Salvin Creek Catchment Inflow Points (with HEC-RAS Chainage)

3.0 Hydraulic Modelling

3.1 General

The hydraulic analysis was undertaken using the HEC-RAS (Version 3.1.3) hydraulic modelling software for steady flow conditions. Section 3.2 details the set-up and assumptions used in the modelling. The modelling results are presented in Section 3.3.

No recorded stream levels exist in the catchment and therefore model calibration was not undertaken.

3.2 HEC-RAS Model Setup

The Salvin Creek main reach and Glengariff reach were both modelled in HEC-RAS to the extents described in Section 2.2. As mentioned above the main reach is divided into Upper and Lower reaches, with the separation point being the confluence with the Glengariff reach. In the HEC-RAS model reported in this study the main reach of Salvin Creek was extended from Glenheaton Court, Carindale down to the confluence with Bulimba Creek.

Salvin Creek has one bridge crossing and four culvert crossings and all of them are located in the main reach. A description of the location of each of these structures is given in Section 3.2.4.

3.2.1 Cross Sections

Cross section survey was undertaken in the main reach of Salvin Creek in March 2001 to enable the development of an earlier HEC-RAS model. A total of 18 cross-sections were surveyed in the main reach from immediately downstream of Cavendish Road to Glenheaton Court. A further 12 sections were extracted in 2004 from the ALS data (2002) to enable the lower reach to be extended downstream to the Bulimba Creek confluence.

Five cross sections were surveyed for the Glengariff reach in July 2000. An additional five cross sections were extracted in association with this Salvin Creek study from the ALS data (2002).

The reach lengths between each cross section were measured and chainages assigned to each cross section with zero chainage representing the most upstream cross section. Interpolated cross sections were introduced into the upper reach of Salvin Creek using the function supplied within HEC-RAS. These were placed at locations where the channel shape varied linearly between cross sections.

The locations of the model cross sections are shown in Figure 3.1: Salvin Creek - HECRAS Model Cross Section Layout. The cross section identifiers adopted for the survey, location descriptions and chainages (where appropriate) are included in Table 3.1.

3.2.2 Minimum Vegetated Riparian Corridor (MRC)

The vegetation along the edge of a waterway is called riparian vegetation i.e. it is the vegetation attached to the creek. It is a key contributor to waterway health, acting as a buffer between the waterway and adjacent lands. A well-vegetated riparian zone can improve water quality by filtering

overland flow and reducing erosion along creek banks. Shady trees protect vulnerable organisms from extremes of temperature; root systems and woody debris become habitat for fauna; and organic matter sustains aquatic food webs. Vegetation also provides habitat and forage for fauna and adds to a waterway's recreational value. The *Waterway Management Plan* (BCC, 2003c) process allows the hydrological and ecological impacts of riparian revegetation to be assessed and managed in an integrated manner.

This study calculates anticipated flood levels assuming a MRC width along the entire creek system. This hydraulic investigation does not in any way imply that Council is planning to establish a minimum riparian vegetated corridor width in the Salvin Creek Catchment. The minimum vegetated riparian corridor is modelled solely in recognition that at some unspecified time in the future, revegetation may occur, either through natural regeneration or as a result of human planting programs. The results of this modelling are intended to ensure that the habitable floor levels of developments within the floodplain take account of possible future revegetation. This type of forward planning is supported by Guidelines for Flood Regulation Line and Minimum Fill Level Assessment (BCC, 1994).

A MRC was incorporated into the HEC-RAS modelling by increasing the hydraulic roughness parameters in the riparian zone. A Manning's 'n' value of 0.15 was used to represent the MRC, which typically incorporates a distance of 15m either side of the top of the creek bank.

3.2.3 Manning's Roughness (n)

For areas outside the MRC, the Manning's 'n' values were obtained from site inspections conducted in March 2001, aerial photography and hydraulic roughness literature. A significant variation in Manning's values was found along each tributary. Following the observation of debris collected at crossings in the storm event in March 2001, it was considered reasonable to assume that bridge or culvert handrails would be blocked during a storm event, irrespective of their size. Table 3.1: Mannings' Roughness - Salvin Creek lists the Manning's roughness values chosen for Salvin Creek.

Table 3.1: Manning's Roughness – Salvin Creek

			Manning's Roughness Value			
Chainage (m)	Cross Section ID	Location Description	Left overbank	Main channel	Right overbank	
Upper Read	2lı		773			
2130	SC110	Downstream of Cavendish Road	0.08	0.045	0.08	
1930	SC100	Adjacent to Wisteria Crescent	0.08	0.035	0.08	
1610	Culverts	Bevan Street Bridge Crossing	0.08	0.05	0.08	
1515	SC90	North of Bevan Street	0.08	0.045	0.08	
1275	SC80	South of Pine Mountain Road	0.08	0.035	0.08	
1145	SC70	South of Pine Mountain Road	0.08	0.035	0.08	
1144	SC60	Pine Mountain Road weir profile	N/A	N/A	N/A	
1115	-SE50 \	North of Pine Mountain Road	0.12	0.06	0.06	
1103	SC50-copy	South of Pine Mountain Road	0.12	0.06	0,06	
1095	SC50-copy	DS of Energy dissipater	0.12	0.035	0.06	
1035	ALS-I	South of Glengariff merging point	0.10	0.04	0.10	
Lower Read	ch					
913	ALS-2	48m US of SC40	0.10	0.04	0.1	
865	SC40	Upstream of Creek Road	0.08	0.035	0.08	
805	ALS-4	Upstream of Creek Road	0.10	0.035	0.10	
767	SC30	Upstream of Creek Road	0.10	0.035	0.10	
736	SC20	Creek Road weir profile	N/A	N/A	N/A	
735	SC10	Downstream of Creek Road	0.03	-0.045	0.08	
670	ALS-5	Downstream of Creek Road	0.06	0.04	0.01	
486	CS1	South of Donnington Street	0.03	0.04	0.06	
430	CS2	South of Donnington Street	0.03	0.06	0.06	
420	ALS	Im upstream Donnington Street	0.03	0.03	0.06	
419.5		Donnington Street culvert	N/A	N/A	N/A	
385	ALS-6	Downstream of Donnington Street	0.06	0.045	0.06	
348	CS3	North of Donnington Street	0.035	0.045	0.035	
257	CS4	Adjacent to 11 Norham Court	0.035	0.045	0.035	
175	CS5	Adjacent to 15 Norham Court	0.035	0.05	0.035	
100	CS6	N-W of Glenheaton Court	0.08	0.05	0.08	
0	CS7	N-E of Glenheaton Court	0.08	0.05	0.08	
-20	RS-1	20m DS of CS7	0.13	0.06	0.13	
-66	RS-2	66m DS of CS7	0.13	0.06	0.13	
-108	RS-3	108m DS of CS7	0.13	0.06	0.13	
-146	RS-3.5	146m DS of CS7	0.13	0.06	0:13	
-153	RS-4	183m DS of CS7,US Donnington Street	0.13	0.06	0.13	
-181	RS-6	181m DS of CS7,DS Donnington Street	0.13	0.06	0.13	
-187	RS-6.5	187m DS of CS7	0.13	0.06	0.13	

			Manning's Roughness Value			
Chainage (m)	Cross Section ID	Location Description	Left overbank	Main channel	Right overbank	
-226	RS-7	226m DS of CS7	0.13	0.06	0.13	
-280	RS-8	280m DS of CS7	0.13	0.06	0.13	
-329	RS-9	396m DS of CS7	0.13	0.06	0.13	
-381	RS-10	381m DS of CS7	0.13	0.06	0.13	
-428	RS-11	428 m DS of CS7	0.13	0.06	0.13	
-479	RS-12	479m DS of CS7	0.13	0.06	0.13	
Glengariff 3	Cributary	The state of the s				
910	SC1040	Adjacent to Pine Mountain Road	0.08	0.06	0.08	
730	SC1030	White Hill Reserve	. 0.08	0.06	0.08	
510	SC1020 \	White Hill Reserve	0.08	0.06	80.0	
410	SC1010\\	End of Olivia Drive	0.08	0.045	0.08	
90	SC1000	Adjacent to Glengariff Street	0.10	0.045	0.10	
40	ALS-3	North of Pine Mountain Road	0.08	0.035	0.08	

3.2.4 Hydraulic Structures

Within the model there are five hydraulic structures; one bridge and four culverts and are modelled in the main branch of Salvin Creek. Table 3.2 contains the configuration details of each of these structures.

Table 3.2: Hydraulic Structure Details

HEC-RAS Chainage (m)	Structure	Configuration				
Salvin Creek:	Upper Reach					
1609	Bevan Street culverts	3 / 3300 x 1500mm RCBCs (Plan no. WP1081)				
1144	Pine Mountain Road culverts	3 / 2700 x 1800mm RCBCs (Plan no. W9418)				
Salvin Creek:	Lower Reach					
736	Creek Road Bridge	Four span (18m total) concrete bridge				
419.5	Donnington Street culverts (No.1)	3 / 3600 x 2400mm RCBCs (W5674 S04B)				
-5	Donnington Street culverts (No.2)	3 / 6000 x 3500mm RCBCs				



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3.2.5 Boundary Conditions

Peak discharges were obtained from the WBNM hydrologic model of Bulimba Creek and used as the upstream boundary conditions in the HEC-RAS model. These discharges were applied to the Upper Reach at chainage 2130 and at chainage 910 in the Glengariff Reach. Flow change locations as listed in Table 2.1 were introduced into the model to represent the increase in discharge in the downstream direction.

At the downstream boundary of the HEC-RAS model a known water level was used for all ARI events modelled. The adopted value of 7.7m AHD corresponds to the 2 year ARI design flood level from Bulimba Creek at its confluence with Salvin Creek (i.e. model cross section BM60).

3.3 Modelling Results

3.3.1 General

The HEC-RAS model was run for the 2, 5, 10, 20, 50 and 100 year ARI events. The complete table of extracted HEC-RAS model results for each event are shown in Appendix I-2. The flood level and velocity results are discussed separately in Sections 3.3.2 and 3.3.3 respectively.

From the results, it is apparent that the bank full capacity of the main channel is quite variable and ranges from less than the 2 year ARI discharge to the 100 year ARI discharge.

3.3.2 Flood Levels

The peak flood levels obtained from HEC-RAS model results for the 2, 5, 10, 20, 50 and 100 year ARI events are given in **Table 3.3** and presented graphically in **Figure 3.2 and 3.3**. The corresponding flood inundation plots for each ARI event are provided in **Appendix J**.

The tail water level adopted for the HEC-RAS modelling was that corresponding to the 2 year ARI event at Bulimba Creek or 7.7m AHD. Therefore, design flood levels in the lower reach of Salvin Creek near the confluence with Bulimba Creek will be dominated by Bulimba Creek design flood levels for events greater than the 2 year ARI event.

3.3.3 Flow Velocities

The average velocities along the reach at the surveyed cross sections for each event are presented in **Table 3.4.** The variability in channel velocity results is significant and this may reflect a lack of accuracy in the model due to the limited availability of surveyed channel cross sections. Design flow velocities exceed 3m/s in several locations. Possible explanations for these are as follows:

- Immediately downstream of Creek Road the flow is restricted to a narrow section.
- Approaching Creek Road, Glengariff Tributary has a steeper gradient and that meets the main reach about 180m upstream of the Creek Road crossing. From there the flow constricts to a narrow section.
- 170m downstream of Donnington Street there is a sharp drop in bed levels and narrowing section at this location.

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The main reach of the Salvin Creek consists of natural channel and shows average velocities that appear reasonable along most of the channel (up to 2.5m/s for the 100 year ARI event). However there appears to be higher velocities at the junction where main reach meets with the Glengariff reach. There is an energy dissipating device upstream of this location. The velocities are quite varied adjacent to the structure and reduce as it flows along the Creek. Glengariff reach shows higher velocities at the start of the reach (2.85 m/s) due to the steep gradient, but these reduce as it flows along the reach.

Table 3.3: Flood Level Results

HEC-RAS Chainage		Vater Surface	Level (m AH)	D) - Ultimate C	Eatchment Dev	elopment
(m)						100 year ARI
Upper Reach			anagtarari	MK DAMA DEBAR		Maria employa Arras
2130	26.42	26.74	26.97	27.16	27.40	27.58
1930	25:70	26.04	26.27	26.46	26.69	26.86
1610	21.34	21.75	22.06	22.44	22.63	22.78
1609	Bevan Street	Culverts				
1595	20.64	20.90	21.08	21.23	21.40	21.53
1515	20.05	20.33	20.49	20.63	20.79	20.90
1275	18.40	18,60	18.74	18.85	19.19	19.36
1145	17.49	17.96	18.32	18.64	19.13	19.31
1144	Pine Mounta	in Road Culv	erts		****	
1115	16.24	16.55	16.77	17.00	17.21	17.38
1103	16.13	16.41	16.61	16.79	17.04	17.21
1095	16.13	16,42	16.64	16.84	17.07	17.24
1035	15.99	16.29	16.52	16.73	16.99	17.17
Lower Reach						
913	14.65	14.96	15.16	15.37	15.6	15.83
865	14.02	14.40	14.69	14.94	15.39	15.82
805	13.24	13.70	14.10	14.35	15.07	15.63
767	13.22	13.68	14.08	14.32	15.06	15.68
736	Creek Road	Bridge				e e
735	12.92	13.29	13.74	13.88	14.06	14.18
670	12,80	13.20	13.71	13.86	14.07	14.20
486	11.91	12.86	13.54	13.67	13.87	13.99
430	11.72	12.77	13.49	13.61	13.81	13.97
420	11.71	12.74	13.45	13.63	13.83	13.97
419.5	Donnington !	Street Culver	ts No.1			
385	11.19	11.59	11.85	12.06	12.32	12.50
348	11.02	11.43	11.69	11,92	12.20	12.40
257	10.14	10.48	10.69	10.87	11.04	11.15
175	9.80	10.17	10.41	10.64	10.89	11.06
100	9.54	9.93	10,17	10.4	10.66	10.85
0	9.16	9,49	9.71	9.91	10.16	10.34
-1(-20)	8.92	9.22	9.42	9.62	9.88	10.07
-2(-66)	8.61	8.98	9.23	9.46	9.75	9.97
-3(-108)	8.49	8.86	9.11	9.35	(9.65)	(9.87)
-3.5(-146)	8.16	8.50	8.76	(9.00)	(9.31)	(9.54)
-4(-153)	8.23	8.57	8.82	(9.05)	(9.34)	(9.57)

HEC-RAS Chainage	Peak Water Surface Level (m AHD) - Ultimate Catchment Development							
(m)	2 year ARI	5 year ARI	10 year ARI	20 year ARI	50 year ARI	100 year ARI		
-154	Donnington	Street Culver	ts No. 2	1.	~			
-6.0(-181)	8.06	8.28	(8.44)	(8.58)	(8.75)	(8.87)		
-6.5(-187)	8.03	8.24	(8.40)	(8.54)	(8.71)	(8.84)		
-7(-226)	7.89	(8.01)	(8.11)	(8.21)	(8.32)	(8.41)		
-8(-280)	7.80	(7.88)	(7.95)	(8.02)	(8.11)	(8.18)		
-9(-329)	7.76	(7.81)	(7(86)	(7.91)	(7.97)	(8.03)		
-10(-381)	7.73	(7.76)	(7.79)	(7.82)	(7,87)	7.90)		
-11(-428)	7.73	(7.75)	(7.77)	₹ (7.80)	(7.83)	(7.87)		
-12(-479)	7.70	(7.70)	(7.70)	\(7.70)	(7,70)	(7,70)		
Glengariff Reach								
910	23.93	24.11	24.20	24.28	24.40	24.52		
730	22.28	/ 22.52	22.72	22.87	23.05	23.15		
510	20.05	20.28	20.34	20.38	20.48	20.60		
410	18.92	19.23	19.43	19.57	19.71	19.81		
90	15.93	16.27	16.52	16.72	16.98	17.16		
40	15.69	16.02	16.26	16.48	16.75	16.93		

Note: Levels in brackets are based on Bulimba Creek flooding

Table 3.4: Channel Velocities

	Peak Average Flow Velocity (m/s)							
HEC-RAS Chainage	2 year ARI	5 year ARI	10 year ARI	20 year ARI	50 year ARI	100 year ARI		
Upper Reach								
2130	0.8	0.8	0.9	0.9	0.9	0.9		
1930	1.4	1.5	1.6	1.7	1.8	1.8		
1610	1.1	1.1	1.2	1.2	1.3	1.4		
1609	Bevan Street	Culverts	: :					
1595	1.9	2.1	2.2	2.4	2.6	2.7		
1515	1.8	2.0	2.2	2.4	2.6	2.8		
1275	2.4	2.6	2.7	2.8	2.4	2.4		
1145	1.0	1.1	1.1	1.1	1.0	1.1		
1144	Pine Mounta	in Road Culv						
1115	1.6	1.9	2.1	2.1	2.3	2.4		
1103	1.7	2.0	2.3	2.5	2.5	2.6		
1095	1.5	1.7	1.8	1.9	2.0	2.1		
1035	1.5	1.6	1.7	1.8	1.8	1.8		
Lower Reach								
913	3.1	3.5	3.7	3.9	4.1	4.2		
865	1.5	1.6	1.7	1.8	1.8	1.7		
805	3.1	3.2	3.0	3.2	2.6	2.3		
767	2.1	2.3	2.4	2.5	2.1	1.6		
736	Creek Road	Bridge						
735	1.8	2.1	2.1	2.4	2.8	3.1		
670	1.2	1.4	1.3	1.4	1.6	1.7		
486	2.2	1.1	0.9	0.9	1.0	1.1		
430	1.4	1.2	1.1	1.2	1.3	1.0		
420	1.4	1.3	1.3	0.9	1.0	1.1		
419.5	Donnington :	Street Culver	t No. 1		· · · · · · · · · · · · · · · · · · ·			
385	1.7	2.1	2.3	2.5	2.7	2.9		
348	1.9	2.2	2.3	2.3	2.8	2.4		

			Peak Average	Flow Velocity	(m/s)	
HEC-RAS Chainage	2 year ARI	5 year ARI	10 year ARI	20 year ARI	50 year ARI	100 year ARI
257	2.4	2.8	3.0	3.2	3.5	3.8
175	1.4	1.6	1.7	1.7	1.7	1.7
100	1.1	1.2	1.3	1.4	1.4	1.5
0	1.1	1.3	1.5	1.6	1.7	1.7
-20	1.8	2.1	2.2	2.3	2.3	2.4
-66	1.5	1.6	1.6	1.6	1.6	1.7
-108	1.1	1.3	1.3	1.4	1.5	1.5
-146	2.1	2.3	2.3	2.4	2.4	2.4
-153	1.3	1.6	1.8	1.9	2.1	2.2
-154	Donnington	Street Culver	t No. 2			4
-181	1.3	1.7	1.9	2.1	2.3	2.5
-187	1.4	1.8	2.0	2.2	2.4	2.5
-226	1.5	1.9	2.2	2.4	2.7	2.9
-280	1.0	1.3	1.5	1.7	1.9	2.0
-329	0.8	1.1	1.3	1.4	1.6	1.7
-381	0.6	0.8	1.0	1.1	1.3	1.4
-428	0.5	0.6	0.8	0.9	1.0	1.1
-479	0.6	0.8	1.0	1.2	1.4	1.5
Glengariff Reach						
910	1.4	1.8	2.1	2.4	2.7	2.9
730	1.5	1.4	1.4	. 1.4	1.5	1.6
510	1.6	1.8	2.1	2.4	2.7	2.6
410	2.3	2.3	2.1	2.0	2.0	2.0
90	1.4	1.4	1.5	1.5	1.6	1.6
40	1.6	1.8	1.9	1.9	2.0	2,1

3.3.4 Inundation Mapping

The flood inundation plots provided in Appendix J indicate the flood extent at various locations along the watercourse. However, the elevation data for the region is based on ALS data obtained in 2002 and may not depict the current surface elevations.

3.3.5 Hydraulic Structures

Model results for the crossings of Salvin Creek are provided in Table 3.5: Structure Flood Immunity Results.

Table 3.5: Structure Flood Immunity Results

Structure	Upstream 100 year ARI Flood Level (m AHD)	Afflux ¹ (m)	Road Flood Immunity	Peak Structure Velocity (m/s)
Bevan Street	22.78	1.25	>20 year	3.8
Pine Mountain Road	19.31	1.93	>20 year	4.3
Creek Road	15.68	1.51	>20 year	4.0
Donnington Street No.1	13.97	1.47	>10 year	3.9
Donnington Street No.2	9.58	0.67	>100 year ARI	3.2

^{1.} Measured as the difference between flood levels immediately upstream and downstream of the structure.

Flows within the structures are predominantly sub-critical for the full range of ARI events modelled. However, super-critical flow is present at the Pine Mountain Road culverts located in the Upper Reach due to the presence of a drop structure immediately downstream of the culvert.

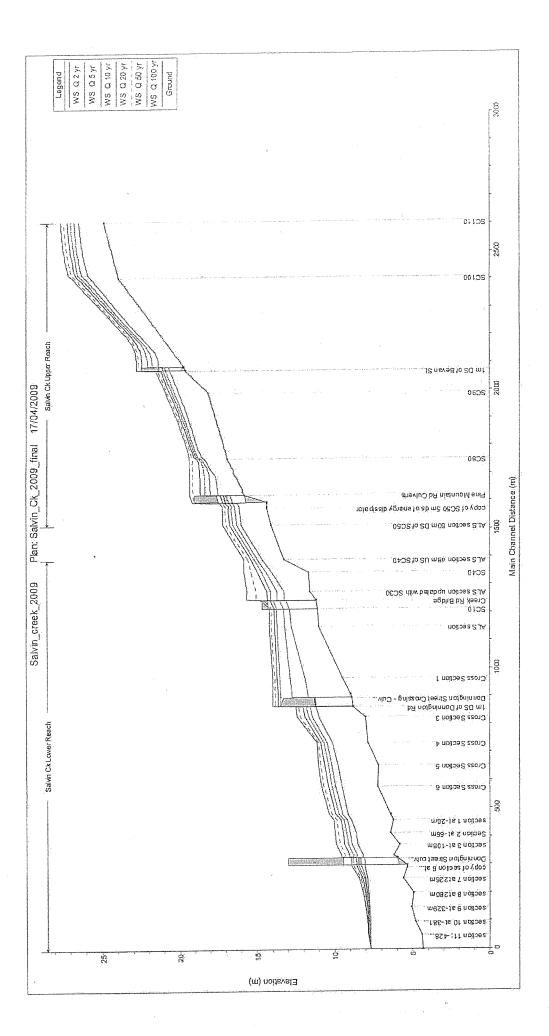


Figure 3.2: Upper & Lower Reaches - Longitudinal Flood Profile obtained from HEC-RAS model

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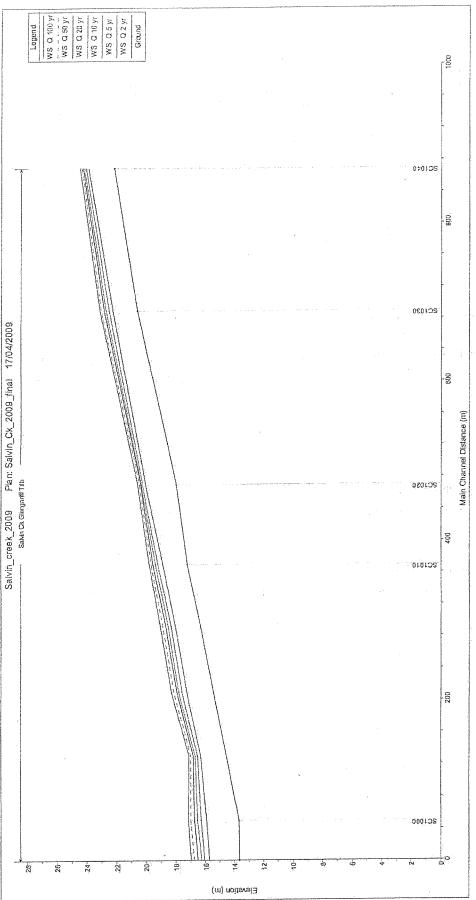


Figure 3.3: Glengariff Reach - Longitudinal Flood Profile obtained from HEC-RAS Model

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BCC.079.1090

4.0 Conclusion

Hydraulic modelling of Salvin Creek has been undertaken using HEC-RAS (Version 3.1.3): steady flow conditions. The HEC-RAS model was created using the surveyed cross sections of 2001/2002 together with extracted cross sections from ALS data of 2002. The hydraulic modelling assumed the presence of Minimum Vegetated Riparian Corridor (MRC) for both the Main and Glengariff reaches.

The HEC-RAS model developed for Salvin Creek in 2001 up to Glenheaton Court was extended to the Bulimba Creek confluence in 2004. In 2009, with the present study, this model was reviewed and refined by adding additional ALS (2002) cross sections.

The model incorporates five (5) hydraulic structures, a bridge and 4 culverts. Flow data used in the HEC-RAS model was obtained from the Bulimba Creek hydrology model WBNM (2001).

The results of the hydraulic modelling indicate that:

- Creek Road and Pine Mountain Road structures have flood immunity approximately up to a 20 year ARI event;
- The Donnington Street culvert No.1 (upstream) has approximately 10 year flood immunity
- The Donnington Street culvert No.2 (upstream) has approximately 100 year flood immunity

In addition, the velocities are quite varied along the length of the study reach in all events. This is predominantly because of the effects of hydraulic drop-structures, steeper gradients and natural channels and the MRC.

The flood inundation plots show that:

- Creek Road is inundated during the 50 and 100 year ARI events, with similar results at the Pine Mountain Road crossing;
- A few properties adjacent to Lower Reach would experience minor flooding in the 50 year and 100 year ARI events,
- · Glengariff reach flooding is mostly contained within the waterway corridor.

5.0 References

Waterway Management Plan (BCC, 2003c)

Guidelines for Flood Regulation Line and Minimum Fill Level Assessment (BCC, 1994).

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Appendices



Appendix A Catchment Details used in Hydrologic & Hydraulic Models



Table A1: Subcatchment Details for Hydrologic Model WBNM

	Catchment Cer	ntroid (GDA94)	Area	Fraction Impervious (%)		Catchment Outlet (GDA94)		
ID .	Easting	Northing	(km²)	Existing	Ultimate	Easting	Northing	
A1a	506,407.81	6,945,141.50	1.75	42.0	61.5	506,534.03	6,945,859.92	
Alb	506,237.81	6,946,194.50	1.30	42.0	61.5	506,459.56	6,946,615.67	
A2	506,691.25	6,946,596.50	1.13	42.0	61.9	506,856.51	6,947,150.39	
A3	506,444.16	6,947,685.00	1.19	42.0	62.0	506,465.37	6,948,149.08	
В	506,755.56	6,948,695.00	1.56	33.9	47.4	507,443.73	6,949,540.62	
Cla	507,579.12	6,947,548.50	1.08	41.5	59.2	507,362.65	6,948,153.54	
C2b	508,092.91	6,948,736.00	1.73	41.5	59.2	507,443.73	6,949,540.62	
D	505,948.47	6,952,918.00	2.76	46.3	52.7	506,741.74	6,952,511.86	
E	506,959.53	6,952,217.00	2.15	45.8	64.9	\\507,252.76\	6,951,308.65	
F	506,813.91	6,950,850.50	1.9	52.9	66:3	<i>∕∕ 5</i> 07,719 _, 70	6,950,132.25	
G	506,811.75	6,949,968.00	1.99	53.4	64.1	5 07,719.70	\ 6,950,132.25	
H	508,232.16	6,950,266.00	1.56	55.7	68.7	508,694.17	6,950,589.05	
I1	508,752.88	6,951,087.50	2.37	44.2	62.4	509,628.92	6,951,214.87	
12	509,495.84	6,950,787.00	2.1	44\2	62.4	510,236.01	6,951,333.96	
J1	507,672.16	6,946,245.00	0.49	20.0	74.6	507,848.63	6,946,434.07	
J2	507,993.12	6,946,327.00	0.99	50.0	68.2	508,605.64	6,946,848.61	
K1	508,968.12	6,947,247.00	1.58	42.0	46.2	509,457.01	6,947,986.81	
K2	508,354.53	6,947,603.50	0.57	30.0	57,4	508,609.28	6,947,733.13	
К3	508,986.94	6,947,800.50	0.47	25.0	40.8	509,448.81	6,947,969.50	
LI	509,782.81	6,948,271,00	0.45	10.0	52.0	509,708.25	6,948,546.89	
L2	509,142.78	6,948,650.00	1.47	35.0	63.2	509,658.78	6,948,992.15	
M1	509,707.13	6,949,218.00	0.45	40.0	74.0	510,085.29	6,949,261.88	
M2	510,509.66	6,947,228.50	0.98	20.0	75.0	510,561.00	6,947,804.03	
МЗ	510,483.59	6,948,173.50	0.45	40.0	81.0	510,450.73	6,948,604.66	
M4	511,551.62	6,947,499.00	0.32	20.0	74.0	511,339.36	6,947,826.63	
M5a	512,192.75	6,947,531.50	1.01	30.0	67.0	511,339.36	6,947,826.63	
M5b	511,246.41	6,947,971.00	0.17	30.0	79.0	511,043.04	6,948,202.46	
M6	511,679.22	6,948,332.50	0.46	30.0	55.0	511,074.20	6,948,166.93	
M7	511,108.94	6,948,440.00	0.47	30.0	67.0	510,532.15	6,948,519.64	
M8	510,507.09	6,948,926.00	0.67	30.0	71.0	510,085.29	6,949,261.88	
NI	510,215.06	6,949,785.50	0.66	50.0	73.5	510,519.92	6,950,306.09	
N2a	511,581.59	6,949,133.00	1.4	5.0	68.4	510,942.36	6,949,481.33	
N2b	511,497.41	6,949,876.50	1.13	5.0	60.2	510,519.92	6,950,306.09	
N2c	510,650.28	6,950,796.50	0.61	5.0	40.6	510,271.29	6,950,977.45	
O	510,831.44	6,951,469.00	1.97	22.1	53.3	511,185.85	6,952,353.83	
P	512,443.66	6,950,867.50	4.38	24.7	50.6	511,185.85	6,952,353.83	
Q	511,726.41	6,952,747.00	2.04	33.8	70,4	510,994.61	6,953,618.91	
R	509,417.38	6,952,828.50	3.75	52.0	68.1	510,987.28	6,953,581.41	
S	511,007.34	6,954,035.00	1.33	42.0	39.8	511,187.73	6,954,866.27	
<u>T1</u>	512,005.72	6,953,916.00	1.91	42.0	49.3	511,205.19	6,954,900.71	
T2	511,029.31	6,955,031.00	1.06	42.0	49.2	510,179.46	6,955,166.09	
U1	507,993.12	6,953,530.00	1.86	42.0	55.9	508,821.44	6,954,171.81	
	1 7 7 18 7 7 7 7 7	L	<u> </u>		L			

	Catchment Cer	itroid (GDA94)	Area	Fraction In	pervious (%)	Catchment C	outlet (GDA94)
ID	Easting	Northing	(km^2)	Existing	Ultimate	Easting	Northing
U2	508,944.44	6,954,345.00	0.86	33.9	69.0	509,360.98	6,954,678.06
U3	509,803.53	6,954,357.50	1.51	53.7	70.4	510,179.46	6,955,166.09
V	509,910.94	6,955,790.50	1.55	45.0	59.4	510,645.21	6,956,540.00
W1	512,814.06	6,954,777.00	2.00	5.0	26.0	511,923.24	6,955,007.76
W2	512,104.94	6,955,438.50	1.48	25.0	55.0	511,269.03	6,956,028.17
W3	511,431.81	6,956,254.00	1.52	10.0	44.0	510,645.21	6,956,540.00
X1	508,241.78	6,955,266.00	1.45	42.8	60.3	508,688.75	6,955,474.69
X2	509,128.28	6,955,683.50	0.75	41.2	57.7	509,481.10	6,956,324.83
X3	508,019.88	6,956,557.00	1.6	18.2	27.8	508,897.16	> 6,956,486.27
X4	509,074.47	6,956,648.00	0.41	25.6	25.3	509,492.54	6,956,392.05
X5	509,701.56	6,956,687.00	1.19	36.6	55.0	> 510,612.15	6,957,228.09
Y1	510,719.19	6,956,915.00	0.51	30.0	40.0	510,613.05	6,957,223.58
Y2	510,255.94	6,957,632.50	0.94	50.0	62.6	510,705.74	6,958,272.22
Z	508,940.81	6,957,976.00	4.21	41.2	54.9	510,705.74	6,958,272.22
AA	511,739.31	6,957,989.00	3.08	21.3	43.1	511,878.07	6,958,800.09
BB1	511,779.41	6,959,191.50	1.77	25.0	42.0	511,144.09	6,959,564.94
BB2	509,540.31	6,959,436.00	2,34	46.0	48.0	510,641.50	6,960,417.16
BB3	512,138.77	6,960,461.08	1.26	38.0	52.0	511,675	6,960,991.51
ВВЗа	511,237.35	6,959,906.2	\0.86\	20,0	25.0	510,631.14	6,960,426.36
BB4	510,096.69	6,960,073,50	2,30	42.0	42.0	510,221.82	6,961,146.38
CC	509,219.56	6,960,141.50	2.22	27.5	44.5	510,221.82	6,961,146.38
DD	510,181.19	6,961,667.50	2.38	43.4	56.4	511,002.87	6,962,222.50
EE	511,641.50	6,961,778.00	1.31	31.8	49.0	512,184.97	6,961,891.82
FF	513,227.69	6,956,774.50	3.99	3.0	11.0	513,307.66	6,958,239.68
GG	513,707.78	6,958,205.00	3.05	18.4	12.0	513,519.47	6,959,475.78
HH1	514,235.41	6,960,009.50	2.44	24.0	38.0	513,195.83	6,961,305.56
HH2	513,457.50	6,960,182.50	2.27	48.0	66.0	513,195.83	6,961,305.56
HH3	512,947.78	6,961,572.00	1.41	12.5	40.0	512,195.39	6,962,047.85
II ·	511,642.47	6,962,815.00	2.57	27.2	50.0	512,137.66	6,963,751.80
JJ	514,555.22	6,961,594.00	3.18	30.1	57.7	513,829.58	6,962,450.35
KK	513,895.38	6,962,958.00	3.74	25.0	38.8	512,134.06	6,963,725.28
LL	511,684.03	6,963,883.00	1.02	60.1	63.9	511,121.52	6,964,234.66
MM	513,857.69	6,964,464.50	4.82	30.7	68.6	512,584.21	6,964,911.37
NN	512,331.44	6,964,809.50	1.28	60.0	83.3	512,790.58	6,965,980.99
Total			124.9	33.37%	43,88%		

Table A2: Cross section details of MIKE-11 model

Creek Branch	MIKE11 Chainage(m)	AMTD equivalent (m)	Cross section ID	Details (source)
BULIMBA	0	38965		
BULIMBA	10	38955	BM 214	RUBICON model
BULIMBA	17	38948	Nemies Rd	RUBICON model
	40	38925	Copy of BM214	RUBICON model
BULIMBA	120	38845	BM213	RUBICON model
BULIMBA	215	38750	BM212	RUBICON model
BULIMBA	355	38610	BM211	RUBICON model
BULIMBA	370	38595	Brandon Rd	RUBICON model
BULIMBA	385	38580	Copy of BM211	RUBICON model
BULIMBA	470	38495	BM 209	RUBICON model
BULIMBA	540	38425	BM 208	RUBICON model
BULIMBA		38365	BM 207	RUBICON model
BULIMBA	600	38225	BM 206	RUBICON model
BULIMBA	740		BR 1	Survey 2006
BULIMBA	800	38165 38155	Brandon Rd DS weir	Survey 2006
BULIMBA	810	38140	BR 2	Survey 2006
BULIMBA	825		BM 205	RUBICON model
BULIMBA	840	38125		Survey 2006
BULIMBA	890 <	38075	BR_3 BR 4	Survey 2006
BULIMBA	2.9.5	38060 /	BR 4 BR 5	Survey 2006
BULIMBA	942	38023	BR 5 copy	Survey 2006
BULIMBA	960	38005		RUBICON model
BULIMBA	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	37975	Copy BM 204	RUBICON model
BULIMBA	1075	37890	BM 203	RUBICON model
BULIMBA	1160	37805	BM 202	RUBICON model
BULIMBA	1300	37665	BM 201	RUBICON model
BULIMBA	1365	37600	BM 200	RUBICON model
BULIMBA	1545	37420	BM 199	RUBICON model
BULIMBA	1670	37295	BM 198	
BULIMBA	1800	37165	ВM340-MHG	Interpolated
BULIMBA	1830	37135.	BM 197	RUBICON model
BULIMBA	1845	37120	Beenleigh Road weir	RUBICON model/ALS
BULIMBA	1860	37105	Copy of BM 197	RUBICON model
BULIMBA	1900	37065	BM195-I	Interpolated
BULIMBA	1940	37025	BM 194	RUBICON model
BULIMBA	1960	37005	Copy of BM 194	RUBICON model
BULIMBA	2045	36920	BM 192	RUBICON model
BULIMBA	2115	36850	Copy of BM 191	RUBICON model
BULIMBA	2117	36848	St Lawrence FBridge	ALS
BULIMBA	2125	36840	BM 191	RUBICON model
BULIMBA	2255	36710	BM190	RUBICON model
BULIMBA	2370	36595	Copy of BM188-6	RUBICON model
BULIMBA	2375	36590	Altandi_St_FB_weir	ALS
BULIMBA	2380	36585	BM188-6 ALS	ALS
BULIMBA	2470	36495	BM188-2 ALS	ALS
BULIMBA	2500	36465	BM188-1 ALS	ALS
BULIMBA	2670	36295	BM187	RUBICON model
BULIMBA	2785	36180	BM186	RUBICON model
BULIMBA	2985	35920	BM185	RUBICON model
BULIMBA	3165	35800	BM184	RUBICON model
	3295	35670	BM183	RUBICON model
BULIMBA	3435	35530	BM182	RUBICON model

Creek Branch	MIKE11 Chainage(m)	AMTD equivalent (m)	Cross section ID	Details (source)
BULIMBA	3625	35340	BM181	RUBICON model
BULIMBA	3765	35200	MHG-320	Interpolated
BULIMBA	3800	35165	BM180	RUBICON model
BULIMBA	3960	35005	BM179	RUBICON model
BULIMBA	3965	35000	Malbon St FB weir	RUBICON model/ALS
	3970	34995	Copy of BM179	RUBICON model
BULIMBA	4150	34815	BM178	RUBICON model
BULIMBA		34705	BM177-MHG310	RUBICON model
BULIMBA	4260	34645	BM177A	ALS
BULIMBA	4320		BM176-US	RUBICON model/ALS
BULIMBA	4385	34580		RUBICON model/ALS
BULIMBA	4415	34550	BM176 DS	RUBICON model
BULIMBA	4460	34505	BM 175	1"
BULIMBA	4515	34450	Bm175-174	RUBICON model
BULIMBA	4590	34375	BM 174	RUBICON model
BULIMBA	4700	34265	BM174A	RUBICON model/ALS
BULIMBA	4765	34200	BM174B	ALS
BULIMBA	4780	34185	BM173- MHG300	RUBICON model
BULIMBA	4785	34180	Blesby Rd FB weir	RUBICON model/ALS
BULIMBA	4790	34175	Copy of BM 173	RUBICON model
BULIMBA	4905	34060	BM172	RUBICON model
BULIMBA	4995	33970	BM171 \	RUBICON model
BULIMBA	5120	33845	BM170	RUBICON model
BULIMBA	(5285,	33680	BM169	RUBICON model
BULIMBA	5405	33560	BM168	RUBICON model
BULIMBA	55,20	33445	BM167	RUBICON model
BULIMBA	5615	33350	CopyBM 167-MHG290	RUBICON model/ALS
BULIMBA	5715	33250	Copy BM 165	RUBICON model/ALS
	5730	33235	BM165	RUBICON model
BULIMBA	5785	33180	SurveyXs-5	Logan Rd survey 2006
BULIMBA	5845	33120	SurveyXs-4	Logan Rd survey 2006
BULIMBA		33063	SurveyXs-3	Logan Rd survey 2006
BULIMBA	5902			Logan Rd survey 2006
BULIMBA	5918	33047	SurveyXs-2 BM158 Xs-1	Logan Rd survey 2006
BULIMBA	5935	33030	The second secon	HECRAS model-Bikeway
BULIMBA	5985	32980	HEC2937-MHG280	
BULIMBA	6050	32915	BM157	RUBICON model
BULIMBA	6160	32805	BM156	RUBICON model
BULIMBA	6240	32725	BM155	RUBICON model
BULIMBA	6340	32625	BM154	RUBICON model
BULIMBA	6450	32515	BM153_ALS	ALS
BULIMBA	6650	32315	BM151	RUBICON model
BULIMBA	6860	32105	BM149	RUBICON model
BULIMBA	6930	32035	BM148-BM147	Survey Craig street
BULIMBA	6935	32030	Survey Xsec	Craig_St Foot Bridge_weir
BULIMBA	6945	32020	Copy of BM148	RUBICON model
BULIMBA	6985	31980	BM148	RUBICON model
BULIMBA	7185	31780	BM146	RUBICON model
	7420	31545	BM144	RUBICON model
BULIMBA	7420	31475	BM143	RUBICON model
BULIMBA		31365	ALS-142	ALS section
BULIMBA	7600			RUBICON model
BULIMBA .	7735	31230	BM141	RUBICON model
BULIMBA	7915	31050	BM139	
BULIMBA	7985	30980	BM138	RUBICON model
BULIMBA	8070	30895	BM137	RUBICON model

Creek Branch	MIKE11 Chainage(m)	AMTD equivalent (m)	Cross section ID	Details (source)
BULIMBA	8200	30765	BM136	RUBICON model
BULIMBA	8325	30640	BM135	RUBICON model
BULIMBA	8475	30490	BM134	RUBICON model
BULIMBA	8555	30410	MHG-260	Interpolated
BULIMBA	8570	30395	BM132	Gauge BMA 804
BULIMBA	8780	30185	BM131	RUBICON model
	8840	30125	BM130	RUBICON model
BULIMBA	8950	30015	BM129	RUBICON model
BULIMBA	9115	29850	BM127	RUBICON model
BULIMBA	9215	29750	BM126	RUBICON model
BULIMBA		29600	BM126a	ALS
BULIMBA	9365	1	BM126b	AES
BULIMBA	9530	29435	BM120	RUBICON model
BULIMBA	9670	29295	_1	RUBICON model
BULIMBA	9765	29200	BM121	RUBICON model
BULIMBA	9890	29075	BM119	RUBICON model
BULIMBA	9920	29045	BM118	RUBICON model
BULIMBA	10100	28865	BM117	
BULIMBA	10205	28760	BM116 \ \ \	RUBICON model
BULIMBA	10315	28650	BM115	RUBICON model
BULIMBA	10400	(28565 /	BM114	RUBICON model
BULIMBA	10510	28455	BM112 \	RUBICON model
BULIMBA	10575	28390	BM1 L1=MHG250	Interpolated
BULIMBA	10685	28280	BM110	RUBICON model
BULIMBA	10725	28240	BM110-copy	RUBICON model
BULIMBA	10875	28090	BM108	RUBICON model
BULIMBA	10965	/ 28000	BM107	RUBICON model
BULIMBA ,	11095	27870	BM106	RUBICON model
BULIMBA	11255	27710	BM104	RUBICON model
BULIMBA	11515	27450	BM102	RUBICON model
BULIMBA	11620	27345	BM101	RUBICON model
BULIMBA	11695	27270	BM100	RUBICON model
BULIMBA	11820	27145	BM99	RUBICON model
BULIMBA	11910	27055	BM98	RUBICON model
BULIMBA	12035	26930	BM97	RUBICON model
BULIMBA	12135	26830	ВМ97сору	RUBICON model
	12155	26810	BM97copy	RUBICON model
BULIMBA BULIMBA	12215	26750	BM94	RUBICON model
1) OLUMBIA	12320	26645	MHG240	ALS section
BULIMBA	12385	26580	BM93	RUBICON model
BULIMBA		26460	Copy BM90	RUBICON model
BULIMBA	12505	26275	Copy_BM90	RUBICON model
BULIMBA	12690		BM88	RUBICON model
BULIMBA	12820	26145		RUBICON model
BULIMBA	13140	25825	BM87	RUBICON model
BULIMBA	13440	25525	BM84	RUBICON model
BULIMBA	13530	25435	BM83	I make the second secon
BULIMBA	13670	25295	BM81	RUBICON model
BULIMBA	13765	25200	BM80	RUBICON model
BULIMBA	13910	25055	BM78	RUBICON model
BULIMBA	13965	25000	Copy BM78 BMA831	RUBICON/Gauge BMA 83
BULIMBA	14115	24850	BM77	RUBICON model
BULIMBA	14360	24605	BM76	RUBICON model
BULIMBA	14460	24505	BM75	RUBICON model
BULIMBA	14625	24340	BM74-BM72	ALS

Creek Branch	MIKE11 Chainage(m)	AMTD equivalent (m)	Cross section ID	Details (source)
BULIMBA	14785	24180	BM72	RUBICON model
BULIMBA	14845	24120	BM71-MHG-230	RUBICON model/ALS
BULIMBA	14960	24005	BM70	RUBICON model
BULIMBA	15160	23805	BM69	RUBICON model
BULIMBA	15340	23625	BM67	RUBICON model
BULIMBA	15460	23505	BM66	RUBICON model
BULIMBA	15540	23425	Copy Bm66	RUBICON model
BULIMBA	15570	23395	BM64 copy	RUBICON model
BULIMBA	15585	23380	BM64	RUBICON model/ALS
BULIMBA	15600	23365	BM64-MHG250	RUBICON model
BULIMBA	15790	23175	BM63	RUBICON model
BULIMBA	15965	23000	BM62	RUBICON model
BULIMBA	16015	22950	BM61	RUBICON model
BULIMBA	16190	22775	BM60	RUBICON model
BULIMBA	16390	22575	BM-59.	RUBICON model
BULIMBA	16435	22530	BM59 mod	RUBICON model ALS
BULIMBA	16445	22520	Meadowbank St FB	RUBICON model/ALS
BULIMBA	16455	22510	BM 55-mod	RUBICON model/ALS
BULIMBA	16680	22285	BM57-mod	RUBICON model/ALS
BULIMBA	16785	(22180 /	BM56	RUBICON model
BULIMBA	17080	21885	BM 55-mod	RUBICON model
BULIMBA	17240	21725	BM55-54	ALS *
BULIMBA	17240	21665	BM54	RUBICON model
BULIMBA	1/338	21627	Winstanly St weir	RUBICON model
BULIMBA	17355	21610	CD09	Cardno Survey data
	17540	21425	BM52	RUBICON model
BULIMBA	17765	21200	CD07	Cardno Survey data
BULIMBA	17850	21115	BM50-49 BMA707	RUBICON model/BMA707
BULIMBA .	17920	21045	CD06	Cardno Survey data
BULIMBA	17960	21045	CD05	Cardno Survey data
BULIMBA	18025	20940	CD04	MHG: BM190
BULIMBA	18065	20900	BM47-mod	RUBICON model
BULIMBA	18110	20855	BM46-mod	RUBICON model
BULIMBA	18320	20645	CD02	Cardno Survey data
BULIMBA	18495	20470	BM44 mod	ALS
BULIMBA	18690	20275	BM43-mod	ALS
BULIMBA	18995	19970	BM42-mod	ALS
BULIMBA	19165	19800	BM42-mod MHG180	RUBICON model/ALS
BULIMBA		19770	Copy of BM41	RUBICON model
BULIMBA	19195	19770	Scrub Rd FB weir	RUBICON model/ALS
BULIMBA	19205	19760	BM41-mod	RUBICON model/ALS
BULIMBA	19215	19750	BM5GHD	RUBICON model
BULIMBA	19375		Bm5GHD	RUBICON model
BULIMBA	19640	19325	BM7GHD	RUBICON model
BULIMBA	20050	18915		RUBICON model
BULIMBA	20260	18705	BM8GHDcopy Meadowlands weir	RUBICON model/ALS
BULIMBA	20270	18695		RUBICON model/LBCFS
BULIMBA	20290	18675	Bm8GHD	RUBICON model/LBCFS
BULIMBA	20510	18455	BM9GHD	RUBICON model
BULIMBA	20850	18115	Bm37	The second secon
BULIMBA	21090	17875	BM17GHD	RUBICON model/LBCFS
BULIMBA	21555	17410	BM18GHD	RUBICON model/LBCFS
BULIMBA	21875	17090	BM18GHDcopy	RUBICON model/LBCFS
BULIMBA	21885	17080	Preston_Rd_FBweir	RUBICON model/ALS

Creek Branch	MIKE11 Chainage(m)	AMTD equivalent (m)	Cross section ID	Details (source)
BULIMBA	· 21895	17070	BM19 GHD	RUBICON model/LBCFS
BULIMBA	22305	16660	MHG170	Interpolated
BULIMBA	22775	16190	BM23GHD	RUBICON model/LBCFS
BULIMBA	23165	15800	MHG160	Interpolated
BULIMBA	23285	15680	BM10GHD	RUBICON model
BULIMBA	23600	15365	BM11GHD	RUBICON model
BULIMBA	24695	14370	BM13a	ALS/LBCFS
BULIMBA	24890	14075	BM13GHD	RUBICON model/LBCFS
BULIMBA	25515	13450	MHG19-old	Interpolated
BULIMBA	25565	13400	MHG20-old	Interpolated
BULIMBA	25865	13100	BM26 MHG150	RUBICON model
BULIMBA	25885	13080	Wynnum Rd weir	ALS
BULIMBA	25905	13060	Copy of BM 26	RUBICON model
BULIMBA	26015	12950	MHG140	Interpolated
BULIMBA	26145	12820	BM24	RUBICON model
BULIMBA	26365	12600	BM23	RUBICON model
BULIMBA	26620	12345	BM 22	RUBICON model
BULIMBA	26710	12255	Copy of BM22	RUBICON model
BULIMBA	26730	12235	Murarrie Rd weir	ALS
BULIMBA	26750	12215	Copy of BM22	RUBICON model
BULIMBA	26780	12185	MHG120	ALS
BULIMBA	26940	12025	Copy of BM22	RUBICON model
BULIMBA	26990	11975	Copy BM42AGHD	RUBICON model/LBCFS
BULIMBA	27100	11865	BM42A-mod	ALS/LBCFS
BULIMBA	27300	11665	BM42AGHD copy	RUBICON model/LBCFS
BULIMBA	27355	11610	BM42AGHD	RUBICON model/LBCFS
BULIMBA	27755	11210	BM43AGHD	RUBICON model/LBCFS
BULIMBA	28025	10940	BM44AGHD	RUBICON model/LBCFS
BULIMBA	28815	10150	BM44BGHD	RUBICON model/LBCFS
	29075	9890	BM43BGHD	RUBICON model/LBCFS
BULIMBA BULIMBA	29730	9235	BM43CGHD	RUBICON model/LBCFS
	30635	8330	BM43CGHD	RUBICON model/LBCFS
BULIMBA	31600	7365	BM45GHD	RUBICON model/LBCFS
BULIMBA	32110	6855	BM46CGHD MHG100	RUBICON model/LBCFS
BULIMBA	32355	6610	BM46BGHD	RUBICON model/LBCFS
BULIMBA	33330	5635	BM46AGHD	RUBICON model/LBCFS
BULIMBA	34300	4665	Copy BM52 GHD	RUBICON model/LBCFS
BULIMBA	34490	4475	Copy BM52 GHD	RUBICON model/LBCFS
BULIMBA	34510	4455	BM52 GHD	RUBICON model/LBCFS
BULIMBA	34700	4265	Copy BM52 GHD	RUBICON model/LBCFS
BULIMBA		3705	BM7	RUBICON model
BULIMBA	35260	3703	BM6	RUBICON model
BULIMBA	35670	3293 3275	Copy BM6	RUBICON model
BULIMBA	35690	3273	BM 48	RUBICON model
BULIMBA	35785		BM 48	RUBICON model
BULIMBA	36370	2595		RUBICON model
BULIMBA	37040	1925	BM3	Interpolated
BULIMBA	37465	1500	BM2_copy	RUBICON model
BULIMBA	38070	895	BM 2	RUBICON model
BULIMBA	38610	355	BM 1	
Bulimba_US_extension	0	39900	Copy BM222	Survey 2006
Bulimba_US_extension	65	39835	BM 222	Survey 2006
Bulimba_US_extension	175	39725	BM 221	Julyey 2000
Bulimba_US_extension	270	39630	BM220	Survey 2006

Creek Branch	MIKE11 Chainage(m)	AMTD equivalent (m)	Cross section ID	Details (source)
Bulimba US extension	415	39485	BM219	Survey 2006
Bulimba US extension	560	39340	BM218	Survey 2006
Bulimba US extension	736	39164	BM217	Survey 2006
Bulimba US extension	900	39000	BM216	Survey 2006
Bulimba US extension	935	38965		End of branch
BULIMBA EAST	1 939	30300		
BULIMBA EAST	60	6220	BE289	SMP Study:2001
BULIMBA EAST	170	6110	BE288	SMP Study: 2001
	250	6030	BE287	SMP Study: 2001
BULIMBA_EAST	388	5892	BE286	SMP Study:2001
BULIMBA_EAST	525	5755	BE285	SMP Study:2001
BULIMBA EAST	612	5668	BE284	SMP Study:2001
BULIMBA EAST		5620	HEC2146	HECRAS model-Railway
BULIMBA_EAST	660		BE283	SMP Study:2001
BULIMBA EAST	708	5572 5525	HEC2030	HECRAS model-Railway
BULIMBA_EAST	755	5525		SMP Study:2001
BULIMBA_EAST	799	5481	Copy of BE283 BE282US	SMP Study:2001
BULIMBA_EAST	815	5465		SMP Study:2001
BULIMBA_EAST	835	5445	BE281DS	SMP Study:2001
BULIMBA_EAST	840	5440	BE280	HECRAS model-Railway
BULIMBA_EAST	844	(5436)	BE279HEC	
BULIMBA_EAST	<i>-</i> -852√	5428	BE278 \(\)	SMP Study:2001
BULIMBA_EAST	875	5405	BE277-HEC	HECRAS model-Railway
BULIMBA EAST	946	5334	BE 277-HEC DS	HECRAS model-Railway
BULIMBA EAST	956	\ \5324\	BE277-A	ALS section
BULIMBA EAST	978	5302	Copy BE277-A	ALS section
BULIMBA EAST	\ 981	/ 5299	XS-7450	SMP Study:2001
BULIMBA EAST	991	5289	XS-7460	SMP Study:2001
BULIMBA EAST	1011	5269	Xs-7480	SMP Study:2001
BULIMBA EAST	1031	5249	XS-7500	SMP Study:2001
BULIMBA EAST	1051	5229	XS-7520	SMP Study:2001
BULIMBA EAST	1071	5209	XS-7540	SMP Study:2001
BULIMBA EAST	1091	5189	XS-7560	SMP Study:2001
BULIMBA EAST	1111	5169	Xs-7580	SMP Study:2001
BULIMBA EAST	1131	5149	Xs-7600	SMP Study:2001
BULIMBA EAST	1151	5129	Xs-7620	SMP Study:2001
BULIMBA EAST	1171	5109	XS-7640	SMP Study:2001
	1191	5089	XS-7660	SMP Study:2001
BULIMBA EAST	1211	5069	XS-7680	SMP Study:2001
BULIMBA EAST	1231	5049	Xs-7700	SMP Study:2001
BULIMBA_EAST	1251	5029	XS-7720	SMP Study:2001
BULIMBA_EAST		5009	XS-7740	SMP Study:2001
BULIMBA_EAST	1271	4989	XS-7760	SMP Study:2001
BULIMBA_EAST	1291		Xs-7780	SMP Study:2001
BULIMBA EAST	1311	4969		SMP Study:2001
BULIMBA EAST	1331	4949	XS-7800	SMP Study:2001
BULIMBA_EAST	1341	4939	Xs-7810	
BULIMBA_EAST	1355	4925	BE273	SMP Study:2001
BULIMBA_EAST	1498	4782	BE 272	SMP Study:2001
BULIMBA_EAST	1565	4715	BE272	SMP Study:2001
BULIMBA EAST	1600	4680	BE271_ALS	ALS section
BULIMBA EAST	1730	4550	BE270	SMP Study:2001
BULIMBA EAST	1915	4365	BE269	SMP Study:2001
BULIMBA EAST	2020	4260	BE268	SMP Study 2011
BULIMBA EAST	2145	4135	BE267	SMP Study:2001

Creek Branch	MIKE11 Chainage(m)	AMTD equivalent (m)	Cross section ID	Details (source)
BULIMBA EAST	2245	4035	BE 266	SMP Study:2001
BULIMBA EAST	2410	3870	BE265	SMP Study:2001
BULIMBA EAST	2500	3780	BE264	SMP Study:2001
BULIMBA EAST	2605	3675	BE263	SMP Study:2001
BULIMBA EAST	2765	3515	BE 262	SMP Study:2001
BULIMBA EAST	2767	3513	Underwood Rd weir	ALS section
BULIMBA EAST	2785	3495	BE 261	SMP Study:2001
BULIMBA EAST	2990	3290	BE259	SMP Study:2001
BULIMBA EAST	3200	3080	BE258	SMP Study;2001
BULIMBA EAST	3320	2960	BE257	SMP Study:2001
BULIMBA EAST	3425	2855	Copy BE257	SMP Study:2001
BULIMBA EAST	3490	2790	BE256	SMP Study:2001
BULIMBA EAST	3670	2610	BE255	SMP\Study:2001
BULIMBA EAST	3695	2585	Copy-BE255	SMP Study:2001
BULIMBA_EAST	3725	2555	BE255 mod	ALS section
BULIMBA EAST	3735	2545	Copy BE254	SMP Study:2001
BULIMBA EAST	3745	2535	BE254	SMP Study:2001
BULIMBA EAST	3785	2495	BE253	SMP Study:2001
BULIMBA EAST	3810	2470	interpolated	SMP Study:2001
BULIMBA EAST	3925	(2392)	BE251	SMP Study:2001
BULIMBA EAST	4020	2392	BE250 \	SMP Study:2001
BULIMBA EAST	4110	2170	BE249	SMP Study:2001
BULIMBA EAST	(4230)	2050	BE248	SMP Study:2001
BULIMBA_EAST	4300	1980	BE247	SMP Study:2001
BULIMBA EAST	43.60	1,920	Copy BE247	SMP Study:2001
BULIMBA EAST	4419	1861	BE246	SMP Study:2001
BULIMBA EAST	4507	1773	BE246A_ALS	ALS section
BULIMBA EAST	4602	1678	BCFS 4612	RUBICON model
BULIMBA EAST	4638	1642	Copy BCFS 4612	RUBICON model
BULIMBA EAST	4656	1624	BE244	SMP Study:2001
BULIMBA EAST	4660	1620	ALS	ALS section
BULIMBA EAST	4695	1585	BCFS 4665	RUBICON model
BULIMBA EAST	4730	1550	BCFS 4685	RUBICON model
BULIMBA EAST	4750	1530	BCFS 4705	RUBICON model
	4870	1410	BE241	RUBICON model/ALS
BULIMBA_EAST	4980	1300	BE240	RUBICON model/ALS
BULIMBA_EAST BULIMBA_EAST	5050	1230	BE239	RUBICON model/ALS
BULIMBA EAST	5175	1105	BE238	RUBICON model/ALS
The second secon	5330	950	BE236	RUBICON model/ALS
BULIMBA EAST	5470	810	BE235	RUBICON model/ALS
BULIMBA_EAST	5712	568	BE232	RUBICON model/ALS
BULIMBA_EAST	5810	470	BE231	RUBICON model/ALS
BULIMBA_EAST	5895	385	BE230	RUBICON model/ALS
BULIMBA_EAST		305	BE229	RUBICON model/ALS
BULIMBA_EAST	5975	225	BE228	RUBICON model/ALS
BULIMBA_EAST	6055	145	BE227	RUBICON model/ALS
BULIMBA_EAST	6135	147	133661	

T. N. S.	MIKEII	Cross Section ID	Details
Creek Branch		C1033 Section 1D	(Source)
	Chainage (m)		(Som So)
BULIMBA EAST Railbypass			
BULIMBA EAST Railbypass	33	BE 276	SMP Study:2001/ALS
BULIMBA EAST Railbypass	144	BE275	SMP Study:2001/ALS
	226	BE 274	SMP Study:2001/ALS
BULIMBA EAST Railbypass	347	BE 273 US	SMP Study:2001/ALS
BULIMBA EAST Railbypass	443	BE273 DS	SMP Study:2001/ALS
BULIMBA EAST Railbypass		BE 273A	ALS
BULIMBA_EAST Railbypass	488	BE Z/3A	End of branch
BULIMBA_EAST Railbypass	520		End of branch
TRIB_A		2 217 69	ALS
TRIB_A	100	Copy of ALSI	
TRIB_A	320	ALSI	ALS
TRIB A	600	ALS2	ALS
TRIB A	950	BE-1060	SMP Study:2001/ALS
TRIB A	1400	BE-1040	SMP Study:2001/ALS
TRIB A	1770	BE-1030	SMP\Study:2001/ALS
TRIB A	2070	BE-1020	SMP Study:2001/ALS
TRIB A	2125	CSI-1	Interpolated
TRIB A	2235	BE-1010	SMP Study:2001/ALS
TRIB A	2535	BE-1005-ALS	SMP Study:2001/ALS
TRIB A	2555	BE-1005-ALS	SMP Study:2001/ALS
	2735	Copy of BE1005	SMP Study:2001/ALS
TRIB A	2765	BE1000	SMP Study:2001/ALS
TRIB_A	1	BE1000 modified	SMP Study:2001/ALS
TRIB_A	2935\\		SMP Study:2001/ALS
TRIB_A	3015	BE1000-modified	SIVIE Study:2001/4 YES
TRIB_A1		North Control of the	GNAD GALLENOOT/ATS
TRIB_A1	_280 /	A1-1050	SMP Study:2001/ALS
TRIB_A1	500/	ALS-1	ALS section
TRIB_A1	720	ALS-2	ALS section
TRIB A1	750	ALS-3	ALS section
TRIB A2			
TRIB A2	80	SMP-1	SMP Study:2001/ALS
TRIB A2	475	SMP-2	SMP Study:2001/ALS
TRIB A2	690	SMP-3	SMP Study:2001/ALS
TRIB A2	1035	SMP-4	SMP Study:2001/ALS
TRIB_A2	1042	SMP-5	SMP Study:2001/ALS
TRIB B			
TRIB B	1055	BE2030	SMP Study:2001/ALS
	1075	Copy of BE2030	SMP Study:2001/ALS
TRIB B	1215	BE2020	SMP Study:2001/ALS
TRIB B	1340	Copy of BE2020	SMP Study:2001/ALS
TRIB B	<u></u>	BE2010	SMP Study:2001/ALS
TRIB_B	1394		SMP Study:2001/ALS
TRIB B	1432	BE2000	End of branch
TRIB_B	1492		End of Dranch
TRIB_C	-1		(a) (b) (c) (c) (c) (c) (c) (c) (c) (c) (c) (c
TRIB C	10	BE-3050	SMP Study:2001/ALS
TRIB C	390	BE-3040	SMP Study:2001/ALS
TRIB C	545	BE-3030	SMP Study:2001/ALS
TRIB C	665	BE-3020	SMP Study:2001/ALS
TRIB C	810	BE-3010	SMP Study:2001/ALS
TRIB C	1000	BE3000	SMP Study:2001/ALS
	1005	Copy BE-3000	SMP Study:2001/ALS
TRIB C	1100	Copy BE3000	SMP Study:2001/ALS
TRIB_C	1110	ALS-C1	ALS
TRIB_C	1110	Jaco vi	

Creek Branch	MIKE11	Cross Section ID	Details
	Chainage (m)		(Source)
TRIB C	1120	ALS-C2	ALS
TRIB B1	1000	ALS-B1	ALS
TRIB BI	1002	ALS-B2	ALS
TRIB B1	1020	ALS-B3	ALS
TRIB B1	1055	ALS-B4	ALS
TRIB B1	1140	ALS-B5	ALS
TRIB B1	1145	ALS-B5	End of branch
PADSTOW			
PADSTOW	32	BM177	RUBICON model
PADSTOW	105	BM177-176ALS	RUBICON model /ALS
PADSTOW	175	BM176-US-ALS	RUBICON model /ALS
PADSTOW	205	BM176-DS-ALS	RUBICON model /ALS
PADSTOW	258	BM175	RUBICON model
PADSTOW	325	BM175-174ALS	RUBICON model /ALS
The state of the s	352	BM174	RUBICON model
PADSTOW PADSTOW	375		End of Branch
GARDEN CITY	1 313		1 2 2 2
GARDEN CITY	5285	BM169	RUBICON model
75	5405	BM168	RUBICON model
GARDEN_CITY	5510	BM167	RUBICON model
GARDEN CITY	5615	Copy BM167	RUBICON model
GARDEN CITY	5715	Copy BM165	RUBICON model
GARDEN CITY	5730	Bm165	RUBICON model
GARDEN CITY	5785	XS5	Logan-survey
GARDEN_CITY	5850	XS4	Logan-survey
GARDEN CITY	5935	Copy XS4	Logan-survey
GARDEN_CITY	5938	Copy XS4	End of branch
GARDEN CITY	2320	Copy.zca+	
MIMOSA Creek	5	Mi 40 Hecras	Mimosa HECRAS model
MIMOSA	96	Mi 40a ALS	ALS
MIMOSA	200	Mi39	Mimosa HECRAS model
MIMOSA		MI38	Mimosa HECRAS model
MIMOSA	330	Mi37	Mimosa HECRAS model
MIMOSA	1	Mi36	Mimosa HECRAS model
MIMOSA	506		Mimosa HECRAS model
MIMOSA	558	Mi35	Mimosa HECRAS model
MIMOSA	660	Mi34	Mimosa HECRAS model
MIMOSA	696	Mi33	Mimosa HECRAS model
MIMOSA	811	Mi32	Mimosa HECRAS model
MIMOSA	952	Mi31	Mimosa HECRAS model
MIMOSA	1037	Copy of Mi31	Mimosa HECRAS model
MIMOSA	1186	Mi29	Mimosa HECRAS model
MIMOSA	1302	Mi28	
MIMOSA	1322	Mi27	Mimosa HECRAS model
MIMOSA	1366	Mi26	Mimosa HECRAS model
MIMOSA	1439	Mi25	Mimosa HECRAS model
MIMOSA	1549	Mi24	Mimosa HECRAS model
MIMOSA	1588	Mi23	Mimosa HECRAS model
MIMOSA	1719	Mi22	Mimosa HECRAS model
MIMOSA	1738	Mi21-2	Mimosa HECRAS model
MIMOSA	1752	Mi21-1	Mimosa HECRAS model
MIMOSA	1762	Mi20	Mimosa HECRAS model
MIMOSA	1882	Mi19 85	Mimosa HECRAS model
MIMOSA	1892	Mi19-4	Mimosa HECRAS model

Creek Branch	MIKE11	Cross Section ID	Details
Creek Drancu	Chainage (m)		(Source)
· ·	Chamage (m)		
MIMOSA	1964	Mi19-1	Mimosa HECRAS model
MIMOSA	2023	Mi18	Mimosa HECRAS model
MIMOSA	2086	Mi17	Mimosa HECRAS model
MIMOSA	2133	Mi16	Mimosa HECRAS model
	2224	Mi15	Mimosa HECRAS model
MIMOSA	2248	Mi13-3	Mimosa HECRAS model
MIMOSA	2255	Kessels Road weir	ALS
MIMOSA	2284	Mi13-2	Mimosa HECRAS model
MIMOSA	2325	Mi13	Mimosa HECRAS model
MIMOSA	2516	Mi12	Mimosa HECRAS model
MIMOSA	2635	Mi11	Mimosa HECRAS model
MIMOSA	· · · · · · · · · · · · · · · · · · ·	Mi10-2	Mimosa HECRAS model
MIMOSA	2664		Mimosa HECRAS model
MIMOSA	2718	INTE	Mimosa HECRAS model
MIMOSA	2828	Mi8	Mimosa HECRAS model
MIMOSA	2955	Mi7	Mimosa HECRAS model
MIMOSA	3069	Mi6	Mimosa HECRAS model
MIMOSA	3221	Mi5	Mimosa HECRAS model
MIMOSA	3388	Mī4	Mimosa HECRAS model
MIMOSA	3496	Mi3	Mimosa HECRAS model
MIMOSA	3585	(Mi2)	
MIMOSA	3801 \	Mí1	Mimosa HECRAS model
MIMOSA	3890 \		End of Mimosa Creek
MINNIPPI BYPASS			
MINNIPPI bypass	80	ALS1\	ALS
MINNIPPI bypass	125	Minnippi_new1	ALS
MINNIPPI bypass	√230 /	Minnippi_new2	ALS
MINNIPPI bypass	400	Minnippi_new3	ALS
MINNIPPI bypass	542	Minnippi_new4	ALS
MINNIPPI bypass	650	Minnippi_new5	ALS
MINNIPPI bypass	720	new_A	ALS
MINNIPPI bypass	710	Stanton Rd	ALS
MINNIPPI bypass	730	New_B	ALS
MINNIPPI bypass	745	Minnippi new6-US	ALS
MINNIPPI bypass	748	Gateway Motorway	
MINNIPPI bypass	810	Minnippi_uew7-DS	RUBICON model
MINNIPPI bypass	825	New E	RUBICON model
MINNIPPI bypass	860	New G	ALS
MINNIPPI bypass	870	New 7a	ALS
MINNIPPI bypass	945	Minnippi new8	RUBICON model
MINNIPPI bypass	1015	BM31GHD_modified	RUBICON model
	1115	Minnippi-6 ALS	ALS
MINNIPPI bypass	1125	Wynnum Road weir	ALS
MINNIPPI bypass	1150	BM 31GHD-copy	RUBICON model
MINNIPPI bypass	1310	BM36 GHD	RUBICON model
MINNIPPI bypass	1560	Minnippi_new[1]	ALS
MINNIPPI bypass	1850	BM 42B GHD	RUBICON model
MINNIPPI bypass		BM42BGHD	RUBICON model
MINNIPPI bypass	2004	DWAYDOWD	Todaroot intouct
MURARRIE Bypass	1	NOTE ATO	ALS section
MURARRIE bypass	20	MUI_ALS	ALS section
MURARRIE bypass	160	New_MU2_ALS	
MURARRIE bypass	275	New_MU3_ALS	ALS section
MURARRIE bypass	310	Copy_new_MU3	ALS section
MURARRIE bypass	390	New_MU5_ALS	ALS section

Creek Branch	MIKE11 Chainage (m)	Cross Section ID	Details (Source)
MURARRIE bypass	470	Mu_6_ALS	ALS section
MURARRIE bypass	475	Gateway culverts	
MURARRIE bypass	545	MU_7_ALS	ALS section
MURARRIE bypass	595	MU_9_ALS	ALS section
MURARRIE bypass	640	MU5_ALS	ALS section
MURARRIE bypass	650		End of branch
KIANAWAH PARK Branch			
KIANAWAK PARK Branch	0	WY-1 ALS	ALS section
KIANAWAK PARK Branch	48	WY-1 ALS	ALS section >
KIANAWAK PARK Branch	210	WY-2 ALS	ALS section
KIANAWAK PARK Branch	260	WY-3 ALS	ALS section
KIANAWAK PARK Branch	340	WY-4 ALS	ALS section
KIANAWAK PARK Branch	430	WY-5 ALS	ALS section \
KIANAWAK PARK Branch	530	WY-6 ALS	ALS section
KIANAWAK PARK Branch	660	WY-7 ALS	ALS section
KIANAWAK PARK Branch	780	WY-8 ALS	ALS section
KIANAWAK PARK Branch	860	WY-9 ALS	ALS section
KIANAWAK PARK Branch	945	WY-10 ALS	AES section
KIANAWAK PARK Branch	985	WY-11 ALS	ALS section
KIANAWAK PARK Branch	1006	End 4	ALS section
in the state of th	1 1		
ALS: Airborne Laser Scanning da	ta;2002, \ \		

Table A3: Hydraulic Structures included in the MIKE11 model

No.	Location	Branch	Chainage	Structure
1.	Nemies Road	Bulimba Creek	17	Box culverts(8/1.5 x1.5)
2	Brandon Road	Bulimba Creek	370	Box culverts(4 / 2.7 x0.9)
3 .	Beenleigh Road	Bulimba Creek	1845	Box culverts(4/3.6 1.2)
4	Beenleigh Road	Bulimba Creek	1950	Bridge
<u> </u>	StLawrences Foot Bridge	Bulimba Creek	2117	Foot Bridge
6	Altandi Sreet Foot Bridge	Bulimba Creek	2375	Foot Bridge
7	Malbon Street Foot Bridge	Bulimba Creek	3965	Foot Bridge
8	Padstow Road	Bulimba Creek	4390	Box culverts(7/3.35x2.2)
9	Padstow Road No.2	Bulimba Creek	177	Box culverts(3 / 3 x2.1)
10	Blesby Road Foot Bridge	Bulimba Creek	4785	Foot Bridge
11	South-East Freeway	Bulimba Creek	5625	Box culverts(5/3.1x3.1)
12	South-East Freeway No. 2	Garden City branch	5620	Box culverts(2/3.1x3.1)
13	Logan Road	Bulimba Creek	5790	Box culverts (5/3x3)
14	Logan Road No.2	Garden City branch	5790	Box culverts(2/3x3)
15	Craig Street Foot Bridge	Bulimba Creek	6935	Foot Bridge
16	Mt Gravatt CapalabaRoad	Bulimba Creek	10702	Bridge
17	Wecker Road Bridge	Bulimba Cřeck	12139	Bridge
18	Pine Mountain Road	Bulimba Creek	15555	Bridge
19	Meadowbanks St FootBridge	Bulimba Creek	16445	Foot Bridge
20	Winstanly St	Bulimba Creek	17338	Bridge
21	Old Cleveland Road	Bulimba Creek	17935	Bridge
22	Scrub Road Foot Bridge	Bulimba Creek	19205	Foot Bridge
23	Meadowlands Road	Bulimba Creek	20270	Bridge
24	Preston Road foot Bridge	Bulimba Creek	21885	Foot Bridge
25	Wynnum Road	Bulimba Creek	25885	Bridge
26	Murarrie Road	Bulimba Creek	26730	Bridge
27	Cleveland-Rail	Bulimba Creek	34500	Bridge
28	Lytton Road	Bulimba Creek	35680	Bridge
29	Wynnum Road Minnippi	Minnippi branch	1125	Bridge
30	Beenleigh Road-South	Bulimba Creek east	820	Box culverts (4/1.65x 0.6)
31	Beenleigh Road rail	Bulimba Creek east	845	Box culverts(10 / 1.5x1.15)
32	Beenleigh Road-Gateway	Bulimba Creek east	876	Pipe culverts (3 / 2.4dia.)
33	Underwood Road	Bulimba Creek east	2767	Box culverts (4/3.7x 1.8)
34	Gateway Motorway	Bulimba Creek east	3330	Bridge
35	Logan Road (box culvert)	Bulimba Creek east	3748	Box culverts (2 / 2.4x2.4)
36	Logan Road pipe culvert	Bulimba Creek east	3748	Pipe culverts (4 / 2.4dia.)
37	Pacific Motorway	Buliniba Creek east	4305	Box culverts (5 / 3.05x2.7)
38	Eight Mile Plains	Bulimba Creek east	4608	Bridge
39	Miles Platting Road	Bulimba Creek east	4660	Bridge

Bulimba Creek Flood Study

No.	Location	Branch	Chainage	Structure
40	Gateway on-off_ramp	Bulimba Creek east	5010	Bridge
41	Nagel Street Bridge	Mimosa Creek	1739	Bridge
42	Mimosa Creek at Pacific Motorway	Mimosa Creek	1895	Box culverts (3/3x2.7)
43	Kessels Road	Mimosa Creek	2255	Bridge
44	Parkway Street	Mimosa Creek	2648	Bridge
45	School Road to Freeway	Tributary A	2072	Box culverts(3/3.1x2.1)
46	South-east Freeway-off ramp	Tributary A	2545	Box culverts(9/2.4x1.8)
47	Gateway Motorway	Tributary A	2805	Box culverts (3 / 3.3dia.)
48	Gateway Motorway No.2	Tributary A	2805	Box culverts (3 / 3.5 dia.)
49	Dance Court No.1	Tributary B	1062	Box culverts(3 / 3.65x1.5)
5	Dance Court No.2	Tributary B	1062	Box culverts(1 / 3.65x1.7)
51	Logan Road-Trib B	Tributary B	1361	Box culverts(1/3x2.6)
52	Gateway in TribC	Tributary C	1008	Pipe culverts (4/2.7dia.)
53	Gaskell Street	Tributary B1	1030	Box culverts(3/3x1.5)
54	Gateway Motorway culvert	Minnippi	770.	Box culverts (6/3x3)
55	Gateway Motorway Bridge	Bulimba Creek	26950	Bridge (via duct)
56	Gateway Motorway culverts	Murarrie	475	Box culverts (9/2x1.6)

Table A4: Manning's Roughness (n) Values used in the MIKE11 Model

Bulimba Creek	
Nemies Road to Brandon Road weir	0.085
Brandon Road weir to Logan Road	0.09-0.1
Logan Road to Greenwood Street	0.08-0.09
Greenwood Street to Wecker Road	0.065-0.07
Wecker Road to Green meadow Street	0.07-0.075
Green meadow Street to Old Cleveland Road	0.06-0.065
Old Cleveland Road to Scrub Road	0.05-0.06
Scrub Road to Minnippi Parklands	0.04-0.05
Minnippi Parklands to Boundary Road	0.035
Boundary Road to confluence with Brisbane River	0.03
Mimosa Creek	1 1
Klumpp Road to Hoad Street	0.07-0.08
Hoad Street to Pacific Motorway	0.08-0.10
Pacific Motorway to Sheraton Street	0.07-0.075
Sheraton Street to Bulimba Creek confluence	0.09
Bulimba Creek East Arm	
Persse Road to upstream of Beenleigh Road	0.095-0.09
Beenleigh Road to downstream of railway bridge	0.055
Railway bridge downstream to Gateway Motorway downstream	0.090-0.095
Gateway Motorway downstream to Logan Road	0.09-0.08
Logan Road to Pacific Motor way upstream	0.08-0.07
Pacific Motorway to Bulimba Creek confluence	0.080.09
Other Branches	
Garden City branch	0.09
Padstow branch	0.08-0.09
Bulimba -East Left arm	0.1
Tributary A in Bulimba East Arm	0.08
Tributary A1 in Bulimba East Arm	0.08
Tributary A2 in Bulimba East Arm	0.08
Tributary B in Bulimba Eat Arm	0.06-0.08
Tributary B1 in Bulimba Eat Arm	0.08
Murarrie Bypass branch	0.045
Minnippi Bypass branch	0.09

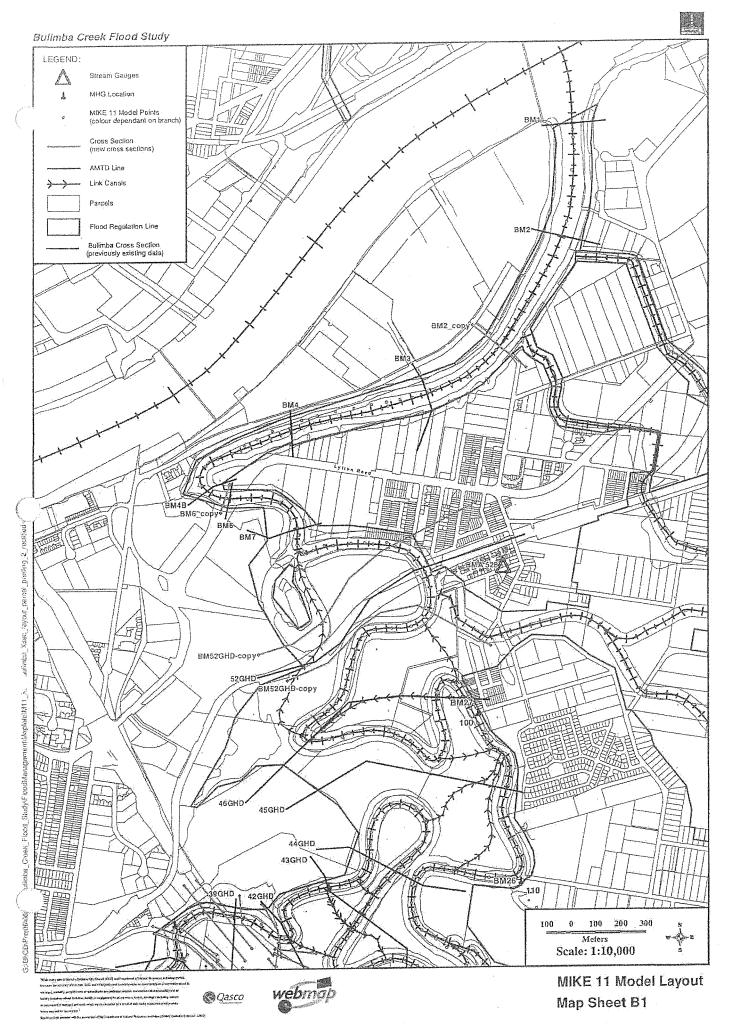
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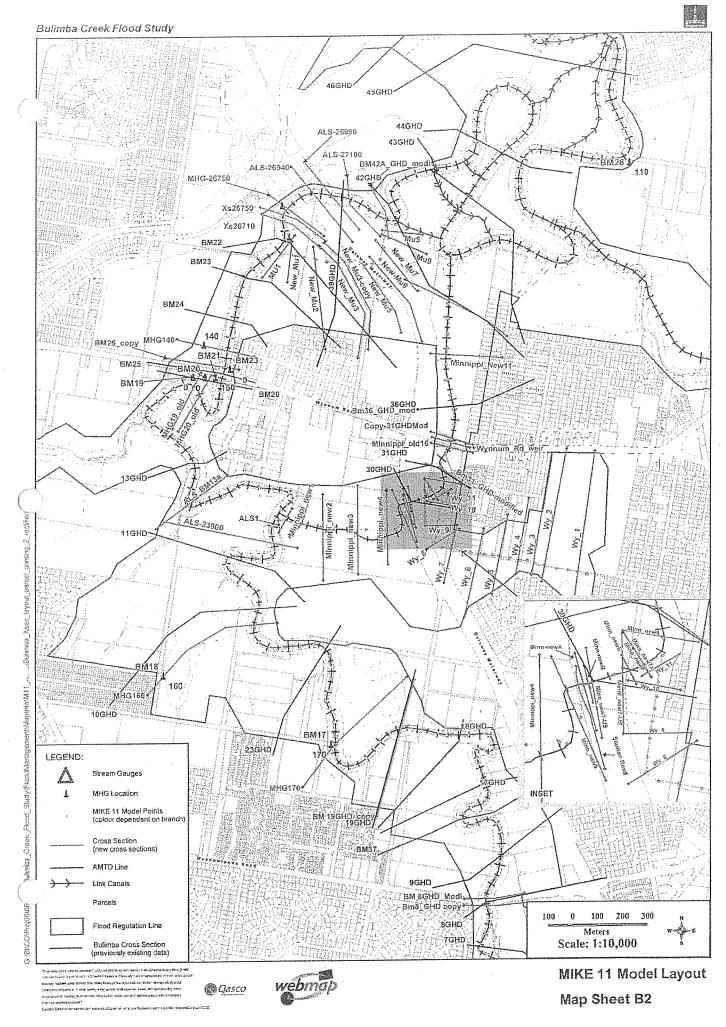


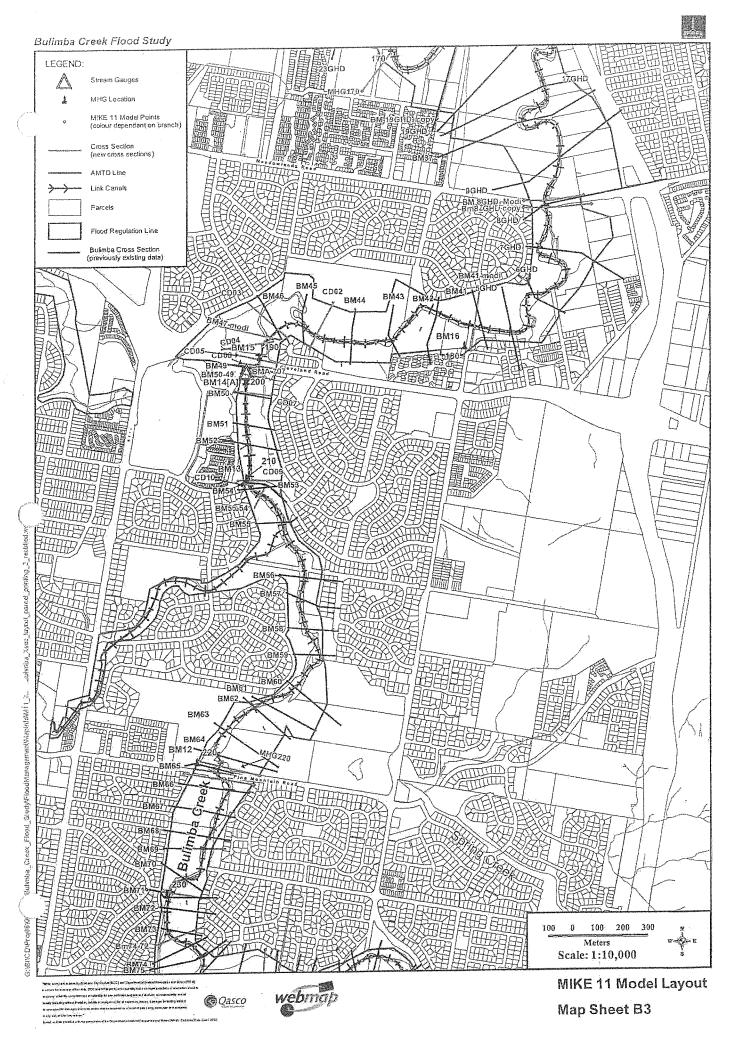
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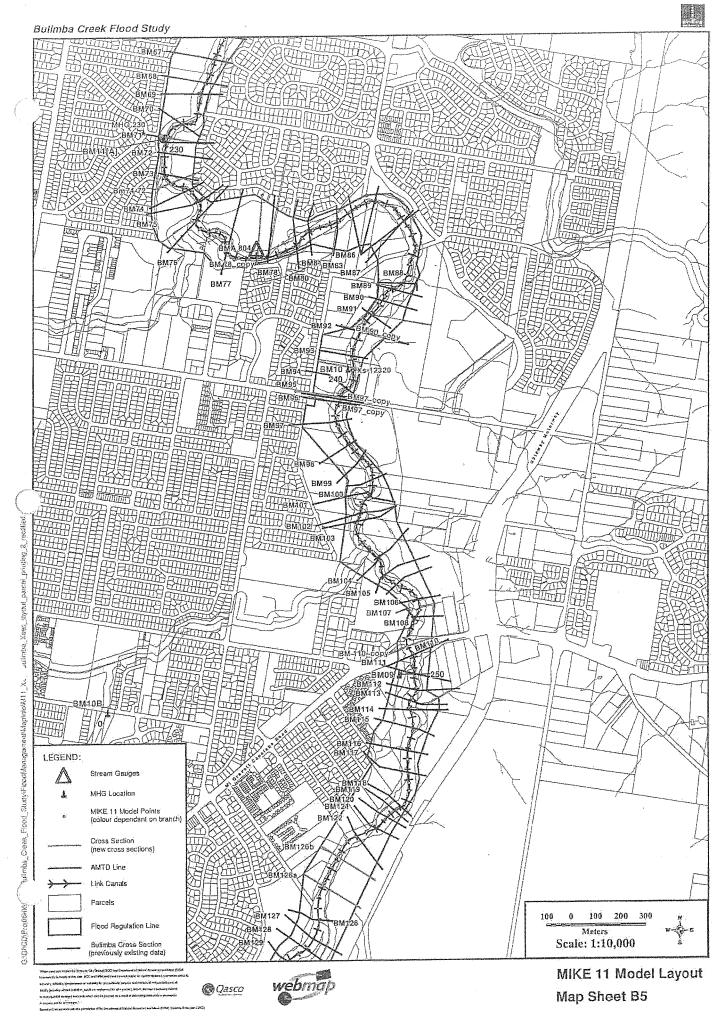
Appendix B MIKE11 Model Cross Section Layout

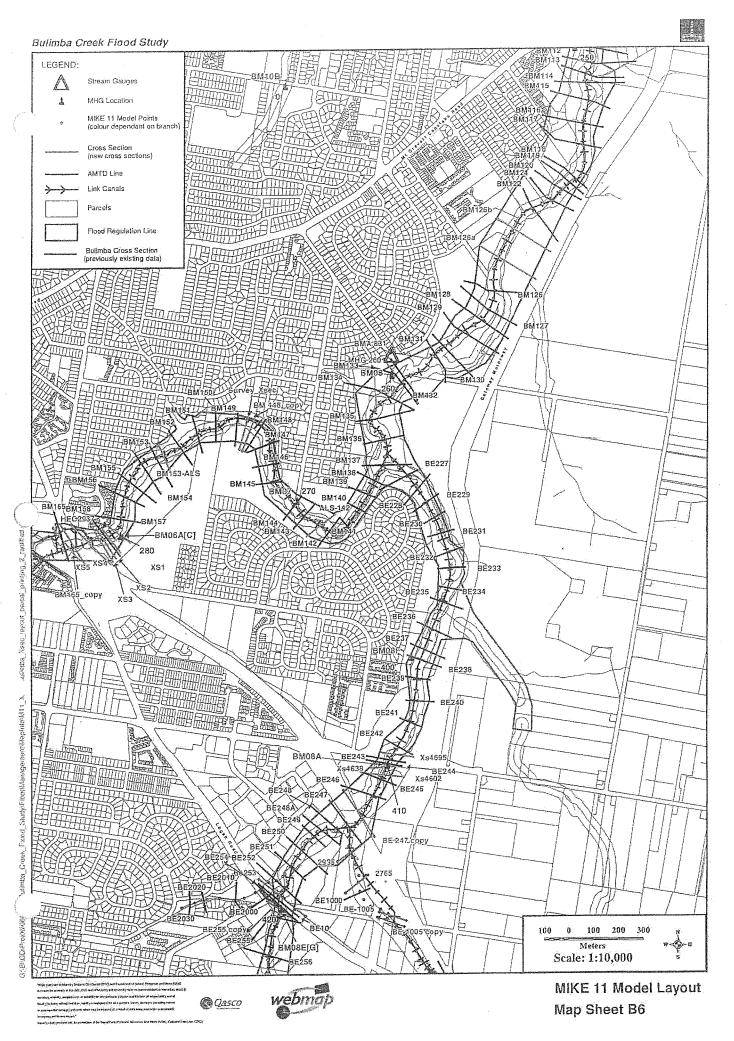


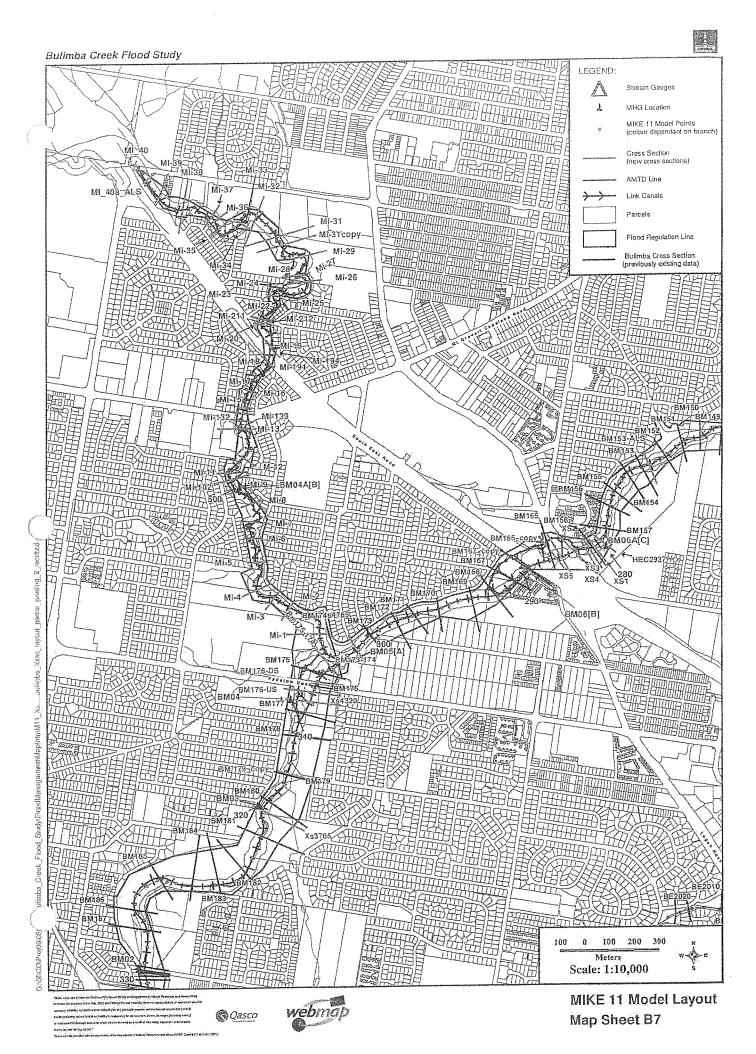


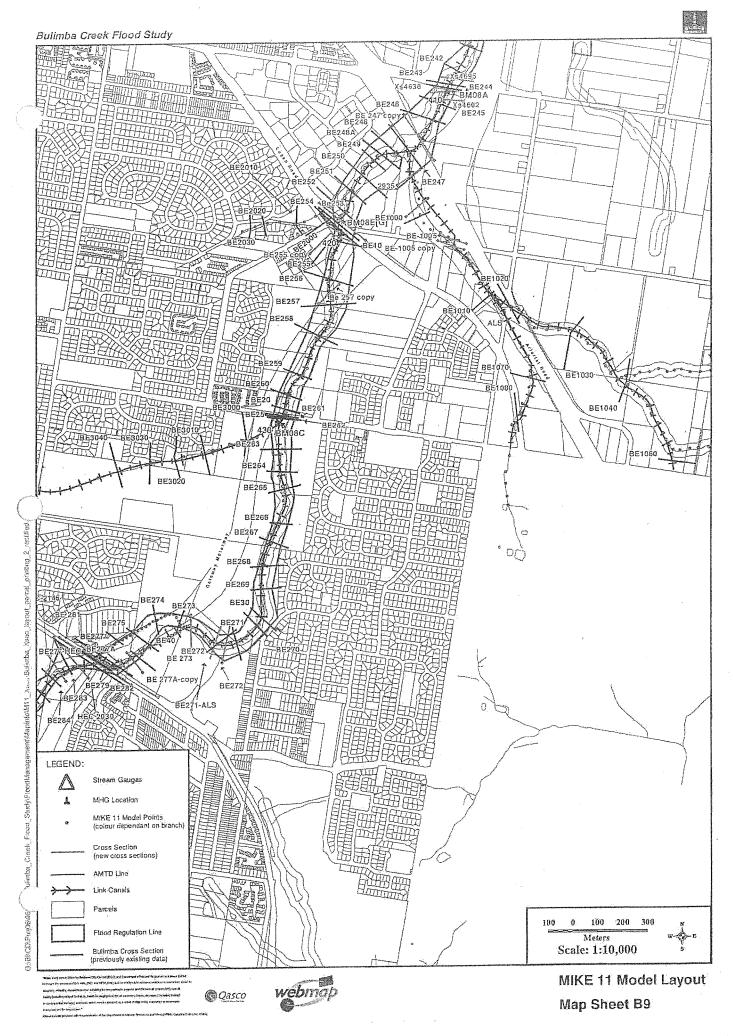














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Appendix C Cumulative Rainfall & Rainfall Distribution Adopted for Calibration/Verification events



Cumilative Rainfall: March 1992 Event

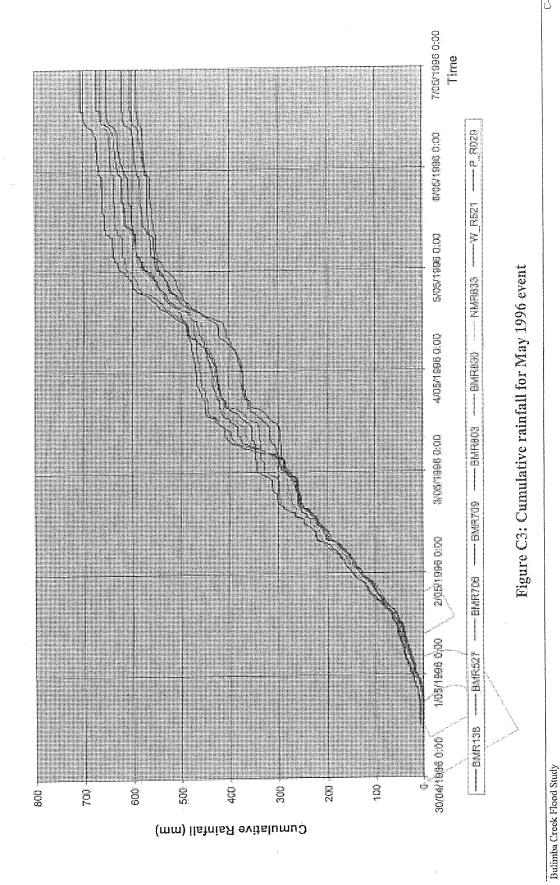
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Bulimba Creek Flood Study

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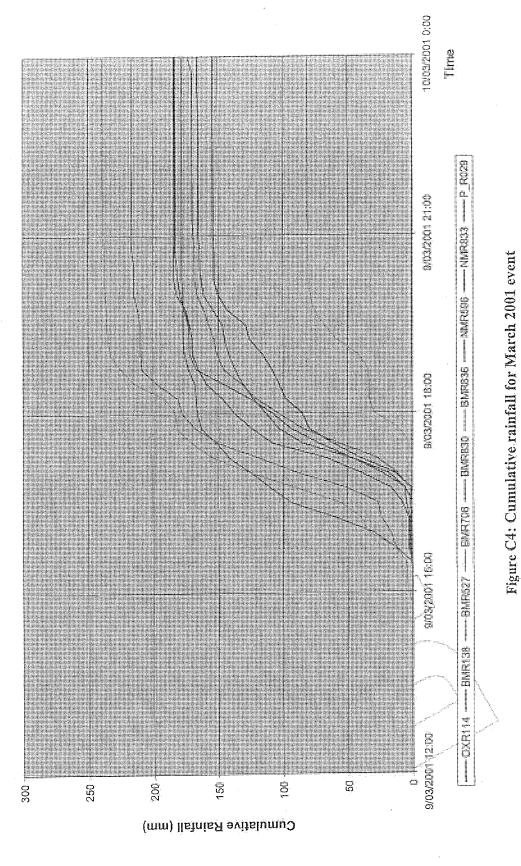
Cumilative Rainfall: January 1994 Event

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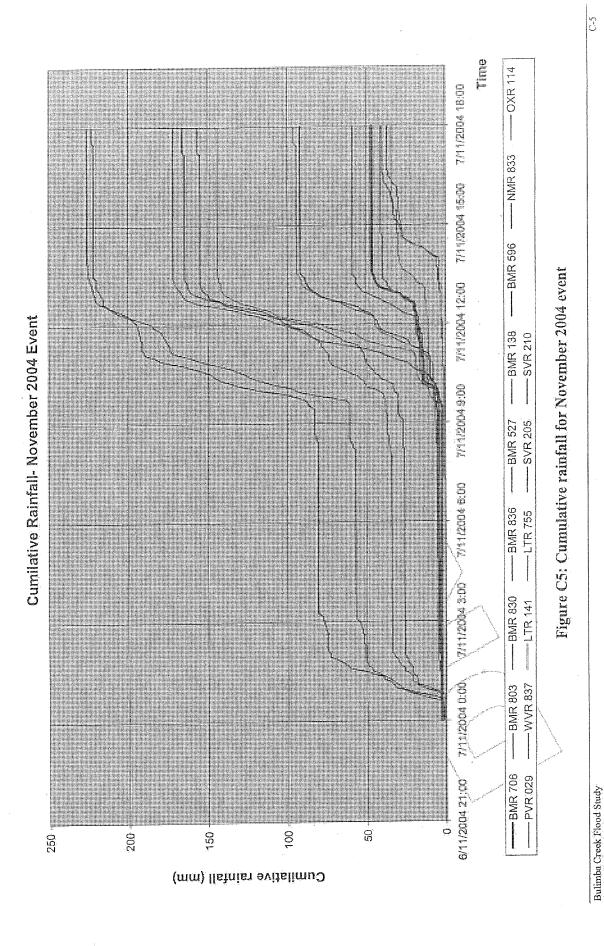
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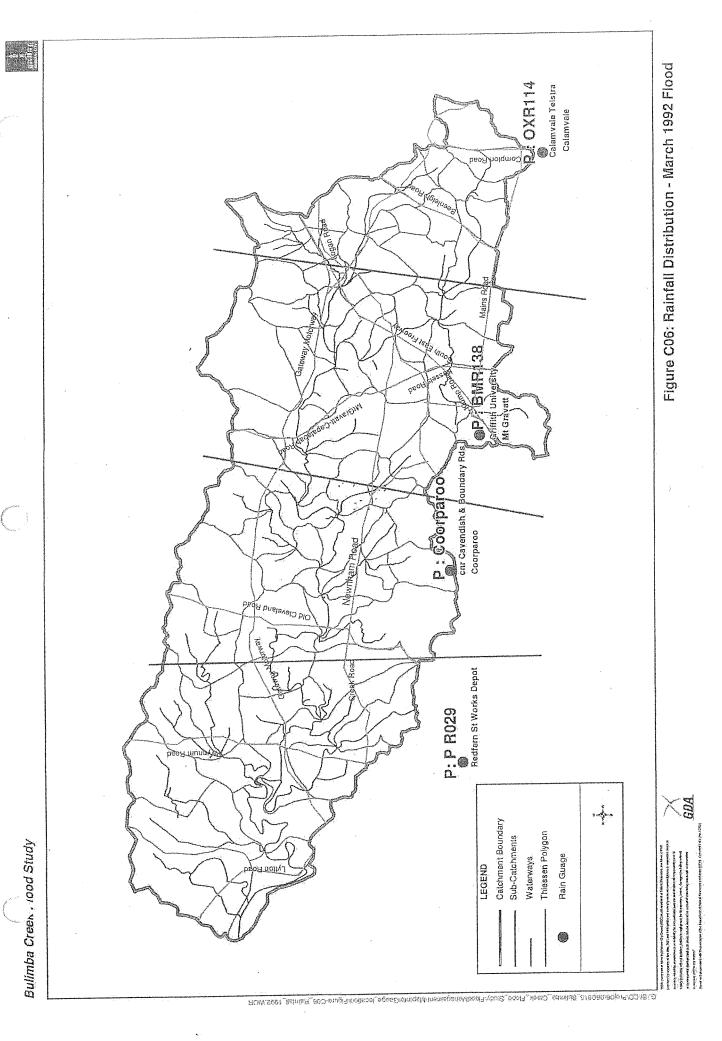


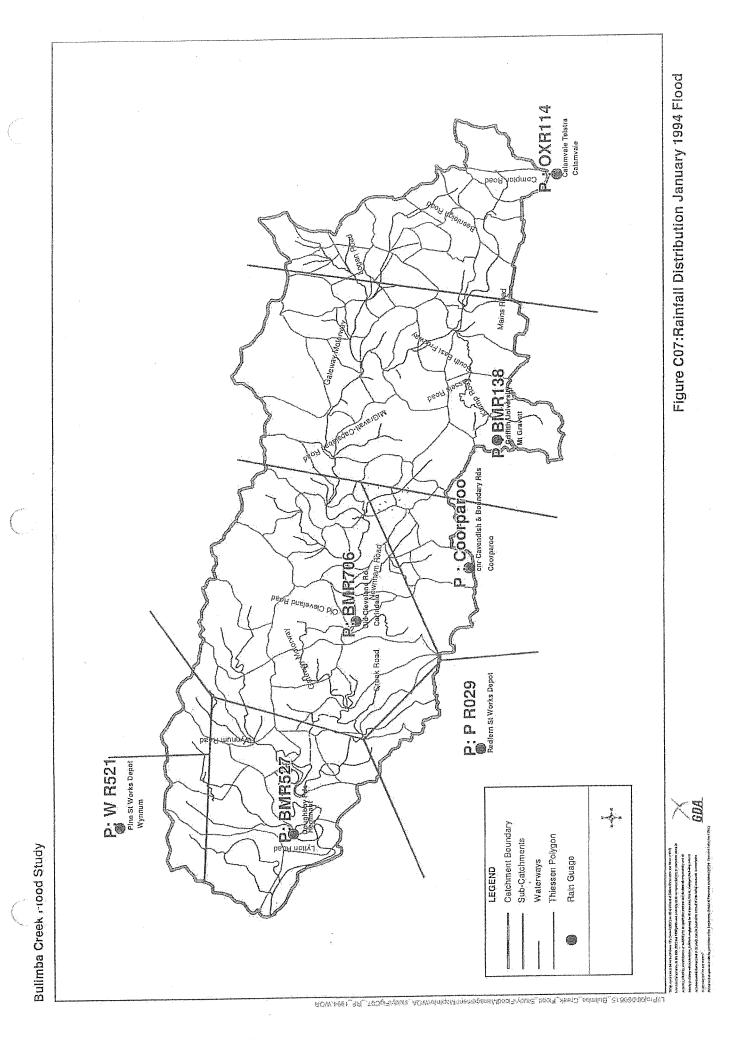
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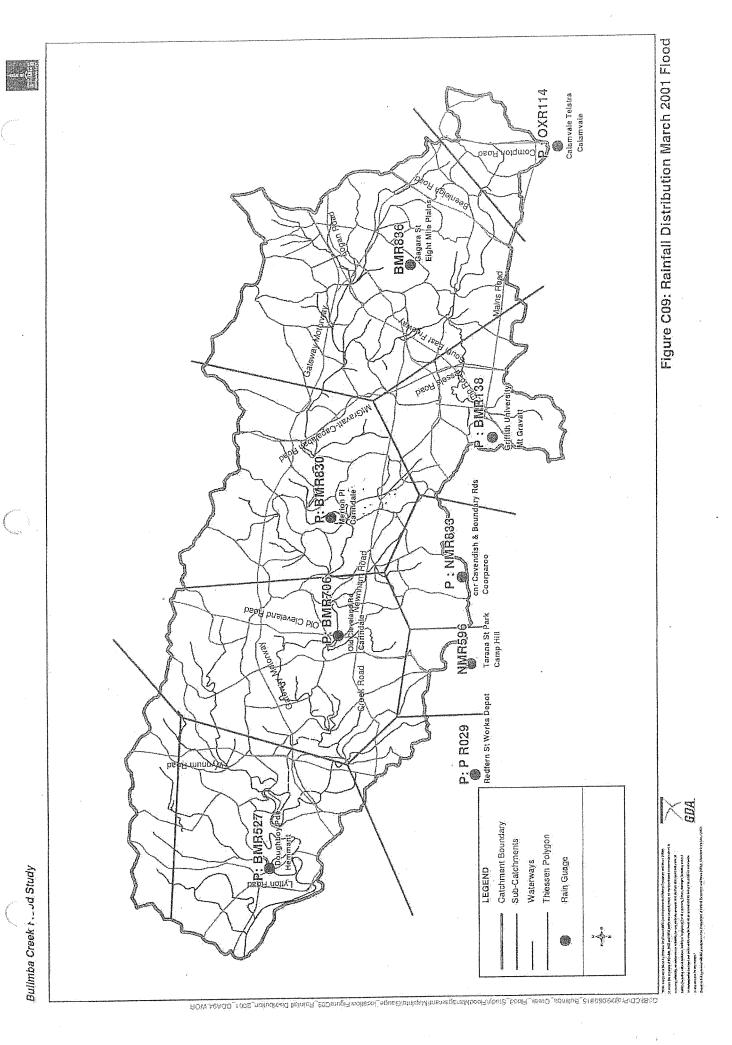
Bulimba Creek Flood Study

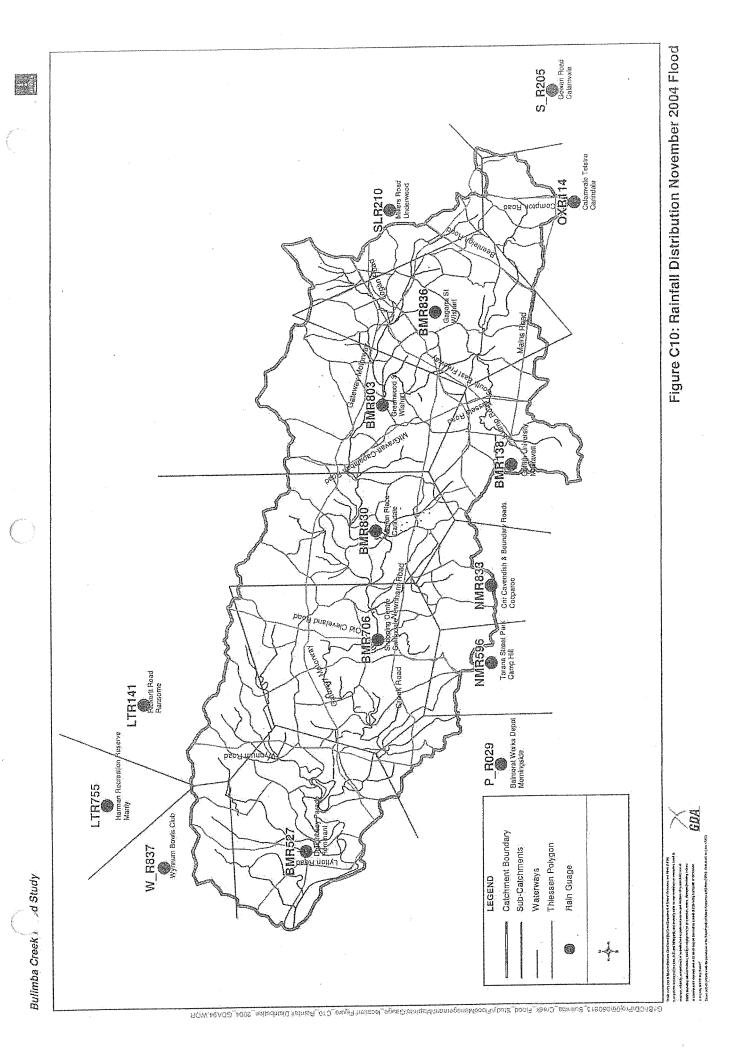


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Appendix D MIKE11 Flood Levels & Peak Water Level Plots for Calibration/Verification Events

D1 MIKE11 flood levels for calibration/verification events



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				Table I)1: MHG am	=	ge records co	mparison wi	h hydraulic	model result	s for calibra	ion and veri	fication ever	nts		-	-	***************************************	-
Calibrat	Calibration results		MIKEII		March 1992 event (17/09/1992)		January 1994 event (19/01/1994)	14 event (19	(01/1994)	May 1996	May 1996 event (3/05/1996)	7	March 20	March 2001 event (01/03/2001)	(03/2001)	Noven	November 2004 event (4/11/2004)	rent (4/11/2	7004)
MH	MHG No.	Location	41	MIKEII	Gauge		MIKEII	Gauge					MIKELI	Gauge	2	MIKE 11	Gauge	```	•
New ID	OI PIO		(m)	Cale.	(m AHD)	nun (m)	Cale.	6	Jun. (m)		(m. AHD)	m. (m)	Cale.	(m AHD)	Linn. (m)	Calc.	(nt AHD)	m).ima	Average
		Bulimba Creek Main Branch																-	
340		Beenleigh Road U/S	1800	46.19	46.48	-0.29	46.25	46.97		46.68	46.84	-0.16	47.03	47.20	-0.17	47.26	46.96	0.30	
330	2	Daw Road	2470	43,67	43.82	-0.15	43.66			43.9	44.05	-0.15	44.14	44.53		44.21	44.36	-0.15	
320	3	Kimmax Street	3765	36.8		1	36.68	37.16		37.22	37.36	-0.14	37.58	37.72	-0.14	37.67	37.75	-0.08	
310	4	Padstow Road U/S	4260	33.78		-0.08	33.67	1	1	34,09	34.50 *	0.41*	34.89	35,05	-0.16	34.81	35.15		
300	S	Bleasby Road	4780	32.59		0.30*	32.4	32.41	10.01	32.83	33.21		33.85	33.82#	0.03*	33.65	33.25		
067	٥	South East Freeway U.S	5005	20.2	0C*97		20.02	/0.07	0.00	C.22	/6.67	-0.07	57.05	1 8	1 000	30.98	30.30		
780	6A	Logan Koad D/S	2982	28.31	:	Marie	87	when	-	17.07	1	18	30.11	# 77.67	0.89	29.85	ı	-	
		Kayanagh Koad	7420	24.20		1 8	23.9			24.72	74.09	0.03	66.62	75.69	0.76	19.07			
260	oo.	Greenwood Street	8555	21.86	21.57	0.29	21.42	21.61	-0.19	22.16	22.41	-0.25	22.93	22,84#	0.16*	22.65	22.69	-0.04	
BMA804	c	Greenwood Street (BMA804)	8570	21.78			21.38	****	1	22.1	22.50		727.87	1 0.00	1 727	22.63	22.77	-0.14	
240	۲ ۲	Wit Gray-Capaigoa Nodo O/S	00201	19.42	12 17 #	#7"n	12.00	13 471 %	7 13*	10.3	31 71	7.0	14 07	10.19 7	01.0	5 2	14.91	07.0-	
BMA831	10	Merion Place (BM 4831)	13965	30.6	10.11	50 0-	0.04	10.08	P1 0	11.06	11 32	77.0-	11 97	11 00	-0 0-	11.53	11.58	-0.06	
230	111	Dewdrop Street	14845	9.42	9,32	0.10	8.96	8.79	0.17	9.76	10.06	-0.30	10.52	10.70#		10,10	10.19	-0.09	
220	1.2	Pine Mountain Road D/S	15600	8.35	7,86 *		7.9	7.42 *	0.48*	8.6	8.65	-0.05	9.64	#60'01	ı	10.6	8.69		
210	13	Winstanley Street D/S	17370	√6.36 >	6.13	0.23	5.88	5.89	-0.01	6.55	6.93		7.60	8.00#	1	96.9		I	
200	41	Old Cleveland Road U/S	17810	5.66	1	1	5.28	1	-	5.82	6.11	-0.29	6.85	7.01	-0.16	6.20	60.9	0.11	
BMA707		Old Cleveland Rd (BMA707)	17850	5.59	Acres	1.	5.13	4.87	0.26	5.74	90.9	=	6.78	6.83	-0.05	6.12	6.03	0.02	
150	15	Old Cleveland Road D/S	18025	5.26	5.08	0.18	4.81	4.88	-0.07	5.48	5.85	7	6.33	>6.76	1	5.68	5.7#	1	
180	16	Scrub Road Footbridge U/S	~19165	14.71		1	4.10		-	4.82	5.09	-0.27	5.65	5.77	-0.12	4.99	4.96	0.03	
170	17	Fursden Road	22305	3.6	T	1	3.00			3.6	3.81	-0.21	3.96	4.11	-0.15	3.51		***	161
160		Wood Avenue	23165	3.32	2.99		2.68	ui jam	1	3.3	3.49	-0.19	3.65	3.70	-0.05	3.14	**	1	
Closed	- 19	Wynnum Road U/S.1	~25515	2.93	2.81	0.12	2.34		1	2.92	3.41	7	3.23	3.54	Ŧ	2.73		-	
Closed	> 20 €	Wynnum Road U/S 2	25565	2.92	2.75	0.17	2.3	1	1	2.9	3.30		3.19	3.42	-0.23	2.66	1	-	
150	\21	Wynnum Road U/S 3	25865	2.86	2.66	0.20	2,28	-	*****	2.88	3.18	-0.30	3.13	3,26	-0.13	2.62	2.52	0.10	
Closed	23	Verdun Street	25915	2.75	2.58	0.17	2.23	1		2.75	2.98	-0.23	2.97			2.55	1		
140	22	Wynnum Road D/S	26015	2.71	2.63	0.08	2.2	W. Print	-	2.71	2.98	-0.27	2.92	3.10	-0.18	2.51	****	***************************************	
130	24 >	Murarrie Road U/S	26640	2.48	2,40	0.08	2.02		***	2.5	2,90		2.62	2.78	-0.16	2.31	1	***	
120	25	Murarrie Road D/S,	26780	2:47	2,36	0.11	1.98	-		2.42	2,60	-0.18	2.52	2.67	-0.15	2.30	,	-	
110	26	Fleming Road	31165	1,92	400	!	1.48	-	-	1.97	1.99	-0.02	1.98	1.82	0.16	1.69	1		
HMIA 528	-	Stream Gauge (BMA528)	34400	1.62		1. 1	1.05			1.04	1.75	-0.10	70,7	1.70	0.12	131		****	
	-	Average (m)				0.12			-0.11			-0.24			-0.09			0.03	4
		Bulimba Creek East Branch	-	-			- to the same of t	VIII.									***************************************		
430	3C	Underwood Road U/S	2700.	37.96	úrain.		36.94	-	44.00	37.7	37.89	-0.19	38.74	39.04	-0.30	38.74	39.11		
420	8B/E	Logan Road U/S	3725	31.97	.	-	31.57	a page	**	31.83	1		32.71	33.99#	* t-t-1	33.3	33.43	-0.13	-
410	8A	Miles Platting Road U/S	4600	28.42	28.31 *	0.11	28.05		,	28.6			29.51	29.78	-0.27	29.15	29.43	-0.28	
Closed	08 08	Gateway Arterial On-Ramp	2000	27.17	ļ		26.81	-	ı	27.35	27.42	-0.07	28.20		-	27.87	***************************************	***	
400	SF.	Daydream Place	5045	27			26.71		tuenn	27.2			27.96	27,95	0.01	27.65	27.6	0.05	
1	2000			0000		-0.11	17 05			72 43		-0.13	0000	2000	-0.19	67.07		-0.18	
Closed	BIMIUB		60	00.28	-	1	00.41	1	1	60.D4	1	1	00.30	00.77	c7'0-	00.00		-	
200	BM4A(B)	Mimosa-Parkway St US	2718	58.43	38.28	0.15	38,4	38.2	-0.20	38.42	38.37	0.05	39.40	40.37*	1.15*	38.93	38.38	0.76	
Rec	Recorded)	Recorded Maximum Height Gunge level (mAHD)	HD)					33 86 *	Recorded fly	do farral ob	rained min	to existing	ett enite he	Recorded flood lastel obtained mine to existing etracture hains in place				***************************************	
Sale Cale	Calculated	Calculated water level at this location (mAED)	(200		***************************************			130	Maximum F	Journal Gang	entition participants	d Peak floo	d level obta	Maximum Height Gauge overtonged Peak flood level obtained from debris mark	phris mark				
nier	Difference	Difference between recorded and calculated mea't flood lane (m)	year flood to	(m) Jour					Maximum	Joinht Gang	outdies o	J Dealt flow	d level cetir	Maximum Height Game agartomed Deak flowd level cetimored from nearby manner	pearly conce	ð.			
- Tarke	TOTAL CARC	Tools and and and and and and	year moon it	, vc. (111)					D.E.	ingin Oung	addays a a	1 (-4- / 47 m	1 1 1 1 1 1 1 1	marca nom	100 Eng	ca.			
									Dinetence	ופראפפוו זפרי	ממבות מחתי הם	lomaten vic	or reverse	Difference between recorded and calculated mod jevel is greater than soonni.	элчини.				

Table D2: MIKE11 Flood Levels for Calibration and Verification Events

Chainage	& AMTD	Calibrati	on events		Verification	events
MIKE-11 Chainage	AMTD (m)	Mar-92	Јап-94	Mar-01	May-96	Nov-04
to Nemies F	load load					MANUFACTURE CONTRACTOR OF THE STATE OF THE S
0	39900	60.48	60.64	60.77		60.97
65	39835	60.31	60.44	60.56	60.54	60.72
175	39725	59.97	60.08	60.21	60.17	60.36
270	39630	59.51	59.58	59.72	59.67	59.85
415	39485	58.42	58.60	58.93	58.84	59.14
560	39340	57.37	57.66	57.99	11	58.25
736	39164	56.59	56.82	57.14	l	<u> 57.51</u>
900	39000	55.64	55.89	56.42	√ 56.20 √	56.96
olum a processor constitutiva constitutiva constitutiva	-	Lacronia de la composition del				
0	38965	55.17	55.47	56.14	55.85	56.79
	L		55.45	\$6.13	55.83	56.77
	<u> </u>				} 	À
				***************************************	55.55	55.96
	1					55.51
			1			54.95
			1.0	<u> </u>	1	53.82
						3.74.74
W				·	F 52.20	53.61
385	13 3		<u> </u>	1	1	52.78
			<u> </u>	1		52.38
	3 44 - 32%	1"		<u> </u>		52.23
1 1 2				<u> </u>		52.23
1 1	I		I	<u> </u>	1	52.00
\800	38165	₹ a y a a van da a a a a			51./4	32.01
805	38160	Brandon Ro	ad downstre	am weir	***************************************	
825	38140	50.66	50.78	51.03		51.20
840	38125	50.42	50,55	50.84		51.02
890	38075	50.23	50.35	50.62	1	50.80
905	38060	50.16	50.27	50.53	<u> </u>	50.70
942	38023	50.03	50.13	50.37	1	50.53
960	38005	49.94	50.04	50.27	50.18	50.42
990	37975	49.78	49.88	50.11	50.01	50.26
1075	37890	49.40	49.48	49.74	49,63	49.92
1160	37805	49.10	49.18	49.49	49.36	49,68
1300	37665	48.65	48.76	49.10	48.96	49.30
L	37600	48.32	48.38	48.69	48.56	48.84
1545	37420	47.29	47.32	47.67	47.51	47.83
	37295	46.75	46.79	47.32	47.07	47.54
	37165	46.19	46.25	47.03	46.67	47.29
<u>L.</u>	37135	46.06	46.13	46.96	46.60	47.22
<u> </u>			1	and weir	<u> </u>	Name of Street, or other Persons of Street, or other Persons or other Pers
<u> </u>		1			46.16	46.47
			<u> </u>	1.00		46.14
1900	37065	45.57	45.55	45.88	45.72	46.07
	MIKE-11 Chainage to Nemies F 0 65 175 270 415 560 736 900 0 10 17 40 120 215 355 370 385 470 540 600 740 800 805 825 840 890 905 942 960 990 1075 1160 1300 1365	Chainage to Nemies Road 0 39900 65 39835 175 39725 270 39630 415 39485 560 39340 736 39164 900 39000 0 38965 10 38955 17 38948 40 38925 120 38845 215 38750 355 38610 370 38495 540 38425 600 38365 740 38225 800 38165 805 38160 825 38140 840 38125 890 38075 905 38060 942 38023 960 38005 990 37975 1075 37890 1160 37805 1300 37665 <t< td=""><td>MIKE-11 Chainage AMTD (m) Mar-92 to Nemies Road 0 39900 60.48 65 39835 60.31 175 39725 59.97 270 39630 59.51 415 39485 58.42 560 39340 57.37 736 39164 56.59 900 39000 55.64 0 38965 55.17 10 38955 55.15 17 38948 Nemies Road 40 38925 55.09 120 38845 54.84 215 38750 54.32 355 38610 53.16 370 38595 Brandon Ro 385 38580 52.93 470 38425 51.82 600 38365 51.66 740 38225 51.56 800 38165 51.53 805 38160 Brandon Ro</td><td> MIKE-II AMTD (m) Mar-92 Jan-94 </td><td> MIKE-11 AMTD (m) Mar-92 Jan-94 Mar-01 </td><td> MIKE-II AMTD (m) Mar-92 Jan-94 Mar-01 May-96 </td></t<>	MIKE-11 Chainage AMTD (m) Mar-92 to Nemies Road 0 39900 60.48 65 39835 60.31 175 39725 59.97 270 39630 59.51 415 39485 58.42 560 39340 57.37 736 39164 56.59 900 39000 55.64 0 38965 55.17 10 38955 55.15 17 38948 Nemies Road 40 38925 55.09 120 38845 54.84 215 38750 54.32 355 38610 53.16 370 38595 Brandon Ro 385 38580 52.93 470 38425 51.82 600 38365 51.66 740 38225 51.56 800 38165 51.53 805 38160 Brandon Ro	MIKE-II AMTD (m) Mar-92 Jan-94	MIKE-11 AMTD (m) Mar-92 Jan-94 Mar-01	MIKE-II AMTD (m) Mar-92 Jan-94 Mar-01 May-96

Branch name & Cross section	Chainage &	AMTD	Calibration	events	alangan mendedenga kelanga kelangan pengengan mendedelepan panah sebagai pengengan pendedelepan panah sebagai	Verification	events
ID	MIKE-11 Chainage	AMTD (m)	Mar-92	Jan-94	Mar-01	May-96	Nov-04
BM 194 copy	1960	37005	45.37	45.39	45.54	45.48	45.63
BM 192	2045	36920	44.74	44.76	45,15	44.87	45.26
BM 191 copy	2115	36850	44.59	44.60	45.13	44.74	45.24
St lawrence Fbridge	2117	36848	St Lawrenc	e Foot-Bridg	e and weir	Constitution of the Consti	
Bm 191	2125	36840	44.45	44.44	45.12	44,73	45.23
BM190	2255	36710	44.24	44.23	45.10	44.67	45.21
ВМ188-6 сору	2370	36595	44.14	44.12	45.07	44.63	45.18
Altandi St FB weir	2375	36590	Altandi str	eet foot bridg	e and weir	terresione de la companya de la comp	<u> </u>
	2380	36585	44.00	43.99	44,50	44.25	44.57
BM188-6 BM188-2 ALS	2470	36495	43.67	43.66	44.14	43.90 <	44.21
BM188-1 ALS	2500	36465	43.45	43.44	43.91	43,66	43.98
BM187	2670	36295	42.72	42.70	43.12	42.91	43.19
BM186	2785	36180	42.49	42.48	42.88	42.68	42.94
BM185	2985	35980	41.89	41.87	42.24	42.06	42.29
BM184	3165	35800	40.87	40.85	41.27	41.07	41.32
BM183	3295	35670	39.69	39.66	\40.22\	39.97	40.30
BM182	3435	35530	38.96	38.93	39.42	39.18	39.49
BM181	3625	35340	37.51	37.48	38.11	37.83	38.19
MHG-320	3.765	35200	∠36.80 \	36.68	37.58	37.22	37.67
BM180	3800	35165	36.66	36.51	37.50	37.11	37.60
BM179	(3960)	35005	35.86	35.73	36.62	36.19	36.73
Malbon_St_FB_weir	3965	35000	Malbon Str	eet foot brid	ge and weir		
ВМ179 сору	3970	34995	35.73	35.62	36.59	36.09	36.70
BM178	4150	34815	34.22	34.12	35.15	34.51	35.14
BM177-MHG310	4260	34705	33.78	33.67	34,89	34.09	34.81
BM177A	4320	34645	33.43	33.28	34.69	33.78	34.51
BM176-US	4385	34580	33.27	33.05	34.62	33.65	34.40
Padstow Rd	4390		Pastow Ros	id culverts at	id weir		
BM176 DS	4415	34550	33.26	33.05	34.53	33,64	34.34
BM 175	4460	34505	33.24	33.01	34.50	33,62	34.31
ВМ175-174	4515	34450	33.22	32.99	34.48	33.60	34.29
BM 174	4590	34375	33.15	32.92	34.41	33.53	34.22
BM174A	4700	34265	32.88	32.65	34.14	33.25	33.95
BM174B	4765	34200	32.67	32,46	33.89	32.99	33.70
BM173-MHG300	4780	34185	32.60	32.41	33.85	32.94	33.65
Blesby_Rd_FB_weir	4785	34180	Blesby Roa	d Foot bridg	e and weir		
	4790	34175	32.60	32.39	33.83	32.92	33.63
BM 173 copy BM172	4905	34060	32.24	32.04	33.49	32.56	33,28
BM171	4995	33970	31.85	31.63	33.16	32.19	32.93
BM170	5120	33845	31.16	30.91	32,62	31.49	32.31
	5285	33680	29.90	29.64	32.07	30.33	31.60
BM169 BM168	5405	33560	29.51	29.24	31.97	30.02	31.48
	5520	33445	29.28	29.01	31.90	29.81	31.39
BM167 BM 167 copy-MHG290	5615	33350	28.90	28.63	31.84	29.50	30.98
			1	freeway box	1		,l
South-east Freeway	5625	<u> </u>	Donen-cast.				

Branch name & Cross section	Chainage	& AMTD	Calibration	events	neraccours serves dans (C.C.C.C.C.C.C.C.C.C.C.C.C.C.C.C.C.C.C.	Verification	events
ID	MIKE-11 Chainage	AMTD (m)	Mar-92	Jan-94	Mar-01	May-96	Nov-04
BM 165 copy	5715	33250	28.67	28.33	30.92	29.30	30.65
BM165	5730	33235	28.65	28.31	30.92	29.28	30.64
SurveyXs-5	5785	33180	28.50	28,17	30.89	29.17	30.61
Logan Road	5790	33175	Logan road	culverts and	weir	hannes anno anno anno anno anno anno anno ann	
	5845	33120	28.47	28.16	30.22	28,91	29.96
SurveyXs-4 SurveyXs-3	5902	33063	28.41	28.10	30.20	28.86	29.93
SurveyXs-2	5918	33047	28.40	28.09	30.19	28.85	29.92
BM158 Xs-1	5935	33030	28.39	28.08	30.18	28.84	29.92
HEC2937-MHG280	5985	32980	28.31	28.00	30.11	28.77	29.85
BM157	6050	32915	28.15	27.83	29.98	28.60	29.71
BM156	6160	32805	27.73	27.35	29.45	28:20	29.14
	6240	32725	27.38	27.01	28.91	27.84	\ 28.67
BM155 BM154	6340	32625	26.99	26.60	28:49	27.44	28.23
BM153 ALS	6450	32515	26.58	26.12	28.13	27.04	27.86
BM151	6650	32315	26.21	25.77	27.71	26.64	27.43
BM149	6860	32105	25.84	25.41	27.34	26,28	27.06
BM148-BM147	6930	32035	25.64	25.21	27/15	26.06	26.86
	6935	32030	E	t Footbridge			Marca David Commence Complete Commence
Craig_St_FB_weir		32020	25.60	25.19	27.11	26.03	26.83
BM148 copy	6945	31980	25.54	25:13	27.07	25.97	26.78
BM148	6985	31780	24.99	24.63	26.68	25.46	26.37
BM146	7185	31545	24.26	23.90	25.95	24.73	25.61
BM144	7 420 7490	/31475	24.10	23.72	25.77	24.57	25.45
BM143	7600	31365	23,84	23.41	25.55	24.34	25.24
ALS-142	7,735	31230	23.45	22.96	25.21	23.97	24.88
BM141	7915	31050	22.86	22.39	24,30	23.25	24.01
BM139	7913	30980	22,66	22.20	24.03	23.02	23.75
BM138	8070	30895	22.61	22.13	23.96	22,96	23.68
BM137	8200	30765	22.42	21.94	23.74	22.77	23.47
BM136	8325	30640	22.29	21.82	23.54	22.61	23.27
BM135	8475	30490	22.05	21.61	23.22	22.35	22.97
BM134 MHG-260	8555	30410	21.82	21.42	22.93	22.10	22.69
	8570	30395	21.78	21.38	22.87	22.06	22.63
BM132 BM131	8780	30185	20.91	20.52	22.03	21.19	21.78
	8840	30125	20.62	20.14	21.86	20.94	21.59
BM130	8950	30015	20.35	19.86	21.63	20.68	21.35
BM129 BM127	9115	29850	19.82	19.31	21.16	20.17	20.87
	9215	29750	19.46	18.98	20,84	19.81	20.53
BM126	9365	29600	19.14	18.63	20.56	19.50	20.23
BM126a	9530	29435	18.88	18.31	20.37	19.28	20.03
BM126b BM122	9670	29295	18.63	18.02	20.14	19.03	19.79
	9765	29200	18.51	17.90	20.00	18.91	19.64
BM121	9890	29075	18.38	17.79	19.80	18.76	19.46
BM119	9920	29045	18.32	17.73	19.73	18.70	19.39
BM118	10100	28865	17.80	17.23	19.23	18.18	18.87
BM117	10205	28760	17.53	16.98	18.98	17.91	18.62
BM116	10203	28650	17,34	16.82	18.77	17.71	18.41
BM115	ากวาร	ا مرووم	L * (e - /]	1 10.02	L		

Branch name & Cross section	Chainage	& AMTD	Calibration	events		Verification	
ib	MIKE-11 Chainage	AMTD (m)	Mar-92	Jan-94	Mar-01	May-96	Nov-04
BM114	10400	28565	17.00	16.43	18.53	17:41	18.15
BM112	10510	28455	16.57	16.02	18.16	17.01	17.76
BM111-MHG250	10575	28390	16.42	15.85	18.03	16.90	17.63
BM110	10685	28280	16.29	15.72	17.92	16.73	17.51
Mt Gravatt Capalaba Road	10702	28263	Mt Gravatt	Capalaba Ro	oad bridge a	nd weir	
BM110 copy	10725	28240	16.15	15.61	17.57	16.55	17.21
ВМ108	10875	28090	15.88	15.39	17.24	16.25	16.88
BM107	10965	28000	15.65	15.17	16.98	/16.00	16.60
BM106	11095	27870	15.32	14.83	16.70	15.67	16.29
3M104	11255	27710	15.13	14.61	/16.57	15.50	16.13
BM102	11515	27450	14.89	14.27	16.41	15.28	₹ 15.96
BM101	11620	27345	14.83	14.19	16.35	15.23	15.90
BM100	11695	27270	14.75	14.12	16.25	15.14	15.80
BM99	11820	27145	14.48	13.86	15.95	14.87	15.51
BM98	11910	27055	14.24	13.66	15.66	14.61	15.23
BM97	12035	26930	13.94	\13.40	\15,36	14.30	14.92
ВМ97сору	12135	26830	1/3.81	13.26	<u>15.22</u>	14.17	14.78
Wecker Road bridge	12139	26826	Wecker Ro	d bridge and	l weir		and the second
ЗМ97сору	12155	26810	13.75	13.21	15.15	14.10	14.71
ВМ94	12215	26750	13:66	13.10	15.08	14.02	14.63
BM94-93-MHG240	12320	26645	3.50	12.90	14.96	13.88	14.50
BM93	12385	26580	13.34	12.68	14.85	13.73	14.38
ВМ90 сору	12505	26460	13.07	12.36	14.64	13.49	14.15
ВМ90 сору	12690	26275	12.84	12.05	14.45	13.27	13,95
BM88	12820	26145	12.72	11.93	14.30	13.14	13.81
BM87	13140	25825	12.38	11.59	13.89	12.78	13.42
BM84	13440	25525	11.70	10.92	13.29	12.14	12.80
BM83	13530	25435	11.58	10.80	13.16	12.02	12.67
BM81	13670	25295	11,45	10.69	12.95	11.86	12.49
BM80	13765	25200	11.34	10.58	12.79	11.74	12.34
BM78	13910	25055	10.96	10.22	12.36	11.35	11.93
ВМ78 сору	13965	25000	10.60	9.94	11.97	10.96	11.52
BM77	14115	24850	10.32	9.76	11.55	10.63	11.12
BM76	14360	24605	10.19	9.64	11.43	10.49	10.99
BM75	14460	24505	10.14	9.59	11.37	10.44	10.93
BM74-BM72	14625	24340	10.01	9,47	11.21	10.31	10.78
BM72	14785	24180	9.59	9.12	10.65	9.84	10.24
BM71-MHG230	14845	24120	9.42	8.96	10.52	9.76	10.10
BM70	14960	24005	9.30	8.84	10.39	9.55	9.96
BM69	15160	23805	9.06	8.62	10.15	9.30	9.70
BM67	15340	23625	8.70	8.27	9.89	8.95	9.37
BM66	15460	23505	8.57	8.15	9.83	8.84	9.28
ВМ66 сору	15540	23425	8.51	8.08	9.79	8.78	9.22
Pine mountain_Rd	15555	1	Pine Mount	tain Road br	idge and wei	r	
BM65	15570	23395	8.42	8,00	9.70	8.68	9.12
BM64 -MHG250	15600	23365	8.35	7.92	9.64	8.62	9.01

Branch name & Cross section	Chainage	& AMTD	Calibration	events	***************************************	Verification	events
10	MIKE-11 Chainage	AMTD (m)	Mar-92	Jan-94	Mar-01	May-96	Nov-04
BM64	15660	23305	8,25	7.77	9.59	8,54	9.01
BM63	15790	23175	8.17	7.64	9.55	8.47	8.96
BM62	15965	23000	8.10	7.54	9.50	8:41	8.90
BM61	16015	22950	8.09	7.52	9.50	8.40	8.89
BM60	16190	22775	8.02	7.45	9.45	8.33	8.83
BM59	16390	22575	7.83	7.23	9.31	8.15	8.66
BM59_mod	16435	22530	7.76	7.17	9.24	8.08	8.59
Meadow St FB weir	16445	22520	Meadow Str	eet Footbrid	ge and weir	and the same of th	\
Bm55-mod	16455	22510	7.75	7.15	9.22	8:06	8.57
BM57-mod	16680	22285	7.44	6.87	8.89	7.74	8.23
BM56	16785	22180	7.28	6.72	8.69\\	7,56	8.03
Bm55-mod	17080	21885	6.80	6.28	8.14	7.04	7.47
BM55-54	17240	21725	6.54	6.03	₹7.87.~	6.78\	7.20
BM54	17300	21665	6.48	5.97	7.80	6.71	7.13
CD10	17325	21640	6.43	5:93	7.72	6.65	7.06
Winstaly_St_weir	17338	21627	ι	treet Footbr	idge and wei	ľI	
	17355	21610	\6.39	5.92	7,62,/	6.59	6.97
CD09	17540	21425	6.11	5.68	7.30	6.29	6.65
BM52	17765	21200	∠5,75	5.31	6.95	5.92	6.29
CD07 BM50-49-BMA707	17850	21115	5.59	5.13	6.78	5.75	6.12
CD06	(17920	21045	5,39	4.92	6.46	5.55	5.82
	17935	21030		nd Road brid		<u> </u>	
Old_Cleveland_Rd	17960	21005	5.39	4.90	6.38	5.54	5.80
CD05	18025	20940	5.26	4.72	6.33	5.40	5.68
CD04	18065	20900	5.20	4.63	6.29	5.34	5.62
BM47-mod	18110	20855	5.17	4.58	6.26	5.31	5.58.
BM46-mod	18320	20645	5.05	4:45	6.10	5.18	5.43
CD02	18495	20470	4.96	4.35	5.98	5.08	5.31
BM44 -mod	18690	20275	4.87	4.27	5.86	4.99	5.20
BM43-mod BM42-mod	18995	19970	4.77	4.16	5,72	4.88	5.06
BM42-mod-MHG180	19165	19800	4.72	4.10	5.64	4.82	4.99
	19195	19770	4.70	4.08	5,62	4.81	4.97
BM41 copy	19205	19760	1	Footbridge:		<u> </u>	
Scrub_Rd_FB_weir			4.69	4.08	5.62	4.80	4.96
BM41-mod	19215	19750		4.02	5.54	4.74	4.89
BM5GHD	19375	19590 19325	4.63 4.44	3.85	5,24	4.53	4.63
Bm5GHD	19640	18915	4,44	3.66	4.93	4.32	4,36
BM7GHD	20050	18705	4.24	3.60	4.82	4,25	4.27
BM8GHD copy	20260			ds Road bric		Andrews and the second	L
Meadowlands_st_weir	20270	18695	<u> </u>		, , , , , , , , , , , , , , , , , , , 	110	4.25
Bm8GHD	20290	18675	4.16	3.55	4.75	4.18 4.14	4.23
BM9GHD	20510	18455	4.12	3.52	4.69		4.20
BM37	20850	18115	4.03	3.43	4.56	4.05	3.99
BM17GHD	21090	17875	3.96	3.35	4.47	3.97	
BM18GHD	21555	17410	3.83	3.21	4.30	3.83	3.82
BM18GHDcopy	21875	17090	3,72	3.09	4.14	3.71	3.67
Preston Rd_FB_weir	21885	17080	Preston Ros	ıd footbrideg	e and weir		

Branch name & Cross section	Chainage	& AMTD	Calibration	events	nen en	Verification events		
ID	MIKE-11 Chainage	AMTD (m)	Mar-92	Jan-94	Mar-01	Мау-9б	Nov-04	
BM19_GHD	21895	17070	3.71	3.09	4.14	3.70	3.66	
MHG-170	22305	16660	3.59	2.99	3.96	3.58	3.49	
ВМ23СНО	22775	16190	3.45	2.85	3.78	3.44	3.31	
MHG-160	23165	15800	3.32	2.67	3.64	3.30	3.11	
BM10GHD	23285	15680	3.31	2.67	3.63	3.29	3.11	
BM11GHD	23600	15365	3.28	2.65	3.60	3.26	3.07	
ALS-23900	23900	15065	3.26	2.62	3.57	3.24	3.05	
BM13GHD-mod	24595	14370	3.18.	2.55	3.49	3.17	2.96	
BM13GHD	24890	14075	3.10	2.49	3.40	3.09	2.88	
MHG19-old	25515	13450	2.93	2.34	3.20	2.92	2.69	
MHG20-old	25565	13400	2.92	2.33	3.19	2.91	2.68	
BM26-MHG150	25865	13100	2.86	2.28	3.15	2.87	2.62	
	25885		Wynnum R	oad bridge a	nd weir	1	Laire and the same of the same	
Wynnum_Rd_weir BM 26 copy	25905	13060	2.75	2.22	2.97	2.75	2.53	
вм 26 сору MHG-140	26015	12950	2.71	2.20	2.92	2.71	2.48	
	26145	12820	2.65	2.15	2.84	2.65	2.42	
BM24	26365	12600	2.56	2.10	2.73	2.57	2.34	
BM23	26620	12345	2.47	2.04	2.61	2.48	2.25	
BM22	26710	12255	2.45	2,02	2.59	2.46	2.22	
BM22 copy	L	12235		oad bridge a		1	<u>L</u>	
Murarrie Rd weir	26730 26750	12215	2.39	2.01	2.56	2.45	2.23	
BM22 copy	26780	12185	2:37	1.97	2.52	2.42	2.19	
MHG-120	26940	12025	2.33	1.95	2.48	2,38	2.15	
BM22 copy	26990	11975	2.31	1.93	2.45	2.35	2.12	
BM42AGHD copy	26990,2	11665	2.26	1.90	2.38	2.30	2.08	
BM42AGHD copy	1	11610	2.25	1.90	2.38	2.29	2.07	
BM42AGHD	27355	11210	2.11	1.80	2.20	2,16	1.92	
BM43AGHD	27755	10940	2.07	1,77	2.16	2.13	1.88	
BM44AGHD	28025	10150	2.04	1.70	2.12	2.10	1,81	
BM44BGHD	28815	9890	2.04	1.67	2.13	2.10	1.79	
BM43BGHD	29075		2.04	1.62	2.11	2.09	1.74	
BM43CGHD	29730	9235 8330	1,96	1.51	2.04	2.03	1,63	
BM43CGHD	30635	7365	1.88	1.42	1.93	1.94	1.52	
BM45GHD	31600	6855	1.79	1.35	1.83	1.84	1.41	
BM46CGHD-MHG110	32110	6610	1.77	1.30	1.80	1.82	1.34	
BM46BGHD	32355	1	1.71	1,22	1.71	1.74	1.21	
BM46AGHD	33330	5635 4665	1.71	1.06	1.59	1.66	0.92	
BM52 GHD copy	34300	<u>t</u>	1.65	1.03	1.55	1.65	0.92	
BM52 GHD copy	34490	4475	1	Road bridge a	<u> </u>	L	L	
Cleveland Rail bridge	34500	4465	1		-	1.60	0.92	
BM52 GHD	34510	4455	1.50	0.98	1.50	1	1	
BM52 GHD copy	34700	4265	1.42	0.93	1.49	1.57	0.91	
ВМ7	35260	3705	1.36	0.91	1.48	1.54	0.90	
BM6	35670	3295	1.29	0.90	1.48	1.50	0.90	
Lytton Road	35680	3285		d bridge and	eller er e		6.30	
ВМ6 сору	35690	3275	1.29	0.90	1,47	1.47	0.90	
BM48	35785	3180	1.29	0.90	1.47	1.46	0.90	
	1 5.000	2595	1,27	0.89	1.47	1.44	0.89	
Bm4	36370	2000	1.27.	0.89	1.46	1,42	0.89	

D-6

Chainage	& AMTD	Calibration events			Verification events		
MIKE-11 Chainage	AMTD (m)	Mar-92	Jan-94	Mar-01	May-96	Nov-04	
37465	1500	1.26	0.88	1.46	1.41	0.88	
38070	895	1.25	0.88	1.45	1.39	0.88	
38610	355	1.25	0.87	1.45	1.39	0.87	
38965	0	1.25	0.87	1.45	1.39	0.87	
		L,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	<u> </u>	The state of the s			
0	6280	55.31	55.39	55.75	55.47	55.74	
60	6220	55.24	55.31	55.67	55.39	55.66	
170	6110	54.26	54.32	54.62	54.40	54.61	
	6030	53.32	53.39	53.69	53.46	53.67	
	5892	52.95	52.73	53,20	52.84	> 53.16	
	5755	52.01	51.78	52.24	51.92	52,18	
	5668	51.08	50.90	51.26	/51,01	51.21	
660	5620	50.42	50.28	50.56	50.36	₹ 50.52	
708	5572	50.13	50.01	50,26	50.08	\$0.21	
755	5525	49.98	49.80	50.16	49.90	50.11/	
799	5481	49.96	49.78	₹ 50.14	49.88	50.10	
	5465	49.95	49.76	\50.13\	49,86	50.08	
		Beenleigh R	oad culverts	and weir			
	5445		49.25	49.97	49.43	49.87	
		♣ + 5 d + 1 d d	49.26	49.97	49.45	49.87	
		No. 12	49.26	49.97	49.45	49.87	
A Comment of the Comm	1		ast Rail bride	ge culverts a	nd weir		
	5428		49.09	49.78	49.09	49.64	
V :		l	48.67	49.77	48.98	49.62	
	 	£	oad pipe cul	vert and wei	<u>.l.</u>	<u> </u>	
	5334		-		<u> </u>	48.37	
	<u> </u>			<u> </u>		48.38	
	l	<u> </u>	<u> </u>			48.36	
				Ē	1	48.36	
L	1	f		f	<u> </u>	48.34	
	1	·		<u> </u>	<u> </u>	48.30	
<u> </u>	<u> </u>	<u> </u>		<u> </u>	47.89	48.26	
			47.61	48.31	47.86	48.22	
	<u> </u>		<u> </u>	48.28	47.83	48.19	
1	1		47.56	48.25	47.80	48.17	
<u> </u>		47.95	47.54	48.22	47.78	48.14	
<u> </u>	<u> </u>	47.92	47.51	48.19	47.75	48.11	
t		47.88	47.47	48.15	47.72	48.07	
<u> </u>	1	47.82	47.43	48.09	47.66	48.01	
I	<u> </u>	47.68	47.32	47.93	47.53	47.85	
<u> </u>	5069	47.41	47.01	47.69	47.24	47.60	
1	5049	47.29	46.91	47.57	47.13	47,47	
<u> </u>	5029	47.15	46.79	47.41	46.99	47.32	
	5009	46.95	46.64	47.19	46.81	47.10	
<u> </u>	<u> </u>	46.73	46.44	46.95	46.60	46.87	
		46,57	46.26	46.80	46.43	46.72	
1331	4949	46,49	46.19	46.71	46.35	46.64	
						.	
1341	4939	46.48	46.17	46.70	46.34	46.63	
	MIKE-11 Chainage 37465 38070 38610 38965 0 60 170 250 388 525 612 660 708 755 799 815 820 835 840 844 845 852 875 876 946 956 978 981 991 1011 1031 1051 1071 1091 1111 1131 1151 1171 1191 1211 1231 1251 1271 1291 1311	Chainage (m) 37465 1500 38070 895 38610 355 38965 0 0 6280 60 6220 170 6110 250 6030 388 5892 525 5755 612 5668 660 5620 708 5572 755 5525 799 5481 815 5465 820 835 835 5445 840 5440 844 5436 876 5428 875 5405 876 5324 978 5302 981 5299 991 5289 1011 5269 1031 5249 1051 5229 1071 5209 1091 5189 1111 5169	MIKE-11 Chainage (m) AMTD (m) Mar-92 (m) 37465 1500 1.26 38070 895 1.25 38610 355 1.25 38965 0 1.25 0 6280 55.31 60 6220 55.24 170 6110 54.26 250 6030 53.32 388 5892 52.95 525 5755 52.01 612 5668 51.08 660 5620 50.42 708 5572 50.13 755 5525 49.98 799 5481 49.96 815 5465 49.95 820 Beenleigh R 835 5445 49.61 844 5436 49.61 844 5436 49.61 845 Beenleigh R 852 5428 49.24 875 5405 49.22	MIKE-11 Chainage (m) AMTD (m) Mar-92 Jan-94 (m) 37465 1500 1.26 0.88 38070 895 1.25 0.88 38610 355 1.25 0.87 38965 0 1.25 0.87 0 6280 55.31 55.39 60 6220 55.24 55.31 170 6110 54.26 54.32 250 6030 53.32 53.39 388 5892 52.95 52.73 525 5755 52.01 51.78 612 5668 51.08 50.90 660 5620 50.42 50.28 708 5572 50.13 50.01 755 5525 49.98 49.80 799 5481 49.96 49.78 815 5465 49.95 49.76 820 Beènleigh Road eûlverts 835 5445 49.58 49.25	MIKE-11 Chainage AMTD (m) Mar-92 (m) Jan-94 (m) Mar-01 37465 1500 1.26 0.88 1.46 38070 895 1.25 0.88 1.45 38610 355 1.25 0.87 1.45 38965 0 1.25 0.87 1.45 60 6220 55.31 55.39 55.75 60 6220 55.24 55.31 55.67 170 6110 54.26 54.32 54.62 250 6030 53.32 53.39 53.69 388 5892 52.95 52.73 53.20 525 5755 52.01 51.78 52.24 612 5668 51.08 50.90 51.26 660 5620 50.42 50.28 50.56 708 5572 49.98 49.80 50.16 799 5481 49.96 49.78 50.14 815 5465 <t< td=""><td>MIKE-11 Chainage (m) AMTD Chainage (m) Mar-92 Jan-94 Mar-01 May-96 37465 1500 1.26 0.88 1.46 1.41 38070 895 1.25 0.87 1.45 1.39 38965 0 1.25 0.87 1.45 1.39 38965 0 1.25 0.87 1.45 1.39 0 6280 55.31 55.39 55.75 55.47 60 6220 55.24 55.31 55.67 55.39 170 6110 54.26 54.32 54.62 54.40 250 6030 53.32 53.39 53.69 53.46 288 5892 52.95 52.73 53.20 53.49 612 5668 51.08 50.90 51.26 51.01 660 5620 50.42 50.28 50.56 50.36 708 5572 50.13 50.01 50.26 50.08 799<!--</td--></td></t<>	MIKE-11 Chainage (m) AMTD Chainage (m) Mar-92 Jan-94 Mar-01 May-96 37465 1500 1.26 0.88 1.46 1.41 38070 895 1.25 0.87 1.45 1.39 38965 0 1.25 0.87 1.45 1.39 38965 0 1.25 0.87 1.45 1.39 0 6280 55.31 55.39 55.75 55.47 60 6220 55.24 55.31 55.67 55.39 170 6110 54.26 54.32 54.62 54.40 250 6030 53.32 53.39 53.69 53.46 288 5892 52.95 52.73 53.20 53.49 612 5668 51.08 50.90 51.26 51.01 660 5620 50.42 50.28 50.56 50.36 708 5572 50.13 50.01 50.26 50.08 799 </td	

Branch name & Cross section ID	Chainage	& AMTD	Calibration events		Verification events		
	MIKE-11 Chainage	AMTD (m)	Mar-92	Jan-94	Mar-01	May-96	Nov-04
BE272	1498	4782	45,91	45,67	46.08	45.82	46.03
BE272	1565	4715	45.44	45.22	45.62	45.34	45.56
BE271	1600	4680	45.28	45.06	45.48	45.18	45.41
BE270	1730	4550	44.52	44.15	44.81	44.35	44.69
BE269	1915	4365	43.79	43.44	44.30	43.73	44.17
BE268	2020	4260	43.21	42.78	43.77	43.14	43.60
BE267	2145	4135	42.55	42.19	43.02	42.49	42.87
BE266	2245	4035	41.87	41.64	42.21	41.84	42.12
BE265	2410	3870	40.65	40.42	40.94	40.60	40.87
BE264	2500	3780	40.08	39.82	40.33 🤇	40.04 \	40.28
BE263	2605	3675	38.89	38.44	39.28	38.85	39.16
BE262	2765	3515	37.66	36.85	3,8:53	37.31	₹ 37.95
Underwood Road culverts	2767	3513	Underwood	Road culver	ts and weir	\	
BE261	2785	3495	37.59	3,6.83	38.35	37.31	37.95
BE259	2990	3290	36.89	36.24	37.37	36.65	37.19
BE258	3200	3080	35.61	34.97	36.12	35.42	35.92
BE257	3320	2960	34.92	34.30	35.35	34.75	35.17
Gateway Mway culverts	3330		Gateway M	otorway cul	verts and wei	r	
BE257 copy	3425	2855	ŕ34, <u>9</u> 1	34.27	35.34	34.72	35.16
BE256	3490	2790 <	34.60	34.02	35.02	34.42	34.85
BE255	3670	2610	32.98	32.55	33.39	32.85	33.20
BE255 copy	3695	2585	32.63	32.22	33.08	32.50	32.85
BE255 -mod	3725	2555	31.97	31.57	32.75	31.84	32.35
BE254 copy	3735	2545	31.97	31.36	32.75	31.82	32.35
BE254	3745	2535	31.97	31.32	32.75	31.80	32.35
Logan Road culvert	3748	2532	Logan Road	l culvert and	l weir	S. 11 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
BE253	3785	2495	31.26	30.83	31.94	31.23	31.63
interpolated	3810	2470	31.26	30.82	31.93	31.23	31.62
BE251	3925	2392	31.17	30.76	31.87	31.15	31.55
Be250	4020	2392	30.87	30.43	31.70	30.86	31.35
BE249	4110	2170	30.30	29.84	31.51	30.39	31.14
BE248	4230	2050	30.02	29.60	31:44	30.20	31.07
BE247	4300	1980	29.96	29.51	31.43	30.16	31.06
BE247 copy	4360	1920	29.67	29.36	30.52	29.81	30.28
BE246	4419	1861	29.36	28.97	30.30	29.52	30.04
BE246A-ALS	4507	1773	28.89	28.49	29.88	29.07	29,61
BCFS 4612	4602	1678	28.42	28.05	29.51	28.59	29.15
Eight mile plains bridge	4608	Eight Mile	Plains buswa	y access roa	d bridge and	weir	
Copy BCFS 4612	4638	1642	28.09	27.68	29.32	28.30	28.97
BE244	4656	1624	28.03	27.63	29.24	28.25	28.86
Miles Platting Road bridge a	4660	1	Miles Platti		dge and weir	4660	
	4695	1585	27.99	27.61	29.12	28.19	28.77
BCFS 4665	4730	1550	27.85	27.50	28.82	28.03	28.52
BCFS 4685	4750	1530	27.84	27.48	28.84	28.02	28.53
BCFS 4705 BE241	4870	1470	27.55	27.21	28.57	27.73	28.24
BE241 BE240	4980	1300	27.23	26.86	28.32	27.42	27.97
	5010	1270		framp bridg			<u></u>
Gateway offramp BE239	5050	1230	27.02	26.71	27.95	27.18	27.64

Branch name & Cross section	Chainage	& AMTD	Calibration	events	entrana anno anno anno anno anno anno anno	Verification Events		
ID	MIKE-11 Chainage	AMTD (m)	Mar-92	Jan-94	Mar-01	May-96	Nov-04	
BE238	5175	1105	26.74	26.44	27.64	26.90	27.35	
BE236	5330	950	25.96	25.62	26.98	26.16	26.67	
BE235	5470	810	24.93	24.47	26.30	25,25	25,92	
BE232	5712	568	24.16	23.76	25.41	24.43	25.04	
BE231	5810	470	23.90	23.53	25.13	24.17	24.77	
BE230	5895	385	23.56	23.22	24.78	23.82	24.44	
BE229	5975	305	23.17	22.76	24.47	23,47	24.15	
BE228	6055	225	22.92	22.43	24.26	23.24	23,95	
BE227	6135	145	22.75	22.24	24.10	23.08	23,80	
BE227 .	6280	0	22.61	22.13	23.95	ر 22.96 سر	· 23,67	
Tributary A								
ALS1-copy	0		51.24	51.48	52.30	51.71	52.29	
ALS1-copy	100		51.09	51.30	52.10	51.52	₹52.08	
ALS1	320		50.33	50,48	51:15	50.64	51.13	
ALS2	600		45.70	45.96	46.87	46.27	46.77	
BE-1060	950		43.79	44.13	44.82	44.37	44,79	
BE-1040	1400	JAN PROPERTY.	40.75	40.82	41.24	40.98	41.13	
BE-1030	1770		36.80	36.88	37.63	37.13	37.60	
BE-1020	2070		34.15	34.31	35.49	34.59	35.37	
School Road	2072		School Road	l to Freeway	culvertsa no	weir		
CSI-1	2125		>34.11	34.26	35.18	34.51	35.10	
BE-1010	2235	1:1	33.59	33.74	34.71	33,99	34.61	
BE-1005-ALS	2535		31.67	31.69	32.91	32.03	32.78	
Freeway offramp	2545		Freeway of	ramp culver	ts and weir	Annual State of the State of th	žauciae die de la company	
BE-1005-ALS	2555	/	31.63	31.65	32.76	31.98	32.65	
BE1005-ALS	2735	<u> </u>	30.77	30.77	31.98	31.08	31.80	
	2765	<u> </u>	30.14	29,84	31.80	30,45	31.48	
BE1000	2702			otorway Cul	verts and we	ir	E-proposition of the second	
Gateway Mway	2025		30.12	29.80	31.70	30.41	31.39	
BE1000 modified	2935		30.12	29.57	31.46	30.20	31.10	
BE1000 modified	3015		29,99	29.56	31.43	30.18	31.07	
BE1000 modified	3021		29,99	27.30	71.17	33		
Tributary Al						40.55	50:02	
A1-1050	0		49.22	49.42	50.04	49.58	49.16	
A1-1050	280		48,61	48.72	49.18	48.84	49.16	
ALS-I	500		44.24	44.33	44.74	44.44	41.16	
ALS-2	720		40.77	40.84	41.26	40.99	41.13	
ALS-3	750		40.75	40.82	41.24	40.30	11.17	
Tributary A2			44.64	44.69	44.99	44.77	45.00	
	0		44.04	44.09	44.62	44.44	44.63	
SMP-1	80	 	44.36	40.02	40.39	40.13	40,30	
SMP-2	475	<u> </u>	1	38.44	38.79	38.55	38.67	
SMP-3	690		38.36 34.06	34.22	35.14	34.45	35.04	
SMP-4	1035		1	34.22	35.13	34.45	35.04	
SMP-5	1042	1	34.05	34.41	23.13	1 27:72	1 22.03	

Branch name & Cross section ID	Chainage	& AMTD	Calibration	events	Verification event		events
	MIKE-11 Chainage	AMTD (m)	Mar-92	Jan-94	Mar-01	May-96	Nov-04
Tributary B	4 - 4 - 12 - 12 - 12 - 1		diameter and the second				w.co.c.
BE2030	1000		35.61	35.78	36.31	35.93	36.22
BE2030	1055		34.50	34.69	35.36	34.87	35.25
Dance Court 1	1062		Dance Cour	t culvert and	weir		
ВЕ2030 сору	1075		34.03	34.23	34.85	34.42	34.78
BE2020	1215		33.85	34.00	34.54	34.17	34.48
BE2020 copy	1340		32.87	33.00	33.60	33,20	33.44
Interpolated	1360		32.71	32.88	33.52	33.10	33.48
Logan Road culverts	1361		Logan Road	l culverts and	l weir		
BE2010	1394	<u> </u>	32.56	32.78	33.35	33.03	33.24
BE2000	1432		31.23	30.85	31.91 A	31.23	31.59
BE2001	1492		31.22	√ 30.81 🛝	31.90	31.20	31.59
Tributary C	******************************	<u> </u>			\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \		<i>"</i>
BE-3050	0		48.93	49.01	∖49.24∖	49.08	49.20
BE-3050	10		48.89	48.95	49.20	49.03	49.14
BE-3040	390		46.49	46.56	46.93	46.65	46.85
BE-3030	545_		45.16	45.31	45.64	45.43	45.58
BE-3020	665		44.41	44.16	44.57	44.26	44.48
BE-3010	810	1.1.	42.75	42.46	42.92	42.60	42.83
BE3000	/1000 /		39.29	39.05	39.45	39:17	39.36
BE-3000 copy	1005		38.50	38.50	38.77	38.50	38.50
Gateway culvert	1008	7 25	Gateway Pi	pe culvert an	d weir		
BE3000 copy	1100		38.0	37.3	38.7	37.7	38.4
ALS-C1	1110		38.0	37.2	38.7	37.7	38.4
ALS-C2	1120		38.0	37.2	38.7	37.7	38.4
Tributary B1							
ALS-B1	1000		32.71	<i>32.8</i> 9	33.52	33.10	33.40
ALS-B2	1002		32.58	32.78	33.41	3.01	33.30
ALS-B3	1020		31.98	31.56	32.76	31.86	32.34
ALS-B4	1055		31.98	31.54	32.74	31.85	32.34
ALS-B5	1140		31.98	31.53	32.68	31.83	32.32
	1145	Y N' Y	31.98	31.53	32.68	31.83	32.32
Padstow Branch							
BM177	0		34.22	34.12	35.15	34.51	35.14
BM177	32		34.16	34.07	35.13	34.46	35.12
BM177-176ALS	105		33.86	33.76	35,08	34.25	35.05
BM176-US-ALS	175		33.51	33.30	35.05	34.10	35.01
Padstow Road at 177	177		Padstow Re	oad culverts a	ind weir		
BM176-DS-ALS	205	_	33.41	33.23	34.50	33.77	34.34
BM175	258		33.37	33.18	34.48	33.73	34.32
BM175-174ALS	325		33,27	33.05	34.46	33.64	34.28
BM174	352		33.22	32,99	34.45	33.60	34.27
BM175	375		33.20	32.97	34.44	33.57	34.26

Branch name & Cross section ID	Chainage	Chainage & AMTD		Calibration events		Verification	
	MIKE-11 Chainage	AMTD (m)	Mar-92	Jan-94	Mar-01	May-96	Nov-04
Garden City	······································						***************************************
BM169	5280		29.93	29.67	32.12	30.35	31.65
BM169	5285		29.92	29.67	32.12	30.35	31.64
BM168	5405		29.77	29.53	32,03	30.18	31.52
BM167	5510		29.42	29.16	31.95	29.88	31.43
ВМ167 сору	5615		29.08	28.72	31.92	29.66	31.39
ВМ165 сору	5615		29.08	28,72	31.92	29.66	31.39
BM165 copy	5715		28.80	28.52	30.92	29.25	30.66
Bm165	5730		28.77	28,46	30.92	29.23	30.65
XS5-logan-survey	5785		28.51	28.16	30.87	29.02	30.61
XS4-logan-survey	5850		28.43	28.12	30,26	28.88 \	29.96
XS4 copy	5935		28.39	28.08	30.18	28.84	29.91
XS4 copy	5938		28.39	28.08	30.18	28.84	29.91
Mimosa Creek							
Mi 40 Hecras	0		54.48	54.57	55.30	54,46	<u> </u>
Mi 40 Hecras	5		54.46	54.55	\ 55.27\	54,45	55.07
Mi 40a	96	and the second	54.06	54.12	54.76	54.06	54.58
Mi39	200		53.38	53.38	54.08	53.34	53.88
MI38	330		52.28	52.31	53.23	52.23	52.98
Mi37	484	\\-	50.98	50.99	51.84	50.96	51.63
Mi36	506		50.77	50.78	51.57	50.75	51.35
Mi35	558	7 7	50.36	50.39	51.25	50.34	50.98
Mi34	660	1 1	> 49.69	49.73	50,58	49.66	50.36
Mi33	696		49.46	49.51	50.41	49.43	50.18
Mi32	811	/	48.85	48.87	50.04	48.84	49.77
Mi31	952		48.22	48.21	49.41	48.20	49.08
Мі31-сору	1037		47.76	47.76	48.90	47.74	48.49
Mi29	1186		46.66	46.66	47.75	46.64	47.46
Mi28	1302		45.95	45.91	47.22	45.93	46.90
Mi27	1322		45.79	45.73	47.14	45.77	46.82
Mi26	1366		45.66	45.60	47.03	45,65	46.72
Mi25	1439		45.45	45.39	46.80	45.44	46.51
Mi24	1549		44.70	44.65	46.16	44.69	45.90
Mi23	1588	ja sa 1960 na nambuu Nga 1901 na na	44.51	44.47	46.03	44.50	45.77
Mi22	1719		43.94	43.90	45.46	43.92	45.24
Mi21-2	1738		43.77	43.74	45.36	43.76	45.09
Nagel st bridge	1739		Nagel st brid	lge and weir		***************************************	
Mi21-1	1752	***************************************	43.67	43.63	45.30	43.65	44.98
Mi20	1762		43.57	43.52	45.24	43.55	44.89
Mi19	1882		42.95	42.91	44.86	42,92	44.29
Mi19-4	1892		42,92	42.88	44.85	42.90	44.27
Pacific Mway			Pacific Moto	<u></u>	L		***************************************
Mi19-1	1964		42.45	42.41	43.72	42,42	43.39
VIII9-1 VIII8	2023		42.45	42.12	43.28	42.13	42.98
Mi17:	2023		41.72	41.68	42.86	41.70	42.54
vii1/	2133		41.72	41.32	42.66	41.76	42.31
Mi15	2133	- P	40.76	40.70	42.00	40.75	41.65
	2244	· · · · · · · · · · · · · · · · · · ·	40.76	40.70	41.93	40.73	41.56
Mi13-3		aka la la				-10.00	+,1.00
Kessels Road Mi13-2	2255 2284		40.58	Bridge and 40.51	41,71	40.57	41.45

D-11

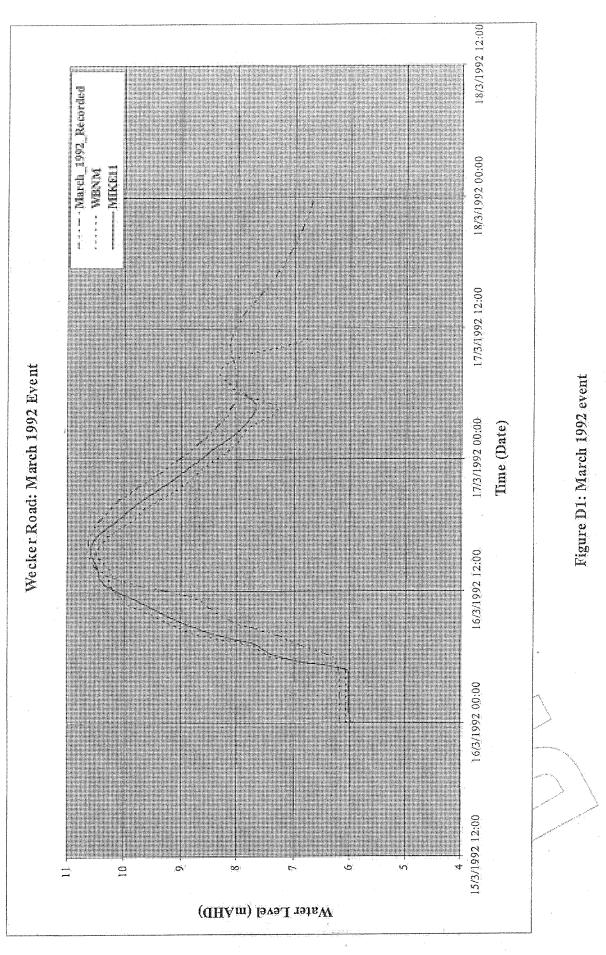
Branch name & Cross section	Chainage	Chainage & AMTD Calibration events		ents	Verification Events		
	MIKE-11 Chainage	AMTD (m)	Mar-92	Jan-94	Mar-01	May-96	Nov-04
Mi13	2325	1	40.46	40.39	41.57	40.44	41.31
Mi12	2516		39.45	39.40	40.53	39.44	40.26
Mill	2635	<u> </u>	38.68	38.63	39.83	38.69	39.53
Parkway St	2648		Parkway S	treet bridge a	ind weir	<u>L.:</u>	Bananyuminimimimimi
Mi10-2	2664	1	38.61	38.57	39.64	38.60	39.38
Mi9	2718		38.43	38.39	39.40	38.42	39.14
Mi8	2828		37.74	37.64	38.93	37.69	38.60
Mi7	2955		37.35	37.14	38.64	37.24	38,28
Mi6	3069		37.07	36.87	38.23	36.96	37.93
Mi5	3221		36.52	36.35	37.63	36:42	37,31
Mi4	3388		35.74	35.51	37.06	35.62 <	36.69
Mi3	3496		35.36	35.14	36:63	35,26	36.25
Mi2	3585		35.03	34.82	36.16	34.93	35.82
MiI	3801		33.95	33.71	35.10	34.03	∖34.82
Mi2	3890		33.22	32.99	34.47	33.59	34.28
Minnippi BypassBranch							<u>,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,</u>
Minnippi newl	80		3.21	2.62	3.52	3.20	2.99
Minnippi_new2	125	and the second	3.10	2.62	3.51	3.19	2.97
Minnippi new3	230		3,07	2.62	3.47	3.16	2.95
Minnippi_new4	400-		<i>4</i> 3,01	2.62	3.42	3.09	2.91
Minnippi_new5	542	7,000	2.97	2.62	3.39	3.04	2.89
Stanton_RD	(650√	7 7 7	2,95	2.62	3.37	3.02	2.88
new_A	720		2.85	1.77	3.30	2.99	2.65
new B	730		2.84	2.00	3.28	2.98	2.55
Minnippi new6-US	745		2.84	1.20	3.27	2.98	2.55
Gateway culverts	748		Gateway Cı	lverts	<u> </u>	L	
Minnippi new7-DS	810		2.84	1.14	3.26	2.97	2.55
new_E	825		2,83	1.30	3.25	2.96	2,54
new_G	860		2.81	2.20	3.22	2.94	2.52
new 7a	870		2.78	1.58	3.20	2.92	2.49
Minnippi new8	945		2.50	1.68	2.88	2.66	2.15
BM31GHD modified	1015		2.34	1.67	2.74	2.51	1.98
Minnippil-6 ALS	1115		2.25	1.67	2.64	2.41	1.89
Wynnum Road bridge	1125		Wynnum R	oad bridge at	ıd weir		***************************************
BM 31GHD-copy	1150		2.17	1,66	2.39	2.28	1.88
BM36 GHD	1310		2.13	1,66	2.32	2,/22	1.84
Minnippi_new11	1560		2.08	1.66	2.23	2.17	1.81
BM 42B_GHD	1850		2.06	1.66	2.17	2.12	1.79
BM42BGHD	2004		2.04	1.66	2.13	2,10	1.78
Murarrie Bypass Branch				,			***************************************
MULALS	20		2.49	2.04	2.63	2,50	2.26
New MULALS	35		2,48	2.03	2.62	2,49	2.25
New MU2_ALS	160		2.47	2.02	2.62	2.48	2.24
New_MU3_ALS	275		2.47	2.02	2.61	2.48	2,24
Copy_new_MU3	310		2.46	2.01	2.61	2.48	2.23
New MU5 ALS	390		2.46	2.00	2.60	2.47	2.23
Mu 6 ALS	470		2.45	1.99	2.60	2.47	2.21
Gateway culverts							· · · · · · · · · · · · · · · · · · ·
MU 7 ALS	EAE		2.28	1.93	2.40	2.32	2.10
Mr. (Are	545		۷.40	1.70	2.70	4.34	4. I. V

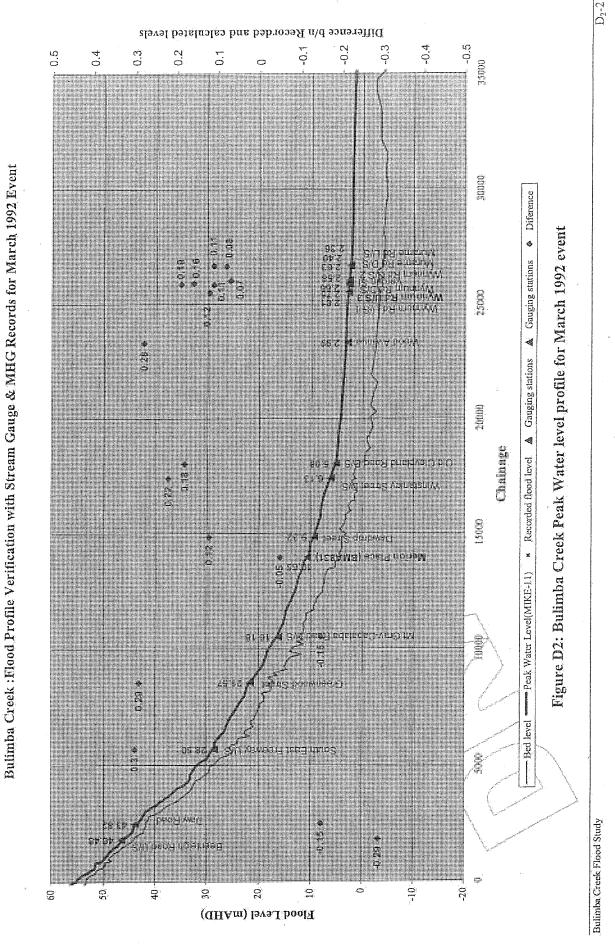
D-12

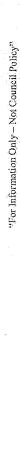
Branch name & Cross section ID	Chainage & AMTD		Calibration events			Verification events	
section in	MIKE-11	AMTD	Mar-92	Jan-94	Mar-01	May-96	Nov-04
	Chainage	(m)					
MU_9_ALS	595	***************************************	2.27	1.92	2.40	2.31	2.09
MU5_ALS	640		2.26	1.91	2.38	2.30	2.08
	650	· · · · · · · · · · · · · · · · · · ·	2.26	1.90	2.38	2.30	2.08
Bulimba East Leftarm		Communication of the Communica	·	. <u></u>	Sammer and the same same same same same same same sam		
BE276	0		48.19	47.78	48.46	48.02	48.39
BE276	33		48.11	47.62	48.39	47.87	\ 48.29
BE275	144		47.80	47.80	47.80	47.80	47.80
BE274	226		46.97	46.95	47.39	46.95	47.23
BE273 US	347		46.88	46.87	لار 47.31 <i>/</i>	46.87	47.14
BE273 DS	443		46.56	46.56	46.88	46.56	∖46.76
BE273A	488		46.40	√ 46.39 ∖	46.64	46,39	46.57
BE273A	520		46.40	46.11	46.61	46.27	46.55
Cleveland Rail		ethy i septimise and explicitly the desire and the desire and the analysis of the analysis of the analysis of The analysis of the analysis of			1	Constitution of the Consti	
CLEV_RAIL	0	And the second second	\1.71	1)22.	1.71	1.74	1.20
CLEV_RAIL	939 (1.36	0.91	1.48	1.54	0.91

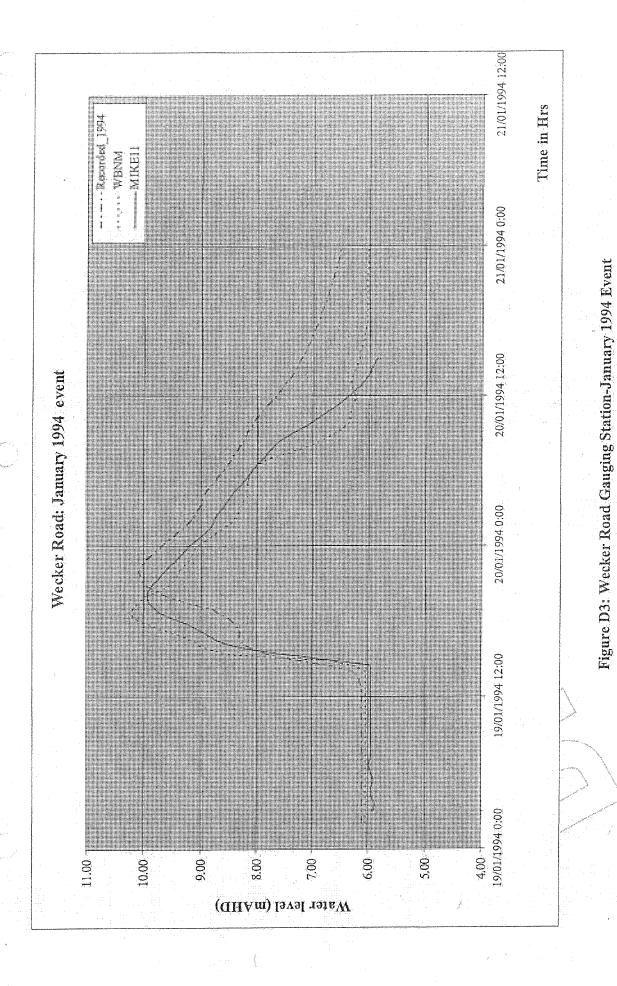
D2 Peak water level plots for calibration/verification events

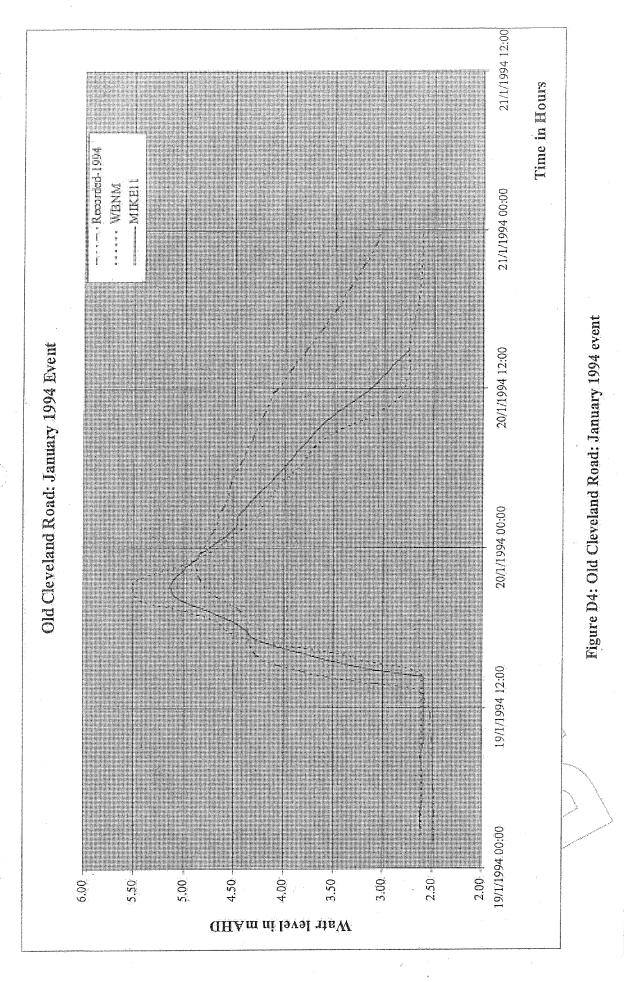












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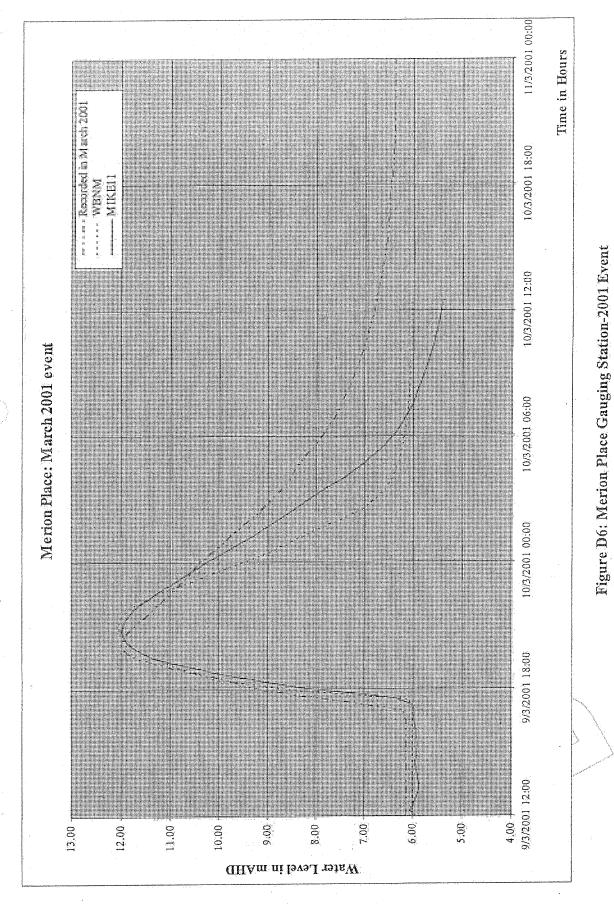
Bulimba Creek Flood Study

-22

Surface Elevation (mAHD)

Difference b/n Recorded and calculated levels

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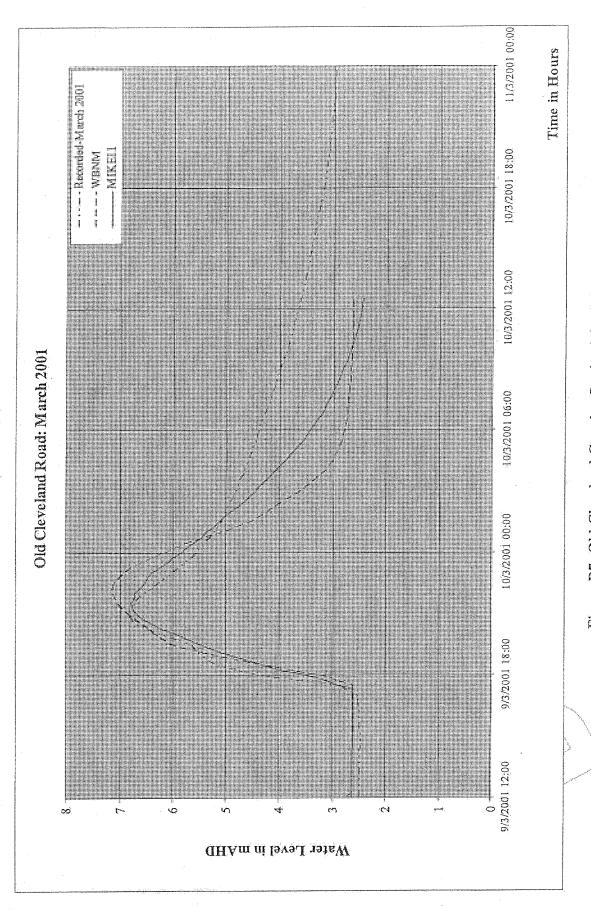
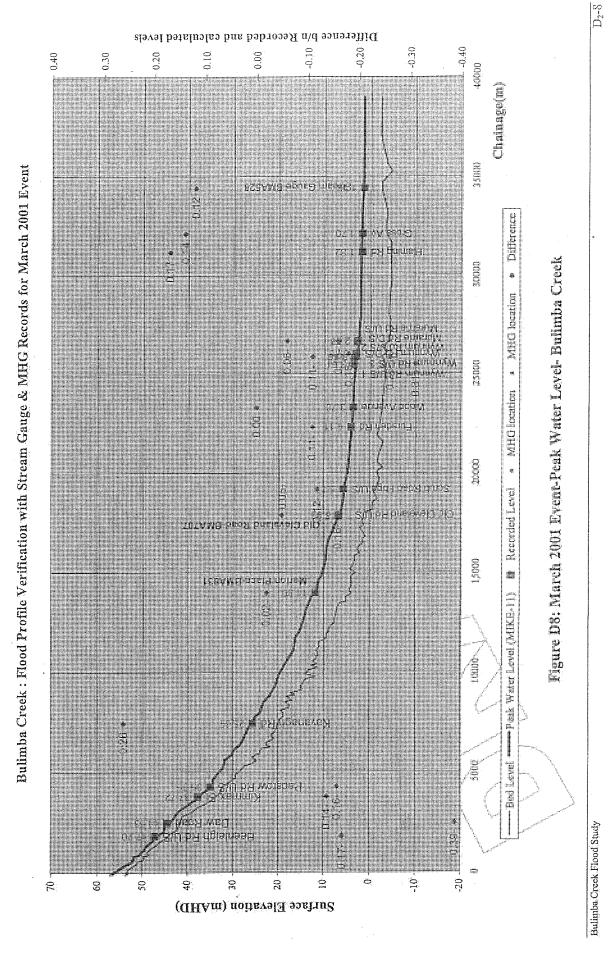


Figure D7: Old Cleveland Gauging Station-March 2001 event

Bulimba Creek Flood Study

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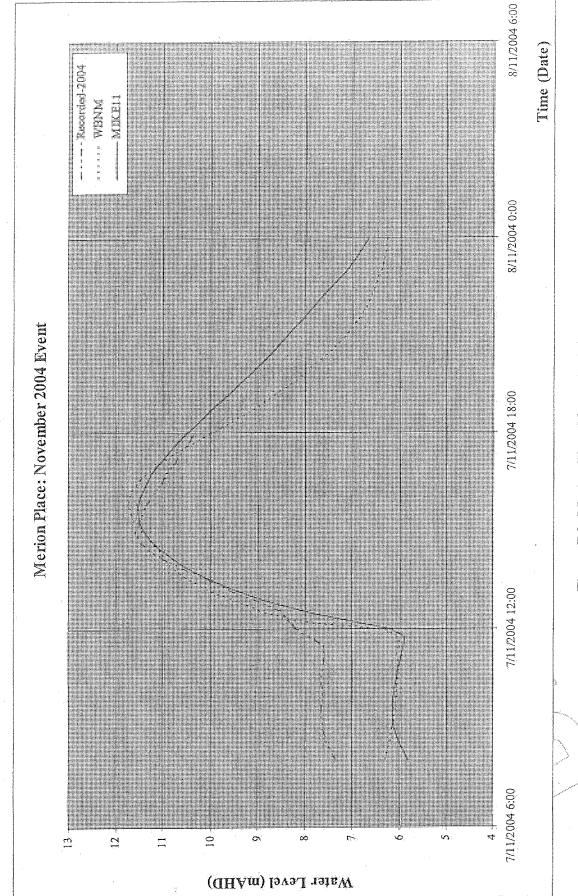


Figure D9: Merion Place-November 2004 Event



Time (Date)

8/11/2004 0:00

7/11/2004 18:00

7/11/2004 6:00

20

7

22

23

24

6

Water Level (m AHD)

18

[]

-- Recorded-2004

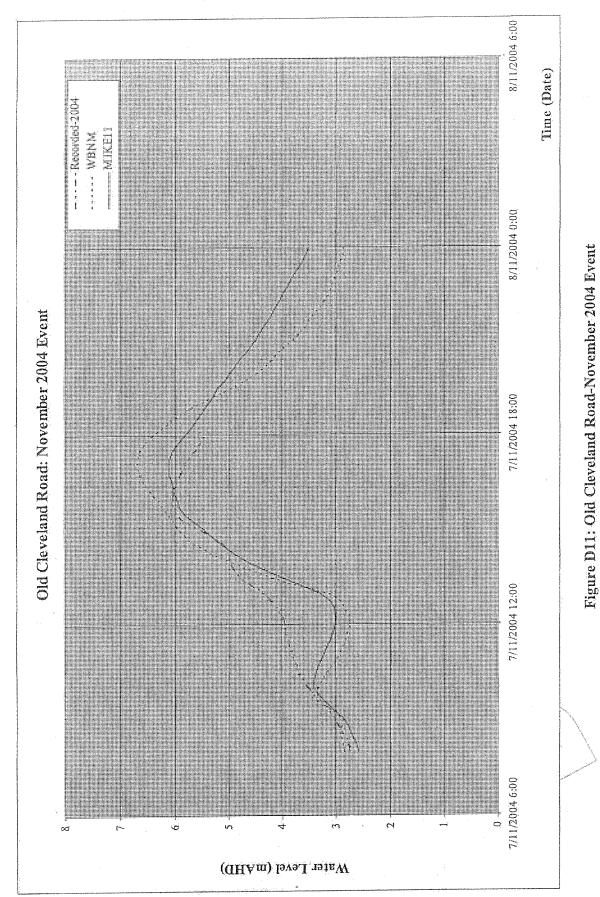
Greenwood Street: November 2004 Event

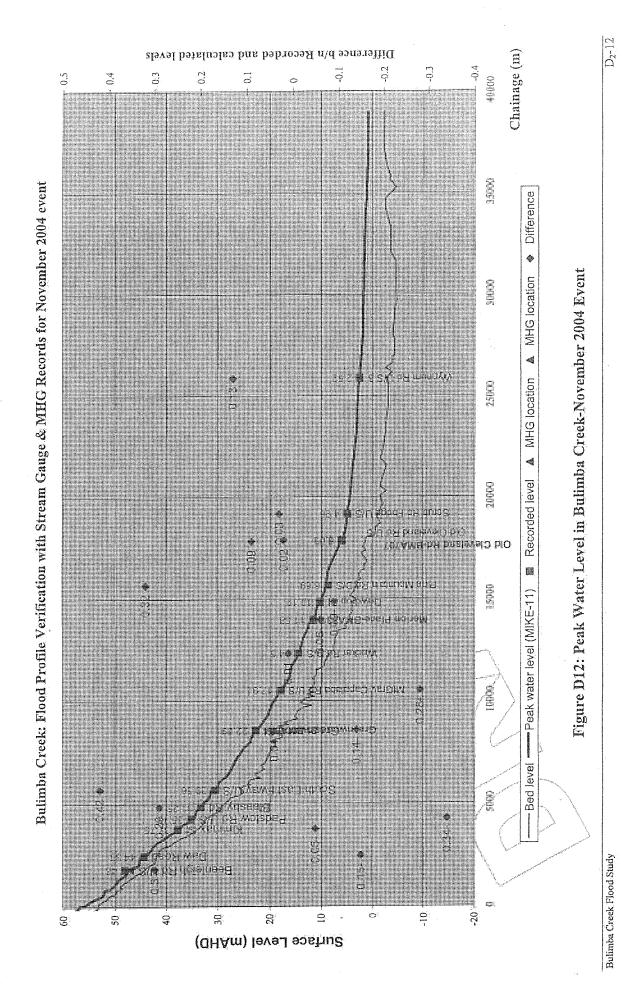
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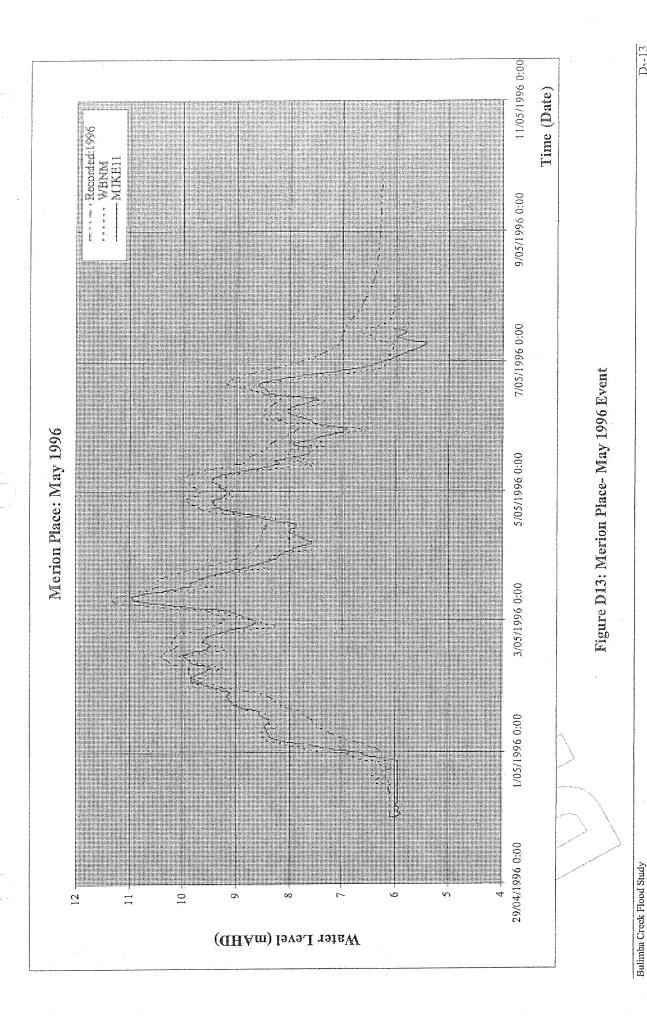


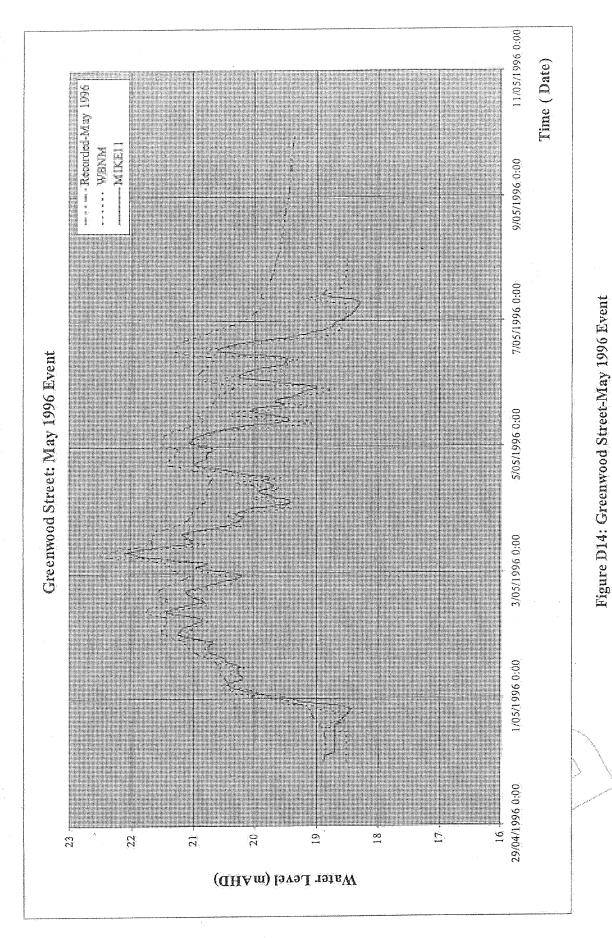


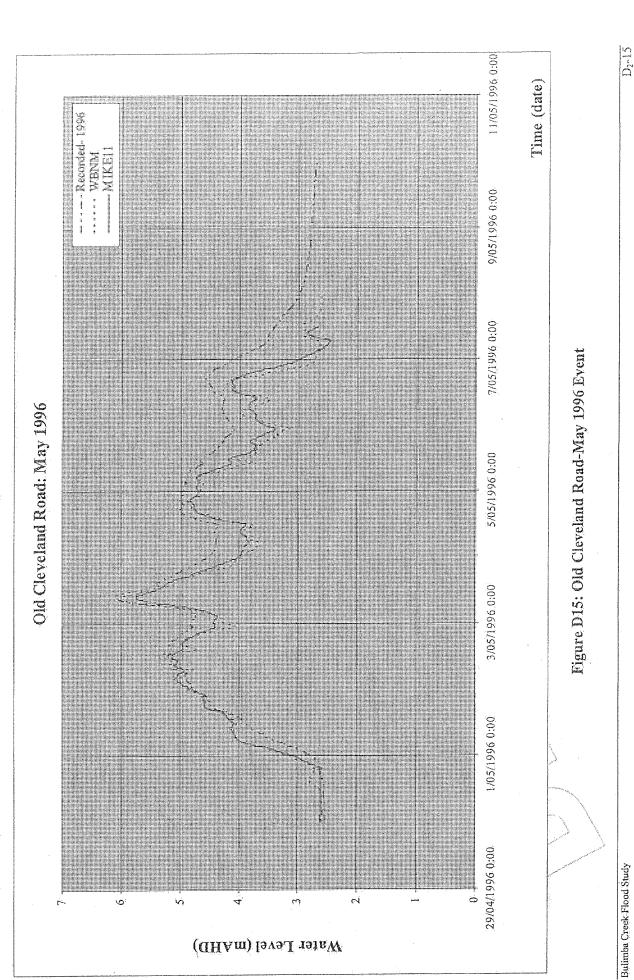












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Bulimba Creek: Flood Profile Comparison with Stream Gauge & MHG Records for May 1996 event

Bulimba Creek Flood Study

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D₂-16

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Appendix E Downstream Boundary Levels Adopted for Calibration/Verification Events



TIDAL TAILWATER LEVEL March 1992 - Brisbane River at Pinkenba

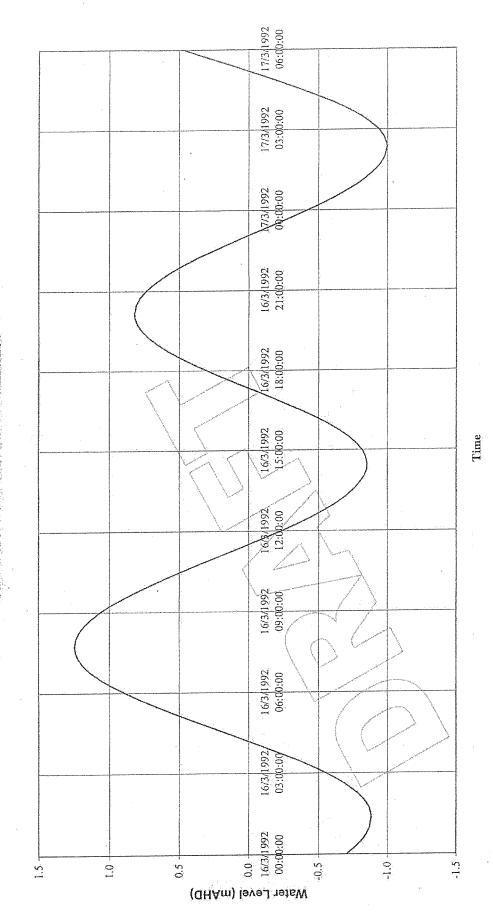


Figure E1: Tidal tail water level at Pinkenba for March 1992 event

TIDAL TAILWATER LEVEL January 1994 - Brisbane River at Pinkenba

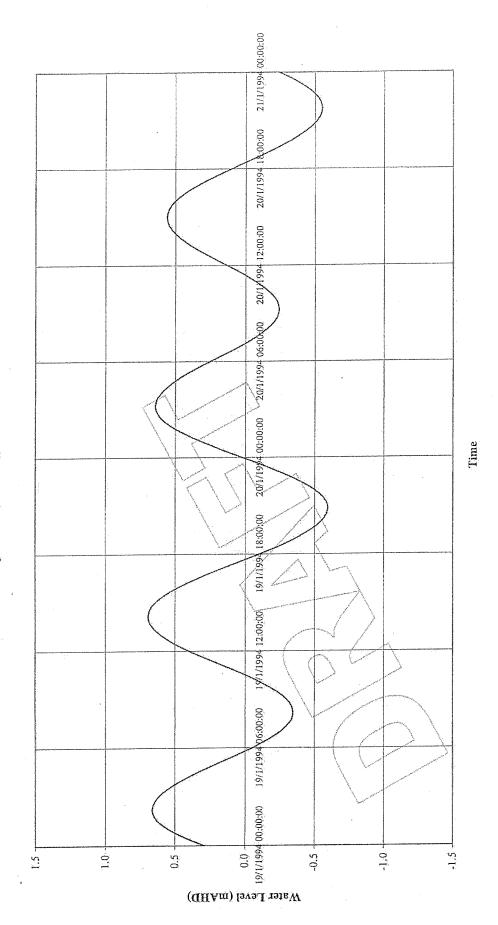


Figure E2: Tidal tail water level at Pinkenba for January 1994 Event

TIDAL TAILWATER LEVEL May 1996 - Brisbane River at Pinkenba

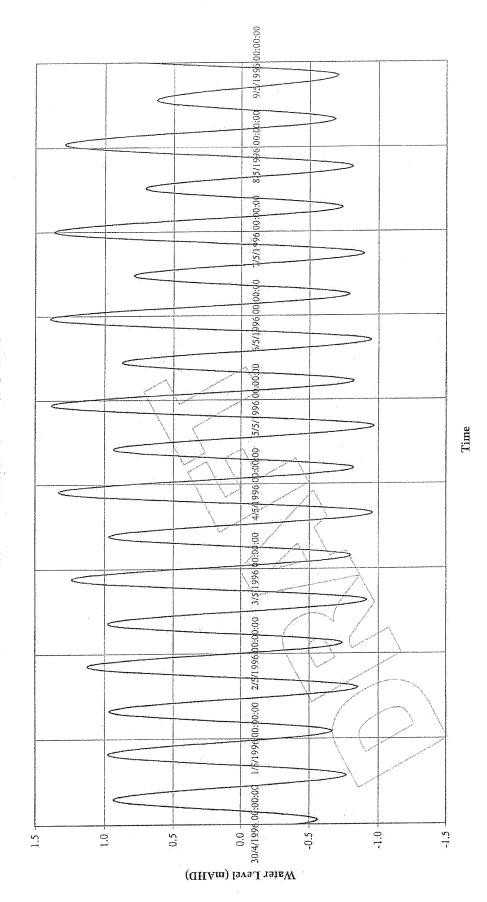


Figure E3: Tidal tail water level at Pinkenba - May 1996 Event

March 2001 - Brisbane River at Pinkenba TIDAL TAILWATER LEVEL

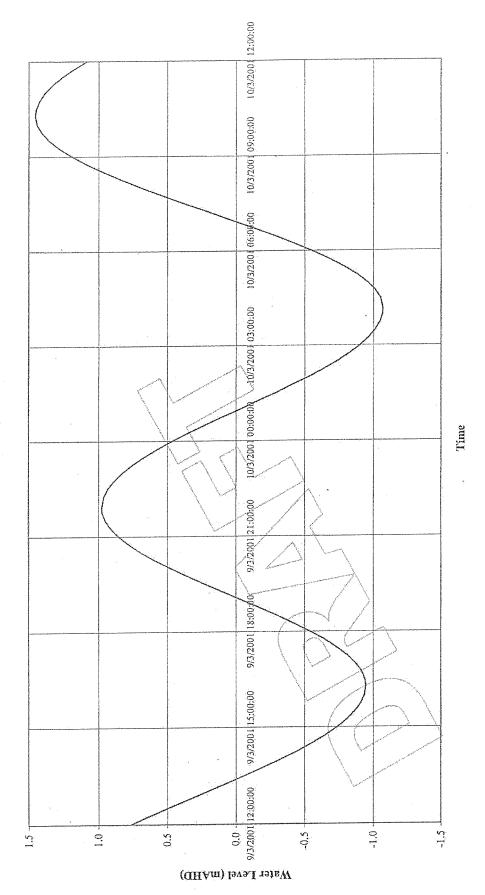


Figure E4: Tidal tail water level at Pinkenba - March 2001 Event

Tidal Tailwafer Levels- 2004 November Event

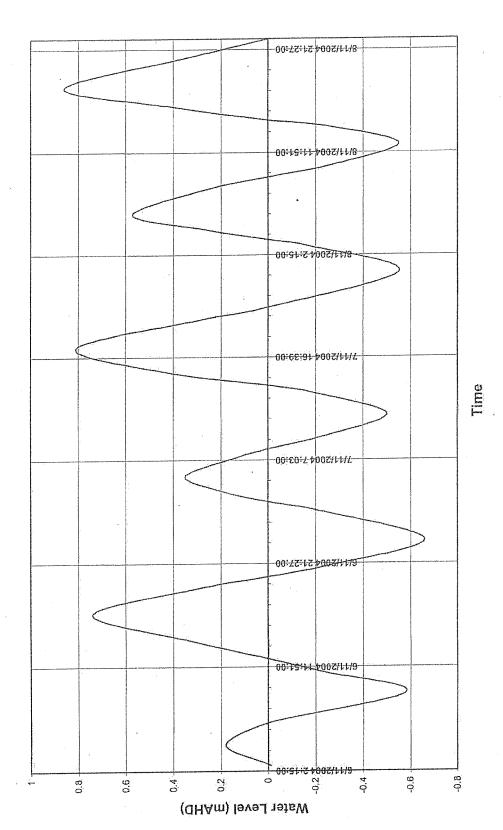


Figure E5: Tidal tall water level: November 2004 event

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Appendix F Muskingum Analysis





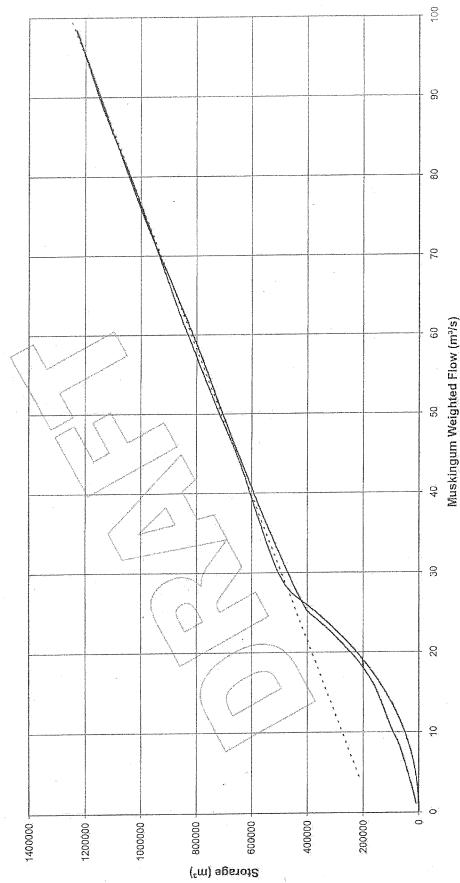


Figure F1: Muskingam analysis for Bulimba Creek: Nemies Road to confluence with Last Arm

F-1

Bulimba Creek Flood Study



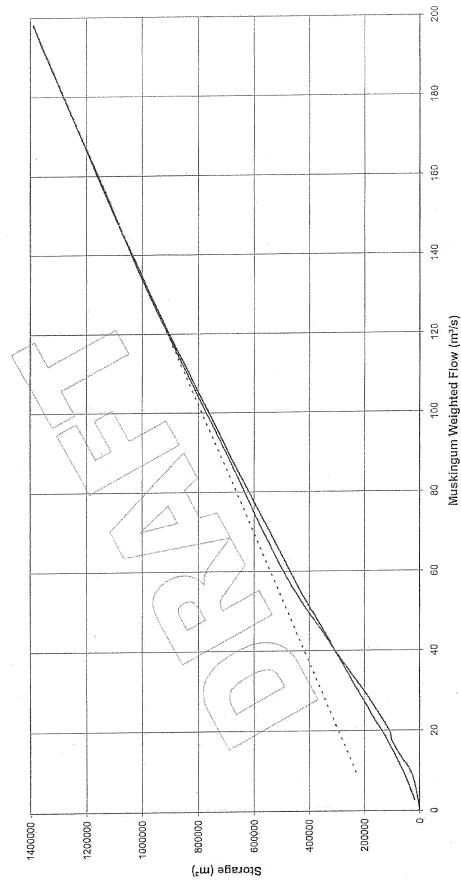
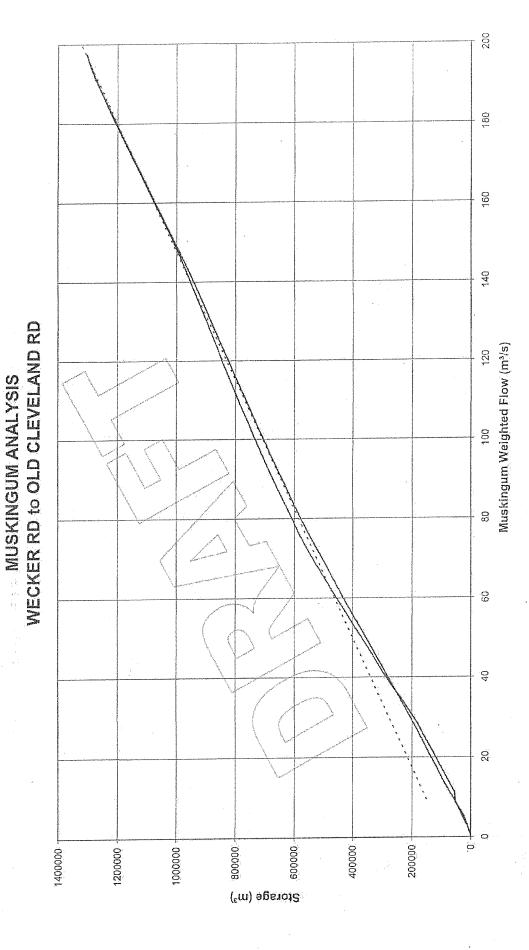


Figure F2: Muskingam Analysis-Bulimba Creek from East arm confluence to Wecker Road

F-2

Bulimba Creek Flood Study



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Figure F3: Muskingam Analysis-Bulimba Creek from Wecker Road to Old Cleveland Road

F-3

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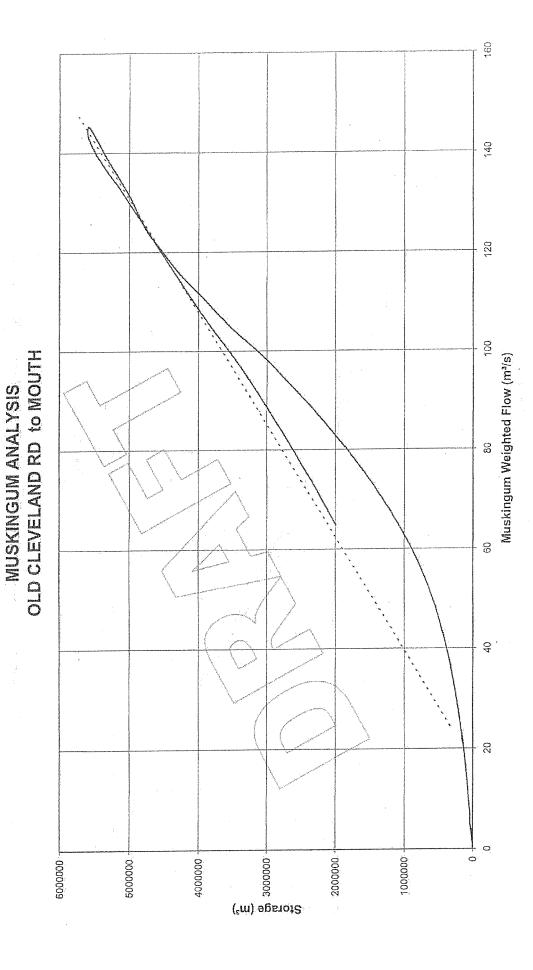


Figure F4: Muskingam Analysis for Bulimba Creek from Old Cleveland Road to Mouth

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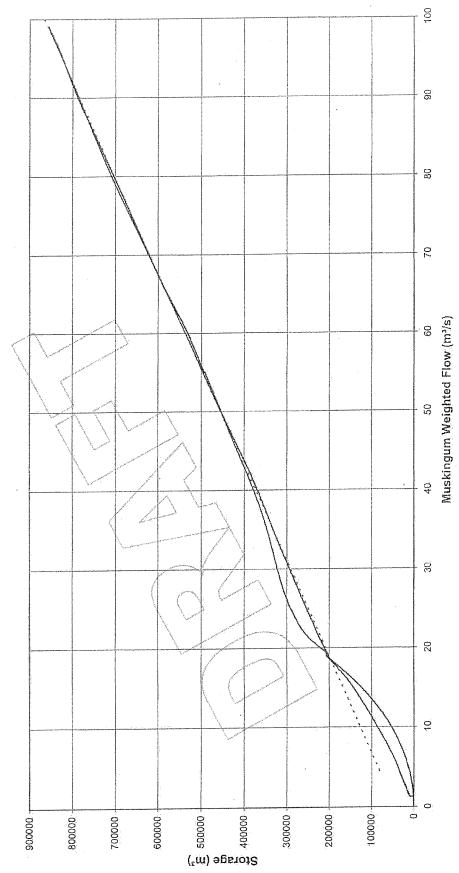


Figure F5: Muskingam Analysis-Bulimba Creek East Branch

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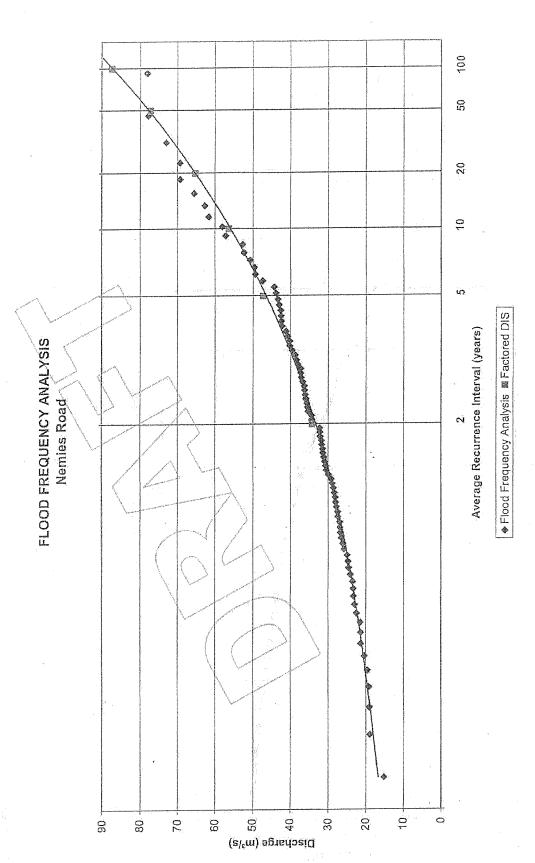
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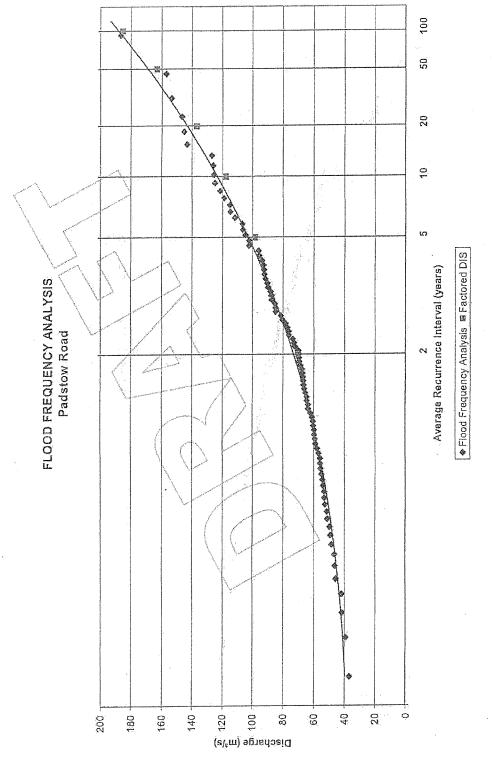
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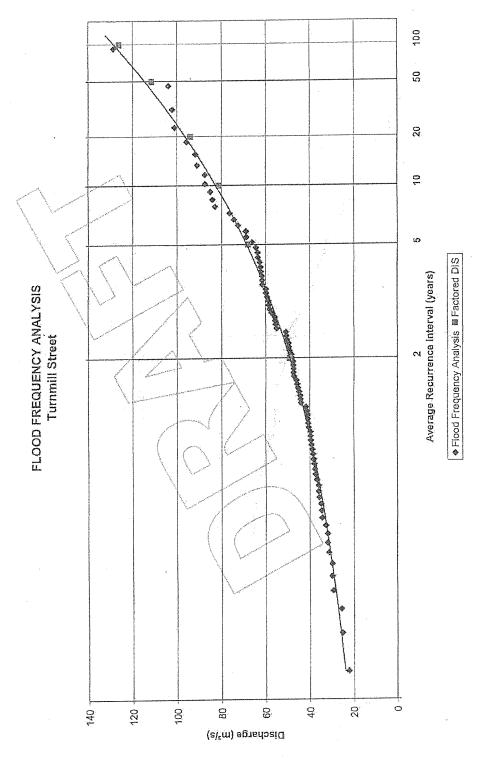
Appendix G Flood Frequency Analysis



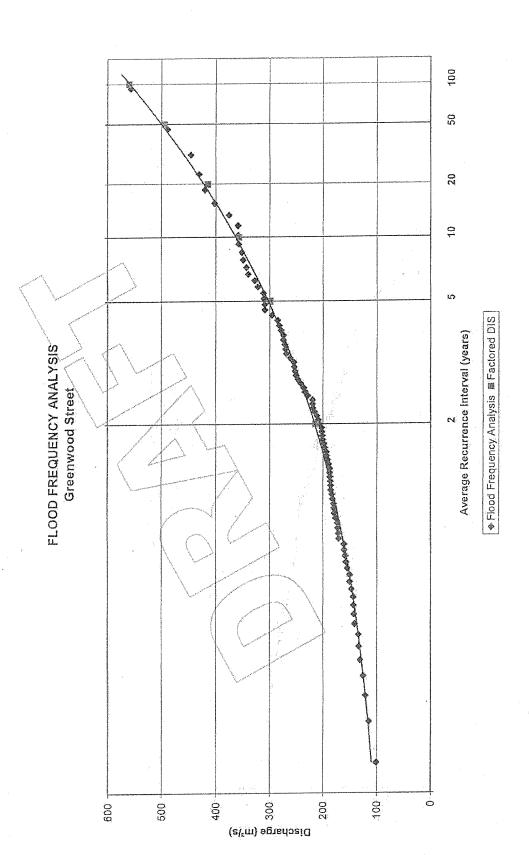


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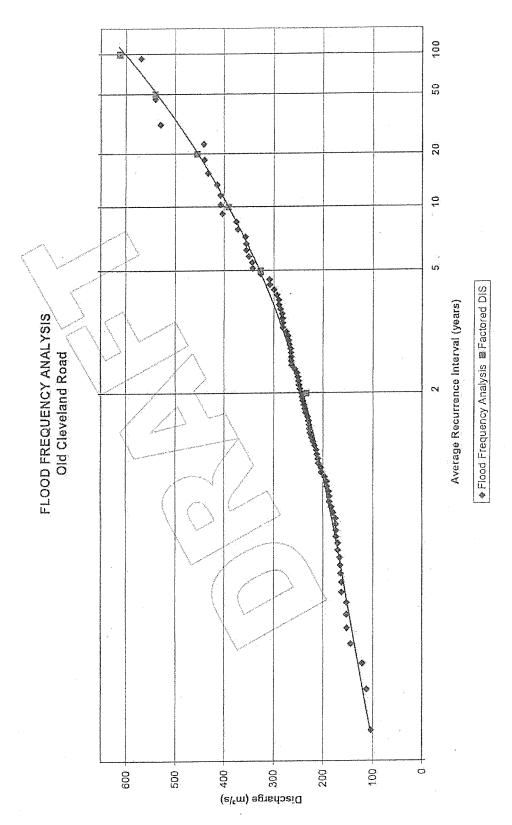








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Appendix H Design Peak Flood Discharges at Sub- catchment Outlets



Table H1: Peak flow discharges at each sub-catchment outlet for design events (from WBNM hydrology model)

ıb-catchment ID		Peak flood Dis	charge at each	sub-catchment	outlet (m3./sec)	
	100yr	50yr	20yr	10yr	5yr	2yr
Ala	60.3	56.5	47.7	41.4	34.8	24.2
A1b	86.6	77.6	65.5	56.6	47.5	33.9
AŽ	103.4	92.4	77.9	67.1	56.2	39.8
A3	115.5	101.7	85.7	سر 73.8	61.7	44.4
В	121.5	106.6	89.6	77:2	64.5	46.5
Cla	39.5	36.9	31.2	27.1	₹22.8 •	15.9
C2b	78.1	67.7	57.2	49.3	41.2	30.2
D	88.3	83.0	70.1	60,8	51.1	35.3
E	109.9	94.6	80.0	69.0	57.8	42.9
F	125.2	109.0	92.0	79.3	66.4	48.6
G	183.7	160.0	134.4	115.5	96.3	69.3
Н	307.0	266.7	224.1	192.8	160.9	116.7
11	316.3	276.1	231.7	199.5	166.5	120.0
12	322.0	282.4	√237.0	204.1	170.3	122.2
	21.7	20.2	17.1	14.9	12.6	8.9
-\frac{1}{12}	48.8	41:5	35.1	30.3	25.5	19.2
KI \	65.9	57.4	48.5	41.6	34.8	25.3
K2	21.8	20.3	17.1	14.8	12.5	8.7
K3 \	30.2	27.0	22.8	19.6	16.4	11.6
LI	98.8	86.6	73.0	62.7	52,5	37.8
L2	120.3	105.9	89.1	76.5	63.9	45.7
M1	124.0	109.3	92.0	79.0	66.0	47.2
M2	41.7	38.9	33.1	28.8	24.4	17.2
M3	46.6	43.0	36.5	31.6	26.6	18.6
M4	11.2	10.4	8.7	7.5	6.3	4.3
M5a	34.1	31.8	26.8	23.2	19.4	13.4
M5b	49.3	44.6	37.5	32.4	27.1	19.1
M6	17.8	16.6	14.0	12.1	10.1	7.1
M7	66.4	59.7	50.3	43.3	36.2	.25.5
M8	114.1	102.0	86.1	74.2	62.2	44.3
NI	230.7	201.8	169.9	146.1	122.1	88.1
N2a	33.2	31.0	25.7	22.1	18.3	12.2
N2b	52.5	45.0	37.5	31.9	26.3	18.7
N2c	267.5	234.8	197.3	169.7	141.8	102.0
0	557.7	488.7	410.4	353.4	295.1	212.0
P	97.2	91,1	76.2	65.6	54.6	36.9
	581.0	510.7	429.0	369.2	308.3	220.9
Q	119,4	112.4	95.1	82.6	69.5	48.1
R	587.2	516.3	434.0	373.3	312.1	223,4
S		57.3	48.3	41.9	35.2	24.3
TI	61.2 583.8	513.4	431.7	371.4	310.5	222,0

Sub-catchment ID	ALCO ACCOUNTS OF THE PROPERTY	Peak flood Dis	charge at each	sub-catchment	outlet (m³./sec)	
Andrew Control of the	100yr	50yr	20yr	10yr	5yr	2yr
UI	61.3	57.4	48.5	42.0	35.3	24.4
U2	74.5	66.3	56.0	48.3	40.5	29.0
U3	90,4	78.8	66.5	57.1	47.8	34.6
V	586.3	516.2	434.0	373.1	311.8	222.4
W1	52.1	48.7	40.8	35.1	29.3	19.9
W2	63.0	54.7	45.7	39.1	32.4	23.0
W3	80.3	70.1	58.6	50,1	41.5	29.4
X 1	50.3	47.1	39.7	34.5	29.0	20.1
X2	54.0	اد 47.5	40.1	34)5	28.9	20.7
X3	42.9	40.0	33.5	28.8	24.0	16.3
X4	46.2	39.7	33.2	28.5	23.7	17.0
X5	99.0	86.7	>72.7	62.4	52.0	37.1
Y1	600.6	528.8	444.9	382.5	319.8	228.5
Y2	611.1	538.6	453.1	389.3	325.4	232.2
12	120.7	113.5	95.8	83.0	69.7	47.9
AA	606.8	534:7	449.6	386.4	322.9	230.4
BB1	593.5	522.6	439.3	377.6	315.5	224.7
BB2\	69,6	65.2	54.9	47.5	39.8	27.4
BB3	589.3	518.9	436.3	374.9	313.3	223.1
, BB4	586.8	516.6	434.4	373.3	311.9	222.1
CC	64.8	60.7	51.1	44.2	37.0	25,4
DD	584.2	514.3	432.6	371.6	310.4	221.0
EE	565.3	497.5	418.4	359.3	300,1	213.6
FF .	71.5	62.5	51.7	44.0	36.2	24.5
GG	89.7	78.0	64.7	54.8	45.1	31.3
HH1	60.0	56.1	46.9	40.4	33.6	22.8
HH2	89.7	78.5	65.2	55.7	46.2	32.1
ннз	119.3	104.5	87.0	74.5	61.7	, 43.4
II.	559.7	492.5	414.7	355.9	297.3	211.7
	98.1	92.2	77.8	67.5	56.7	39.1
KK	109.0	94.6	79.5	68.3	57.0	41.4
LĻ.	558.6	491.5	414.1	355.3	296.7	211.4
MM	155.2	146.5	124.0	107.8	90.9	62.9
NN	547.6	481.9	406.1	348.4	291.0	207.3

city design



Dedicated to a hetter Brisbane

Appendix I Anticipated Peak Design Flood Levels & Flood Discharges



Table I1: Estimated Peak Design Flood Levels for Bulimba Creek

Branch name & cross section	MIKE11 Chainage	AMTD(m)	Design Eve	ent flood lev	els (Ultima	te) in mAH	D	*
ID	(m)	ANTED(III)	2 yr	5 yr	10yr	20 yr	50 yr	100 yr
Bulimba Creek: Compton Roa	d to Nemics	Road		Activities and All Control				
Start	T 0	39900	60.86	61.07	61.18	61.28	61.40	61.45
BM222	65	39835	60.63	60.82	60.91	61.00	61.11	61.14
Bm221	175	39725	60.23	60.41	60.50	60.58	60.68	60.71
BM220	270	39630	59.72	59.85	59.94	60.02	60,12	60.19
BM219	415	39485	58.94	59.11	59.24	59.36	59.51	59.66
BM218	560	39340	58.02	58.23	58.38	58.52	58.67	58.86
BM217	736	39164	57.19	57.50	57.69	57.86	<i>5</i> 8.05	58.23
BM216	900	39000	56.45	56.96	57.21	757.41	57.64	57.86
End	935	38965	56.17	56.79	57.05	57.26	\57.50°	57.73
Bulimba Creek-Main Branch	^	Bulimba	Creek-Mai	n Branch				
BM214	0	38965	56.17	56.79	57.05~	57.26	57.50	57.73
BM 214	10	38955	56.15	56.77	57.04	57,25	57.49	57.71
Nemies Road	17	38948	Nemies Ro	ad Culverts	1			
BM214 copy	40	38925	55.69	55.97	36.14	56.29	56.48	56.66
BM213	120	38845	55.33	55.54	55.68//	55.79	55.94	56.08
BM212	215	38750	/54.80	55:00	755.11	55.22	55.35	55.47
BM211	355	38610	53.64	53.84	53.93	54.00	54.09	54.17
Brandon Road	370	38595	Brandon F	load Culver	ts	- 8		
BM211 copy	385	38580	53.40	53.65	53.76	53.84	53.94	54.03
BM 209	470	38495	52.60	52.78	52.89	52.98	53.09	53.17
BM 208	540	38425	52.20	52.36	52.47	52.61	52,77	52.86
BM 207	600	38365	52.05	52.23	52.35	52.45	52.63	52.74
BM 206	740	38225	51.88	52.06	52.18	52.28	52.44	52.58
BR_I	800	38165	51.79	51.96	52.07	52.17	52.32	52.45
Brandon Road	805	38160	Brandon R	oad downst	ream weir			
BR 2	825	38140	51.03	51.21	51.32	51.41	51.51	51.63
BM 205	840	38125	50.82	51.02	51.14	51.23	51.35	51.47
BR 3	890	38075	50.60	50.80	50.91	51.00	51.12	51.25
BR 4	905	38060	50.52	50.71	50.81	50.90	51.01	51.14
BR 5	942	38023	50.36	50,54	50.63	50.72	50.82	50.93
BR 5 copy	960	38005	50.26	50.43	50.53	50.61	50.71	50.81
BM 204 copy	990	37975	50.09	50.26	50.34	50.42	50.52	50.62
BM 203	1075	37890	49.66	49.84	49.95	50.06	50.18	50.28
BM 202	1160	37805	49.40	49.59	49.73	49.85	49.98	50.09
BM 201	1300	37665	49.00	49.19	49.34	49.47	49.61	49.71
BM 200	1365	37600	48.61	48.79	48.92	49.05	49.20	49.31
BM 199	1545	37420	47,55	47.72	47.80	47.89	48,03	48,14
BM 198	1670	37295	46.95	47.23	47.40	47,55	47.71	47.86
BM340-MHG	1800	37165	46.60	46.99	47.22	47.39	47.58	47.74
BM 197	1830	37135	46.57	46.97	47.21	47,38	47.57	47.72
Beenleigh Road	1845	37120	Beenleigh	CHICAGO COLORO C		· ·		
BM 197 Copy	1860	37105	46.12	46.30	46,44	46.55	46.69	46.81
ВМ 197 Сору ВМ195-I	1900	37065	45.78	45.97	46.13	46.26	46.42	46.56
BM 194	1940	37025	45.74	45.91	46.05	46.18	46.34	46.49
DIN 12T	1,40	- U/U#U			لستهتئت	L	L	l

Branch name & cross section	MIKE11		Design Eve	nt flood lev	els (Ultima	te) in mAH	D	
ID	Chainage	AMTD(m)	2 yr	5 yr	10yr	20 yr	50 yr	100 yr
	(m)		1 2 31		103.			
	10.00	37005	45.54	45.62	45.68	45.74	45.81	45.88
ВМ 194 сору	1960	37005	·	45.02	45.14	45.29	45.49	45.63
BM 192	2045	36920	44.88 44.62	44.89	45.14	45.24	45.47	45.62
BM 191 copy	2115	36850		ce Foot-Bri	Language Commission of the Com	Zarzania wanania manania wanania wa		L
St Lawrence Foot Bridge	2117	36848		puncususususususususus		gonnersson management of the second	15.16	45.61
Bm 191	2125	36840	44.60	44.88	45.06	45.24 45.20	45.46 45.44	45.58
BM190	2255	36710	44.47	44.83 44.76	45.02 44.96	45.14	45.44	45.52
BMI88-6 copy	23.70	36595	44.36	The same of the sa	AND DESCRIPTION OF THE PROPERTY OF THE PROPERT	Contraction of the Contraction o	, C. C+	73.32
Altandi Street Foot Bridge	2375	36590		reet Foot Bi	Section of the Party of the Par	The second second second second second	44.00	4400
BM188-6	2380	36585	44.12	44.34	44.49	.44.61	<u>44.80</u>	44.98
BM188-2 ALS	2470	36495	43.84	44.04	44.1.7	44.29	44.47	44.64
BM188-1 ALS	2500	36465	43.60	43.79	43.91	44.02	44.20	44.37
BM187	2670	36295	42.88	43.05	43:18	43.30	43.45	43.61
BM186	2785	36180	42.64	42.80	42:93	43.04	43,17	43.31
BM185	2985	35980	42,01	42.16	42.27	42.37	√42.49	42.59
BMI 84	3165	35800	40.96	41.14	41.21	41.30	41.41	41.51
BMI 83	3295	35670	39.84	40.04	40.16	40.26	40.41	40.54
BMI 82	3435	3.5530	39.07	39.24	39:37	39.48	39.63	39.77
BM181	3625	35340	<i>₹</i> 37.61	₹37.83	37.99	38.11	38.27	38.41
BM320-MHG	3765	35200	36.79	37.06	37.25	37.40	37.57	37.72
BM180	3800	35165	36,64	36.92	37.12	37.28	37.46	37.61
BM179	3960	3,5005 \	35.90	36.14	36.31	36.46	36.61	36.73
Malbon Street Foot Bridge	3965	35000	Malbon St	reet Foot B	ridge and W	/eir		
BM179 copy	3970 /	34995	35.77	36.04	36.23	36.41	36,55	36.68
BM178	4150	34815	34.27	34.52	34.71	34.92	35.17	35,35
BM177-MHG310	4260	34705	33.84	34.15	34.36	34.60	34.91	35.13
ALS	4320	34645	33.48	33:87	34.08	34.32	34.65	34.92
LC	4375	34590	33.29	33.76	33.97	34,21	34.56	34.84
BM176modified with ALS	4385	34580	33.29	33.75	33.97	34.20	34.55	34.84
Padstow Road	4390	34575	Padstow R	oad Culvert	s and Weir			yang ang ang ang ang ang ang ang ang ang
BM176 DS	4415	34550	33.28	33.74	33.96	34.18	34.49	34.72
BM 175	4460	34505	33.25	33.72	33.94	34.15	34.45	34.68
BM175-174	4515	34450	33.24	33.71	33.93	34.14	34.44	34.67
Mimosa Merge	4555	34410	33.23	33.71	33.92	34.14	34.43	34.66
Padstow Merge	4575	34390	33.21	33.68	33.89	34.11	34.39	34,62
BM 174	4590	34375	33.14	33.60	33.81	34.02	34.30	34.52
BM174A	4700	34265	32.83	33.28	33.49	33.70	33.98	34.21
BM174B	4765	34200	32.65	33,08	33.28	33,48	33.75	33.97
BM173- MHG300	4780	34185	32.61	33.04	33.24	33.45	33.73	33.96
Blesby Road Foot Bridge	4785	34180	e Company and a superior and a super	d Footbrid	Entere contract contr	kanuturukan kanuturuk		
CONTRACTOR OF THE PROPERTY OF	4789	34175	32.59	33.03	33.23	33.44	33,71	33.93
BM 173 copy			32.21	32.65	32.86	33.09	33.38	33.63
BM172	4905	34060	***************************************	32.24	32.45	32.69	33.01	33.30
BM171	4995	33970	31.79		31.76	32.02	32.45	32.85
BM170	5120	33845	31.12	31,55		31.16	31.81	32.34
Garden City connection	5280	33685	29.94	30.45	30.75	31.15	31.80	32.33
BM169	5285	33680	29.91	30.43	30.73	31.13	21.00	الدائد المائد

Branch name & cross section	MIKEII		Design Eve	ent flood lev	els (Ultima	te) in mAH	D	<u>anganggunampanakolikoka Habinda Paddicini Sanich</u>
ID	Chainage	AMTD(m)	AND DESCRIPTION OF THE PARTY OF	5 yr	10yr	20 yr	50 yr	100 yr
	(m)	7.75.0	2 yr	faranceamanner mounts			E	32.25
BM168	5405	33560	29.54	30.14	30.52	30.99	31.70 31.62	32.19
BM167	5520	33445	29.31	29.94 29.70	30.35 30.15	30.87 30.74	31.54	32.13
CopyBM 167-MHG290	5615	33350	28.99	Luummaanamaan	L	30.74	71.74	1 72,17
South-East Freeway	5625	33340	Encourant management	Freeway co	STATEMENT PROFESSION OF THE PROPERTY OF THE PR	20.01	20.72	1 20.00
BM 165 copy	5715	33250	28.74	29.39	29.79	30.24	30.72	30.98
BM165	5730	33235	28.72	29.38	29.77	30.23	30.70	30.97
SurveyXs-5	5785	33180	28.58	29.26	29.70	30.18	30.67	30.94
Logan Road	5790	33175	Sameuniimaniimaniima	d Culverts	The state of the s			I 20.10
SurveyXs-4	5845	33120	28.46	29.02	29.30	29.56	29.88	30.12
SurveyXs-3	5902	33063	28.41	28.96	29.25	29.51	29.84	30.09
SurveyXs-2	5918	33047	28.40	28.95	29.23 <	29.50	29.83	30.08
BM158 Xs-1	5935	33030	28.38	28.93	29.22	29.48	29.82	30.07
Garden City Branch start	5938	33027	28.38	28.93	29:22	29.48	29.82	30.07
HEC2937-MHG280	5985	32980	28.30	28.85	29.14	29.40	29.73	29.99
BM157	6050	32915	28:13	28.66	28.94″	29.20	√29.55	29.81
BM156	6160	32805	27.68	28,20	28.47	28.71	29.04	29.30
BM155	6240	32725	27.34	27.84	28.11	28.35	28.68	28.94
BM154	6340	32625	26.94	27.44	27:71	27.95	28.28	28.55
BM153_ALS	6450	32515	26.48	27.03	27.31	27.56	27.90	28.18
BM151	6650	32315	26.09	26.63	26.91	27.16	27.49	27.77
BM149	6860 \	32105	25,69	26.20	26.47	26.71	27,04	27.30
BM148-BM147	6930	32035	25.48	25.96	26.24	26.47	26.80	27.07
CraigStreet Foot Bridge \	6935	32030	Craig Stre	et Foot Brid	lge and Wei	r	·	
BM148 copy	6945	32020	25.44	25.92	26.19	26,43	26.75	27.02
BM148	6985	31980	25.39	25.87	26.14	26.38	26.70	26.97
BM146	7185	31780	24.97	25,44	25.72	25.97	26.31	26.59
BM144	7420	31545	24,26	24.81	25.14	25.41	25.77	26.05
BM143	7490	31475	24.09	24.66	24.99	25,27	25.63	25.91
ALS-142	7600	31365	23.8 Ĺ	24.42	24.77	25.05	25.42	25,71
BM141	7735	31230	23.42	24.04	24.41	24.70	25.07	25.38
BM139	7915	31050	22.85	23,35	23.68	23.94	24.26	24.53
BM138	7985	30980	22.67	23.15	23.47	' 23.72	24.03	24,29
BM137	8070	30895	22.62	23.10	23.41	23.66	23.97	24.23
BM136	8200	30765	22.42	22.90	23.21	23.45	23.76	24.02
BM135	8325	30640	22.28	22.74	23.04	23.26	23.56	23.80
BM134	8475	30490	22.04	22.46	22.74	22.95	23.21	23.44
MHG-BM260	8555	30410	21.83	22.23	22.50	22.69	22.94	23.16
BM132	8570	30395	21.79	22.19	22.45	22.65	22.89	23.10
BM13I	8780	30185	20.91	21.29	21.54	21.73	21.98	22.19
BM130	8840	30125	20.57	20.99	21,28	21.50	21.78	22.02
BM129	8950	30015	20.31	20.75	21.04	21.27	21.58	21.83
	9115	29850	19.75	20.21	20.52	20.77	21.09	21.35
BM127	9215	29750	19.38	19.85	20.17	20.43	20.77	21,03
BM126	9365	29600	19.09	19.58	19.91	20.18	20.52	20.79
BM126a			18.85	19.38	19.73	20.00	20.36	20.64
BM126b	9530 9670	29435 29295	18.61	. 19.16	19.73	19.79	20.16	20.45
BM122	20 /0	ムフムラス	10.01	, 1,7,1U	1 / · · · 1	12117	440 F E U .	

Branch name & cross section	MIKE11		Design Eve	ent flood lev	els (Ultima	te) in mAH	D	neral activities and provide the control of the con
ID	Chainage	AMTD(m)	2 yr	5 yr	10yr	20 yr	50 yr	100 yr
	(m) 9765	29200	18.48	19.01	19.35	19.63	19.98	20.26
BM121	ł	29200 29075	18.36	18.87	19.20	19.46	19.80	20.07
BM119	9890 9920	290/3	18.29	18.79	19.11	19.37	19.71	19.98
BM118		28865	17.72	18.22	18.54	18.81	19.15	19.43
BM117	10100 10205	28760	17.45	17.96	18.29	18.56	18.91	19.19
BM116	····	<u> </u>	1	17.76	18.09	18.35	18.71	18.98
BM115	10315	28650	17.27 16.93	17.46	17.81	18.10	18.47	18.76
BMI 14	10400	28565	<u> </u>	17.05	17.41	17.72	18.11	18.43
BM112	10510	28455	16.51 16.36	16.91	17.27	17.58	17.98	18.31
BM111-MHG250	10575	28390 28280	16.23	16.78	17.14	17:45	17.85	18.17
BM110	10685		£		Road Bridg	CONTRACTOR OF THE PROPERTY OF	Activities and a second and a second	Same and the same of the same
Mt Gravatt Capalaba Road	10702	28263	danamanan manamanan manamanan manamanan manamana	Contraction of the Contraction o	/16.92	17.19	17.54	17,81
BM110 copy	10725	28240	16.09	16.59	16.92	16.90	17.24	17.51
BM108	10875	28090	15.84	16.32	16.40	16.90	16,99	17.27
BM107	10965	28000	15.62	16.09		16.30	16.66	16.96
BM106	11 095	27870	15,19	15.69	16.02	i	§	#
BMI 04	11255	27710	15.00	15.53	15.88	16.17	16.55	16.86
BM1 02	11515	27450	14.75	15.33	15.69	16.00	16.40	16.72
BM101	11620	2.7345	14.69	15.27	15.64	15.95	16.34	16.67
BM100	11695	27270	/ 14.62	. (15.19)	15,55	15.86	16.25	16.56
BM99	11820	27145	14:35	14.91	15.26	15.55	15.94	16.24
BM98	11910	27055	14.09	14:62	14.97	15:26	15.63	15.93
BM97	12035	26930	13.80	14.33	14.68	14.97	15.34	15.65
ВМ97сору	12135	26830	13.65	14.19	14.54	14.83	15.20	15.51
Wecker Road Bridge	12139	26826	Çanızanın en en en en en en en en en	ad Bridge				15.44
ВМ97сору	12/155	26810	13.60	14,12	14.47	14.76	15.13	15.44
BM94	12215	26750	13.50	14.04	14.38	14.68	15.05	15.36 //
BM94-93	12320	26645	13,30	13.88	14.24	14.54	14.93	15.24
BM93	12385	26580	13.12	13.72	14.09	14.40	14.80	15.11
ВМ90 сору	12505	26460	12.83	13.45	13.83	14.14	14.54	14.86
вм90	12690	26275	12.55	13.21	13.60	13.92	14.32	14,65
BM88	12820	26145	12.41	13,06	13.45	13.77	14.17	14.49
BM87	13140	25825	12.06	12:70	13,07	13.38	13,76	14.07
BM84	13440	25525	11.40	12.09	12.48	12.80	13.19	13.49
BM83	13530	25435	11.29	11.97	12.35	12.67	13.05	13.35
BM81	13 670	25295	11.16	11.81	12.18	12.48	12.85	13.13
BM80	13765	25200	11.05	11.69	12.06	12.34	12.70	12.97
вм78	13910	25055	10.69	11.32	11.68	11.96	12.31	12.58
ВМ78 сору	13965	25000	10.36	10.96	11.31	11.61	11.98	12.27
BM77	14115	24850	10.11	10.66	11.00	11.29	11.66	11.95
BM76	14360	24605	10.01	10.57	10.90	11.20	11.57	11.86
BM75	14460	24505	9.96	10.52	10.86	11.15	11.52	11.81
BM74-BM72	14625	24340	9.85	10.40	10.73	11.02	11.37	11.66
BM72	14785	24180	9.48	9.98	10:28	10.55	10.89	11.16
BM71-MHG-230	14845	24120	9.35	9.85	10.16	10.43	10.78	11.06
AND THE RESERVE WITH THE PARTY OF THE PARTY	14960	24005	9.20	9.70	10.01	10.28	10.63	10.93

generalization de contrata de la contrata del la contrata de la contrata del la contrata de la contrata del la contrata de la contrata de la contrata del la contrata de la contrata del la contra	MIKEII	gangangan and adi in an indisident on only with the proposed of the de	Design Fue	ent flood lev	els (I)ltima	te) in mAH	D	:
Branch name & Cross section	Chainage	AMTD(m)	CONTRACTOR OF THE PARTY OF THE	1	10yr	20 yr	50 yr	100 yr
	(m)	42007	2 yr	5 yr	9.62	9.89	10.24	10.54
BM69	15160	23805 23625	8.88	9.33 8.99	9.32	9.61	9.99	10.34
BM67	15340		8.51		9.32	9.54	9.93	10.25
BM66	15460	23505	8.38 8.32	8.89 8.84	9.23	9.50	9,90	10.22
ВМ66 сору	15540	23425	Annua manana	tain Road I	and the second s			10.22
Pine Mountain Road	15555	23410				A CONTRACTOR OF THE PARTY OF TH	9.82	10.14
BM64 copy	15570	23395	8.24	8.76	9.10	9.41		10.14
BM64-MHG250	15600	23365	8.18	8.70	9.05	9.36	9.77 9.73	10.09
BM64	15660	23305	8.09	8.64	9.01	9,32	<u> </u>	
BM63	15790	23175	7.98	8.56	8.94	9.27	9.68	10.01
BM62	15965	23000	7.88	8.49	8.88	9.21	<u>9.63</u>	9.96
BM61	16015	22950	7.85	8.47	8.86	9.19	9.61	9.95
BM60	16190	22775	7.69	8.34	8:75	9.10	9.54	9.88
BM59	16390	22575	7.45	8.13	8,55	8.92	9.37	9.72
BM59 mod	16435	22530	7.38	8.06	8.48	8,85	9:30	9.65
Meadow Sreett Foot Bridge	16445	22520		treet Foot B	intercontential intercept in the content in the con	Anni de la company de la compa		0.40
Bm55-mod	16455	22510	7.37	8.04	8.46	8.83	9.28	9.63
BM57-mod	16680	22285	7.06	7.72	8.13	8.50	8.93	9.27
BM5.6	16785	22180	6.91	7.56	7:97	8.33	8.77	9.11
Bm55-mod	17080	21885	6.45	7.08	7.48	7.84	8.26	8.59
BM55-54	17240	21725	6.19	6.83	7.23	7.58	7.99	8.32
BM54 🤇 🦿	17300	21665	6.14	6.77	7.16	7.51	7.92	8.25
CD10	17325	21640	6,10	6.72	7.12	7.47	7.88	8.20
Winstaly Street Bridge	17338	21627	Winstanly	Street Foot	Bridge and	Weir	TOTAL CONTRACTOR OF THE PERSON AND T	
CD09	17355 /	21610	6.08	6.66	7.03	7.37	7.79	8.13
BM52	17540	21425	5.82	6.35	6.71	7.03	7.44	7.76
CD07:	17765	21200	5.46	5.98	6.34	6.66	7.09	7.39
BM50-49-ALS	17850	21115	5.28	5.83	6.19	6.49	6.88	7.22
CD06	17920	21045	5.04	5,56	5.93	6.26	6.65	6.95
Old Cleveland Road	17935	21030	Old Clevel	and Road b	ridge and V	Veir		pranting and the second
CD05	17960	21005	5.04	5.55	5.94	6.26	6.63	6.92
CD04	18025	20940	4.86	5.46	5.83	6.17	6.58	6,90
BM47-mod	18065	20900	4.78	5.41	5.79	6.13	6.54	6.87
BM46-mod	18110	20855	4.75	5,37	5.76	6.10	6.49	6.84
CD02	18320	20645	4.64	5.25	5.62	5,96	6.36	6:70
BM44 mod	18495	20470	4.53	5.13	5.51	5.84	6.25	6.57
BM43-mod	18690	20275	4.44	5.03	5.39	5.72	6.12	6.44
BM42-mod	18995	19970	4.32	4.89	5.25	5.56	5.95	6.26
BM41-mod	19165	19800	4.24	4.81	5.16	5.48	5.86	6.17
BM41 copy	19195	19770	4.22	4.79	5.14	5.45	5.83	6.14
Scrub Road Foot Bridge	19205	19760	ALTERNATION AND STREET	d Foot Brid	ge and Wei	T		
BM41	19215	19750	4.21	4.78	5.13	5.45	5.82	6.14
BM5GHD	19375	19590	4.14	4.70	5,04	5.35	5.72	6.03
**************************************	19640	19325	3.97	4.48	4.80	5,09	5.43	5.72
BM6GHD		18915	3.78	4.27	4.56	4,82	5,13	5.40
Bm7GHD	20050 20260	18705	3.72	4.19	4.47	4,72	5.03	5.30
BM8GHD copy	LUZUU.	TO / 02	J.14	F. L.	1. 1.	A T AM		

Branch name & Cross section	MIKEII		Design Eve	nt flood lev	els (Ultimat	te) in mAH	D	occupió i manere de estación cum
ID	Chainage	AMTD(m)	2 yr	5 yr	10yr	20 yr	50 yr	100 yr
	(m) 20270	18695	Proceedings and proceedings and proceedings and proceedings and proceedings are proceedings and proceedings and proceedings are proceedings are proceedings and proceedings are proceedings and proceedings are proceedings are proceedings ar	Commence and the second	idge and W	emanuse manistration		
Meadowlands Road Bridge	Separation and the second	18675	3.71	4.17	4.44	4.67	4.93	5.15
Bm8GHD	20290	1		4.14	4.40	4.62	4.87	5.08
BM9GHD	20510	18455	3.68	4.14	4.29	4.50	4.75	4.96
BM37	20850	18115	3.58			4.42	4.68	4.88
BM17GHD	21090	17875	3.50	3.95	4.21	4.42	4.56	4.78
BM18GHD	21555	17410	3.35	3,80 3,67	4.06 3.93	4.29	4.46	4,69
BM19GHDcopy	21875	17090	3.22			<u>L</u>	4,40	1.02
Preston Road Foot Bridge	21885	17080		Lumenimeniment management	dge and W	A. (2. (2. (2. (2. (2. (2. (2. (2. (2. (2	115	160
BM19 GHD	21895	17070	3.21	3.66	3.92	4.16	^\ 4.45	4.68 4.54
MHG170	22305	16660	3.09	3.52	3.77	4.01	<u></u> 4.31	-
BM23GHD	22775	16190	2.95	3.37	3.62 <	3.86	4.16	4.40
MHG160	23165	15800	2:.85	3.26	3.52	3.76	4.07	4.32
BM10GHD	23285	15680	2.84	3.25	3:51	3.75	4.06	4.31
BM11GHD	23 600	15365	2.81	3.22	3.48	3.72	4:03	4.27
ALS23900	23 900	15065	2.79	3.20	3.45	3,69	4.00	4.25
Minnippi connection	24000	14965	2.78	3.19	3.45	3.69	4.00	4.25
BM13a	24695	14270	2.69	3.11	3.37	3.61	3.92	4.17
BM13GHD	24890	14075	2.64	3.05	3.30	3.54	3.85	4.10
MHG19-old	25515	13450	2.49	2.88	3.12	3.35	3.65	3.88
MHG20-old	25565	13400	2:49	2.87	3.11	3.34	3.64	3.87
BM26_MHG150 🤇 🐇	25865	13100	2.43	2.81	3.05	3.28	3.58	3.81
Wynnum Road Weir	25885	13080	Wynnum I	load bridge	and weir	Superioren minimisco de para la compansa de la compansa del compansa de la compansa de la compansa del compansa de la compansa	grammara-makena marana	
BM 26 copy	25905	13060	2.37	2.71	2.92	3.11	3.37	3.57
MHG-140	26015	12950	2.33	2.66	2.87	3.06	3.32	3.52
BM24	26145	12820	2.29	2.60	2,80	2.98	3.23	3.42
ВМ23	26365	12600	2.23	2.52	2.71	2.89	3.13	3.31
Murrarie connection	26550	12415	2.19	2.47	2.66	2.84	3.08	3.26
BM22	26620	12345	2.18	2.47	2.65	2,83	3.07	3.25
ВМ22 сору	26710	12255	2.17	2.45	2,63	. 2.81	3.05	3.23
Murarrie Road Weir	26730	12235	Murarrie)	Road bridge	and weir			
BM22 copy	26750	12215	2.12	2.38	2,54	2.71	2.94	3.13
MHG-120	26780	12185	2.11	2.37	2.54	2.70	2.93	3.12
BM22 copy	26940	12025	2.09	2.35	2.51	2.67	2.89	3.08
Gateway Motorway	26950	12015	Gateway N	CONTRACTOR				
BM42AGHD copy	26990	11975	2.07	2.31	2.48	2.64	2.87	3.07
BM42A-mod	27100	11865	2.06	2.31	2.47	2.63	2.85	3.05
BM42AGHD copy	27300	11665	2.04	2.27	2.43	2.58	2.79	2.98
	27305	11660	2.04	2.27	2.43	2.58	2.79	2.98
Murrarie connection	27355	11610	2.03	2.26	2.41	2.56	2.77	2.96
BM42AGHD	1	1	1.93	2.14	2.29	2.44	2.65	2.85
BM43AGHD	27755	11210	1.90	2.14	2.26	2.41	2.62	2.82
LC	27912	11053	· §	1		2.40	2.62	2.81
BM44AGHD	28025	10940	1.89	2.11	2.25	2.40	2.60	2.80
BM44BGHD	28815	10150	1.85	2.08	2.23	<u> </u>	2.60	2.80
LC	28855	10110	1.85	2.08	2.23	2.39		2.81
LC.	28930	10035	1.85	2.08	2.24	2.40 2.40	2.61	2.82
BM43BGHD	29075	9890	1.84	2.08	2.24	4×30	I ~. OZ	2.02

Branch name & Cross section	MIKE11		Design Eve	nt flood lev	els (Ultima	te) in mAH	D	
ID	Chainage (m)	AMTD(m)	2 yr	5 yr	10yr	20 yr	50 yr	100 yr
LC	29150	9815	1.84	2.08	2.24	2.40	2.62	2.82
LC.	29325	9640	1.84	2.08	2.24	2,40	2.62	2.83
LC	29420	9545	1.84	2.08	2.24	2.40	2.62	2.83
LC	29652	9313	1.82	2.07	2.23	2.40	2.62	2.82
BM43CGHD	29730	9235	1.82	2.07	2.23	2.39	2.61	2.82
BM43CGHD	30635	8330	1.75	2.02	2.18	2.35	2.57	2.78
LC	30800	8165	1.73	1.99	2.15	2.32	2.55	2.75
BM45GHD	31600	7365	1.65	1.92	2.09	2:27	2.50	2:71
ĹĊ	31740	7225	1.64	1.90	2.08	2.26	^ 2.49	2.71
BM46CGHD	32110	6855	1.57	1.83	2.01	2:20	2.45	2.67
BM46BGHD	32355	6610	1.54	1.82	2.00 <	2.19	2.44	2.66
LC	32650	6315	1.55	1.82	2.01	2.19	2.44	2.66
BM46AGHD	33330	5635	1.48	1.77	1:97	2.16	2.42	2.64
BM52 GHD copy	34300	4665	1.40	1.72	1.92	2.12	2:38	2.61
BM52 GHD copy	34490	4475	1.40	1.70	1.91	2.11	2.37	2.60
Cleveland Rail Bridge	34500	4465	Cleveland	Road Bridg	e and Weir	S		
BM52 GHD	34510	4455	1.34	1.62	1.80	1.99	2.22	2.43
BM52 GHD copy	34700	4265	1.28	1.57	1.76	1.95	2.20	2.41
BM52 GHD copy	35260	3,705	1.26	1.49	1.66	1,84	2.08	2.29
BM52 GHD copy	35670	3295	1.22) 1.42	1.57	1.73	1.94	2.13
Lytten Road	35680	3285	Lytton Roz	d Bridge a	nd Weir			
BM6 copy	35690	3275	1.19	1.36	1.50	1.64	1.83	2.00
BM48	35785	3180	1.17	1.33	1.46	1.59	i.77	1.94
Bm4	36370	2595	1.14	1.27	1.37	1.48	1.64	1.79
BM3	37040	1925	1.09	1.19	1.27	1.35	1.47	1.59
BM2 copy	37465	1500	1.08	1.14	1.20	1.26	1.36	1.46
BM2	38070	895	1,04	1.07	1,11	1.15	1.21	1.27
BM1	38610	355	1.02	1.03	1.05	1.06	1.09	1.12
Brisbane River Boundry	38965	0	1.00	1.00	1.00	1.00	1.00	1.00
Bulimba-East Branch								
BE289	0	6280	55.58	55.71	55.77	55.83	55.90	55.93
BE289	60	6220	55.50	55.62	55.69	55.75	55.82	55.85
BE288	170	6110	54.48	54.64	54.70	54.76	54.83	54.84
BE287	250	6030	53.58	53.64	53.70	53.76	53.84	53.93
BE286	388	5892	52.91	53.09	53.19	53.27	53.38	53.39
BE285	525	5755	52.01	52.11	52.19	52.27	52.35	52.47
BE284	612	5668	51.07	51.16	51.23	51.29	51.35	51.44
HEC2146	660	5620	50,43	50.51	50.56	50.61	50.67	50.74
BE283	708	5572	50.13	50.22	50.27	50.32	50.38	50.44
HEC2030	755	5525	49,95	50.10	50.17	50.22	50.29	50.34
Acres were a	+	1	· · · · · · · · · · · · · · · · · · ·	50.08	50.15	50,20	50.27	50.32
BE283 copy	799	5481	49.93	20:00	10:10	30.20	1 20.21	<u></u>

Branch name & Cross section	MIKE11	eroomaly points of the temposylete inte sseen	Design Eve	nt flood lev	els (Ultimai	te) in mAH	D	<u> </u>
ID	Chainage	AMTD(m)	2 yr	5 yr	10yr	20 yr	50 yr	100 yr
	(m) 820	5460		Road culver	······································	THE PROPERTY OF SECURITY OF SECURITY OF	Laurent de la company de la co	
Beenleigh Road Culverts	835	5445	49.49	49.80	49.95	50.07	50.22	50.27
BE281DS	840	5440	49.52	49.80	49.95	50.07	50.22	50.27
BE280	040	J110	1	Rail Culver	AND THE PERSON NAMED IN COLUMN TWO PARTY OF TH	CONTRACTOR OF THE PARTY OF THE	Compression and Compression of the Compression of t	Santa anno anno anno anno anno anno anno
Beenleigh Rail Culverts	0.11		49.52	49.80	49.95	50.07	50.22	50.27
BE279HEC	844	5436		49.44	49.65	49.88	50.12	50.20
BE278	852	5428	49.14 49.12	49.44	49.64	49.87	50.11	50.19
BE277-HEC	875	5405 5404		Road Pipe (Carrie and Association Control		L.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	***************************************
Beenleigh Road Culvert-2	876	5404		48.29	48.39	48.48	48.57	48.68
BE Rail bypass	930	5350	48.09	48.29	48.37	48.45	48.55	48.66
BE277-HEC DS	946	5334	48.07		48.38	48.47	48.56	48.67
BE277-A	956	5324	48.08	48.28	1,000	48:45	\48.54	48.65
BE277-A copy	978	53.02	48.07	48.26	48.36		48.55	48.66
XS-7450	981	5299	48.06	48.26	48.37	48.45	48.53	48.64
XS-7460	991	52.89	48.04	48.24	48.34	48.43	48.53	48.64 48.60
Xs-7480	1011	52.69	48.00	48.20	48.31	48.39		
XS-7500	1031	5249	47.96	48.16	48.27	48.36	48.45	48.57
XS-7520	1051	5229-	47.92	48.13	48.23	48.32	48.42	48.53
XS-7540	1071	5209	47.89	48.10	48.20	48,29	48.39	48.50
XS-7560	1091	5189	/47.86	48,07	48.17	48.26	48.36	48.47
Xs-7580	nu \	5169	47.84	48.04	48.15	48.23	48.33	48.44
Xs-7600	1131	5149	47.81	48.01	48.11	48.20	48.29	48.40
Xs-7620	1151	5129	47.76	47.97	48.07	48.15	48.25	48.36
XS-7640	1171	5109	47.70	47.90	48.00	48.09	48.19	48.29
XS-7660	1191	5089	47.57	47.76	47.86	47,94	48.03	48.14
XS-7680	1211	5069	47.33	47.54	47.64	47.73	47.83	47.94
Xs-7700	1231	5049	47.22	47.43	47.53	47.61	47.71	47.81
XS-7720	1251	5029	47.09	47.28	47.37	47.45	47.54	47.64
XS-7740	1271	5009	46.89	47.06	47.14	47.21	47.30	47.39
xs-7760	1291	4989	46.66	46.82	46.91	46.98	47.07	47.16
Xs-7780	1311	4969	46.46	46.65	46.74	46.81	46.91	47.00
XS-7800	1331	4949	46.38	46.55	46.64	46,72	46.82	46.90
Xs-7810	1341	4939	46.36	46.54	46.63	46.71	46.81	46.90
BE273	1355	4925	46,34	46.51	46.60	46.68	46.78	46.87
BE Rail Bypass	1380	4900	46.29	46.44	46.53	46.61	46.71	46.80
BE272	1498	4782	45.85	45.95	46.01	46.08	46.17	46.23
BE272	1565	4715	45.38	45.49	45.56	45.63	45.71	45,77
BE271_ALS	1600	4680	45.23	45.35	45,42	45.49	45.56	45.64
BE270	1730	4550	44.40	44.61	44.72	44.81	44.93	45.03
BE269	1915	4365	43.64	43.89	44.03	44.15	44.31	44.43
E	2020	4260	43.01	43.30	43.46	43.59	43.77	43.91
BE268	2145	4135	42.38	42.61	42,75	42.87	43.02	43.14
BE267	2245	4035	41.77	41.92	42.02	42.11	42.23	42.32
BE266		3870	40.56	40.70	40.78	40.87	40.97	41.06
BE265	2410	1	40.00	40.14	40.78	40.27	40.35	40,42
BE264	2500	3780	1	38.99	39.10	39.20	39.42	39.53
BE263	2605	3675 3515	38.78 37.25	37.63	37.89	38.15	38.59	38.73
BE262	2765	3515		d Road Cul	<u> Barrier de la companya del companya de la companya del companya de la companya </u>	kama managa ka		Žennus siirinis saar
Underwood Road Culverts	2767	3513		37.56	37.78	37.98	38.43	38.59
BE261	2785	3495	37.22	1 37:30	1 37.70	2,.,0	1	I

Branch name & Cross section	MIKE11		Design Eve	ent flood lev	els (Ultima	te) in mAH	D	enggenedidade gist sindatowerson-betromen with a ben
ID	Chainage (m)	AMTD(m)	2 yr	5 yr	10yr	20 yr	50 yr	100 yr
DEGCO	2990	3290	36.56	36.86	37.04	37.20	37.38	37.56
BE259 BE258	3200	3080	35:30	35.64	35.82	35.97	36.12	36.29
BE257	3320	2960	34.59	34.93	35.11	35.24	35.36	35.50
Gateway Motorway Culverts	3330	2950	<u> </u>	<u> </u>	ulverts and	Weir	Emmercanian Company	Economic de maria de la composition della compos
BE257 copy	3425	2855	34.58	34.91	35.09	35.22	35.35	35.49
	3490	2790	34.28	34.58	34.76	34.89	35.01	35.13
BE256 BE255	3670	2610	32.75	32.97	33.12	33.24	33.41	33.60
BE255 copy	3695	2585	32.41	32.63	32.79	32.94	33.15	33.38
BE255 copy -mod	3725	2555	31.76	32.06	32.32	32.57	^ 32.88	33.19
Trib B start	3726	2554	31.75	32,08	32.35	32.59	32.89	33.20
	3735	2545	31.69	32.08	32.37 <	32.66	32.96	33.23
BE254 copy BE254	3745	2535	31.68	32.08	32.36	32,67	32.98	33.26
Logan Road Culvert	3748	2532	A	d Culvert a	Z.		Selection of the select	I.
	3785	2495	31.15	31.43	31.62	31.81	32.04	32.22
BE253	3810	2470	31:14	31.43	31.62	31.80	32.02	32.21
Interpolated			31.11	31.39	31.58	31.77	31,99	32.18
Trib B end	3888	2392	31.06	31.34	31.53	31.73	31.96	32.14
BE251	3925		31.00	31.06	31:30	31.53	31.80	32.00
Be250	4020	2260	<u> </u>	31.00	31.05	31.35	31.65	31.85
BE249	4110	2170	30.26	30.70	30.97	31.30	31.60	31.81
BE248	4230	2050	30.08		30.97	31.29	31.60	31.80
Trib A_DS	42.84	1996	30.04	30.58 30.56	30.96	31.28	31.59	31.80
BE247	4300	1975		torway Cul	Annual and a second	51,25		
Pacific Motorway Culverts	4305		29.74	30.04	30.21	30.39	30.64	30.86
BE247 copy	4360	1920	!	29.79	29.98	30.17	30.42	30.66
BE246	4419	1861	29.45			29.73	30.01	30.26
BE246A-ALS	4507	1773	28.99 28.51	29.34 28.86	29.53 29.04	29.73	29.63	29.92
Old4612	4602	1678	f		way Access	Marine and American Street, Sans		
Eight Mile Plains Bridge	4608	1672	***********	CONTRACTOR	Section of the sectio	1	29.39	29,69
Copy Old 4612	4638	1642	28.15	28.57	28.81 28.75	29.06 28.99	29.33	29.63
BE244	4656	1624	28.09	28.51	and the second second second		47,JJ .	22.05
Miles Platting Road Bridge	4660	1620	Name and Association of the Party of the Par	Annual management of the second	ridge and V	A THE OWNER WHEN THE PARTY OF T	20.17	20.34
Old 4665	4695	1585	28.04	28.43	28.65	28.87	29.17	29.44
Old 4685	4730	1550	27.90	28.27	28.47	28.68	28.96	29.22
Old 4705	4750	1530	27.89	28.27	28.49	28.70	28.99	29.25
BE241	4870	1410	27,65	28.02	28.23	28.45	28.74	29.00
BE240	4980	1300	27.33	27.72	27.95	28.18	28.48	28.76
Gateway Off-ramp	5010	1270			idge and W			
BE239	5050	1230	27.09	27.42	27.60	27.79	28.03	28.24
BE238	5175	1105	26.76	27.08	27.26	27.45	27.69	27.90
BE236	5330	950	25.97	26.35	26.55	26.74	27.02	27.24
BE235	5470	810	24.98	25.47	25.73	25.95	26.27	26.53
BE232	5712	568	24.08	24.50	24,74	24.96	,25.26	25.52
BE231	5810	470	23.79	24.20	24.44	24.66	24.95	25.21
BE230	5895	385	23,45	23.85	24.10	24.32	24,63	24.88
BE229	5975	305	23.14	23,58	23.85	24.09	24.40	24.66

Branch name & Cross section	MIKEII		Design Eve	ent flood lev	els (Ultima	te) in mAH	D	-do-scret-demonstration description of the screen and screen
ID	Chainage	AMTD(m)	Commitment of the State of the	The state of the s	10yr	20 yr	50 yr	100 yr
	(m)	225	2 yr 22.91	5 yr 23.39	23.68	20 yı 23.93	24.24	24.51
BE228	6055	1	1	<u> </u>	23.54	23.79	24.10	24.36
BE227	6135	145	22.75 22.62	23.23	23.41	23.66	23.97	24.23
BE227	6280	0	-furnimentalization	1	22,771	45.00	Consequence and the consequence of the consequence	Ensurant market and the second
Tributary A		A CONTRACTOR OF THE PARTY OF TH	Tributary	Tarana da la company de la La company de la company de	£3.47	52.60	52.76	52.82
ALS1-copy	0	_	51.96	52.32	52.47		52.45	52,65
ALS1-copy	100		51.71	52.06	52.20	52.31	ğ	51,67
ALS1	320	<u> </u>	50.81	51.07	51.18	51.33	51.48	
ALS2	600		46.69	46.88	47.03	47.16	47.35	47.58
BE-1060	950		44.85	45.02	45.08	45.13	^ 45.19	45,27
BE-1040	1400	<u> </u>	41.05	41.19	: 41.28	41:37	41.46	41.52
BE-1030	1770	ļ	37.23	37.45	37.58	37.71 <	37.87	38.04 36.54
BE-1020	2070	Andrea (and and and and and and and and and and	34,79	35.16	35.45	_35 <i>i</i> 75	36.09	30.34
School Road	2072		Parameter and the second	d to Freew	Seatmonness contrarament of the	Summummummensumm		
interpolated	2125		34.71	35.00	35.18	35.33	35.52	35.68
Interpolated	2163	:	34,66	34.95	35,13	35.28	35.47	35.62
BE-1010	2235		34.20	34.52	34.72	34.89	35.09	35.25
BE-1005	2535		32.19	32.60	32.90	33.19	33.57	33.77
Freeway Off-ramp	2545			ff-ramp Cu	Range and the same a	Incompanies de la companie de la com		<u> </u>
BE-1005	2555		/ 32.12	32.51	32.74	32.96	33.25	33.45
BE1005 copy	2735		31,17	31.52	31.76	32.04	32.38	32.66
BE1000	2765		30.47	30.98	31.38	31.78	32.19	32.50
Gateway Motor way	2805		Gateway N	Iotorway C	ulverts and	Weir		
BE1000 modified	2935		30.42	30.92	31.30	31.65	31.98	32.19
BE1000 modified	3015		30.09	30.60	30.99	31.32	31.64	31.84
BE1000 modified	3021		30.07	30.58	30.97	31.29	31.60	31.80
Tributary A1	Y		Tributary	Al	general programme of the control of			
A1-1050	0		49.72	50.01	50.16	50.28	50.42	50.47
A1-1050	280		48.91	49.11	49.21	49.30	49.42	49.43
ALS	500		44.50	44.65	44.74	44.83	44.94	44.96
ALS	720		41.06	41.20	41.30	41.38	41.48	41,54
ALS	750		41.05	41.19	41.28	41.37	41.46	41.52
Tributary A2			Tributary.	A2				
TRIB A2	0		44.93	45.07	45.13	45.18	45.25	45.27
SMP	80		44.55	44.66	44.72	44.76	44.82	44.83
SMP	475		40.27	40.36	40.44	40.51	40.59	40.71
SMP	690	1	38.69	38.80	38.87	38.92	38.99	39.08
SMP	1035		34.66	34.96	35.13	35.29	35.47	35.63
SMP	1042		34.66	34.95	35.13	35.28	35.47	35.62
Tributary B			Tributary	bernamentali	herene manierani minis			
BE2030	1000		36,12	36.37	36.51	36.80	36.88	36.91
BE2030	1055	<u> </u>	35.09	35.44	35.63	35.71	35.99	36.04
Dance Court 1	1062		I	rt Culvert :	Santana and the santana and th	***************************************	annan mananan maraka	Consumer of the Consumer of th
			34.56	34.85	34.98	35.07	35.21	35.24
BE2030 copy	1075		34.30 34:33	34.51	34.61	34.69	34.78	34.83
BE2020	1215		1	33.51	33.64	33.74	33.84	33.96
BE2020 copy	1340		33.36 33.27	33.41	33.52	33.62	33.72	33.84
Interpolated	1360	<u> </u>	33.41	7-14-1	المكاف و ليرو	سکان با		

Branch name & Cross section	MIKEII		Design Eve	ent flood lev	els (Ultima)	e) in mAH	D	
ID	Chainage (m)	AMTD(m)	2 yr	5 yr	10yr	20 yr	50 yr	100 yr
Logan Road Culverts	1361			ad Culveri	Commence of the contract of the party of the contract of the c	Continue of the Continue of th		
BE2010	1394		32.92	33.02	33.09	33.15	33'.23	33.35
BE2000	1432		31.16	31.43	31.61	31.79	32.01	32.19
BE2000	1492		31.11	31,39	31.58	31.77	31.99	32.18
Tributary C	11/2		Tributary	American menter alla anticolor della constantica della constantica della constantica della constantica della c				
	0		49.14	49.23	49.27	49.31	49.36	49.37
BE-3050	10		49.09	49.15	49.19	49.23	49.28	49.34
BE-3050	·		46.73	46.86	46.94	47.00	47.08	47.13
BE-3040	390 545	 	45.48	45.57	45.64	45.70	△ 45.77	45.80
BE-3030	4		44.29	44.41	44.49	44.57	44.66	44.74
BE-3020	665		42.62	42.75	42.84	42.92	43.02	43.10
BE-3010	810		4	39.37	39.47	39.56	39.65	39.73
BE3000	1000		39.21 38.50	38.50	38:50	38.55	38.95	39.11
BE-3000 copy	1005			Pipe Culve	AND THE PROPERTY OF THE PARTY O	AND DESCRIPTION OF THE PERSON NAMED OF THE PER	1 20.55	
Gateway Culvert	1008				38.22	38.48	38.90	39.04
ВЕ3000 сору	1100		37,58	37.97		38.49	38.91	39.05
ALS	1110		37.58	37.98	38.22	38.48	38.91	39.04
ALS	1120		37.58	37.97	38.22	30.40	30.71	12.04
Tributary BI			Tributary		200	72./0	22.70	72.04
ALS	1000		33.27	33.41	33.52	33.62	33.72	33.84
AIS	1002		33.17	33.30	33.42	33.51	33.61	33.74
ALS (1020	7	31.99	32.19	32.37	32.62	32.92	33.23
ALS	1055		31.75	32.08	32.35	32.60	32.90	33.21
ALS	1140		31.75	32.08	32.35	32.59	32.89	33,22
ALS	1145		31.75	32.08	32.35	32.59	32.89	33,20
Padstow Branch	10/1/20		Padstow l	Branch	200000000000000000000000000000000000000			
BM177	0	,	34.27	34.52	34.71	34.92	35.17	35.35
BM177	32		34.21	34.47	34.66	34.88	35.14	35.32
BM177-176ALS	105		33.89	34.25	34.52	34.79	35.08	35.26
BM176-US-ALS	175	. 1	33.52	34.10	34.43	34.74	35.04	35.23
Padstow Road			Padstow l	Road Culve	erts and W	eir		
BM176-DS-ALS	205		33.42	33.82	34.01	34.20	34.46	34.68
BM175	258		33.37	33.79	33.97	34.17	34.44	34.67
BM175-174ALS	325		33.27	33.72	- 33.92	34.13	34.41	34.64
BM174	352		33.23	33.70	33.91	34.12	34.40	34.63
BM175	375		33.21	33.68	33.89	34.11	34.39	34.62
Garden City		***************************************	Garden C	City Brancl	1			
BM169	5280		29.94	30.45	30.75	31.16	31.81	32.34
BM169	5285		29.94	30.44	30.74	31.16	31,81	32.34
BM168	5405	1	29.78	30.26	30.54	30.99	31.70	32:25
BM167	5510		29.43	29.99	30.35	30.86	31.61	32.19
BM165 copy	5615		29.09	29.81	30.24	30.80	31.57	32.16
	5715		28.80	29.37	29.78	30.24	30.72	30.98
BM165 copy			28.76	29.35	29.77	30.23	30.72	30.97
Bm165	5730 5785		28.51	29.18	29.66	30.16	30.67	30.92
XS5-Logan Road survey	1 2/03	1	1 20,21	I			Sancer in the Contract of the	Sections

Branch name & Cross section	MIKE11		Design Eve	ent flood lev	els (Ultima	te) in mAH	D	***************************************
ID	Chainage	AMTD(m)	THE RESERVE THE PROPERTY OF THE PERSON NAMED IN COLUMN TWO IS NOT THE PERSON NAMED IN COLUMN TWO IS NAMED IN COLUMN TWO I	THE RESERVE TO SERVE THE PARTY OF THE PARTY	10yr	20 yr	50 yr	100 yr
	(m)		2 yr	5 yr	Contraction of the Contraction o	LU YI	30 yr	XOO YL
Logan Road	5790	THE PROPERTY OF THE PROPERTY O	28.43	ad culvert 28.98	29.27	29.54	29.90	30.20
XS4-logan-survey	5850		28.43	28.98	29.27	29.48	29.82	30.08
XS4 copy	5935 5938		28.38	28.93	29.22	29.48	29.82	30.07
XS4 copy	1 3230		Mimosa (Armenia de la compansión de				
Mimosa Creek	_	50000	54.81	55.08	55.22	55.35	55.51	55.56
Start of model	0	58880		1	55.20	55.32	55.47	55.53
Mi 40 Hecras	5	58875	54.79	55.06 54.55	54.67	54.77	54.91	54.95
Mi 40a	96	58784	54.32			***************************************	54.14	54.25
Mi39	200	58680	53.60	53.75	53.88	54.00 53.15	53.29	53.44
MI38	330	58550	52.68	52.89	53.03	51.69	51.83	52.01
Mi37	484	58396	51.23	51.63	51.57		g	51.74
Mi36	506	58374	50.98	51.33	51:30	.51\42 32	51.57	ğ
Mi35	558	58322	50.55	50.93	50,90	51.02	\$1.17	51.32
Mi34	660	58220	49.88	50.30	50.27	50.38	50.52	50.64
Mi33	696	58184	49,64	50.10	50.07	50.18	50:31	50.45
Mi32	811	58069	48.95	49.56	49.49	49.65	49.83	49.97
Mi31	952	57928	48.33	48.85	48.77	48.94	49.14	49.24
Мі31-сору	1037	57843	47.88	48.33	48,27	48.42	48.61	48.71
Mi29	1186	57694	46.79	47:31	47.26	47.41	47.60	47.76
Mi28	1302	57578	46.02	46.71	46.63	46.83	47.07	47.28
Mi27	1322	57558	45.88	46.62	46.54	46.75	46.99	47.21
Mi26	1366	57514	45.78	46.54	46.45	46.67	46.91	47.13
Mi25	1439	57441	45,58	46.32	46.24	46.45	46.69	46.89
Mi24	1549	57331	44.86	45.64	45.53	45.78	46.01	46.19
Mi23	1588	57292	44.68	45.48	45.37	45.62	45.86	46.04
Mi22	1719	57161	44.11	44,82	44.75	44.97	45.21	45.36
Mi21-2	1738	57142	43,95	44.64	44.57	44.82	45.11	45,27
Nagel Street Bridge	1739	57141	Nagel Stre	et Bridge ar	id Weir			
Mi21-1	1752	57128	43.85	44.49	44.44	44.61	44.92	45.11
Mi20	1762	57118	43.74	44.40	44.35	44.53	44.82	45.02
Mi19	1882	56998	43:10	43.77	43.71	43.92	44.23	44.48
Mi19-4	1892	56988	43.07	43.75	43.68	43.89	44.20	44.45
Pacific Motorway Culverts	1895	56985	Pacific Mo	torway Cul	verts			
Mi19-1	1964	56916	42.67	43.21	43.24	43.42	43.65	43.85
Mi18	2023	56857	42.42	42.85	42.93	43,10	43.31	43.51
Mi17	2086	56794	41.96	42.40	42.48	42.67	42.89	43.08
	2133	56747	41.59	42.12	42.21	42.43	42.68	42.89
Mi16	2224	56656	40.95	41.46	41.54	41.78	42.06	42.26
Mi15 Mi13-3	2248	56632	40.81	41.34	41.43	41.70	41.99	42.19
	22.55	56625	e Securitarismi construction in the con-	ad Bridge a	Contraction and Contraction of the Contraction of t	Second to the second se	Economic de la company	
Kessels Road Bridge		CONTRACTOR OF THE PARTY OF THE	40.77	41.27	41.35	41.54	41.75	41.93
Mi13-2	22.84	56596	•	1		41.39	41.60	41.77
Mi13	2325	56555	40.65	41.13	41.21		40.55	40.74
Mi12	2516	56364	39.62	40.05	40.13	40.32 39.62	40.33 39.87	40.07
Mill	2635	56245	38.87	39,33	39.42	J7.U4	J9.07	70.07
Parkway Street Bridge	2648	56232	หรื องเพาะเกษาจากการเกราะการเกราะการ	treet bridge		20.45	39.67	39.84
Mi10-2	2664	56216	38.79	39.19	39.28	39,45	לס.ענ /	33.04

grammoning configuration in the configuration of th	MIKEII		Decim Kye	ent flood lev	els (Ultimat	te) in mAH	D	
Branch name & Cross section ID	Chainage	AMTD(m)	Compression more amount distance in		ATTENDED BY THE PROPERTY OF THE PARTY OF THE	20 yr	50 yr	100 yr
	(m)		2 yr	5 yr	10yr		<u> </u>	39.57
Mi9	2718	56162	38.59	38.95	39.03	39.20 38.59	39.40 38.81	38.97
MI8	2828 2955	56052 55925	37.88 37.40	38.29 37.90	38.39 38.03	38.23	38.47	38:62
Mi7	3069	55925	37.40	37.56	37.68	37.86	38:08	38.24
Mi6	_		36.49	36.97	37.09	37.26	37.44	37.61
Mis	3221	55659	1	36.29	36.44	36.64	36.88	37.07
Mi4	33.88	55492	35.79	35.86	36.01	36.22	36.46	36.65
Mi3	3496	55384	35.41		35.61	35.80	36.02	36.19
Mi2	3585	55295	35.08	35.48		34.70	34.94	35.12
Mi1	3801	55079	33.96	34.38	34.52		34.43	34.66
Bulimba Main merge	3880	55000	33.23	33.71	33.92	34.14	94.43	34.00
Minnippi Bypass Branch				ypass Bran	gazno crossara anno mano mano mano mano mano mano man		1	105
Start	0		2.78	3.19	3.45	_/3:69	4.00	4.25
Minnippi_newl	80		2.78	3.16	3,40	3.64	3.96	4.22
Minnippi_new2	125		2.78	3.15\	3.40	3.64	3,96	4.21
Minnippi_new3	230	Ą.	2.77	3.12	3.36,/	3.61	3:94	4.19
Minnippi_new4	400		2.77	3:05	3.31	3.58	3.92	4.18
Minnippi_new5	542	and the same of th	2.76	3.00	3.27	3.55	3.90	4.17
ALS	650	, 10 m	2.76	2.97	3,26	3.54	3.89	4.16
Stanton Road	710		Stanton Ro	ad overfloy				*****
New A	720	Y	2,56	2.95	3.22	3.47	3.77	3.98
New B	730	1.5	2.24	2.93	3.20	3.45	3.75	3.96
Minnippi_new6-US	745		2.24	2.93	3.20	3.45	3.76	3.97
Gateway Motorway	748		Gateway N	1otorway C	ulverts			
Minnippi new7-DS	810		2.24	2.93	3.19	3.41	3.66	3,85
New E	825		2,24	2.92	3.18	3,40	3.65	3,83
New G	860	: :	2.23	2.90	3.15	3,38	3,62	3.81
New 7a	870		2.01	2.88	3.14	3.36	3.62	3.80
Minnippi_new8	945		1.92	2.61	2.88	3.13	3.42	3.62
BM31GHD-mod	1015		1.87	2.43	2.71	2.99	3.32	3.53
BM31GHD-mod	1115	1	1.85	2.31	2,60	2.89	3.25	3.47
Wynnum Road				Road Bridge				San and the san
BM31-GHD copy	1150		1.85	2.22	2.41	2.58	2.78	2.96
BM36GHD copy	1310		1.84	2.16	2.34	2.51	2.72	2.91
	1		1.84	2.11	2.28	2.45	2.67	2.86
Minnippi_newl1	1560		1.84	2.09	2,25	2.41	2.64	2.84
BM42BGHD BM42BGHD	1850 2004		1.84	2.08	2,24	2.40	2.62	2.83
	4004	and the second s		Bypass Brai	haanaan aan daa daa daa daa daa daa daa d		Lacoccamonatorico	<u> </u>
Murrarie Bypass		ancolation position and a second second second		2.47	2.66	2.84	3.08	3.26
ALS	0	<u></u>	2.19	·		······································	3.08	3.26
MUI ALS	20		2.19	2.47	2.65	2.83	į	<u> </u>
ALS	35		2.18	2.46	2.65	2.82	3.07	3.24
New_MU2_ALS	160		2.17	2.46	2.64	2.82	3.06	3.24
New_MU3_ALS	275		2.16	2,45	2.64	2.82	3.06	3.24
Murrarie Road	280			Road Bridge	r		,	***************************************
Copy_new_MU3	310		2.16	2.45	2.63	2,81	3.06	3,23
New_MU5_ALS	390		2.15	2.44	2.63	2,81	3.05	3.23

Chainage	MIKE11 Chainage AMTD(m)	Design Event flood levels (Ultimate) in mAHD							
(m)	AMID(III)	2 yr	5 yr	10yr	20 yr	50 yr	100 yr		
470		2.13	2.43	2.62	2.80	3.05	3.23		
475		Gateway N	I'way ME (Culverts					
545		2.06	2.29	2.44	2.59	2.80	2.99		
595	1	2.05	2.29	ļ		<u> </u>	2.99		
640		2.04	2.27	ļ			2.98		
650		2.04	december and the second		2.58	2.79	2.98		
		Bulimba E	ast Rail By	pass		gagagatagagagagagagagagaga	PROBERT CONTRACTOR		
0		48.09	48.29	48.39	48.48	^\ 48.57	48.68		
33		48.00	48.22	48.32	48.41	48.50	48.60		
144		47.80	47.80	47.80 🤄	47.80	47.84	47.94		
226		46.94	47.05	47.21	47. 36	47.53	47.70		
347		46.86	46.95	47.13	47.28	47.46	47.62		
443		46.56	46.61	46:75	₅ 46.86 \	46,98	47.10		
488		46.39	46.44	46.53	46.61	46.73	46.82		
520		46.29	46.44	46.53	46.61	46.71	46.80		
**************************************		Kianawah	Park Branc	eh 🔪 🗦					
0.4		2.67	2.81	2.89	3.09	3.33	3.50		
48		2.65	€2.77	2.87	3.09	3.33	3.50		
210	1000	2.56	2.66	2.87	3.09	3.33	3.50		
260	1	2.55	2.65	2.87	3.09	3.33	3.50		
340	N. V	2.51	2.63	2.87	3.09	3.33	3.50		
430		2.48	2.63	2.87	3.09	3.33	3:50		
530		2.47	2,63	2.87	3.09	3,33	3.50		
660		2.44	2.63	2.87	3.09	3.33	3.50		
780		2.40	2.63	2.87	3.09	3.33	3.50		
		2.27	2,63	2.87	3.09	3.33	3.50		
945		2.13	2.62	2.87	3.09	3.33	3.50		
985		1.99	2.62	2.89	3.13	3.42	3.63		
1006		1.94	2.62	2.89	3.13	3.42	3.63		
	475 545 595 640 650 0 33 144 226 347 443 488 520 0 48 210 260 340 430 530 660 780 860 945 985	475 545 595 640 650 0 33 144 226 347 443 488 520 0 48 210 260 340 430 530 666 780 860 945 985	475 Gateway N 545 2.06 595 2.05 640 2.04 650 2.04 Bulimba E 0 48.09 33 48.00 144 47.80 226 46.94 347 46.86 443 46.56 488 46.39 520 46.29 Kianawah 0 2.67 48 2.65 2.10 2.56 2.60 2.55 340 2.51 430 2.48 530 2.47 660 2.44 780 2.40 860 2.27 945 2.13 985 1.99	475 Gateway M'way ME Co	A75 Gateway M'way ME Culverts	A75 Gateway M'way ME Culverts	A75		

Table I2: Estimated Peak Design Flood Discharges

MIKE11	AMTD(m)	Cross section	MIKE11 N	Iodel Peak I	Discharges	(m^3/s)		
Chainage			2 year	5 year	10 year	20 year	50 year	100 year
Rulimba C	reek:Compt	on Road to Ne		lo <u>san saaritkaanin musaa</u>	and a supplied that the supplied of the suppli	Acres menting a manuscriptor		
0	39900	Start	25.8	37.1	44.0	50.6	59.7	63.7
-65	39835	BM222	25.0	36.2	43.0	49.5	58.5	62.2
175	39725	Bm221	22.9	34.2	40.9	47.3	56.1	59.2
270	39630	вм220	20.3	31.5	37.8	43.9	52.3	54.6
415	39485	BM219	29.2	38.3	46.5	54.5	65.2	73.3
560	39340	BM218	38.0	48.5	57.4	66.2	7.7,8	94,9
736	39164	BM217	38.9	51.2	60.4	69.4	81.5	97.4
900	39000	BM216	39.1	53.3	63.3	72.9	85.8	99.9
935	38965	End	47.5	64.9	77.8	89.8	10,5.3	124.2
NAME OF THE OWNER OF THE OWNER, WHEN THE OWNER	eek-Main Bra	Name and Address of the Owner, which we have a second or the owner, where the owner, which is the owner, where the owner, where t						
0	38965	Start	47.5	64.9	77.8	89.8	∖105.3∖	124.2
. 10	38955	BM 214	46.0	62.6	74,5	86.1	101.4	118.8
17	38948		Nemies Roa	Anne construction of the contract of the contr		Samuel Communication of the Co	taring a second property of	
40	38925	ВМ214 сору	46.6	63.60	75.7	87.5	103.2	120.7
120	38845	BM214 copy	45:4	62.65	74.6	86.3	101.8	118.5
215	38750	BM212	45.7	63\78	76.0	88.0	104.0	120.7
355	38610	BM211	(38.8)	57.66	69.1	80.3	95.4	108.3
Charles Management Comments of the Comments of	38595	13141211	Brandon Ró	Maria Company of the		***************************************		**************************************
370	in a construction of the c	D MOLL comp	44.9	65.9	79.1	92.1	109,4	125.7
385	38580	BM211-copy BM 209	40.3	60.3	73.0	85.7	102.3	115.1
470	38495	BM 208	41.5	57.9	70.5	83.5	100.4	111.6
540	38425	BM 207	43.9	58.5	71.6	85.3	103.4	114.5
600	38365	BM 207	41.4	55.3	65.0	73.8	86.8	100.4
740	38225	BR\1	41.2	55.4	65.2	74.1	85.9	100.9
800	38165	BK71	<u> </u>	ream of Bra	marana manana			
805	38160		Santa de la compansión de	THE PERSON NAMED AND ADDRESS OF THE PERSON NAMED AND ADDRESS O	66.5	75.7	87.8	103.1
825	38140	BR 2	41.8	56.5	72.1	82.3	95.6	112.1
840	38125	BM 205	45.1	61.1	66.0	75.2	87.3	102.2
890	38075	BR_3	40.8	55.9	72.1	73.2 82;4	95.9	112.2
905	38060	BR_4	44.4	61.0	67.7	77.4	90.0	105.1
• 942	38023	BR 5	41.3	57.3		81.9	95.5	111.4
960	38005	BR 5copy	43.4	60.5	71.5 73.2	83.9	97.9	114.1
990	37975	BM204	44.0	61.8	***************************************	***************************************	94.8	110.1
1075	37890	BM 203	40.6	59.0	70.2	80.8 82.2	94.8	112.8
1160	37805	BM 202	40.6	58.5	70.6	76.1	92.4	106.3
1300	37665	BM 201	40.2	53.0	63.8	85.2	104.2	120.1
1365	37600	BM 200	44.0	58.7	71.0		109.4	125.4
1545	37420	BM 199	46.1	63.8	74.8	88.3	109.4	118.7
1670	37295	BM 198	45.0	63.7	75.8	87.3	103.7	116.4
1800	37165	BM340-MHG	41.8	57.7 50.7	71.7	84.7	100.5	121.0
1830	37135	BM 197	43.1	58.7	73.9	87.7	104.0	1.41.11
1845	37120		Beenleigh R				10.50	
1860	37105	ВМ 197 Сору	43,4	58.9	74.1	88.4	105.8	122.4
1900	37065	BM195-I	43.1	58.9	72.9	87.6	105.3	121.9
1940	37025	BM 194	42.4	58.4	70.6	85.8	103.8	120.2
1960	37005	ВМ194 сору	44.3	61.3	74.2	90.3	109.3	126.4

Chainage		\mathbf{p}				(m ³ /s)	30-min	g
CHAMAGO	***************************************		2 year	5 year	10 year	20 year	50 year	100 year
1960	37005	ВМ 194 сору	44.3	61.3	74.2	90.3	109.3	126.4
2045	36920	BM 192	42.6	59.3	69.9	84.7	102.1	117.6
2115	36850	BM 191 copy ⁶	40.6	55.4	65.9	75.5	91.5	105.4
2117	36848	***************************************	St Lawrence	s Foot Bridg	е			***************************************
2125	36840	BM 191	43.9	59.8	71.3	82.4	100.0	115.2
2255	36710	BM190	40.5	53.2	64.4	75.7	91.0	107.8
2370	36595	ВМ188-6 сору	38.4	51.9	62.2	71.8	87.1	104.4
2375	36590		Altandi Stre	et Foot Brid	ge & Weir	·	<u> </u>	
2380	36585	BM188-6	40.8	55.4	66.3	77.2	<94.7	113.2
2470	36495	BM188-2	42.2	57.8	69.4	△ 80.5 △	99.2	118.8
2500	36465	BM188-1	45.2	62.0	74.5	87.9	108.3	129.4
2670	36295	BM187	43.6	59.8	√72.5 <	84.4	\ 102.5	123.2
2785	36180	BM186	44.3	60.3	73.6	86.1	103.0	123.5
2985	35980	BM185	43.8	(59.4	72.3	₹ 85.5	103.1	119.2
3165	35800	BM184	43.1	59.5∖∖	71.2	84.9	103.3	120.6
3295	35670	BM183	43.3	60.0	72.1	84.9	104.0	122.3
3435	35530	BM182	43.8	60.0	72.7	84,3	104.0	123.1
3625	35340	BM181	43.6	59.1	72.3	84.3	102.1	121.5
3765	35200	MHG320	43.1	58.5	71.2	83.8	100.3	118.8
3800		BM180	45.5	62,0	76.0	89.4	107.4	127.6
3960		BM179	48.9	S√67.5	82.7	97.9	118.5	140.5
3970		BM179 copy	\50.7	70.0	86.4	102.2	124.4	147.3
4150		BM178 /	50.4	70.5	85.9	102.3	125.1	145.6
4150	34815	BM179 /	21.4	29.6	37.2	46.4	57.6	63.7
4260	34705	BM177	21.3	29.7	37.5	46.3	58.0	64.5
4320	34645	BM177A	21.3	29.8	37,7	46.3	58.1	64.9
4375	34590	LC	21.5	29.9	37.8	46.3	58.3	65.2
4385	34580	BM176_US	21.5	30.0	37,9	49.2	71.5	87.3
4415	34550	BM176 DS	21.6	30.1	38.0	49.3	71.6	87.5
4460	3 45 05	BM 175	35.5	51.1	60.4	70.8	84.2	99.9.
4515	3:4450	BM175-174	33.3	47.9	56.6	66.3	82.1	65.3
4555	3,4410	LC	32.0	45.2	53.6	62.8	82.6	87.1
4555	34410	LC	66.7	100.2	117.5	142.1	181.6	87.3
4575	34390	LC	66,6	100.1	117.4	142.0	181.5	99.7
4575	34390	LC	89.3	134.5	160.0	189.1	232.7	97.9
4590	34375	BM 174	89.3	134.5	160.0	189.1	232.7	98.5
4700	34265	ВМ173-ВМ174	89.3	134.1	159.9	189.2	232.6	214.2
4765	34200	Interpolated	89.3	134.1	159,9	189.2	232.6	214.1
4780	34185	BM173	89.3	134.1	159.9	189.2	232.6	270.3
4785	34180		Blesby Road	i Foot Bridge	& Weir			
4790	34175	ВМ 173 сору	89.3	134.1	159.9	189.2	232.6	270.2
4905	34060	BM172	89.3	134.3	159.9	189.2	232.5	270.0
4995	33970	BM171	89.2	134.4	159.8	189.1	232.3	269.7
5120	33845	BM170	90.6	136.5	162.6	192.3	235.9	273.5
5280	33685	LC	92.4	139.1	166.0	195.9	239.6	277.7

	AMTD(m)	Cross section	MIKEII N	Iodel Peak I)ischarges ((m³/s)		
Chainage		l D	2 year	5 year	10 year	20 year	50 year	100 year
COOO		Ir A	70.0	99.0	112.3	130.9	156.8	178.9
5280	33685	LC	70.0	99.0	112.3	130.9	156.8	178.8
5285	33680	BM169		99.0	111.8	130.0	155.3	177.2
5405	33560	LC	69.8	<u></u>		138.9	162.3	181.9
5405	33560	LC	69.8	102.6	121.7		161.1	180.7
5520	33445	BM167	69.8	102.2	121.3	138.1	151.3	168.2
5520	33445	LC	69.8	102.2	121.3	134.3		168.1
5615	33350	LC	69.8	101.9	121.2	133.6	151.0	
5615	33350	LC	69.8	101.9	121.2	140.4	17137	199.1
5715	33250	LC	69.8	101.4	121.1	140.1	(17.1.5	199.0
5715	33250	LC	69.8	100:1	119.2	(139.9.	174.4	196.3
5730	33235	BM165	69.8	100.1	1.19.1	//139.9	174.3	196.2
5785	33180	LC.	69.7	100.1	1,19.0	₋ /139.7	174.2	196.1
5785	33180	LC	69.7	10.0:1	119.0	136.0	147.6	150.1
5845	33120	Xsec4	69.7	100.0	118.8	₹ 135.7	147.2	148.9
5902	33063	Xsec3	69.7	99.9	1,18.7	\135.7	147.0	148.6
5918	33047	Xsec2	69.7	99.8 \	<u>,</u> 118.7 \	135.7	147.0	148.6
5935	33030	Xsec1	69.6	99.8	118.8	135.7	147.1	148.7
5938	33027	Garden City	69.6	99.8	1 Ì8.8	135.7	147.1	148.8
5938	33027	Garden City	91.8	136.4	163.3	191.4	233.0	271.4
5985	32980	HEC2937	91/8	13,6:3	163.3	191.5	233.2	271.3
6050	32915\	BM157	√ 91.8√	136.3	163.4	191.5	233.4	271.0
6160	32805	BM156	94,3	139.9	168.0	196.8	239.7	279.2
6240	32725	BM155	96.2	142.5	171.7	200.7	244.6	285.1
6340	32625	BM154	96.2	142.4	171.5	200.7	244.5	284.6
6450	32515	BM153_ALS	96.1	142.2	171.4	200.7	244.6	284.0
6650	32315	BM151	96.0	141.7	171.4	200,6	244.4	284.0
6860	32105	BM149	96.0	141.6	171.2	200.6	242.2	282.4
6930	32035	BM148-BM147	98.0	141.1	171.2	199.1	250.4	298.1
6935	32030			t Foot Bridge	&Weir			
www.comen.com/emergeneenstation	32020	ВМ148 сору	97.4	141.3	171.2	199.3	248.2	295.0
6945	Carionaminaminament commence and the commence of the commence	BM148	96.2	141.8	171.1	200.2	246.3	284.0
6985	31980	BM146	95.8	141.5	170.9	199.8	243.5	283.7
7185	31780	BM144	95.9	141.3	170.8	200.0	243.4	283.4
7420	31545 31475	BM144	95.9	141.3	170.9	200.1	243.3	283.3
7490		ALS-142	97.5	143.4	173.9	203.6	247.1	287.8
7600	31365		97.3	145.4	177.6	207.9	252.3	293.4
7735	31230	BM141	99.4	146.6	178.2	208.5	253.1	293.7
7915	31050	BM139	100.0	147.1	178.7	209.0	253.6	294.3
7985	30980	BM138	<u> </u>	148.3	179.8	210.1	254.7	295.6
8070	30895	BM137	100.9	\$	313.2	362.9	434.3	500.6
8070	30895	Bulimba East	181.5	255.4	312.8	362.7	434.2	500.5
8200	30765	BM136	181.1	255.2	**************************************	362.7	434.1	500.3
8325	30640	BM135	180.6	254.9	312.4	362.2	434.1	500.0
8475	30490	BM134	179.9	254.4	311.8		433.6	499.8
8555	30410	MHG 260	179.5	254.2	311.5	362.0	433.5	499.8
8570	30395	BM132	179.5	254.1	311.4	362.0	4030	72.7.0

	AMTD(m)	ž.	MIKE II M	Iodel Peak I)ischarges ((m^3/s)		
Chainage		<u> </u>	2 year	5 year	10 year	20 year	50 year	100 year
8780	30185	BMI31	179.1	253.I	310:2	361.1	432.7	498.8
8840	30125	BM130	179.1	252.9	310.3	360.7	432,3	498.3
8950	30015	BM129	179.1	253.0	310.3	359.9	431.1	496.9
9115	29850	BM127	181.4	256.5	314.5	364.9	436.7	502.7
9215	29750	BM126	182.5	258.4	316.7	367.7	440.1	506.8
9365	29600	BM126a	181.3	257.5	315.7	366.9	439.7	506.5
9530	29435	BM126b	180.1	256.1	314.0	365.5	438.8	<i>5</i> 05.9
9670	29295	BM122	180.0	255.4	313.0	364.3	438.1	505.2
9765	29200	BM121	179.9	255.5	313.1	363.8	∠43́7.6	504.7
9890	29075	BM119	179;7	255.6	313.3	△ 363.9.√	437.0	503.8
9920	29045	BMI18	181.0	257.4	3)5.5	366.5	440.1	507.4
10100	28865	BM117	188.2	268.1	₹328.5₹	382.0	458.4	528.4
10205	28760	BM117 BM116	187.6	267:9	328.3	382.0	457.2	527.2
10205	28650	BM115	186.9	267.6	328.0	381.8	457.3	<i>5</i> 26.5
10400	28565	BM114	188.1	269.2	330.1	384.4	460.6	529.9
10510	28455	BM112	189.7	271.2	332,7	387.8	464.7	534.2
10575	28390	BM111	189.7	271.0	332.5	387.6	464.6	534.3
10685	28280	BM110 \	189.7	270.5	332:0	387.2	464.4	534.2
10702	28263			t Capalaba	CONTRACTOR OF THE PROPERTY OF	Anna ann an A		Secretaria de la composición de la comp
10725	28240	BMH0 copy	189.7	270:4	331.8	387.1	464.3	<i>5</i> 34.2
10725	28090	BM108 \ \	189.6	269.8	331.0	386.4	463.9	533.8
10965	28000 \	BM107	189.4	269.9	330.5	386.0	463.6	533.5
11095	27870	BM106 /	189.1	269.7	330.1	385.0	462.8	532.8
11055	27710	BM104	189.9	271.9	333.1	388.2	466.8	53.7.5
11515	27450	BM102	192.9	277.2	340.0	397.2	476.6	549.3
11620	27345	BM101	193.2	277.3	340.4	398.1	477.2	549.8
11695	27270	BM100	193.0	276.9	340.1	397.9	477.2	548.9
11820	27145	BM99	192.7	276.2	339.6	397.5	477.1	548.2
11910	27143	BM98	192.5	276.2	339.2	397.2	477.0	548.2
12035	26930	BM97	191.9	276.1	338.2	396.5	476.5	547.9
12135	26830	ВМ97сору	191.3	275.8	337.6	395.6	475.9	547.4
12139	26826	Вигличеру.	Wecker Roa	Language and the second			enegenous proposition of the contract of the c	Acquirica ann bassannas de santa
THE PARTY OF THE P	26810	ВМ97сору	191.2	275.7	337.6	395.4	475.8	547.3
12155 12215	26750	ВM94	191.2	275.5	337.5	394.8	475.3	547.0
12320	26645	BM94-93	191.0	274.9	337.1	394.0	474.5	546.3
**************************************	26580	<u> </u>	190.8	274.5	336.9	393.8	473.9	545.7
12385		BM93 BM90 copy	190.8	273.6	336.2	393.5	472.7	544.6
12505	26460	ВМ90 сору	188.8	272.4	334.9	392.6	471.5	542.5
12690	26275	BM88	188.8	273.1	335.3	393.6	473.1	543.5
12820	26145	- 3	190.3	275.5	338.0	396.9	478.3	549.8
13 140	25825	BM87	189.4	274.5	338.0	39,6.8	478.2	550.6
13440	25525	BM84	189.3	274.4	337.5	396.6	477.6	550.2
13530	25435	BM83	189.3	274.4	337.0 337.0	396.4	476.9	549.7
13670	25295	BM81	107.1	417.4	٠,١٠٠	220.1	1. 17 812"	

MIKE11	AMTD(m)	Cross section	MIKE11 N	Iodel Peak I	Discharges ((m ⁻ '/s)		
Chainage		ID III	2 year	5 year	10 year	20 year	50 year	100 year
THE COMPANY AND THE PARTY OF TH		THE REPORT OF THE PROPERTY OF	Legender Carlo		anna ann an Aireann an	-		
13765	25200	BM80	189.0	27.4.1	336.6	396.2	476.4	549.3
13910	25055	BM78	188,8	273.7	335.8	395.6	476.4	548.3
13965	25000	ВМ78 сору	188.7	273.6	335,8	39 <i>5</i> .3	476.3	547.8
14115	24850	BM77	187.9	272.4	335.2	393.8	475.5	546.6
14360	24605	BM76	190.1	276.2	339.9	400.3	483.5	556.7
14460	24505	BM75	191.1	278,0	342.0	403.3	486.9	560.9
14625	24340	BM74-BM72	190.9	277.8	341.4	403.0	48,6.1	560.4
14785	24180	BM72	190.7	277.6	340.9	402.8	485.5	560.0
14845	24120	BM71	190.6	277.4	340.8	402.6	₃ 485.1	559.7
14960	24005	BM70	190.3	277.1	340.8	△402.2.△	484.9	559.2
15160	23805	BM69	191.0	277.6	341.9	403.3	486.8	560.5
15340	23625	BM67	191.5	278.2	342.6	403.8	488.1	561.3
15460	23505	BM66	191.2	277.9	341.9	402.9	487.4	560.7
15540	23425	ВМ66 сору	191.0	277.6	341\4	₹⁄~402.7	487.0	560.6
15555	23410		Pine Mount	ain_Road Bri	dge			Market State Control of the Control
15570	23395	ВМ64 сору	/190.9	277.5	341.3	402.6	486.8	560.5
15600	23365	BM64-MHG25	190.9	27.7.5	341.2	402.6	486.6	560.4
15660	23305	BM64	190.7	277.3	340:9	402.4	486.3	560.2
15790	23175	BM63.	190.1	276.7	339.9	401.9	485.4	559.7
15965	23000	BM62	189.9	275.8	339.2	401.1	484.1	559.1
16015	22950	BM61	189.8	√275.5	339.2	400.9	484.2	558.9
16190	22775	BM60	192.4	279.6	344.3	407.1	492.7	568.7
16390	22575	BM59	195.3	284.4	350.2	414.5	502.3	580.2
16435	22530	BM59 mod	195.2	284.4	350.1	414.3	502.3	580.1
16445	22520		Meadowban	k Stree Foot	Bridge and '	Weir		
16455	22510	Bm55-mod	195.2	284.3	350.1	414.3	502.3	580.1
16680	22285	BM57-mod	194.8	284.1	349.7	413.7	502.3	579.4
16785	22180	BM56	194,9	284.1	349.6	414.1	502.7	579.4
17080	21885	Bm55-mod	198.8	290.0	357.1	424.3	514.9	594.2
17240	21725	BM55-54	200.6	293.1	360.8	429.8	521.0	601.6
17300	21665	BM54	200.6	293.0	360.8	430.1	521.2	601.4
17325	21640	CD10	200.6	293.0	360.8	430.2	521.3	601.3
17338	21627		Annual Company of the	Street Weir				
17355	21610	CD09	200.6	293.0	360.8	430.3	521.5	601.4
17540	21425	BM52	200.7	293.6	360.9	431.5	522.0	602.1
	21200	CD07	200.4	291.5	3,67.1	436.5	531.2	602.8
17765 17850	21115	BM50-49-ALS	204.2	292.1	369.0	446.8	533.3	601.8
17920	21115	CD06	251.1	359.7	454.5	440.1	573.3	598.3
17960	21045	CD05	241.7	343,9	434.3	421.5	541.9	598.0
18025	20940	CD04	199.4	290.6	366.8	433.4	539.9	602.9
	20940	BM47-mod	199.1	295.6	372.2	444.6	528.5	603.8
18065		BM46-mod	199.0	297.0	373.4	443.3	523.0	602.0
18110	20855	CD02:	201.7	297.3	363.3	436.5	526.0	607.9
18320	20645	LUL	2011	<u></u>	L	<u> </u>	2000	dimmental enteres and the

MIKEII	AMTD(m)	Cross section	MIKE11 N	Iodel Peak I	Discharges ((m³/s)	оружилоро в 2 Шиндиноронны начиний одного од одного од одного од одного од одного од од одного од од одного од	godgegooggewooprjalling assaulscommine meile mit mit distribilitethete
Chainage		l D						400
			2 year	5 year	10 year	20 year	50 year	100 year
18495	20470	BM44 mod	203.6	296.9	366.5	439.7	534.8	613.8
18690	20275	BM43-mod	203.3	295.5	366.0	438.4	530.9	613.5
18995	19970	BM42-mod	202,2	294.8	364.7	435.3	527.4	611.4
19165	19800	BM42-mod	204.0	298.0	367.9	439.2	534.3	618.0
19195	19770	BM41 copy	204.3	298.6	368.7	439.9	535.4	619.2
19205	19760		Scrub Road	Foot Bridge	& weir			
19215	19750	BM41-mod	204.2	298.5	368.6	439.8	535.3	619.0
19375	19590	BM5GHD	203.5	298.0	368.1	438.1	533.3	617.9
19640	19325	Bm5GHD	202.7	297.2	367.1	436.8	532.5	616.8
20050	18915	BM7GHD	200.7	295.0	364.7	435,0	530.8	613.9
20260	18705	BM8GHD copy	199.8	293.8	363.6	433.8	<u> </u>	611.9
20270	18695		Meadowland	ls Road Brid	The second secon		Screenwards for a transmission and	gumerana managana
20290	18675	Bm8GHD	199.8	293.7	_∼ 363.5 _~	433.6	529.2	611.6
.20510	18455	BM9GHD	198.5	292.2	361.8	431.8	527.1	608.9
20850	18115	BM37	195.2	287.3	356.4	427.0	521:1	602.5
21090	17875	BM17GHD	193.0	284.0	√ 3 <i>5</i> 2∖9	423.7	516.9	597.6
21555	17410	BM18GHD	189.2	278.3	3,46.4	\416.3	508.8	587.6
21875	17090	BM18GHDcopy	188.4	276.5	344\5 \	414.5	506.0	585.3
21885	17080	<u> </u>	Preston Roa	d Foot Bridg	e.& Weir			
21895	17070	BM19_GHD	188.4	276.4	344,4	414.3	505.9	585.1
22305	16660	ALS mod	185:8	271.9	338.9	407.3	496.9	574.1
, 22775	16190	⟨BM23GHD\	183,8.	<u>268.6</u>	334.0	401.4	488.4	564.8
23165	15800	ALS mod	180.9	264.6	328.8	394.8	480.1	554.6
23285	15680	BM10GHD /	179.3	262.7	326.2	391.9	475.9	549.9
23600	15365	\BM11GHD	176.2	258.8	321.5	385.8	469.0	541.7
23900	15065	ALS-23900	173.4	255.7	317.7	381.2	463.2	535.4
24000	14965	Minnippi merge	172.4	254.7	316.4	379.3	461.0	532.9
24000	14965	Minnippi merge	166.3	231.8	277.4	324.5	390.5	451.1
24695	14270	BM13GHD-mod	163.5	227.6	272.7	318.9	384.8	446.2
24890	14075	BM13GHD	163.6	227.7	273.0	319.2	385.3	446.9
25515	13450	MHG19-old	164.0	228.3	273.7	320.2	386.6	449.3
25565	13400	MHG20-old	163.9	228.2	273.6	320.1	386.4	449.1
25865	13100	BM26	163.4	227.4	272.8	318.9	385.1	447.9
25885	13080	***************************************	Wynnum Ro	ad Bridge &	Weir			
25905	13060	ВМ 26 сору	163.3	227.3	272.7	318.8	384.9	447.7
26015	12950	MHG-140	163.1	227.1	272.3	318.5	384.4	447.2
26145	12820	BM24	163.0	226.9	272.0	318.1	383.9	446.6
26365	12600	BM23	162.8	226.3	271.3	317.2	382.8	445.4
26550	12415	Murrarie connec	163.2	226.9	272.0	317.7	383.8	446.9
26550	12415	Murrarie connec	135.6	182.9	217.5	254.6	316.2	371.7
26620	12345	BM22	135.8	183.1	217.7	254.9	316.6	372.1
26710	12255	ВМ22 сору	135.6	182.9	217.4	254.5	316.1	371.3
26730	12235	1.2		oad Bridge &	z Weir	www.compourprocesses.co	The second secon	The state of the s
26750	12215	ВМ22 сору	135.6	182.8	217.3	254.4	316.0	371.0

MIKE11	AMTD(m)	\$ E	MIKEII N	Iodel Peak l	Discharges	(m³/s)		
Chainage	<u> </u>		2 year	5 year	10 year	20 year	50 year	100 year
00700	40405	3.000	135.4	182.8	216.7	253.9	314.9	370.3
26780	12185	MHG-120	135.2	182.6	216.4	253.6	314.3	369.6
26940	12025	BM22 copy	135.2	182.5	216.3	253.5	314.1	369.3
26990	11975	BM42 AGHD cop		*	216.1	253.2	313.7	368.8
27100	11865	BM42A-mod	135.1 135.0	182.4 182.2	215.8	252.8	313.1	367.9
27300	11665	BM42 AGHD cop		<u> </u>		252.8	313.1	367.9
27305	11660	Murrarie connec	135.0	182.2	215.8 268.5	313.5	377.3	439.8
27305	11660	Murrarie connec	161.7	224.9		313.4	377.1	439.5
27355	11610	BM42AGHD	161.7	224.9	268.5 201.2	223.8	253.9	283.3
27355	11610	LC	142.0	178.4		222.9	252.7	281.2
27755	11210	BM43AGHD	141.8	178.0	200.7 158.0	169.8	186.5	203.1
27755	11210	LC	125.5	146.2	157.7	169.5	186.0	202.5
27912	11053	BM44AGHD	125.4	146.0 76.2	77.2	80.9	90.3	103.0
27912	11053	LC	78.3	<u> </u>	77.0	80.7	\90.0\	102.7
28025	10940	BM44AGHD	78.2	76.1	72,4	71.7	70.4	69.5
28815	10150	BM44BGHD	73.7	73.1	79.5	78.6	76.8	75.3
29075	9890	BM43BGHD	81.5	80.3	101.0	108.9	123.9	139.3
29730	9235	BM43CGHD	92.7	96.0	121.1	133.5	154.7	176.6
30635	8330	BM44CGHD	102.1	111.9	244.8	281.0	331.5	378.4
30635	8330	LC	152.4	208.2		233.8	266.1	296.5
31600	7365	BM45GHD	145.2	185.8	210.3	232.7	264.6	294.5
31740	7225	45GHD_US2\	145.2	/ 185.4	209.6		319.1	362.3
31740	7225	rc	150.7	204.2	238.9	272.6	249.5	266.2
32110	6855	вм46ССНD√	161.2	198,2	216.2	230.8	216.9	228.6
32110	6855	BM46CGHD	\153.6\	177.5	189.5	201.3 130.9	130.2	129.6
32355	6610	BM46BGHD	142.8	141.0	135.1		<u></u>	
32355	6610	\BM46BGHD	147.9	150.9	145.6	136.1	134.3 135.6	134.0 135.3
32650	6315	45GHD_D\$1	147.4	149.7	144.1	136.2	263.4	291.1
32650	6315	45GHD DS1	155.3	193.2	215.8	234.7	g	279.8
33330	5635	BM46AGHD	154.4	189.9	210.8	227.3	253.4 290.9	326.6
33330	5635	BM46AGHD	156.4	201.4	230.3	254.7		299.5
34300	<u> </u>	BM52 GHD copy	155.7	195.9	220.8	241.4	271.7	474.1
34300	4665	BM52 GHD copy	168.7	244.8	296.1	345.8	413.8 422.8	484.6
34490	4475	BM52 GHD copy	172.7	250.1	302.3	353.4	422.0	-40-4.0
34500	4465		Cleveland R	Perimental de la company de		260.5	401.5	495.0
34510	4455	BM52 GHD	176.3	255.1	308.4	360.7	431.5	
34700	4265	BM52 GHD	175.5	253.7	306.7	358.6	428.8	491.7
35260	3705	BM7	173.5	252.0	306.5	360,5	434.2	500.7
35670	3295	BM6	173.5	252.1	306.5	360.4	434.2	500.6
35690	3275	ВМ6-сору	173.5	252.1	306.5	360.4	434.2	500.6
35785	3180	BM48	173.5	252.1	306.5	360.4	434.2	500.6
36370	2595	Bm4	173.5	252.1	306.5	360.4	434.2	500.6
37040	1925	BM3	175.5	254.8	309.8	364.3	438:6	505.7
37465	1500	BM2_copy	176.9	256.7	312.1	367.1	441.8	509.4
38070	895	BM2	176.9	256.7	312.1	367.1	441.8	509.4
38340	625		176.9	256.7	3,12.1	367.1	441.8	509.4
38610	355	BM1	176,9	256.7	312.1	367.1	441.8	509.4
38965	0	End of branch	176.9	256.7	312.1	367.1	441.8	509.4

MIKE11 Thainage	TATILITY TACILLY	Cross section ID	INTERVETE IA	IUUCI ECAK	riornar Reg (111 137		
mannage			2 year	5 year	10 year	20 year	50 year	100 yea
ılimba Cre	ek East							
. 0	6280	BE289	9.4	13.1	15.5	17.8	20.9	22.6
60	6220	BE289	8.4	12.2	14.4	16.6	19.6	20.9
170	6110	BE288	6.7	10.5	12.6	14.6	17.4	17.9
250	6030	BE287	7.0	9.3	11.2	13.1	15.6:	16.9
388	5892	BE286	13,6	18.0	21.7	25.4	30.3	33.2
525	5755	BE285	20.6	25.9	30.5	35.2	42.4	50.2
612	5668	BE284	21.2	27.2	32.1	36.8	42:7	52.0
660	5620	HEC2146	21.4	27.8	32.7	37.5	43,6	52,7
708	5572	BE283	21.5	28.2	33.2	38.1	44.2	52.9
755	5525	HEC2030	20.7	28.0	33.3	38.4	44.5	52.4
799	5481	BE283 copy	18.9	27.3	33.2	√38.5	44.5	51.3
815	5465	BE282US	18.1	27.0	33.I	38.5	44.5	50.7
820	5460			oad East Cul	verts			
835	5445	BE281DS	17.9	26.4	32,6	× 37.3	44.2	49.8
840	5440	BE280	17.6	26.2	32.5	36.9	44.0	49.5
844	5436	BE279HEC	17.2	25.9	32.3	36.6	44.0	49.4
845	5435		www.commons.commons.commons.com	ail Culverts				
852	5428	BE278	17.6	24.8	31.0	√35.4	43.5	48.8
875	5405	BE277-HEC	(18.2)	23.8	/27.9	32.7	42.5	47.3
876	5404		THE RESIDENCE OF THE PROPERTY OF THE PARTY O	oad Pipe Cul	Lanianananananananananana			<u> </u>
930	5350	Bulima East Ra	NAMES OF TAXABLE PARTY.	23.9	28.0	32.2	41.9	46.6
930	5350	Bulima East Ra	17.9	22.9	26.4	29.8	37.2	40.7
	5334	BE277-HEC DS	17.9	22.9	26.4	29.7	37.0	40.5
946	5324	BE27.7-A	17.9	22.9	26,4	29.6	36.9	40.3
956 978	5302	BE277-A copy/	17.9	23.0	26.5	29.3	36.6	39,9
981	5299	XS-7450	17.9	23.0	26,5	29,3	36.6	39.9
991	5289	XS-7460	17.9	23.0	26.5	29.4	36.3	39.6
1011	5269	Xs-7480	17.9	23.1	26.6	29.5	35,8	38.9
1031	5249	XS-7500	17.9	23,2	26.7	29.6	35.2	38.3
1051	5229	XS-7520	17.8	23.2	26.7	29.7	34.6	37.7
1071	5209	XS-7540	17.8	23.3	26.8	29.8	34.0	37.9
1091	5209 5189	XS-7560	17.7	23.3	26.9	29.9	33.4	38.1
1111	5169	Xs-7580	17.7	23.3	26.9	30.0	33.5	38.3
1131	5149	Xs-7600	17.6	23.4	27.0	30.1	33.7	38.5
1151	5129	Xs-7600 Xs-7620	17.5	23.4	27.0	30.1	33.9	38.6
1171	5109	XS-7640	17.5	23.4	27.1	30.2	34.0	38.8
1191	5089	XS-7660	17.4	23.5	27.1	30.3	34.2	39.0
1211	5069	XS-7680	17.4	23.5	27.1	30.4	34.3	39.1
1231	5049	Xs-7000 Xs-7700	17.3	23.5	27.2	30.4	34.4	39.2
1251	5049	XS-7720	17.3	23.5	27.2	30.4	34.5	39.3
1271	5009	XS-7740	17.2	23.5	27.2	30.5	34.5	39.3
	4989	XS-7760	17.2	23.5	27.2	30.5	34.6	39.4
1291		Xs-7780	17.1	23.4	27.2	30.5	34.7	39.4
1311 1331	4969 4949	XS-7800 XS-7800	16.9	23.4	27.1	30.5	34.7	39.5

MIKE11	AMTD(m)	1	MIKEII N	Iodel Peak I	discharges (m^3/s)		
Chainage		<u>ID</u>	**************************************		1.0	10 vice v	50 year	100 year
No the last of		***************************************	2 year	5 year	10 year	20 year	34.7	39.4
1341	4939	Xs-7810	16.8	23.3	27.1	30.5	34.7	39.4
1355	4925	BE273	16.6	23.2	27.0	30.4	<u> </u>	39.4
1380	4900	Bulima East Ra	16.3	23.0	26.9	30.4	34.7	42.3
1380	4900	Bulimba East Le	16.0	22.9	26.9	30.9	36.7	
1498	4782	BE272	16.4	21.6	25.9	30.0	36.2	41.4
1565	4715	BE272	16.6	21.9	25.6	29.2	35.5	40.4 39.6
1600	4680	BE271_ALS	16.6	22.0	25.7	29.3	34.9	
1730	4550	BE270	16.1	22.2	26.0	29.7	34.4	39.6
1915	4365	BE269	19.8	28.5	33.9	39.1	46.4	53.5
2020	4260	BE268	22.0	32.1	38.4	44.5	53.2	61.3
2145	4135	BE267	22.4	31.8	38.2	44.5	53.5	61.7
2245	4035	BE266	22.6	31.5	38.0	44.4	53.6	61.8
2410	3870	BE265	22.7	31.2	37.4	44.0	53.6	61.8
2500	3780	BE264	22.6	31.5	37.2	43.7	53.4	61.6
2605	3675	BE263	22.4	31.7	37.6	43.2	\$3.0	61.2
2696	3584	Trib_C	22.3	31.9	37.9	43.8	52.7	60.9
2696	3584	Trib_C	29.6	41.2	49.8	∖57.6	69.3	80.4
2765	3515	BE262	29:7	40.6	48:9	57.6	69.2	80.4
2767	3513		Underwood	Road Culver	is 🔍			
2785	3495	BE261:	(29.7)	40.7	49.0	57.6	69.2	80.4
2990	3290	BE259	29.8	41.2	49.6	58.0	68.8	80.1
3200	3080	BE258	31:4	44.2	53.3	61.9	71.6	83.5
3320	2960\	BE257 \	∖ 32.0∖	<u>45.6</u>	55.1	63.9	73.5	87.6
3330	2950		Gateway Mo	torway Culv	erts			
3425	2855	BE257 copy	31.4	45.4	55.0	63,7	73.2	85.1
3490	2790	BE256	30.9	45.1	54.8	63.4	73.2	85.4
3670	2610	BE255	31.3	44.2	54.0	62.3	73.5	85.8
3695	2585	BE255 copy	31.3	44.1	53.9	62.2	73.5	8 5 .9
3725	2555	BE255 copy -mo	31.4	44.0	53.7	62.0	73.6	85.9
3726	2554	Trib B1	31.4	44.0	53.7	62.1	72.7	85.5
3726	2554	Trib_B2	32.8	48.1	59.4	69.7	98.5	92.4
3735	2545	BE254 copy	32.9	47.9	59.2	69.5	92.4	90.4
3745	2535	BE254	33,0	47.6	58.9	69.2	75.4	90.5
3748	2532		Logan Road	Culvert		ATT AND DESCRIPTION OF THE PARTY OF THE PART		
3785	2495	BE253	33.0	47.5	58.4	68.7	82.1	95.2
3810	2470	interpolated	33,1	47.6	58.2	68.3	81.0	95.3
	2392	Trib B	33.2	48.0	58:2	68,2	80.3	93.4
3888	2392	Trib B	40.2	56.3	67.8	78.4	91.2	104.8
3888		<u></u>	40.3	56.5	67.5	78.0	90,8	104.3
3925	2355	BE251	41.2	57.9	68.7	78.9	91.7	106.2
4020	2260	Be250	41.8	58.6	69.1	79,2	94.1	109.0
4110	2170	BE249		Į	70.3	81.1	96.7	111.5
4230	2050	BE248	41.0	58.0	70.3	84.8	99.5	113.1
4284	1996	Trib_A	42.3	60.5	128.1	148.3	177.2	205.5
4284	1996	Trib_A	80.3	109.1	128.1	147.5	176.6	205.0
4300	1980	BE247	79.9	108.8	1.4/.4	1.17.2	1	L

MIKE 11	AMTD(m)	1	MIKEII N	Iodel Peak I)ischarges ((m^3/s)		
Chainage	_	ID	***************************************		10	20	1 E0 1	100 year
			2 year	5 year	10 year	20 year	50 year 174.0	201.8
4360	1920	ВЕ247 сору	78.7	108.6	126.6	146.0		199.9
4419	1861	BE246	79.0	108.5	126.9	146.4	173.6	
4507	1773	BE246A-ALS	79.2	108.3	127.0	146.6	173.9 174.3	200.1 200.6
4602	1678	Old_4612	79.4	108.5	127.2	146.7	1/4.3	200.0
4608	1672			Plains Bridge	CANADA TO THE PARTY OF THE PART		1943	200.7
4638	1642	Copy Old 4612		108.6	127.2	146.7	174.3	200.7
4656	1624	BE244	79.5	108.6	127.2	146.7	174.3	200.0
4660	1620			ng Road Brid			17117	200.8
4695	1585	Old 4665	79.5	108.6	127.2	146.7	174.3	***************************************
4730	1550	Old 4685	79.5	108.6	127.2	146.7	174.3	200.8
4750	1530	Old 4705	79.5	108.6	127.2	146:7	174.3	200.8
4870	1410	BE241	80.6	110.2	129.0	148.5	17,6.7	203.6
4980	1300	BE240	81.5	111.7	130:5	150.0	178.7	206.1
5010	1270		Gateway Of		1 (
5050	1230	BE239	81.3	111.6	130.3	149.6	178.4	205.8
5175	1105	BE238	80.9	111.4	129.9	₹148.8	177.7	205.1
5330	950	BE236	80.2	111.1	129.3 \	147.8	176.6	203.9
5470	810	BE235	84.0	116.6	> 135%	155.1	185.2	213.9
5712	568	BE232 <	~90 <u>.0</u>	125.8	146.8	167.4	199.5	230.2
5810	470	BE231	\89.8	125.2	146.1	166.6	198.3	228,8
5895	385 "	BE230	90,9	126.4	147.6	168.3	200.2	230.8
5975	305√	BE229	91.8	127.3	148.8	169.7	201.9	232.5
6055	225	BE228	\91.6\	126.3	147.8	169.4	201.7	231.7
6135	145	BE227	91.2	125.8	147.4	169.0	201.3	231.3
6280	0	BE227	90.3	125.0	146.4	168.1	200.3	230.1
Fributary A	A.,		Sancaran proportion de la constanta de la cons	<u> </u>				onocia revione de la companie de la
0	·	ALS1-copy	16.8	23.8	28.2	32.4	38.2	40.9
100		ALS1-copy	14.8	21.2	24.7	28.1	32.9	34.4
320		ALS1	12.7	18.4	21.2	23.7	27.3	32.9
600		ALS2	13.6	17.4	21.0	24.3	28.5	33.3
950		BE-1060	16.4	22.2	26.6	30.5	35.6	40.9
1400	1	BE-1040	18.0	25.4	31.3	36.7	43.8	48.9
1400		Trib_ÅI	22.3	32.0	39.4	46.5	55.8	63.3
1770		BE-1030	25.8	34.8	41.3	49.1	59.7	66.9
2070		BE-1020	25.4	35.4	42.8	50.1	59.3	67.7
**************************************			School Road	2	L	Energy Commonwealth Common Com	The second se	\$
2072		interpolated	26.1	36.6	44.4	51.9	61.5	70.1
2125		Trib A2	27.3	38.4	46.6	54.5	64.7	73.7
2163	<u> </u>	<u> </u>	42.4	57.6	69.1	80.4	95.0	109.3
2163	ļ	Trib_A2	Contractor	55.3	66.4	77.3	90.9	104.9
2235		DIT-IOIO	40.4 43.2	60,0	72.2	84.1	99.7	115.5
2535		BE-1005	<u> </u>		1 4.4	N. T. A.	L	
2545		00100	Freeway Of		72.5	84.4	100.1	116.0
2555		BE-1005	43.3	60.2	12.2	F . O.T.	E LOUIL	

	AMTD(m)	Cross section	MIKE11 N	Iodel Peak I)ischarges (m/s)		
Chainage		ID	2 year	5 year	10 year	20 year	50 year	100 year
0705		BE1005 copy	42.3	59.0	71.1	82.5	97.2	112.8
2735		BE1000 copy	42.2	58.8	70.8	82.0	96.5	112.0
2765	LEWINGSON THE WATER CONTRACT OF THE PARTY OF	BEIVOU	Gateway Mo	·····	***************************************	***************************************	AND THE PERSON NAMED IN COLUMN TO PERSON NAM	NATIONAL PROPERTY OF THE PROPE
2805		BE1000 modified		57.9	69.3	78.6	92.8	108.2
2935				57.4	68.6	77.3	91.3	106.5
3015	3	BE1000 modified		57.4	68.5	77.3	91.2	106.3
3021		BE1000 modified	41./	37.4	00.2	11.0		teckinen international administration
Cributary A	1			11.2	13.3	15.3	18.1	19.5
0		A1-1050	7.9			12.8	15.3	15.8
280	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Ã1-1050	5.8	9.1 8.1	11.0 9.8	11.5	13.8	15.0
500		ALS	6.0	6.8	8.3	9.9	12.0	14.6
720		ALS	5.3	6.6	8.1		12.0	14.4
750	<u> </u>	ALS	5.0	0.0	0.1	at in the second	ale management of the second	
ributary A	Z 2		150	24.4	28.8	33,0	38.9	41.6
0		TRIB A2	17.2	24.4 22.4	26.6	~~33,0 √~30.7₃	36.3	38.3
80		SMP	15.1 17.8	22.4	26.3	30.5	36.9	43.6
475		SMP	20.2	26.8	31.7	36.4	42.3	51.1
690		SMP	15:9	23.6	28.8	33.7	40.2	44.4
1035 1042		SMP SMP	15.6	23.0	28.2	33.0	39.4	43.3
OKSONIE DANIE DANI		SWIE .	15.0	23.0				
ributary B		BE2030	22.6	32.3	38.3	44.0	52.0	55.5
1000		BE2030	21.6	31.2	37.0	39.9	49.9	53.3
1055		DE2030	Dance Cour	A STREET WARRANT TO STREET STREET		AND THE PROPERTY OF THE PROPER		
1062		D 70030	21.1	30.7	36.5	39.2	\$ 49.2	52.4
1075		BE2030 copy	17.4	26.7	32.5	37.1	44.4	46.3
1215		BE2020		23.9	29.0	33.6	39.5	45.6
1340		BE2020 copy	18.1 18.3	23.4	28.4	32.9	38.7	45.9
1360		Interpolated BE2010	10.7	12.4	13.7	15.0	17.0	20.3
1360	***************************************	DE2010	Logan Road	E		**************************************		ACCUPATION OF THE PARTY OF THE
1361		D 750000	10.9	12.2	13.3	14.8	16.8	20.8
1394		BE2000 BE2001	10.9	12.3	13.5	15.0	17.0	20.9
1432		<u> </u>	10.7	12.1	13.2	14.7	16.7	20.5
1492		BE2001	10.7	12.1	***************************************			***************************************
Tributary C		DE 2060	9.7	13.7	16.3	18.7	22.1	23.8
0.		BE-3050	9.4	13.4	16.0	18.3	21.7	23.3
10		BE-3050 BE-3040	6.8	9.6	11.6	13.5	16.0	18.3
390		BE-3030	6.5	9.1	11.0	13.0	15.6	17.3
545		BE-3030	8.2	11.3	13.8	16.4	19.7	22.3
665,	<u> </u>	<u> </u>	10.1	14.3	17.4	20.6	24.8	28.7
810		BE3000	10.1	14.1	17.2	20.3	24.4	28.1
1000		BE-3000 copy	10.2	14.1	17.2	20.3	24.4	28.0
1005		DE-SOON coby	B	otorway Culv	Anna Company of the C	WHITE SHEET	Samuel and the same of the sam	
1008		7277000	10.3	14.3	16.9	19.6	23.4	26.9
1100		BE3000 copy		<u> </u>	17.0	19.7	23.0	26.7
1110		ALS	10.3	14.3	<u> </u>	19.7	22.8	26.8
1120	I	End Trib C	10.4	14.3	17.0	17.0	L	20.9

MIKE11	AMTD(m)		MIKE II N	Iodel Peak I)ischarges ((m³/s)		
Chainage	**************************************	ID			10	20	50 year	100 year
			2 year	5 year	10 year	20 year	ou year	LUU YEAL
Fributary B			March September 1997	pamentum meterona territ		100	216	25.6
1.000		ALS	7.5	11.1	14.7	18.0	21.6	25.6
1002		ALS	7.5	11.1	14.7	18.0	21.6	£
1020	-	ALS	7.6	11.2	14.5	17.8	21.2	25.5
1055	:	ALS	7.6	11.3	14.5	17.6	20.4	24.9
1140		ALS	7.0	10.4	12.9	15.0	16.5	19.7
1145		ALS	6.9	10.3	12.8	14.7	16.1	19.2
adstow Bra	nch	Zanjilasiiisasembatoin (kasaasemasemase						
0		BM177	29.0	41.0	48.8	55.9	67.6	82.2
32		BM177	28.9	41.0	48.6	55.8	67.7	81.9
105		BM177-176ALS	28.7	41.2	48.5	55,5	68.Ĭ	82.6
140		LC	28.8	41.3	48.8	,∕~\5\5,4 },	68.2	82.9
140		LC	28.8	41.3	48.8	52.9	55.2	60.9
175	and to a section with	BM176-US-ALS	28.9	41.4	49.1	53.4	₹ 55.3	61.2
177			Padstow Ro	ad culverts			1	
205		BM176-DS-ALS		41.5	49.3	₹53.7°	55.6	61.6
205		LC	29.0	41.5 📉	49.3	53.7	55.6	61.6
258		BM175	29.2	41.8	49.7	\$4.4	56.5	62.3
258		LC	29.2	41.8	49.7	<u>54.4</u>	56.5	65.2
325		BM175-174ÅLS	\$29.6	42.1	J 30.2	55.1	57.5	66.0
352		BM174	29.8	42.3	50.4	55.4	57.9	66.2
375		BM175	29.9 <	42.4	50.5	55.6	58.2	66.4
Garden City	Branch						ुं	
5280		BM169	23.2	40.1	55.1	66.7	84.7	101.2
5285		BM169	23.1	40.1	55.1	66.6	84.6	101.1
5405		BM168 /	23.1	39.9	54.9	65.4	82.8	98.8
5405		LĈ\	23.1	36.0	44.6	56.9	76.4	94.7
5510	<u> </u>	BM167	23.1	35.8	44.2	56.3	75.9	94.4
5510	i i je sa i sa i sa	LC	23.1	35.8	44.4	60.9	86.1	107.2
5615		BM167 copy	23.1	35.7	43.8	60.0	85.4	106.8
5615		LC	23.1	35.7	43.6	52.8	64.1	75.0
5715		Bm165 copy	22.9	35,5	43.6	52.5	63.7	74.8
5715		LC	22.8	36.8	45.2	52.6	61.1	77.9
5730		Bm165	22.9	36.8	45.2	52.5	61.0	77.9
5785		XS5	22.9	36,8	45.2	52.4	60.8	77.8
5850		XS4	22.9	36.7	45.2	52,3	60.8	77.5
5850		LC LC	22.9	36.7	45.2	57.0	88.5	125.6
5935		XS4 copy	22.9	36.6	45.2	57.0	88.7	125.3
2732	<u> </u>	End	22.9	36.7	45.2	57.0	88.7	125.3

Chainage		<u> </u>	1	5 year	10 year	20 year	50 year	100 year
	**************************************		2 year	3 YEAR	10 year	20 (04)		
Iimiosa Cre	ek	FA: 40 Dance	35.3	51.1	60.7	70.0	82.9	88.2
0:		Mi 40 Hecras Mi 40 Hecras	35.2	51.0	60.6	69,9	82.7	88.0
5		Mi 40 Hecias	32.3	48.3	57.7	66.8	79.3	83.9
96			2	43.1.	52.1	60.8	73.0	76.2
200		Mi39	29.2 30.6	39.2	46.7	53.9	64.6	77.5
330		MI38	42.5	69.8	65.3	75.9	91.4	109.1
484		Mi37	44.3	74.3	68.0	78.9	95.2	113.6
506		Mi36		71.8	69.3	80.3	95.2	114.7
558		Mi35	44.8	71.8	71.4	82.7	97.7	116.2
660		Mi34	45.3		71.4	83.2	98.3	116.4
696		Mi33	45.1	74.7		83.9	99.4	115.5
811		Mi32	42.3	75.6	71.8 68.0	/ 83.9 /80.6	96,5	108.7
952		Mi31	38.9	73.1	<u> </u>		93.3	103.2
1037		Mi31-copy	39.6	70.3	64.6	77.3	86.0	101.3
1186		Mi29	39.6	66.5	63.8		87:3	102.1
1302		Mi28	38.4	67.0	63.9	73.9	87.3 87.4	102.1
1322		Mi27	38.0	67.0	63.7	73.9	87.6	102.0
1366		Mi26	36.7	66.8	63.2	73.7 73.3	87.7	102.8
1439		Mi25	36.0	66.4	62.3	72.6	87.5	101.4
1549		Mi24	36,4	65.4	61.0	72.2	87.4	101.4
1588		Mi23	36.5	64\9 63.1	60.3 58.4	70.9	86.7	100.3
1719		Mi22	36.7	63.1/ 62.8	58.5	70.5	86.5	100.0
1738		Mi21-2	36.7		د.ەد	/.0.5		100.9
1739	<u> </u>	and the same of th	Nagel Street	*************************************	l and	70.2	86.1	99.6
1752	7	Mi21-1	36.7	62.7	58.6	70.2	85.9	99.3
1762		Mi20	36.7	62.6	58.6	70.1 68.5	83.2	95.8
1882		Mil9	36.6	62.3	59.6 59.7	68.7	83.0	95.5
1892		Mi19-4	36.6	62.4	39.1	***************************************	ייכט	
1895		Į .	Pacific Moto	CANADA CONTRACTOR CONT		20.0	01.7	94.4
1964		Mi19-1	36.4	62.8	60.0	69.2	81.7	100.7
2023		Mi18	38.4	63.0	63.8	73.7	87.9	100.7
2086		Mil7	40.5	63.2	67.8	78.4	94.4	106.3
2133		Mil6	40.3	63.4	67.9	78.7	93.2	
2224	garana andra M	Mil5	39.9	63.5	68.0	79.1	93.7	108.5
2248		Mi13-3	39.8	63.5	68.1	79.2	94.0	108.8
2255	3.5		Kessels Roa	d Bridge				
2284		Mi13-2	39.6	63.4	68.0	79.3	94.4	109.2
2325		Mil3	39.3	63.4	68.0	79.4	94.7	109.6
2516		Mi12	39.1	62.9	67.7	79.3	95.3	110.5
2635		Mill	39.4	62.3	67.2	78.8	95.3	110.6
2648			Parkway St	reet Bridge				
2664		Mi10-2	39.5	62.1	67.1	78.7	95.3	110.6
2718		Mi9	39.6	61.9	66.9	78.6	95.3	110.5
2828	,	Mi8	39.6	60.7	66.0	77.9	94.8	110.1
2955		Mi7	43.0	65.3	71.7	84.9	104.0	121.0
3069		Mi6	45.8	70.3	77.2	91.3	112.3	130.8

	AMTD(m)	1 1	TATETATATE TA	LOUCE LOUIS	Yidemar Boo	()		
Chainage			2 year	5 year	10 year	20 year	50 year	100 year
2021	1	Mi5	44.8	70.4	77.8	90.6	110.8	129.4
3221		Mi4	44.0	69.5	77.7	91.1	108.9	125.9
3388		Mi3	44.2	68.5	77.3	91.2	109.7	126.1
3496 3585		Mi2	44.3	67.7	77.0	91.1	110.0	126.7
,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		Mil	44.2	67.5	75.5	90.2	110,0	127.3
3801 3890		Mi2	44.0	67.5	75.0	89.8	109.6	127.0
3.1	pass Branch	IIVI12			***************************************	English Commission of the Comm	Z.	
CARCOLOUS HOUSE COMMISSION		ALS-1	6.5	23.6	39.5	54.3	72.4	84.4
0 80		Minnippi_new1	6.3	23.5	39.3	53.8	71.5	83.2
125		Minnippi new2	6.2	23.4	39.1	53.5	71.0	82 .6
	_	Minnippi new3	5.8	23,2	38.5	52.3	69.4	80.6
230		Minnippi new4	4.5	22.8	37.1	<u></u>	66.1	76.5
400 542	-	Minnippi_new5	2.9	22.5	36,2	48.8	64.3	74.7
650		Stanton RD	2.8	22.3	35.8 /	48.3	√ 63.7√	74.0
			2.8	22.2	35.7	48,1	63.4	73.8
720	<u> </u>	new_A new B	2.8	22.2	35.7	48.1	63:4	73.8
730		4	2.8	22.2	35.7	48.1	63.4	73.8
745,	<u></u>	Minnippi_new6-		otorway Culv	NAME AND ADDRESS OF THE OWNER, WHEN PERSONS ADDRESS	1 10.7		
748		Contraction and the Contraction of the Contraction	THE PERSON NAMED IN COLUMN TWO IS NOT THE OWNER.	22.2	35.7	48.1	63,3	73.7
810		Minnippi_new7-	2:8		35.7 35.7	48.1	63.3	73.7
825		new_E	2.8	22.2		48.1	63.3	73.7
860		new G	4.1	22.2 22.2	35.7 35.7	48.1	63,3	73.7
870	<u> </u>	new_7a			32.2	43.2	57.2	67.3
945	<u> </u>	Minnippi\new8\	5.3	20.2	32.1	43.2	57,2	67.3
1015		BM31GHD_mod	\5.3'	20.2	32.1	43.1	57.1	67.2
1115		Minnippi16_AL\$	5.2	20.2	32.1	43.1	37.1	07.2
1125		Commence of the second	Wynnum Ro	Contraction of the Contraction o	20.0	42 N	57.0	67.1
1150		BM 31GHD-cop	5.2	20.2	32.0	43.0	<u> </u>	66.4
1310		BM36_GHD	5.0	20.1	31.8	42.7	56.5	<u> </u>
1560	The state of the s	Minnippi_new11	4.4	20.1	31.5	42.1	55.4	64.9
1850		BM 42B_GHD	3.5	20.2	31.1	41.4	54.1	63.0 62.1
2004		BM42BGHD	3.7	20.4	31.2	41.0	53.5	UZ.1
يمه ون د								¥
*****************************	ypass Branch		27.6	44.2	54.5	64.9	71.0	75.6
0		MU1_ALS	27.6	44.2	54.5	64.9	70.9	75.5
20			27.6	44:2	54.5	64.8	70.8	75.3
35	<u> </u>	New MU1 New MU2 ALS	27.4	43.8	54.0	64.1	69.2	74.3
160		New MUZ ALS	27.1	43.3	53.5	63.1	67.5	73.6
275	1	Copy new MU3	27.0	43.2	53.4	62.8	66.9	73.3
310		New MU5_ALS	26.9	43.1	53.1	62.1	65.9	73.0
390		Mu 6 ALS	26.9	42.9	53.0	61.5	65.2	72.7
470	L Carrier Cali	Commence of the second	20.7.	<u> </u>		A	<u> </u>	Assessment of the second
marken die er	otorway Culv	NAMES AND ADDRESS OF THE OWNERS OF THE OWNERS OF THE OWNER, WHEN THE OWNER, WH	26.8	42.9	52.9	61.2	64.8	72.3
545	-	MU_7_ALS	26.8	42.8	52.9	61.0	64.6	72.1
595	·	MU 9 ALS	26.8	42.8	52.8	60.9	64.4	72.0
640	I	MU5_ALS	۷٥.٥	74.0	- 2270	60.9	64.4	72.0

18E	MIVE I D(M)	Cross section	WILKELLIV	iouei reak l	viscitat Res ((LLK 13)		
Chainage		D	2 year	5 year	10 year	20 year	50 year	100 year
Bulimba East	Rail Rypass							
0	**************************************	Start	0.28	1.03	1.67	2.40	4.71	5.97
33		BE276	0.25	1.09	1.76	2.54	3.88	5.33
144	·	BE275	0.11	1.07	1.90	2.85	4.21	5.85
226		BE274	0.21	0.76	1.50	2.39	3.72	5.14
		BE273 US	0.32	0.58	1.12	1.77	2.81	4.08
347	- 190,	BE273 DS	0.33	0.51	1.09	1.78	2.90	4.19
443		BE273 A	0.32	0.55	1.13	1.84	3.00	4.31
488	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	End	0.32	0.64	1.23	1.95	3.13	4.48
520		End	0.54	\$ 0.0 i				CHARLES AND
Kianawah Pa	rk Branch		10.07	25.98	30.90	35.59	42.13	45.06
0			18.07	23.98	29.22		40.49	43.02
48		WY-1 ALS	16.28	8	18.66	22.46	27.22	32.01
210		WY-2 ALS	11.92	15.93	18.02	21.34	25.40	30.89
260		WY-3 ALS	11.25	14.99	16.77	20.01	24.09	28.84
340		WY-4 ALS	10.10	13.88	15.15	17.98	21\71	25.42
430	, <u>, , , , , , , , , , , , , , , , , , </u>	WY-5 ALS	8.76	12:47	15.10	14.81	17.81	20.30
530	·	WY-6 ALS	7.97	10.50		10.87	12.34	13.65
660		WY-7 ALS	6.19	8,36	9.75	8.75	9.84	10.72
780		WY-8 ALS	5.48	7.05	> 7.87\ 7.10		8.84	9.49
860	and the second s	WY-9 ALS 🛴	₹5.35 <u></u>	6.72	7.49	8.12	8.82	9.30
945		WY-10-ALS \	5.34	6.69	7.43	8.02	8.81	9.29
9.85		ŴY-11 ALS√	5.33	`6,69	7.43	8.01	<u> </u>	9.29
1006		End \	5.33	6.68	7.42	8.01	8.81	9.20
Link Canals	<u>\</u>				panana panana kanatana kanatana	gunnament menter de la companya del companya del companya de la co		157.07
0		42GHD_AB	19.98	46.97	67.92	90.52	124.34	157.87
175	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	42GHD AB	19.98	46.97	67.92	90.52	124.34	157.87
0		43GHD AB	16.66	32.41	43.29	53.57	66.55	78.88
186	<u> </u>	43GHD AB	16.66	32.41	43.29	53.57	66.55	78,88
0		43GHD_BC	9.37	15.75	17.10	18.15	18.76	20.00
191		43GHD_BC	9.37	15.75	17.10	18.15	18.76	20.00
0		44GHD_AB	48.93	70.81	81.14	88.63	95.70	100.83
74		44GHD_AB	48.93	70.81	81.14	88.63	95.70	100.83
0.		44GHD_BC	51.83	98.16	125.11	148.58	177.29	202.24
58	***************************************	44GHD BC	51.83	98.16	125.11	148.58	177.29	202.24
0		45GHD US1	19.89	48.87	70.73	93.03	123.60	151.64
465		45GHD USI	19.89	48.87	70.73	93.03	123.60	151.64
0	**************************************	45GHD US2	5.54	19.07	29.52	40.07	54.63	67.87
5.60		45GHD US2	5,54	19.07	29.52	40.07	54.63	67.87
0		45GHD DS1	9.62	56.55	96.06	137.94	196.70	250.42
190		45GHD DS1	9.62	56.55	96.06	137.94	196.70	250.42
0.		46GHD AB	2.01	12.57	20.18	28.10	38.33	47.27
	<u> </u>	46GHD AB	2.01	12.57	20.18	28.10	38.33	47.27
621		46GHD BC	8.26	21.27	27.56	30.84	32.66	37.74
0		46GHD BC	8.26	21.27	27.56	30.84	32.66	37.74
99.		46GHD DS	13.04	48.98	75.34	104.47	142.19	174.67
0		46GHD DS	13.04	48.98	75.34	104.47	142.19	174.67
294		<u> </u>	0.30	1.87	4.12	7.05	11.80	16.77
0.		CLEV_RAIL		1.87	4.12	7.05	11.80	16.77
939		CLEV_RAIL	0,30	1.0/	7.1.4			

Appendix I2

HECRAS Model Results for Newnham Road Tributary



Reach	Pian: Plac 05 River: Newnha	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chal		Top Width (m)	Fraude# C
			(m3/s)	(m)	(m)	(m)	(m)	(m/m)	(m/s) 1.90	(m2) 45,15	60.78	0
er	1880,00	100yr	60.60	22.75	24.88	24.58	25.02	0.003228	2.11	29,96	54.67	0
ec.	1880.00	50yr	48.30	22.75	24,62	24,28	24.70	0.005898	2.17	24,05	40.52	Ŏ
C	1880.00	20yr	42.00	22.75	24,43	24,19	24.64	0.006148	2.16	21.68	37.21	.0
r	1880,00	10yr	36.70	22.75 22.75	24,36	24.08	24.57	0.006238	2.11	19.42	33.75	0
r.	1680.00	Бут.	35.00	22.75	24.14	23.88	24,35	0.007546	2,05	13.29	21.11	(
Citati	1880.00	2ут	26,20	22.10	29.14							
O SARR		100	60.60	22,71	24.82		25.00	0,003652	2.03	39,48	49,15	
C.	1873,00	100yr		22,71	24.57		24,78	0.005004	2.13	27.73	43.33	
r	1873.00	50yr	48.30	22.71	24,45		24,56	0.005517	2,12	23.03	33.55	
r.axs	1873,00	20yr	42.00	22.71	24,39		24,60	0.005534	2.07	21.25	31.24	
(1997)	1873.00		38.70				24.53	0.005420	1.99	19,50	28,78	14.00 P
r de la	1873.00	5yr	35.00	22.71	24.34		24.30	0.006125	1.87	14.25	19.14	γ.
122	1873.00	2ут	26.20	22.71	24.12							
				00.50	24.77		24,97	0.004033	2,13	36.73	44.53	
Ţ.	1866.00	100уг	60.60	22.50	24.77		24.74	0.005283	2.33	24.75	37.44	
r	1865.00	50yr	48,30	22,50		24,14	24.61	0.007991	2.42	19.37	31.18	
000	1866.00	20yr	42.00	22.50		24.07	24.55	0.008201	2.37	17,71]	28.97	٧.
900	1886.00	10yr	38.70	22.50	24,23	24.00	24.48	9.007762	2.25	16.53	27.30	
r (1866.00	5yr	35.00	22.50		24,00	24.24	0.009279	2,15	12,19	14.28	
r .	1866.00	2ут	26.20	22.50	24,01		E-704-1	2,002272			10.00	
100					04.77		24,94	0.003259	2.12	40.71	47.42	
r iii	1860.00	/ 100yr	60.60	22.28	24,77			0.005048	2,36	27.28	39.63	
r	1860.00	50yr	48,30	22.28	24.46		24,70	0.005843	2.53	20.56	32:16	
(2.00)	1860.00	20yr	42.00	22.28	24,27	A 1 Mar	24.49	0,008538	2.67	17.03	26.92	
ri (S	1860.00	10уг	38.70	22.28	24.15	24,09	24,41	0.011224	2.84	13.64	20.50	
6	1860:00	5ył	25,00	22.28	24.01	24.01	24.41	0.011224	2.89	9.06	9.24	1
	1860,00	2yr	26,20	22,28	23.72	23,67	24.15[V.D 13034				
			ļ				2/ 01	0.002506	1,90	45.38	51,20	
	1854.00	1,00yr	60,60	22.25	24.77		24,91	0.002306	2.07	31.08	42.89	
	1854.00	50yr	48.30		24.47		24.85	0.004915	2.21	23,95	34,66	
	1854,00	20yr	42,00		24.29		24.50	0.004915	2.33	20.06	30.16	
	1654.00	10ут	38.70	22.25	24.17		24.42	0.009021	2,59	15.25	24.39	
	1854.00	5yr	35.00	22.25	23.99	23.83	24,32	0.009021	2,59	9.78	9,71	
	1854,00	2уг	26.20	22,25	23.68	23.56	24,04	0.012431	2.00	3.74	100	
							04.00	0.001685	1.54	41.05	58.71	
oi.	1847.00	100yr	60.60	22,20			24.89		1.70	27.37	33.41	
r	1847.00	50 y r	48,30	22.20			24.63	0,002501	1.84	22.15	25.73	
	1847,00	20yr	42.00	22,20			24.47	0,003579	1.95	19.68	21,09	
(2000)	1847,00	10yr	38,70	22,20			24.37	0.004337	2:20	16.25	19,59	9
r.	1847.00	5γτ	35.00	22.20			24.24	0.006198	2,40	10.93	10.51	<u> </u>
	1847.00	2 yr	26.20	22.20	23.66		23.95	0.009464	2,40	10.33		
			∯-4 ' : <u> </u>						1 12	43,40	52.07	
r	1841.00	100yr	60.60	22.14		: .	24.88	0.001197	1,41		31,64	-1,11
~	1841.00	50yr	46.30	22.14	24:47		24.50	0.001611	1:49	30,90 25,82	25.59	
	1841.00	20уг	42,00	22.14	24.30		24,43	0.002064	1.58		24.43	
ć	1841,00	107	38.70	22.14	24,18		24,33	0.002502	1.66	22,99	22.34	·····
7	1841.00	5ут	35.00	22.14			24.19	0.003667	1.87	19.03	10.98	
r	1841.00	2ут	26.20	22:14	23,64		23.88	0.007476	2,19	11,94	10.30	
			F 5 1	1						40.00	42.01	
ŕ	1834.00	100yr	60.60	22.08	24.74	24,01	24.86	0.001611	1,66	40,20	42.91	
r	1834,00	50yr	48,30	22,08	24.42	23,72	24,59	0,002492	1.87	27.91	27,30	- 1
r	1834.00	20yr	42.00	22.06	24.25	23.59	24.42	0.002859	1,88	23,67	22.19	
Ċ	1834,00	10yr	38,70	22,08	24.13	23,52	24,31	0.003269	1.92	21.17	20.17	
	1834.00	5vr	35,00	22.08	23.96	23,44	24.16	0.004122	2.00	18.02	17.28	
r	1834,00	2yr	26,20	22.09	23.62	23.23	23.62	0.005782	1.99	13,15	11.89	
4000						1						
7	1831,00 215 Creek Fload	F	Bridge		1	w.	7.64.7					
	1001100 1100						1 1 2	E : .			5	
	1828.00	100yr.	60,60	22.03	24.64		24.80	0.002165	1,81	34,90	29.63	
r r	1828.00	50yr	48.30	22.03			24.54	0.002703	1,84	27.04	27.98	
r r	1828.00	20yr	42,00	22.03	4	17.47	24,37	0.002980	1.83	23,07	18.76	
,	1828.00	10yr	38,70	22.03	24.10		24,27	0.003168	1,82	21,35	16.00	
r	1828.00	5yr	35.00	22.03			24.12	0.003567	.1,85	18,93	14.88	; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ;
ς τ	1828.00	2уг	26.20				23.78	8.004626	1.83	14.34	12.47	
•	-		1 - 1 ×	11			0	62 ft 37 ft 1			- 23	- 5 2
r	1821.00	100yr	60.60	21.99	24,58	:	24.78	0.002684	2.01	30,66	22.90	<u> </u>
,	1821.00	50yr	48,30	21.99	24,31		24,52	0.003283	2.02	24,48	22.18	
	1821.00	20yr	42.00	21.99			24.35	0,003448			13.17	<u> </u>
	1821:00	10yr	38,70	21.99		31.01	24.24	0,003528	1.92	20.17	12.91	
	1821.00	Syr	35.00			7.	24.09	0.003932		18,23	12,49	
	1821.00	2yr	26.20			C	23.75	0.004493	1,83	14,30	11.52	
r	1 (NETIMO	- 7		[3a.s.				:		ļ		
	1815,00	100yr	60.60	21.94	24,60	-1 -	24,76	0.001970		34.84	26:12	
	1815.00	50ут	48.30				24,48	0.002514		27,56	25.34	
		20yr	42.00		4		24.32	0.002836	+	23,50	24.88	
r.			38.70				24.22	6.002915		21.98	14.23	
r r	1815.00	Company of The Compan					24.05	0.003261	1.77	19.81	13,68	
r r	1815.00 1815.00	10yr	35.00			.,,	23.71	0.003778	1_70	15,44	12,48	
r r r	3815.00 1815.00 1815.00	5уг.	35.00 26.20	21,94				14 12 1	15		1981 7 6 4	
r r r	1815.00 1815.00		35.00 26.20	21,94			24.73	0.001103		41.49	31.88	
r r r	1815.00 1815.00 1815.00 1815.00	5уг. 2уг	26.20	7.2	24.62					1		
r r r i	1815:00 1815:00 1815:00 1815:00 1808:00	5yr 2yr 100yr	26.20 60.60	21.89			24.46	0.001516	1.53		31.29	
r r f t r	3815:00 1815:00 1815:00 1815:00 1806:00 1808:00	5yr. 2yr. 100yr 50yr.	26.20 60.60 48.30	21.89	24.34		24.46				31,29	
r r t r r	3815.00 1815.00 1815.00 1815.00 1806.05 1806.05	5yr 2yr 100yr 50yr 20yr	60.60 48.30 42.00	21.89 21.89 21.89	24.34		24.46 24.30	0.001516 0.001917 0.001981		27,14		
r r r r	\$815.00 \$815.00 \$815.00 \$1815.00 \$1815.00 \$1808.00 \$1608.00 \$1608.00 \$1808.00	5yr 2yr 100yr 50yr 20yr 10yr	60.60 48.30 42.00	21.89 21.89 21.89	24.34 24.17 24.06		24.46 24.30 24.19	0.001917 0.001981	1,63	27.14 24.44	30.91	
r r t r r	\$815.00 \$815.00 \$815.00 \$815.00 \$16.00 \$66.00 \$66.00 \$68.00 \$68.00 \$68.00 \$68.00	5yr 2yr 100yr 50yr 20yr 10yr 5yr	60,60 60,60 48,30 42,00 38,70	21.89 21.89 21.89 21.89 21.89	24.34 24.17 24.06 23.90		24.46 24.30 24.19 24.03	0.001917 0.001981 0.002337	1,63 1,59 1,63	27,14 24,44 21,71	30.91 17.51	
er er er er er	\$815.00 \$815.00 \$815.00 \$1815.00 \$1815.00 \$1808.00 \$1608.00 \$1608.00 \$1808.00	5yr 2yr 100yr 50yr 20yr 10yr	60.60 48.30 42.00	21.89 21.89 21.89 21.89 21.89	24.34 24.17 24.06 23.90		24.46 24.30 24.19	0.001917 0.001981	1,63 1,59 1,63	27,14 24,44 21,71	30.91 17.51 16.40	
r r r r r r r r	1815.00 1815.00 1815.00 1815.00 1808.00 1808.00 1808.00 1808.00 1808.00	5yr. 2yr. 100yr. 50yr. 20yr. 10yr. 5yr. 2yr.	26.20 60.60 46.30 42.00 38.70 35.00 25.20	21.89 21.89 21.89 21.89 21.89	24.34 24.17 24.06 23.90 23.90 23.56		24.45 24.30 24.19 24.03 23.53	0.001917 0.001981 0.002337 0.003072	1,63 1,59 1,63 1,60	27,14 24,44 21,71 16,48	30.91 17.51 16.40 14.01	
or o	\$815.00 \$815.00 \$815.00 \$815.00 \$16.00 \$66.00 \$660.00 \$680.00 \$680.00 \$680.00 \$680.00 \$680.00	5yr 2yr 100yr 50yr 20yr 10vr 5yr 2yr 10byr	26.20 60.60 48.30 42.00 38,70 35.00 25,20 80.60	21.89 21.89 21.89 21.89 21.89 21.80 21.80	24.34 24.17 24.06 23.90 2.23.56		24.45 24.30 24.19 24.03 23.59 24.72	0.001917 0.001981 0.002337 0.003072	1,63 1,59 1,63 1,60	27,14 24,44 21,71 16,48 43,52	30.91 17.51 16.40 14.01	
or o	1815.00 1815.00 1815.00 1815.00 1815.00 1808.00 1808.00 1808.00 1808.00 1808.00 1808.00 1808.00 1808.00 1808.00	5yr. 2yr. 100yr. 50yr. 20yr. 10yr. 5yr. 2yr. 10yr. 5yr. 2yr.	60.60 60.60 48.30 42.00 38.70 35.00 26.20 80.60 48.30	21.85 21.85 21.85 21.85 21.85 21.85 21.84 21.84	24.34 24.17 24.06 23.90 2.358 1 24.62 1 24.62		24.45 24.30 24.19 24.03 23.59 24.72 24.72	0.001917 0.001981 0.002337 0.003072 0.003072 0.000915	1,63 1,59 1,63 1,60 1,31 1,31	27.14 24.44 21.71 16.48 43.52 34.95	30.91 17.51 16.49 14.01 31.21 30.63	
and the second s	\$815.00 \$815.00 \$815.00 \$815.00 \$16.00 \$66.00 \$660.00 \$680.00 \$680.00 \$680.00 \$680.00 \$680.00	5yr 2yr 100yr 50yr 20yr 10vr 5yr 2yr 10byr	26.20 60.60 48.30 42.00 38,70 35.00 25,20 80.60	21.85 21.85 21.85 21.85 21.85 21.85 21.84 21.84 21.84	24.34 24.17 24.06 23.90 23.56 24.62 24.34		24.45 24.30 24.19 24.03 23.59 24.72	0.001917 0.001981 0.002337 0.003072	1,63 1,59 1,63 1,60 1,31 1,40	27.14 24.44 21.71 16.48 43.52 34.95 29.68	30.91 17.51 16.49 14.01	

Reach	River Sta	Profile	Continued) Q Total	Min Ch El	W.S. Elev.	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chril	Flow Area	Top Width	Froude # Chi
18461346		(370)	(m3/s)	(m)	(m) 23,55	(m)	(m) 23.66	(m/m) 0.002636	(m/s) 1.51	(m2) 17.60	(m) 17,29	0,42
Lower	1802.00	2yr	26,20	21.84	23,55		25.00	0.002.00				
Lower	1795,00	100yr	60,60	21.79	24.60		24.72	0.001141	1,48	40.54 32.26	29.43 28,35	
Lower	1795,00	50yr	48.39	21.79	24.32 24.15		24,43 24,27	0.001482	1,55 1,52	28.13	21,12	
Lower Lower	1795.00 1795.00	20yr 10yr	42.00 38.70	21.79 21.79	24.05		24.15	0,001598	1.48	26,18	18.14	0.34
Lower	17.95.00	5yr	35,00	21.79	23.69		24.00	0.001683	1.51	23.29	17,10 14.86	
Lower	1795,00	2yr	26,20	21.79	23.53		23.65	0.002489	1,49	17.68	. 19.00	0.1
Lower	1790.00	100yr	68.70	21.76	24,22		24.67	0.006973	2.96	23.21	11.33	
Lower.	1790.00	50yr	58.40	21.76	23.97		24.39	0.007335	2.67	20.33	10.93	0.67
Lawer	1790,00	20уг	52.00	21.76	23.84		24,22 24,12	0.007084	2,74	18.11	10.73 10.61	0.65
Lower	1790.00 1790.00	10yr 5yr	48.20 42.60	21.78 21.76	23.76		23.96	0.006765	2,54	16,79	10,41	0.64
Lower	1790.00	2yr	31.30	21,76	23.35		23.61	0.006279	2.25	13,93	9.98	0,61
					24.07		24.65	0.010250	3.37	20.39	11.39	0.80
Lower	1789.00 1789.00	100yr 50yr	68.70 58.40	21.75 21.75	24.07	23,62	24:35	0.014947	3.65	15.98	10.63	0.95
Lower Lower	1789.00	20yr	52.00	21,75	23.49	23.49	24,18	0.015860	3.68	14.13	10.30	1.00
Lower	1789.00	1077	48.20	21,75	23.42	23.42	24.08 23.92	0.016856	3.59 3.47	13.41	10.17	1.00
Lower	1789.00	5ут 2уг	42.60 31.30	21,75 21,75	23.31 23.06	23.31 23.06	23.58	0.017751	3.19	9.83	9.49	1,00
Lowar	1789.00	12,1	51.55									
Lower	1788;80	100yr	68.70	21.05	24.33	22.80	24.54	0.002323	1.99	34,51 30.75	11,92	0.37
Lower	1788.80	50yr	58.40 52.00	21,05 21,05	24.01	22.62 22.51	24,20 23.96	0.002325	1.85	28,15	11.45	0.38
Lower Lower	1788.80 1788.80	10yr	48.20	21.05	23.54	22.44	23.72	0.002774	1.91	25.28	11.23	0.41
Lower	1788.80	5yr	42.60	21,05	23.29	22.33	23.47	0.003023	1.89	22.54 17.61	11.02 10.63	0.42
Lower	1788.80	2yr	31,30	21,05	22.83	22,10	23.00	0.003370	1./8	17.51	10.03	1
Lower	1785,40 215 Cresk Road A		Bridge									
	2,10,20,20,00							0.000===		aner	10.78	0.45
Lower	1782.00	100yr	68.70	20.99	23,97 23,75		24.25 23.98	0.003569 0.003276	2.32	29.61 27.22	10.64	0.43
Lower Lower	1782.00 1782.00	50yr 20yr	58,40 52,00	20.99	23.57		23.79	0.003188	2.05	25.34	10.54	0.42
Lower	1782.00	10yr	48.20	20.99	23.32		23.55	0.003748	2.12	22.73	10.40 10.27	0.46
Lower	1782.00	Syr	42,60	20.99	23.10 22.69		23,32 22,88	0.004005	2.09		10.05	
Lower	1782.00	2yr	31.30	20.99	22.09		22.05	0.0072.00	. 6.1.		. 46.	
Lower	1777.00	100yr	68,70	20.94	24,07		24.19	0.001407	1,51	45.59	20.49	0.32
Lower	1777,00	50уг	58,40		23,83		23.93 23.74	0.001407	1,43	40.71 37.02	19.81	0.32
Lower	1777,00	10yr	52.00 48.20	20.94	23.64 23.59		23.74		1,49	32.28	18,57	0.36
Lower Lower	1777:00 1777:00	5yr	42.50		23.15		23.27	0.002223	1,52	28.01	17,92	
Lower	1777.00	2yr	31.30	20.94	22.72		22,84	0,003049	1:53	20.47	16.69	0,44
		100yr	68.70	80.08	24,07		24.17	0.001218	1:41	. 48,59	21.52	0.30
Lower Lower	1771,00 1771,00	50yr	58.40		23.83		23.92	0.001220	1.34	43.43	20.91	0.8.0
Lower	1771:00	20yr	52,00	20.88	.23.64		23.73	0,001276	1,32	39.52 34,45	20.43 19.80	0.30
Lower	1771,00	10yr	.48,20	20.85 20.85	23,39 23,15		23.49 23.25	0.001644	1,40	29:65	19.20	
Lower	1771:00 1771:00	5ýr 2yr	42.60 31.30	20,88	22,71		22.82	0.002823	1.45	21,61	18.09	0.42
Lower	11771200	-7,										0.00
Lower	1765.00	100yr	68:70	20.82	24.07		24;17 23,91	0.001111	1.40	49.43 43.71	24,05 22,59	0.29
Losvar	1765,00	50yr. 20yr.	58,40 52,00	20.82	23.82 23.63		23.72	0.001231	1,32	39.52	21,45	0.30
Lower Lower	1765.00 1765.00	10yr	48.20	20.82	23.38		23.48	0.001529	1,41	34.24	19.92	
Lower	1765.00	5yr	42,60	20,82	23.14		23,24	0.001887	1,44	29.67 22.10	18.50 15.66	
Lower	1785.00	2yr	31,30	20,82	22.70		22,80	0.002214	1.52	,	.5.50	
Lower	1759.00	100yr	68.70	20,76	24.07		24.15	D.000796	1,29	55,35	28,03	
Lower	1759.00	50 yr	58.40	20.76	23.83	7	23.90	0:000849	1.27	48,43 43,07	27.73 27.49	0.26
Lower	1759.00	20yr	52.00 48.20	20.76	23.63		23.71	0.000935	1,28		26.14	0.31
Lower Lower	1759.00 1759.00	10yr 5yr	42,50	20.76	23.13		23.23	0.001470	1.41	30,69	17.97	0,33
Lower	1759.00	2yr	31.30	20.76	22.69		22.78	0.001852	1,37	23,08	15.48	0.35
		1			55.5-	23.11	24.08	0.001544	3.61	22.05	14.46	0.82
Lower	1753,00 1753,00	100yr 50yr	80.65 89.60	20.16	23.35 23.21	22.90	23,84	0.001449	3.53	20.13	12,90	0,79
Lower Lower	1753.00	20yr	61.60	26,15	23.10		23.58	0.001354	3.30	18.80	11.71	
Lower	1753,00	10yr	52.05	20.16	22,96	***************	23,42 23,20	0.001240	3.01 2.75	17.29 15.85	9,59 9,28	4
Lower	1753.00	5yr 2yr	43.65 31.35		22,81		23,20		2.50	12.53	8,54	
Lower	1753.00	1	1 2.20	24.75								***
Lower	1752.90 Dropstructure 3	100yr	80.65	19,62	23,61		23.97	0,000519	2.71	32.75	15.13 15.02	0.50
Lower	1752.90 Dropstructure 3	50yr 20yr	69.60	19.62 19.62	23.43		23.75 23.57	0,000482	2.35		14,51	
Lower Lower	1752.90 Dropstructure 3 1752.90 Dropstructure 3	20yr 10yr	52.05	19.62	23.12		23.35	0.000408	2.14	25.65	13.69	0,43
Lawer	1752.90 Dropstructure 3	5ут.	43.65	19,62	22.95		23.14	0.000372	1.94	,	12,85	0.41
Lower	1752(90) Dropstructure 3	2yr.	31.30	19.62	22.56		22.70	0.000358	1.69	18,66	11.00	0.39
Course	1690.10	100yr	80.65	1,9,53	23,12	23.13	23.87	0.001704	4,12	25.73	18,63	0,84
Lower Lower	1690.10	50yr	69.60	19.53	22.96	22.96	23,66	0.001692	3,92	22,79	17.98	
Lower	1690:10	20ут	61,50	19.53	22:83	22.83	23,49		3,79 3,62	20.42 17.39	17.44	0.82
Lawer	1690.10	10yr	52.05 43,65	19.53 19.53	22.65	22,65	23.28 23.06		3.50	14.15	15.81	0.83
Lower Lower	1690,10 1690,10	Syr 2yr	31.30		21.92	21.92	22.60		3,57	8.54	6.22	1.90
LOWEL								0.100000	8.97	11.73	9,14	1.70
Lean verticate/sectors	1690.00	100yr 50yr	80,65 69.60	18.43 18.43	21.25	22.01 21.84	23.70 23.49				6.70	
Lower Lower	1690.00					- LUM	20.75					

Reach	Plan; Plan 05 River; Newsham River Sla	Profite	G Total	Min Gh El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slops	Vel Chn(::	Flow Area		Froude # Chl
66.750			(m3/s)	(m)	(m)	(m)	(m)	(m/m)	(m/s)	(m2)	(m) 5,88	1.96
ær	1690,00	1 Dyr	52.05	18.43	20.65	21.52	23,10 22.88	0.185477	6.94 6.93	7.50 6.30	5,46	+
et	1690.00	5yr	43.65 31.30	18.43	20.43	21.33	22,44	0.252358	6.76	4,63	4,81	
er.	1690.00	2yr	3, 3,1,50									
4	1660.00	100yr.	80.65	18.46	22.85	21.63	22.97	0.002423	1,58	52.67	40.93	0.28
r s	1660,00	50yr	69.60	18.46	22.68	21,23	22.80	0,002707	1,61	46.15 98.21	40.40 30.87	0.25
r	1650.00	20yr	61,69	18.45	22.45	21.0B 20.8B	22.58 22.42	0.003215	1.66	33.93	26.84	0.30
r	1660.00	10yr	52.05 43.65	18,46 18,45	21,80	20.66	21.55	0.005404	1,81	24,52	16,02	
r c .,	1660.00 1660.00	5yr 2yr	31,30	18,45	21.35	20,36	21,50	0.006684	1.73	18,12	11.24	0.42
	1820,00	150										
ur.	1643,10	100yr	80.65	18.35	22.55	21,92	22.93	0.000692	3.04	38,49	24.87	0.55
r	1643.10	50yr	69,60	18.35	22.45	21.78	22.77	0.000584	2.74	35.33 30.22	23,86	0.54
(1643,10	20yr	51.60	18.35	22,20	21.65 21.44	22.55	0.000574	2.50	28.30	22.62	0.45
Γ. Σ	1643.10 1643.10	10yr 5yr	52.05 43.65	18.35	21.22	21.22	21.89	0.002122	3.65	12.96	13.08	
r C	1643.10	2уг	31.30	18.35	20.73	20.73	21,42	. 0.002963	. 3.67	8.53	. 6.22	1.00
											26.09	0.23
	1643,00 Dropstructure 1	100yr	80.65	17.64	22.72	21.29	22.86	0.001698	1,45	49.67 46.58	25.22	0.23
	1543 00 Dropstructure 1	50уг	69,60	17.54	22,50 22,36	21.03	22.48	9.001038	1.39	40.80	23.49	0.23
<u>C</u> T	1643.00 Dropstructure 1 1643.00 Dropstructure 1	20yr 10yr	61.60 52.05	17.64	22.25	20.73	22.34	0.001683	1.29	38.13	23,08	0.22
	1643,00 Dropstructure 1	5ут	43.65	17.64	21.43	20,51	21.62	0.005179	1,89	22.76	14.58	
r	1643.00 Drapstructure 1	2yt	31.30	17.64	20,78	20.03	21.01	0.009855	2.18	14,69	10,40	0.45
			1		771		60.00	0.001313	+ 24	54.89	30,58	0.20
	1625.65	100yr	80.65	17.59 17.59	22,70 22,59	21,23	22.83	0.001313	1,16	51.31	29.24	0.19
	1625.68	50yr 20yr	59.60 51.50	17.59	22.34	20.88	22.45	0,001432	1,22	44,43	26.33	0.20
	1625.65	10yr	52.05	17.59	22.23	20.69	22.31	0.001280	1.13	41,48	25.80	0.19
21440	1825.66	5yr	43,65	17,59	21,34	20,47	21,53	0.005174	1.67	22.69	15.21	0,37
	1625.65	2ут.	31,30	17.59	20,36	19,97	20.77	0.020546	2.76	11.47	8.71	. u.bi
		400	92,50	17.48	22.64	21.31	22.78	0.000222	2.06	74,30	57,13	D.32
	1591,00	100yr 50yr	80.80	17.48	22,52	21,13	22.65	0,000208	1.54	67.50	56.58	0.31
r r	1591.00 1591.00	20yr	63,60	17,48	22.30	20,84	22.41	0,000180	1,75	55,97	47,72	0,29
	1591.00	10yr	55.90	17.48	22.18	20,65	55.58	8,000166	1.84	50.80	42,80	
	1591.00	5yr	44.70	17,48	21.24	20.32	21.46	0.000459	2.25 3.04	22.47 10.31	19.53	0.44
	1591.00	2yr	31.30	17,46	20.14	19,87	20.61	0.001760	3,04	19.01	,4,63	
1965 1865 1865	area co and Guard Barrier		Bridge									
	1583,50 285 Creek Road B		i Diage					1				
	1578.00	100yr	92.60	17.45	21.72	21,72	22,14	0.000796	3.28	45.24	54.71	0.59
	1576,00	50yr	60,80	17,45	21.18	21,18	21,92	0.001559	4,05	24,39 19,36	17.64 16.04	0.80
	1576.00	20yr	63,60	17.45	20,88	20.88 20.68	21.58	0.001643	3.83	16.34	14.21	0.E4
	1576.00	10/1	55.90 44,70	17,45 17,45	19.96	20.30	21.15	0.004810	4.63	9.26	6.40	
	1576.00 1576.00	5yr 2yr	31.30	17.45	19.66	19,84	20.57	0.004313	4.22	7,42	5.81	1,19
	107000	- 1									1 1	
	1525,60	100yr	92.60	17.30	20.95		21.06	0.001479	1.73	69.91	85.30 76.19	
	1528,60	50ут	. 80.80	17.30	20.83		20,94	0.001597	1.74	60.02 41.71	55.50	0.39
	1526.60	20yr-	63.60	17,30 17,30	20.55 20.39		20.70	0.002624	1.93	33.78	46.20	0.42
	1526.50	10yr	55,90 44,70	17.30	20,10	7	20.32	0.003606	2.12	22,54	28.50	0.48
	1526.60 1526.60	Syr 2yr	31.30	17,30	19.58		19.80	0.004412	2.05	15.30	9,73	0,52
	1,020,00											
	1411.00	100yr	92.60	16.87	20,58		20.75	0.002036	1,92 1,52	57.09 47.12	79.89 56.95	
	1411.00	50yr	80.80	16.87	20,43		20,61	0,002156	1.80	35,79	24,78	
	1411:00	20/1	63.60 55,90	16.87 16.87	20.17		20.21	0,001957	1.00	33,66	18,11	0.37
	1411,00	10yr 5yr	44.70	16.87	19.86		19.97	0.001591	1,47	30,34	15.13	
	1411.00	2yr	31.30	16.87	19,29		19,39	0.001866	1,41	22.16	13,41	0.35
				177				0.000.100	0.00	129.84	99.02	0,11
	1366.90	100yr	104.47	16.63	20.63 20.48	19,65 19,60	20.67	0:000175	0,61	129.84 115.88	94,58	
	1365,00	50yr	91,10 71.80	16.63 16.63	20.48	18.68	20.23	0.000275	0.69	.89,52	88.37	0.14
	1365.00	20yr 10yr	63.03	16.63	20.07	18,53	20.10	0.000325	0.72	78.33	85,47	
	1365.00	5yr	50.40	16.63	19.83	18.29	19.87	0,000502	0.84	60.18	76.24	
	1366.00	2ут	35.27	16.63	19.15	17.97	19,27	0.002069	1.57	22.51	11,48	0.36
							-			<u> </u>		
	1345,00 Newnham Road	-	Culvert		<u>;</u>			1				
	1217.00	100yr	104.47	16,11	20,09		20,37	0.001899	2.48	49.53	37,87	0,48
	1317.00	50yr	91,10	16.11	19.65		20.09	0.003147	2.97	33.43	31,79	
	1317.00	20yr	71.80	16,11	18.80		19,45	0.006168	3.57	20.12	10.60 10.22	0,83 0.84
	1317,00	10yr	63.03	16,11	18,60		19.23 18.87	0.006458	3,50 3,35	18.03 15.02	9.65	
	1317.00	5yr	50,40	15.11 16.11		17,79	18.44	0.005580	2,80	12.58	9,15	
	1317.00	2/1	35.27	10.11	10.04	17,18	,	3,4,3,650	2,00			
	1282.00	100yr	104.47	16.09	20.01		20,29	8.000404	2,49	49.58	21.40	
-	1282.00	50'yr	91.10	18.09	19,58		19.98	0.000437	2.43	43.75	18.60	
	1282.00	20yr	71.80	16,09			19.22	0.000744	2.72	28.79	17:79	
	1282.00	10yr	63.03	16.09	18.64		18.99	0.000767	2.54	25,06 20,65	17,75 9,71	
	1282,00	5yr	50.40	16.09	18.33		18.63	0.000748	2.44 2.24	20,66 15,76	9.71	
	1282.00	2y1	35.27	16.09	17,82		18,07	0.0008101	4,64	10,10	3.30	
		100	104.47	15,90	20.08	17.98	20.21	0.000149	1.67	72.69	50.72	0.28
		100yr			19.74	17.80	19.88	0.000174	1.69	57,49	34,98	
	1253.00		91.18	15,90	1 13/14	17,60		0.0401111;				
	1253.00	50yr 20yr	91,10 71,80	15.90 15.90	·	17.53	19.10	0.000274	1.81	39,78	16.20	0.37
r r r		50yt			·							0.37

-RAS Plan: Plan 05 River: Newn Reach River Sta	Prolég	Q Total	Min Ch El	W.S. Elev	.CrtW.5	E.G. Elev	E.G. Slope	Vel Chal		Top Width	Freuda# C
		(m3/s)	(m)	(m)	(m)	(m)	(m/m)	(m/s)	(m2)	(m)	18-16-20-20-20-20-20-20-20-20-20-20-20-20-20-
(0.18 50 S Was	usa l	Bridge									
er 1248.00 Bunnings Ware	nou j	S Singy								4 4 4	
rer 1243.00	100yr	104,47	15.89	19,69	18.29	20.05	0.000527	2.68	39.03	11.74	0
er 1243.00	50yr	91.10	15.69	19.27	18.09	19.53	0.000586	2.67 2.52	27,44	11.44	0
er 1243.00	20yr	71.80 53.03	15.89 15.89	18.65 18.51	17.78 17.63	18.62	0.000642	2.48	25.38	11,10	0
rer 1243,00 rer 1243,00	10yr 5yr	50.40	15.89	18.23	17.40	18.49	0,000594	2,25	22.31	10.81	
er 1243.00	2yr	35,27	15.69	17,73	17.08	17.95	0.000630	2,05	17.10	10.28	0
					/# / 6	20.01	0.000421	2.45	51.43	36,00	
er 1219.00	100yr	104.47 91.10	15.72 15.72	19.73	18,13 17,92	20.01	0,000558	2.78		12.25	C
rer 1219.00 rer 1219.00	50yr 20yr	71.80	15.72	18.67	17,61	19.02	0,000683	2,63	27,30	9,81	0
rer 1219.00 rer 1219.00	107	63,03	15.72		17,45	18.80	0.060633	2,46	25.59	9.75	0
er 1219.00	5уг	50.40	15,72	18.22	17,22	18.47	0.000552	2.20	22,95	9.66 9.49	i c
er 1219,00	2yr.	35.27	15.72	17.74	16.90	17.93	0.000520	1,93	10.01	1.5	
2400.05	100/2	104.47	15.60	19.75		19.98	0.000354	2.29	55.48	35.01	C
rer 1190.00	100yr 50yr	91.10	15.60	19,23		19.58	0.000565	2.64	36,92	33.35	C
er 1190.00	20уг	71.80	15.60	18.67	:	18.99	0.000602	2.51	28,55	9.84	
er 1190,00	10yr		15.60	18.50		18,78	0.000553	2.35	26.86 24.21	9.78	1
er 1190.00	5yr	. 50.40	15.60	18.22		18.45 17.91	0.000474	1.80		9.52	
00,0011	2yr	35.27	15.60	17.74		,,,,,,	0.000				
er 1164,00	100yr	104.47	15,44	19.79	17,82	19.95	0,000225	1.96	66.69	36.67	
er 1164,00 er 1164,00	50yr	91.10	15.44	19.30	17.62	19,53	0.000346	2.23	48.63	36.66	
r 1164.00	20уг	71.80	15.44	18.70	17.30	18.95	0.000451	2.29	32.23	12.91	
r 1164.00	10ут	63.03	15,44	18.52	17.15	18.75 18.42	0.000425	2.15 1.92	29,88	11.52	
r (164.00	5yr	50.40 35.27	15,44 15,44	18.24 17.75	16,92 16,61	17.89	0.000329	1.64	21.48	9,75	İ
or 1164.00	2yr	33,21	1,0,77	17770							
er 1160.00 Bunnings Ware	thou	Bridge									ļ
		8				40.70	0.000314	2.30	55.68	36.66	
r 1156,00	100yr	104,47	15.44	19.49		19.73 19.50	0.000344	2.29	46.78	36.66	
r: 1156.00	50yr	91,10	15,44	18.66		18.93	0.000468	2,32		12.90	
r 1156.00 r 1156.00	20yr 10yr	63.03	15.44	18.49		18,73	0.000438	2,17		12.88	
1156.00	5yr	50.40	15.44	18.22		18,41	0.000363	1,93		10.82	
1156.00	2yr	35.27	15.44	17.74		17.88	0,000334	1,65	21.38	0.75	
		201747	16:20	19.29		19,68	0.000621	2.87	43.58	36.00	1
1147.00	100yr	104.47	15,39 15,39			19,44	0.000708	2.90	33.93	31,41	
f 1147,00 f 1147,00	50yr 20yr	71.80	15.39	18.52		02.81	0.000,739	2,74	25.24	9.07	(
r 1147,00 r 1147,00	10уг		15.39			18.70	0.000653	2.52		9.01	
1147,00	5yr	50.40	. 15.39	18.14		18.39	0,009533	2.20	22.89	8.92	
1147,00	2yr	35.27	15.39	17.68		17.86	0.000452	1.87	18.85	8.72	
			45.00	19.33	17,73	19.63	0.000452	2.55	48.54	36.00	1
1135.00	100yr	91.10	15.33 15.33	19,06	17,52	19.38	0.000499	2,55	38.93	35.21	
1135.00 1135.00	50yr 20yr	71.80	15.33	18,55	17,21	18.84	0:000522	2,39	30,08	9.89	
1135,00	10уг	63.03	15.33	18,41	17,05	18.65	0.000462	2.20	28,62	9.84	1
1135.00	5yr	. 50,40	15.33	18.17	16,82	18.35	0.000375	1.92	26:27	9,76	
1135,00	2yr	35.27	15:33	17.70	15,50	17.84	0.000315	1.62	21,(/	0.00	i
Issan an In	heu	Bridge			<u> </u>						
1130,00 Bunnings Ware	I I I	3,03,0									
1127,00	100yr	104.47	15.33	19.02		, 19,47	. 0.000698	2.99	35.80	15.38	
1127.00	50yr	91,10	15,33	18.82		19.22	0.000653	2.78	32.98 30.01	13,21	<u> </u>
1127.00	20ут	71.80	15.33	18.55 18.40		18.84 18.65	0.000525	2.21	28.58	9.84	
1127,00	10yr	63,03 50,40	15,33 15,33	18.40	<u> </u>	16.35	0,000378	1:92	26,23	9.75	
1127.00 1127.00	5yr 2vr	35.27	15,33	17.70		17.83	0,000315	1,62	21.75	9.60	
1127.00	-71										l
1125,00	100yr	104,47	15.24		18.01	19.43	0.003631	2.74		31.02 25.62	
1125.00	50yr	91,10	15,24		17.82 17.52	19.19 18.83	0,003738	2.33		15.95	
1125:00	20yr	71.80 63.03	15.24 15.24	18.55 18.40	17,37	18.65	0,003356	2.19	+	15.59	
1125.00 1125.00	10yr 5yr	50,40	15.24	18,14	17.14	18.35	0,002945	1.99	25.58	14,98	
1125.00	2уг	35.27	15.24		16.82	17.82	0,003006	1.80	19.57	11.38	
				22,22		10.45	0,010798	3.75	28.08	15.18	
1099.00	100yr	104.47	14.80	 	18.24 18.05	19.18 18.98	0,010798	3.75		14.66	
1099.00	50yr 20yr	91.10 71.80	14.80 14.80		17.76	18,65	0,007761	2.95	·	13.64	
1099.00	1Dyr	63.03	14.80				0.007201	2.77		13.15	
1099.00	5yr	50,40	14,80	17.87	17,35	18,20	0.005718	2.53		12.53	
1099.00	2yr	35,27	14,80	17.14	17.03	17.60	0,013958	3.01	11.73	9,62	ļ
	1,22			18,49	17,44	18.75	0.003000	2.26	49.18	34.26	1
r 1066.00	100yr	104.47 91.10	14.52		17:28	18,61	0.002667	2.07		31.27	
1066.00 1066.00	50yr 20yr	71,80	14.52			18.36	0:002291	1,80	40,40	25.34	+
r 1066.00 7 1066.00	10yr	63,63	14.52		16,68	18.22	0.002098	1.67	+	20.99	
r 1066.00	5yr		14.52	17.85	16.66	17,58	0.001878	1,51		18.24	****
r 1065.00	277	35.27	14.52	16.85	16.33	17.13	0.004515	38,f	18,77	14.43	l
			4,00	10.57	16.27	18,61	0.000412	1,05	114:63	109.06	-
r 1047,00	180yr	91,10	14,36 14,36		16.12		0,000396	1.01	105.71	103.20	
CONTRACTOR	50yr		14,36		15.88		0,000397	0.97	88,58	92.78	ļ
	200						+	0.95	7.9,23	86,16	
r. 1047.00		63.03	14,36	18,11	15.76				4		
		63.03 50.40	14,36 14,36 14,36	17.85	15.76	17.90	0.000425	0.93	62.05	73.58 15,71	

Reach	lan: Plan 05 River: Newnham River Sta	Profile	O Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chol	Flow Area	The second second	Froude # Chl.
, ickon			(m3/s)	(m)	(m)	(m)	(m)	(m/m)	(m/s)	(m2)	Section 1	15035000000000
18WC	1029.00 Devlan Street		Culvert.					***************************************				<u> La companya da managan da manag</u>
ower	1013,00	100yr	104.47	13,37	17.47	15.67	17,60	0,001045	1.64	59.85	48,79	
Met.	1013.00	50yr	91,10	13.37		15.52	17.47	0.000918	1.50	55,04 57,98	39,80 32,23	
wer.	1013,00	20yr	71.80	13.37		15.29	17.24	0.000746	1,29	54.63	28.96	·
ower	1013,00	10yr.	63.03	13.37	17,05 16.84	15.18	17.12 16.90	0,000564	1.04	49.23	23.93	
אפר	1013,00	5yr 2yr.	50.40 35.27	(3.37	16.33	14.78		0.000581	0.92	38,44	18.73	0,20
ower:	10(3.00	231										
ower	982.00	100yr	104.47	12.82	17,43	15.37	17.55	0.001202	1.65	71.01	83.48 71.21	
ower	982.00	50yr	91,10	12.62	17.31	15.97	17.42 17.21	861100.0	1.59	64.81 54,70	49.83	
owar	982.00	20yt	71.80	12.82	17.11	15.65 15.51	17.09	0.0011069	1,40	49.80	39.85	
ower	582.00	10yr	63.83 50.40	12.62	16.79	15.25	16.87	0.001021	1,30	42.27	32.87	
ower ower	982.00 982.00	5yr 2yr	35.27	12.82		14.91	16,33	0.001407	1,34	27.10	21,70	0.31
51161	504.00											
ower.	959,00 Access Road		Colven									
		100yr	104.47	12.37	17.02	14,31	17.08	0.000368	1.00	. 98.10	64,51	0.16
ower ower	948.00 948.00	50yr	91.10	12.37	16.89	14.15	16.95	0.000355	0,96	91.18	58.22	0.15
3W81	948.00	20yr.	71.80	12.37		13.91	16,71	0.000339	0,90		51.06 46.98	
ower	948,00	10уг	63,03	12.37		13.80	16,58 16,34	0.000334	0.88 0.82	73.63 63.39	39.10	
ovyer	948,00	5yr	50,40	12.37	16.30 15.68	13.57	15.72	0.000322	0.78		19.38	
new.	948:00	2ут	35.27	12.37	13.00	167596	1207					
ower.	934.00 Secam Strest		Culveri									1
	7.00						100	p.anoana	2.11	76.58	36.04	0.34
wer.	918.00	100yr	116.35		16.40	14.76 14.56		0,000203	1.94	71.50	35.05	
wer	918,00	50yr	101.40 79.90			14.27	16.15	0.000161	1,68	53.54	33.44	0.21
war.	918.00	20yr 10yr	79.90	12,30	15.90	14.13		0.000133	1.55	59,49	32.60	
wer wer	918.00	5yr	56.10		15.71	. 13.91	15,79	0.000110		53.17	31.23	
W07	918.00	2yr	39,23		15.36	13,62	15.42	0.000086	1,11	43.03	27.78	0.21
				1000	15,47	13.94	16.53	0.000055	1:20	129,87	45.20	0.15
ower :	905.00	100yr	116,33	12.30		13.81	16.37	0.000048	1.10		44.31	
ower	905.00	50yr 20yr	79,90			13,59	16,11	380000.0	0.94	112.45	42.86	
wer wer	905.00	10yr	70,17	12,30		13,48		0.000033	0.86	107.01	42.10	
wer	905:00	Буг	56,10	12,30		13,29	15.76	0.000027	0.74		40,86 38,79	
wer	905.00	<u> </u> 2γτ	39.23	12.30	15.38	13.08	15,40	0,000020	0,59	D4.40	055,72	¥77
			+45.07	10.60	16.49		18.52	0,000015	0.80	217.45	64.20	0.11
)wer	904,90	100yr	115.33 101.40				15.36	0:000012	0,70	208,34	54,98	
wer	904.90	50yr 20yr	79.90				16,10	0.000009	0.58	194,79	53,39	
19WCF	904.90	1 Dyr	70.17		15.96		15,97	9,000008	0.53	187.90	52.34	
wer	904.90	5yr	56,10				15,76	0,900006 0,900004	0.44	177,09	51.02 48.93	
sver.	904,90	2yr	39.23	10.60	15,39		(5,40	0.000004	9.27	100.00		
		lano.	. 116.33	10,40	16.44	12.62	16.51	0.000068	1.31	120:44	41.1	
wer	879,00	100yr 50yr	101.40			12,44	16.35	0,000058			40,22	
wer	879.00 879.00	20yr	79.90	,		12.15	15,10	0.000044	1.01		38.79	·
yver	879.00	1.0yr	70.17			12.01	***************************************	0,000038	0.92		38.00 37.0	
over	879,00	5yr	56,10			11.60	15.75 15.40	0.000029	0.78		35.31	
wer	879,00	2уг	39.23	10.40	15.38	11.53	15.40	0.000018	0.01	00311		
ower	871.00 SQID Trash Rack	+	in Shici	 	-							ļ
, wei	107.000 COMO 1.000								2 5	60.63	40,64	0.32
lave	870,00	100yr	115.33				15.45	0.000216 0.000194		98.93	40.84	
wer	870.00	50yr	101,40	+			16.31	0.000194	,		39.10	
WET	870.00	20yr	79,90				15.93	0.000145	+		38,70	3 D.20
wer	870,00	10yr.	70.17 56.10				15.72	0.000122		72.00		
wer	870.00 870.00	2yr	39.23				15,37	0.000104	1,21	58.95	37.0	3 0.2
	070.00						1.5-	0.005282	1.08	117.42	46,1	D.11
wer.	845.00	100yr	116,23				16.37 15.23	0.005242		4	45.6	
war	845:00	50yr	101,40 79,90				15.99				44.71	5 D.1
wer	845.00	20yr 10yr	79.90	4			15.87	0.003622	0.81	95.76		
wer wer	845,00 845,00	5yr	56.10	11.28	15.65		15.87	0.003065		+		
wer	845.00	2yı	39.23		15.31		15:32	0.002603	0.61	72.65	42.2	B -0.1
			<u> </u>	35.7-	1000		16.04	0.006421	1.06	118.74	62,4	2 0.1
ower	798,00	100yr	116.33				15.93				62.1	9 0.1
nwer	798.00 798.00	50yr 20yr	79.90	·			15.74		0.89	101.19		
ower ower	798,00	10yr	70.17				15.64	0.004746				
owor:	798.00	5yr	56.10	11.12	15.46		15,48					
וטאט	798.00	2yr	39.23	11,12	15.14	ļ	15.16	0.004337	0.71	56,65	, 50.8	1 0.1
		7.4	416	10.98	15.75	13,16	15.80	0.005699	1,10	130.83	104,4	9 0.1
wer	759.00	100yr	116.33	-						·	91.7	8 0:1
OWRT.	759,00 759.00	50yr 20yr	79.90					0.003998	0.88			
ower ower	759.00	10yr	70,17			12.56	15.4B					
APPENDENCES	759.00	5yr	56,10	10.98	15.31	12,34						
2wet	759.00	2yr	39.23	10.98	14.99	12.07	15,01	0,002877	0.67	59,08	50,4	11 45.1
100 CO			Dulle -		+	-	 	-				
over ower		and the second s	Culver	<u> </u>		 	+	1	T	T		
ower ower	749.00 Unlarmed Road		7	i	£	1.			-		4	
owal, owel			116.33	3 10.85	14,74		14,83				69.0	
ower ower	749.00 Unformed Road 735.00 735.00		116.33 101,40		14.64		14,83 14,72 14,53	0.016947	1.33	82:65	67,2	6 0.2

	Plan 05 River; Newsham River Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chal	Flow Area	Top Width	Froude # Chi
Reach	rappi Sia	1.0700.00	(m3/s)	(m)	(m)	(m)	(m)	(m/m)	(m/s)	(m2)	jm)	
Lower	735.00	5yr	58.10	10.89			14.25	0,012506	1.11	55.56	53.89	0.2
Lower	735.00	2yr	39.23	10.89			13.94	0.009304	0.93	41.96	34.68	0.2
	1	\$1 (\$255.4356.25)										
ower	621.00	100yr	128.20	10.44	13.51		13.56	0.902704	0,60	142.28	84.90	0,1
_ower	621.00	50yr	111.70	19.44	13,38		13,43	0.002648	0,57	.131.31	84.09	0.1
ower	621.00	20уг	88.00	10.44	13.18		13.22	0,002559	0.53	114,22	82.82	0.1
Lower	621.00	10ут	77.30		13.08		13,11	0.002529	0.51	105.64	81.98	0.1
Lower	621.00	5yr	61,60	10,44	12.91		12.94	0.002494	0.46	92.10	80.21	6.1
ower	621.00	2ут.	43.20	10.44	12.68		12.70	0.002469	0.44	73.82	77,75	0,1
2.0016722000							1		-			
ower	498.00	100yr	128.20	9.52	12,82		12,90	0.009273	1,11	106.04	69.40	0.2
ower	498.00	50 _W	111.70	9.52	12.70		12.76	0.009287	1,07	97.47	67.94	
ower	498.00	20yī	88.00	9.52	12.51		12,56	0.009170	1.01	84.69	65.72	
cwer	498.00	10ут	77.30	9.52	12.41		12.46	0.009078		78.41	64.21	0.2
ower	498.00	5yr	51.60	9,52	12.25		12,29	0.008948		68.55	51.53	
DWGI	498.00	2ут	43.20	9.52	12,63		12.05	0,008856	0.86	55.11	57.93	0.2
Lower	300.00	100yr	128.20	6.90	11.42	9.92		0,002093	0.59	157.09	76,90	0.1
ower	300,00	50yr	111,70	8.90	11.09	9.85		0.002711	0.63	132.13	74,54	0,1
awer	300.00	20уг	88.00	6.90	10.83	9.73	10.87	0.002742	0,59	112.95	72.84	0.1
ower	300.00	10yc	77.30	6.90	10.56	9.58	10.50	0.003800	0.65	93.54	71.07	0.1
.ower	300.00	5yr	61,80	6.90	10.09	9.60	10.15	0.009011	0.87	60,91	67.29	0.2
72.78267384.2	200.00	20r	43.20	6.90	10.09	9,49	10,12	0.004403	0.51	60,91	57,29	0.1

Appendix I2

HECRAS Model Results for Philips Creek



HEC-RAS RESULTS

Reach River St.	: River: Phillips Reac Profile	G Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope		Flow Area	Top Width	Froude # Chl.
Reduct Tarrer St		(m3/s)	(m)	(m)	[m]	(m)	(m/m)	(m/s)	(m2)	(m).	495 S 100 S 100 S 100 S
Upper 1580 1580	Q2	30.50	15.12	17.71	16.89	17.88	0,005288	1.82	16.80	10.25	0.45
Upner 1580 1580	Q5	44,10	15.12	18.34	17.23	18.51	0.004117	1.84	24.83	29,13	0.41
Jpper 1580 1580	Q10	53.50	15.12	18.70	17,44	18.86	0.003552	1,67	35.39	47.66	0.40
Jpper 1580 1580	Q20	65.40	15.12	19.03	17,67	19.23	0,003802	. 1.97	35.88	54,09	0.40
Jpper 1580 1580	Q50	85.10	15,12	19.38	18:00	19.63	0.003919	2.23		62.55	0,43
Jpper 1580 1580	Q100	99,40	15.12	19.59	. 18.28	19,88	0,004172	2.41	45.48	68,63	0.45
			,,,,,		:						
Joper 1533 1533	O2	30.50	15.17	17.50	16.69	17.62	0.003981	1,54	19.78		0.41
Jopan 1533 1533	Q5	44.10	15.17	18.24	16,98	18.34	0.002005	1.42	39,40	55.17	0.31
Jopan 1533 1533	Q10	53.50	15.17	18.64	17,15	18,74	0.001549	1.40	53.81	59.36	0.28
Jpper 1533 1533	G20	65.40	15.17	18.99	17,35	19,09	0.001410	1.45	66.73	63.53	0.27
Jpper 1533 1533	Q50	85.10	15,17	19.36	17.64	19.47	0.001514	1,62	80.16	68.95	0.29
Jopen 1533 1533	O100	99,40	15,17	19.57	17.87	19.71	0,001613	1,75	88.19	85.71	0,30
1						1, 1					
Jopet 1454 1464	O2	30.50	14.82	17.38	16.12	17,44	0.001324	1.05		39.31	0:24
Jpper 1454 1464	O5	44.10	14.82	18.22	16.38	18.25	0,000581	0.87	82.76	83.39	0.17
Jpper 1464 1464	Q10	53.50	14,82	18.64	16.54	18.66	0.000440	. 0.83		90.51	0.15
Jpper 1454 1464	Q20	65.40	14.82	19.00	16.74	19.02	0.000395	0.85		95.91	0.14
Jpper 1464 1464	Q50	85.10	14,82	19,37	17,12	19,40	0.000420	0.93	153.51	111.19	0.15
Jpper 1464 1464	0100	99,40	14.62	19,59	17,34	19.62	0.000445	1.00	167.33	120,36	0,15
		7									
Joper 1898	O2	30.50	14.77	17.23	15.95	17,31	0.002105	1.28		14.40	
Jpper 1396	O5	44.10	14.77	18.12	15.24	18.19	0.001151	1.20		70.93	. 0.23
Upper 1396	010	53:50	14.77	18.54	15.42	18,61	0.000973	1.21	60.77	80.28	0.22
Jpper 1396	020	65,40	14.77	18.89	15.53	18,97	0.000957	1.30	72.10	89.39	0.22
Jpper 1396	0.50	85,10	14,77	19.24	15.95	19.34	0.001 140	1,50	83.24	98.59	0.24
Jpper 1996	Q100	99.40	14.77	19.44	17.17	19.56	0.001279	1,54	89.76	104.04	0.26
							A				<u> </u>
Jpper 1387 Anzac Ro	id	Culvert							<u> </u>	سنشب عددد	
- In the state of							6.71				
Jpper 1377	02	30.60	14.64	16.83	15.58	16.89	D.001584	1,11	27.64	15.21	0.26
Joper 1377	Q5	45.20	14.64	17.27	15.85	17,35	0.002013	1,29	34,99	21,75	0.30
Jpper 1377	010	54.30	14,64	17.46	16.00	17,56	0.002200	1,41	39,00	53:75	0.31
Joper 1377	C)20	00.00	14.64	17:56	16.17	17.78	0.002365	1.59	43,95	73.98	0.33
Jpper 1377	O50	86.40	14.64	17,97	16.45	18.13	0.002500	1.78	52,77	94:30	0,36
Jpper 1377	Q100	101.00	14.64	18.17	16,64	18,35	0,002724	1.91	59,30	100.68	0.37
spiret to 1			;			:					
Jpper 1329 1329	02	30,60	13,89	16,70	15.56	15,78	0.002557	1.24	26.07.	53.11	0.32
Jpper 1329 1329 Jpper 1329 1329	Q5	45,20	13.89	17,17	15,89	17.23	0.001618	1.18	52,19	118.42	0.27
	Q10	54.30	13,89	17.37	16.06	17.42	0.001455	1.19	64.35	124,41	0.26
Upper 1329 1329 Upper 1329 1329	030	66.00	13.69	17,58	16.27	17.64	0.001333	1,22	77.86	131.04	0.25
Jpper 1329 1329	Q50	85.40	13.69	17.91	16.84	17.97	0.001207	1.25	98,44	140.25	0.24
	Q100	101.00	13.89	18.12	16,99	18.18	0.001157	1.30	111,46	144.09	0.24
Jpper 1329 1329	12.00	10,,,,,			2.5	44.5	40,14		A:		1
Joper 1246	O2	30,50	14.16	16,12	15,27	16.27	0.004457	1.69	18,12	10,29	0,41
Jpper 1246	Q5	45,20	14.16	16.77	15,58	16.85	0.D02286	1,40	39.14	.93,34	0.30
Jones 1246	Q10	54.30	14.16	17.00	15.75	17.07	0.001862	1,32	49,68	94,87	0.28
A CONTRACTOR OF THE PARTY OF TH	OSO	85.00	14,15	17,24	15.96	17.30	0.001619	1.29	80.57	97.44	0.26
	Q50	85,40	14,16	17.60	16.68	17.67	0.001331	1.28	78,14	105.33	0.24
The second secon	Q100	101.00	14,16	17,83	16.78	17.90	0.001220	1.29	90.05	110.37	0.23
Joper 1246											
Joper 1234 Gellipoli F	ond	Culvert									
Joper 1234 Gallipoli F											Y
Joper 1222	CD2	30.60	13.96	15.74	14.88	15.84	0,003315	1.42	21.49	13.42	0,36
	Q5	45.20	13.96	16,05	15.14	16.22	0.004165	1.74	25.97	13.97	9.41
	Q10°	54.30	13.96	15.24	15,29	15,43	0.004630	1.91	28,46	14,36	0.43
The second secon	O20	66:00	13.96	15.46	15.47	16,68	0.005091	2.09	31.64	15,00	0.45
	Q50	86.40	13.96	16.87	15.75	17.09	0,004598	2.17	47.05	85.67	0.45
Upper 1222 Upper 1222	Q100	101.00	13.96	17:14	15.94	17,37	0.004251	2.21	59.40	88,18	0.43
Abhri Iree	2,00									, , , , , , , , , , , , , , , , , , ,	11.5
Jeper 1130 1130	Q2	30,60	12,59	14,54	14,23	14.65	0,008797	1.79	25.08	44,86	
	Q5	45,20	12.59	14,90	14,43	14,99	0.005970	1.57	42.91	53.13	
Upper 1130 1130 Upper 1130 1130	010	54,30	12.59	15:04	14.52	15,13	0,005570	1,69	50.67	55,96	0.47
Upper 1130 1130 Upper 1130 1130	Q20	66.00	12,59	15.19	14.75	15.28	0,005501	1.74		.58.53	0.47
Upper 1130 1130 Upper 1130 1130	O50	86.40	12.59	15.40	14.38	15.50	0.005420	1.83	71.89	62.57	0.47
	0100	101.00	12.59	15.53	14.95	15.64	0.005359	1.88	80,44	64.11	0.47
Opper 1130 1130	0100	101100									
Upper 1966 1986	QZ	30,60	11.63	13.99	13.23	14,08	0.003989	1,42	25,43	. 24,05	0.39
	Q5	45.20	11.63	14.35	13.54	14,46	0.003992	1.59	36,87	.42.40	0,41
	Q19	54.30	11.63	14.52		14,65	0.004403	1,77	45,76	65.56	0,43
Upper 1065 1056	Q20	56,00	11.63	14,72		14,65	0.003920	1.79	50.20	76,41	.0,42
Upper 1066 1066	The second control of	86,40	11,63	14,99	14.08	15.12	0.003430	1.84	83:27	89.19	0,40
The second secon	Q50 Q100	101.00	11.53	15.15	14,28	15,28	0.003306	1,89	97,44	91.81	0.39
Upper 1066 1066	UNU	101.00	11.00	744-743					,		
		00.00	11,20	13.44	12.61	13.56	0.004657	1.53	20.05	15.62	0.43
Upper 956 956	CO2	30,60	11.20	13,72	13.06	13.89	0.005529	1,83	25.83	45.47	0,48
Jpper 968 966	Q5	45.20		13.72	13.20	14,05	0.006017	1,98		62,16	
Upper 966 966	010	54.30	11.20		13.20	14,23	0.008451	2.15		77.26	
Upper 966 956	C)20	56.00	11.20	14.00		14,48	0.006423	2.13	51.03	89.16	0.54
Upper 966 966	O58	86.40	11,20	14.24	13.67		0.006210	2.40		91,21	0.53
Upper 966 966	Diop		11,20	14,39	14,00	14,64	01200010	Z.MU	00.00		
are constitution				<u> </u>	30.7	13.11	0.001720	0,91	47.73	55,42	0.26
ipper 861 861	D2	30,50	10.57	13.08	12.14	10.()	P-1011120	. 9,31	77.70	00,14	

HEC-RAS RESULTS (CONTINUED)

Reach pper pper pper pper pper pper pper	861 - 861 861 - 861	Profile OS	Q Total (m3/s)	(m)	CANADO LA CARROLLA	(m)	(m)	Im/m)	(m/s)	(m2)	(rn)	Lagrangia Calabaran
nadc hade hade hade	861 861	ns i			(m)	240104443.300	Same Day barrow					
nadc hade hade hade	861 861		45.20	10.67	13,41	12.32	13.44	0.001597	1.01	68.56	67.02	Ų.2
oper oper oper		Q10	54.30	10.67	13.58	12.42	13.61	0,001559	1.07	80.12	70,19	- 0.2
naqe naqe naqe	861 861	O20	66.00	10.67	13,76	12.53	13.80	0.001539	1.14	93.32	72.12	0.2
oper .		O50	56,40	10.67	14.04	12.62	14.09	0.001540	1.25	113.93	75,03	0.2
opar.	861 861		101.00	10.67	14.22	12.98	14.27	0,001559	1.32	127,10	76.77	0:2
	861 861	0100	101.00	10,07	17.55	, TLTOW					1.364	
	• 200	ACIAN A CONTRACTOR OF THE ACIAN AND ACIAN AND ACIAN AND ACIAN AND ACIAN AND ACIAN AC		0.04	12.30	11,60	12.47	0.004849	1,89	24.05	45,08	0.4
	718 718	O2	31,80	9.94	12.56	11.92	12.77	0,005556	2.22	35,19	50.28	0.4
xper	718 710	Q5	48.70	9,94			12.93	0.005970	2,39	41,10	52.23	0.5
oper.	718 718	Q10	58.30	9,94	12.69	12.29		0.006417	2.59	48.02	54.48	0.5
pel	718 718	Q20	68.60	9,94	12,84	12.53	13.11			59.47	61.06	0.5
poer	718 718	Q50	89.90	9,94	13.07	12.77	13.38	0.007042	2.89	67,65	66.05	0.5
эрег	718 718	0100	105.00	9.94	13.21	12.90	13.55	0.007314	3,06	67,05	90.03	0.0
											4670	0.5
oper	554 554	Q2	31.80	9,49	11.42	10.90	11.58	0.006236	1.61	22.30	44.72	
oper	554 554	Q5	46,70	9.49	11.69	11.20	11.85	0.005872	1.97	36.74	54.29	
		010	59.30	9.49	11.84	11.54	12.01	0.005629	2.05	44.72	55,58	0.5
oper			68.60	9.49	12.00	11.67	12,18	0.005368	2,13	54,24	57.07	0,4
per	554 554	020	89,90	9.49	12.25	11.85	12.44	0.005160	2.26	68.77	59.33	0.4
oper	554 554	COMP GUALINION					12.60	0.005147	2,36	77,85	62.04	0.5
орег	554 554	0100	105,00	9.49	12,40	11,96	12.00	5,000,47				
\$860 X.							11,06	0.002578	1,43	45.11	57.51	0.3
oper:	417 417	OZ	34,10	8.15	10.98	10.13			1.64	61.04	62.52	0.3
орег	417 417	Q5	49,90	8,15	11,25	10.66	11.34	0,002855			64.26	0.
oper	417 417	Q10	60.20	8.15	11,40	10.79	11.50	0.002918	1.73			0.
pper	417 417	Q20	73.80	8.15	11.56	10.93	11.68	0.003079	1.86		66,13	
	417 417	O50	96.80	8.15	11.80	11,13	11,93	0.003331	2.06		58.85	D.
oper	417 417	0100	113.00	B.15		11.27	12.07	0,003614	2.21	106.32	70,30	0.
oper	1417: 513:	S 200 20000 20000 2000 1										<u> </u>
			34,10	8.20	10.34		10.72	0.021631	2.93	17.91	33.83	0.
nper	374 374	C/Z		8.20	10.59	10,59	10,98	0.019121	3.10	26.95	40.85	0.
xoer.	374 374	05	49,90	8.20		10.71	11,13	0.019046	3.28		47.84	. 0
) BCC	374 374	010	60,20				11.30	0.017410	3.38		57.63	. D.
per	374 374	020	73,60	8.20	10,88	10.88			3.53		69,00	
pper	374 374	Q50	96.80	8.20	11.08	11.08	11.53	0.017048			77.70	
pper	374 374	Q100	113.00	8.20	11.24		11.67	0,015152	3,63	56:00	77.60	<u></u>
ASSESSED FOR			Testination		1.4				1 1 1 1			
pper	328 328	02	34.10	8.26	10.09	9.88	10.20	.0,005635	1.72		64.02	
	328 328	Q5	49,90	8.26	10.35	10:05	10,45	0.004723	1,76		65.78	.0.
oper		Q10	60.20	8.26	10,49	10,14	10,59	0.004436	1.80	61.18	66.85	: 0;-
oper		G20	73.80	8.26	~~~	10.23	10.78	0.004008	1.83	73.92	68,13	0.
pper	328 328		96.80	8.25	10.99	10.37	11,09	0.003409	1.86	95,14	70,76	0,
pper	328 328	Q50		8.26	11.24	10.45	11,33	0.002837	1.82	113.53	74.73	0.
pper,	328 328	Q100	113.00	6.40	11.64	10.50						A'.
						8.51	9.25	0.004339	1.56	23,58	21.92	0.
pper	214 214	O2.	34.10	6.80				0.003483	1.57		28.89	0.
per	214 214	Q5	: 49.90	5.80		8.76	9,72				33.20	. 0.
oper	214 214	Q10	60.20	5.80		8.90	9,97	0.003288	1.75		38.45	0.
per	214 214	C)20	73.80	6.80	10.09	9.07	10.25	0:003155				
per		Q50	96,80	6.80	10,46	9.34	10,65	0,003061	2.03		43,51	0.
		Q100	113.00	6.80	18.01	.9.51	10.99	0.002582	2.03	83,33	47.49	9.
oper	C17 C19	0.00				- (1		<u> </u>
<u> </u>	1.2		34,10	6.34	8.79	8.14	8.88	0.003415	1.50	37.22	44.56	D.
oper	125		49.90	6.34		8,44	9.45	0.001744	1.31		55.68	0.
por	125	O5				8,58	9.72	0.001488	1,30		59.18	0.
:per	125	Q10	60,20	6.34			10.01	0,001460	1.34		61,51	0.
oper	125	Q20	73,80	6.34	9,96	8.73		0.001293	1,43		64.71	0
per	125	Q50	96,80	6,34		8,96	10.42				65:73	0
per	125	0100	113:00	6,34	10.74	:9.07	10.79	0,001081	1.40	54.641	80.73	
1			1.745	6.5								
pper	122 Bikeway		Bridge									
100)	122 010110)								l			100
00000000000000000000000000000000000000	1440	G2	34,10	6.34	8.72	8.14	8.82	0.004144	1,61	33,93	42.32	
cper	119		49.90	6.34	9.36	8.44	9,42	0.001873	1,34	65,86	55,17	0
per	119	0.5			9.64	8.58	9,70		1.33		59,00	0
oper	119	Q10	60,20	6.34		8.73	9.99	0.001414	1,36	<u> </u>	51.31	. 0
per	119	Q20	73.80	6,34					1,44		64.65	0
per	119	050	96.80	6.34		8.96	10.40			125,41	65.68	0
per	119	Q100	113,00	5.34	10,72	9.07	10.78	0.001101	1.41	145.56	05.68	
					1					1		ļ
mar.	4 4	02	34.10	. 5.67	8,40	7.09		0.001214	0.98		23.32	
per	4 4	Q5	49.90	5.67	9.20	7.34	9.25	0.000736	0.97		49.50	
pper	control of companies. Parameters the new recomments of	Manager Manager		5.67	9,50	7.48	9.55	0,000708	1.02	79,17	58.47	. 0
pper	4 4	010	60.20		9,80	7,65	9.86	0.000726			67.71	0.
pper	4 4	Q20	73.80	5.67			10.27	0.000775			80.27	. 0.
pper	4 4	Q50	96,80 113,00	5.67 5.67		7.91 8.08		0.000775	1,23		92.25	0

Appendix I2

HECRAS Model Results for Salvin Creek



	Salvin-Final-09 River, Salvin	Ck Reach: Upp	er Feach O Total	Min Gh El	W.S. Elev Co	HWS. E.G. Elev	E.G. Stope	Vel Chril	Flow Area	Top Width	Froude # Cl
Reach	River Sta	1 (0)110	(m3/s):	(m)		(m) (m)	(m/m)	(m/s)	(m2)	(m)	3,800,000,000
er Reach	2130	Q 2 yr	15.90	24,88	26.42	. 26,46	0,004176	0.81	20,91	22.27	
or Reach	2130	Q 5 yr	23,90	24.86	26.74	26.77	0,003881	0.84	26.61	27.83	0
ar Reach	2130	Q 10 yr	30,00	24,88	26.97	27.01	0.003280	0.87	35.81	34,23 39,53	0
er Reach	2130	O 20 ýr.	35.50	24.68	27.16	27,20	0.002918	0.90	42.86	50,19	0
er Reach	2130	Q 50 yr	43.10	24.68	27.40	27.44	0.002593	0.93 0.94	53.00	63,75	0
er Reach	2130	Q 100 yr	49.30	24,68	27,58	27.62	0.602337	0.54	55.011	pa(12	-
						60.42	0.001376	0.83	20,45	21,43	0
er Reach	2120.	Q 2 yr	16.90	24,63	26,40	26,43	0.001378	0.86	27.76	24,46	
er Reach	2120,	O.5 yr	23.90	24,83	26,72	26,79	0.001187	0.83	34.09	25.54	t
ar Reach	[2120,7	Q 10 At	30.00	24.53	26,95	27.19	0,000013	0.92	. 40.21	34,04	0
er Reach	2120,*	Q 20 yr	35.50	24.53	27.14	27.43	0.000824	0.9€	48.59	39.46	1
er Reach	2120,*	Q 50 yr	43.10	24.63	27,38	27.51	0.000773	0,99	55.28	43.51	
er Reach	2120.*	Q 100 yr	49.30	24.83	27.56	27.00					2.11.1
				24.7E	26.38	28.42	0.001515	58,0	20.30	20.E4	
er Reach	2110;	Q 2 yr	16,90	24,78	26.70	25.74	0.001325	0.87	27,41	23.69	
r Reach	2110,4	D 5 yr	30.00	24.78	26.94	26,98	0.001201	0.90	33.31	26.61	1
ir Reach	2130.1	Q 10 yr	35.50	24.78	27,13	27.18	0.001071	0.93	35,52	30.36	- 1
r Reach	2110.*	Q 50 yr	43.10	24.78	27,37	27,42	0.000959	0,97	46.57	35.07	
r Reach	2110."	O 100 yr	49.30	24.78	27,55	27,60	0,000897	1.00	53.12	38.53	
r Reach	Zi iu.	<u> </u>					2.11			4	
r Reach	21.00.*	Q2 yr	16,90	24.74	25:27	26,40	0,001657	0.84	20.20	20,35	
r Reach	2100.	Q.5 yr	23.90	24.74	29.69	26.73	0.001465	83.0		23,03	
r Reach	2100.	Q 10 ÿr	30.00	24.74	25.93	26.97	0.001368	D.91	32.87	25.02	
r Reach	2100.*	O 20 yr	35.50	24.74	27.12	27,17	0.001256	0.94	37.98	27,74	<u> </u>
r Reach	2100.*	Q 50 yr	43.10	24,74	27.36	27,41	0.001116	0.98	45.07	31,81	
r Roach	2100.*	O 100 yr	49.30	24,74	27.54	27.59	0.001039	1,01	51,03	34,01	
			1		حال بنيست		A covere	0,84	20,12	19.93	
r Reach	2090,1	Q 2 yr	16.90	24,69	26.35	26.39	0.001603	0.89	26.97	22.48	4
r Reach	2090,*	Q 5 yr	23.90	24,69	26,67	26.71	0.001515	0.92	32.55	24.35	
r Reach	2090,*	C 10 yr	30.00	24,69	26.91	25.95	0.001515	0,95	37.47	25.90	
(Reach	2090,*	Q 20 yr	35.50	24,59	27.11	27.15 27.40	0.001299	0,98	44.09	29.39	7
r Reach	2090;*	D 50 yr	43.10	24.89	27,35 27.63	27.58	0.001202	1.01		32,10	1 1 1 1
r Reach	2090.*	Q 100 yr	49,30	24.69	41:04	27.50	,			7	11 42 11
	allege of	0.00	15.90	24.64	26.33	26.37	0.001988	0.84	20,06	19,58	13.5%
rReach	2080.*	0.2 97	23,90	24.64	26.65	26,69	0.001790	0.80	26.81	22.01	1,512.5
r Reach	2080,*	Q 5 yr	30.00	24.64	26.89	26.94	0.001699	0.93	32.29	23.79	
r Reach	2080.*	G 20 yr	35,50	24.64	27.09	27.14	0.001629	5.96	37.11	25.27	
(Reach	2080,*	O 50 yr	43.10	24.54	27,33	27:38	0.001531	0.99	43,44	27,58	
r Reach r Reach	2080.*	Q 100 yr	49,30	24,64	27.51	27.57	0,001417	1,02	48.55	29.97	
II:Neach	2000,	- Carlos Je					1.1.	11.41		يتبعث يبسب	
r Reach	2070.*	O2yr	16.90	24,59	26,31	26.35	0.002101	0.84	20.02	19,27	1 1 1 1
r Reach	2070.*	Q 5 yr	23.90	24.59	25,64	26.66	0,001909	0.90		21,59	
r Reach	2070.	Q 10 yr	00,00	24.59	25.87	25:92	0.001824	0.94		23,30	
r Fieach	2070.*	O 20 yr	35.50	24,59	27.07	27,12	0.001758	0,96		24,71	7 1.7.
r Reach	2070.*	C) 50 yr	43.10	24,59	27.31	27.56	0.001703	1,00		28.34	
r Reach	2070.*	C3 100 yr	49,30	24,59	27,50	27,55	0.001606	1.03	47.95	20.04	-
				151			0,002290	0.85	20,00	19.00	
r Reach	2060,*	O 2 yr	16.90	24.54	25.29	26,32	0.002097	0,90		21.24	1.1.1.1.1.1
r Reach	2060,*	Q 5 yr	23.90	24.54	25.61	26.90	0,002016	0,94	31,90	22.88	
r Reach	2060,*	Q 10 yr	30.00	24.54	26.85	27.10	0.001952	0.97	36,55	24.23	
r Reach	2060.*	O 50 At	35.50	24.54	27:05	27.35	0.001902	1.01		25.88	
r Reach	2059."	Q 50 yr	43,10	24.54	27.29	27.53	0.001862	1.04		27.13	100 100 100
r Reach	2050.*	Q 100 yr	49.3D	24.54	27.40		***************************************	11. 1			5
		4	10.00	24,49	26,26	26.30	0.002445	0.85	. 19398	18,77	1
r Reach	2050.*	Q 2 yr	16,90	24.49	26.59	26.63	0.002256	0.90	26.52	20.93	
r Reach	2050.1	Q 5 yr	23.90	24,49	26.63	26.88	0.002182	0.94	31.75	22.50	
r Reach	2050.	Q 10 yr Q 20 yr	35.50	24,49	27,03	27.08	0.002123	0,98	36,34	23.80	
r Reach	2050.7	O 50 yr		24.49	27,27	27,33	0,002080	1,02	42.29	25,39	
er Reach	2050.1	O 100'yr	49,30	24.49	27,45	27,51	0,002044	1.05	47,05	26.59	
r Reach	2050.*	M ING SI	1				1	44.7		2,000	1724 1
r Reach	2040.	O 2 yr	16,90	24.45	26,24	26,27	0,002546	0.85		18,56	
r Heach	2040.*	Q5yt	23.90	24.45	26.57	26,61	0.002455	0.90		20.65	
r Reach	2040.	Q 10 yr	30,00	24.45	26.81	26,86		0,95		22.17	
r Reach	2040."	O 20 yr	35,50	24.45	27.01	27,06	0.002331	0.98		23.42	
r Reach	2040."	Q.50 yr	43.10	24.45	27.25	27.30	0.002295	1.03		24,95 26,10	
r Reach	2040.1	Q 180 yr	49.30	24.45	27,43	27:49	0,002263	1.06	4E.69	ERIL	Trailed
			1	<u> </u>			0.00004		19.94	16.37	1
r Reach	2030,*	Q 2 yr	16.90	24.40	28.21	26.25	0.002814	0.91		20.39	
r Roach	2030.*	Q 5 yr	23.90	24.40	26.54	26.58 26.83	0.002524	0.95		21.86	
r Reach	2030.	O 10 yr	30.00	24.40	25.78 25.99	27.03	0.002515			23,07	
ir Reach	2030.*	0,20 yr	35,50	24.40	25.98	27.28				24.55	
r Reach	2030;	Q 50 yr.	43.10	24.40	27.22	27,47				25.66	
r Reach	2030;	Q 100 yr	49.30	24.40	14-12	1 1,47	1	l .			
		0.2	i i i i i i i i i i i i i i i i i i i	24.35	26.18	26.22	0.002985	0,85	19.91	18.20	
r Reach	2020.	Q2yr	16,90	24.35	26.51	25,56				20.17	
r Reach	2020,*	O.5 yr O.10 yr		24.35	20.76	26.50				21.59	
r Reach	2020.*	O 20 yr	35.50	24.35	26,95	27.01			35.80	22,77	
n Reach	2020,*		43.10	24.35	27.20	27.25		1.04	41.49	24.19	
er Reach	2020.1	O 100 yr	49,30	24.35	27.38	27,44				25.27	1
er Rezch	2020.1	C Ind M	53,50	E			<u> </u>				
. F	10010.5	O 2 yr	16,90	24.30	25.15	25,19	0,003158			18.04	
er Resch	2010.*	O.2.yr O.5.yr	23.90	24.30	26,49	26.53	0,002974	0.91		19,9F	
er Reach	2010.*	0.10 yr	30.00	24.30	26.73	26.77		0,95		21,85	
er Reach	2010.1	G SO At	35.50	24,30	26.93	26.99	0.002894			22.48	
or Reach	2010."	Q 50.yr	43,70	24.30	27.17	27.22				23.67	
er Roach	2010.	Q 100 yr	49.30	24.30	27.35	27,41	0.002873	1.08	45,73	24,91	<u> </u>
er Roach	IN.	1									
er Reach	2000,*	0 2 yr	16.90	24.26	25,12	28.15	0.003360			17.90	
	2000.*	0.5 yr.	23.90	24.26	26,45	26.50				19.78	
er Reach		C) 10 yr	30.00	24.26	26.70	25.74	0.003130	0.98	31.16	21.11	-1

W COMP VOLUME	alvin-Final-09 River: Salvin Ck River Sta	Reach: Uppo Profile	Q Total	Min Ch El	W.S, Elev	Cik W.S. E.G. Elev	E.G. Slope	Vel Chnf	Flow Area	Top Wi≾th	Froude # Cl
Reash	HMet 216	The family of		(m)	(m)	(m). (m)	(m/m)	(m/s)	(m2)	(m)	
er Reach	2900.*	Q 20 yr	35.50	24.25	26,90	26,95	0.003098	1.00	35.49	22.23	0.0
		Q 50 yr	43.10	24.25	27.14	27,19	0.003105	1.05	41.03	23.57	0
	2000.*	Q 100 yr	49.30	24.25	27,32	27,38	0.003097	1.08	45,45	24.59	<u> </u>
G07779-W7147								8.00	19.74	17.77	. D
er Reach	1990.*	Q2yr	16,90	24.21	26,0B	25.12	0.003514	0.85	26,10	19.60	
	1890.*	Q 5 yr	23.90	24.21	25.42	26,45	0.003402	0.92	31.02	20.91	0
	1990.1	Q 10 yr	30,00	24.21	26.66	26.71	0.003374	1,01	35.31	21.99	<u></u>
er Reach		O 20 yr	35,50	24.21	25.86	26.91 27.16	0.003370	1,06	40.78	23.29	0
er Reach		Q 50 yr	45.10	24.21	27.11	27.35	0.003370	1,09		24.28	0
er Reach	1990.*	O 100 Ye	48.30	24.2.1	27.29	21,33	0.00000	1,00			
				5115	26.04	25.08	0,003848	0.86	19,64	17.64	
		Q 2 yı	16.90	24.15	26.39	25.43	0.003609	0.92		19,44	
		Q 5 yr	23,90	24,16	26,53	25.58	0.003592	0.97	. 30.87	20.72	
r Reach	1980.*	Q 10 yr	30.00	24.16 24.16		26.88	0,00357,0	1.01	35,12	21.76	
r Reach	1980.*	O 20 yr	35.50	24.16	27.07	27,13	0,003602	1.06	40.52	23.03	
r Reach	1980.	Q 50 yr	49.30	24.16	27.25	27.31	0,603608	1.10	44.83	23.99	
r Reach	1980.*	Q 100 yr	49.30	. 24,16	2122					1 22 1	
		0.0	15,90	24:11	26.00	26.04	0:004037	0.87	19,52	17.44	
		O S At	23.90	24.11	26.35	26.39	0,003640	0.92	25,86	19.28	1
	1970.*	Q 5 yr	30.00	24.11	26.59	26.64	0.003832	0.98	30.79	20.53	
	1970.*	G 10 yr.	35,50	24.11	26.79	26,84	0.003817	. 1.02			
		O 20 yr	43.10	24,11	27.03	27.09	0,003863	1.07	40.24	22,78	
r Reach	The second secon	G 100 yc	49.30	24,11	27.21	27.28	0.003878	- 1011	44.50	23.72	1
r.Reach	1970,*	G JULY	43.00								
P. C. C.	1067.*	Q 2 yr	16,90	24,05	25.98	26,00	0.004238	0,87			
		Q 5 yr	23.90	24.06	26.31	28.35	0.004092	0.93			
		Q 10 yr	30.00	24.06	25,55	. 26.60	5.004092	0.98	30.49		
r Reach	The state of the s	Q 20 yr	35.50	24.05	25.75	26,80	0.004082	1,02	34.68	21.35	
r Reach	1960.1	Q 50 yr.	43.10	24.06	25,99	27,05	0.004145	1,08	39,93	22.55	
r Reach r Reach	1980.*	O 100 yr	19,30	24.05	27.17	27.24	0.004167	1,12	44.13	23,46	
1701041	1444						4 m 1		<u> </u>	1	1
r Reach	1950."	O.2 yr	16.90	24.02	25,92	25,96	0.004495	0.88	19,24	17.02	
r Reach	1950.	Q 5 yr	23,90	24.02	26.26	28.31	0.004415	0.94	25.51	18.99	
	1950.	C 10 yr	00.00	24.02	28.51	25.56	0.004419	D.59	30.26	20.18	
Reach	1950.*	Q 20.yc	35.50	24.02	25.71	25,76	0.004412			21.15	
r Reach		O 50 yr	43,10	24.02	26.94	27.01	0.004489				
r Heach	1950.*	Q:100 yr	49.30	24.02	27.13	27,19	0.004520	1.13	43,74	23,22	-
									19.08	16.81	
r.P.cach	1940.*	Q 2 yr	16.90	23.57	25.87	25.91	0,004899	0.89			
	1940.*	Q'5'yr	23,90	23,97	26.22	25.28	0.004715				+
	1940,*	Q 10 yr	30,00	23.97	26.46	26.51	0.004720		34.68		
r Reach	1940,*	O 20 yr	35,50	23.97	26.66	26.71	0,004714	1.04		22.10	÷
Reach	1940,*	Q 50 yr.	43,10	23,97	26.50	26.96	0,004807	1,10			
r Reach	1940.*	© 100 yr	49.30	23.57	27.08	27,15	0.004845		100,		1
* 100						25.81	0.019559	1,42	17.01	15.94	
r Reach	1930	Q2yr	24,10	23.92			0.020247	1,52	22.86		
r Fleach	1930	Q.5 yr	34,50	23.92		25,15 25,40					
r Reach	1930	Q 10 yr	43,30	23.92							
r Reach	1930	Q 20 yr	51.60	23.92	26.46	26,85		+		21.14	
r Reach	1930	Q 50 yr	62.50	23.92	26.69	27.03	0.022136	4			
r Reach	1930	Q 100 yr	71.60	23.92	25.86	27,03	3.022.100			2.13	
						25,64	0.013785		15,47	15,75	
r Reach	1920.*	Q 2 yr	24,10	23.79	25.53	25,99					
r Reach	1920.*	Ci 5 yr	34.50	23.79	25.86 26.09	25.23	0,014498				
r Reach	1920.*	C) 10 yr	43.30	23.79	26.26	26,43					
r Reach	1920.1	C) 20 yr	51,60	23.79	26.50	26.67	-		d		· · ·
r Reach	1920.*	C1 50 yr	£2,50	23.79		26,85				21,74	
r Reach	1920,*	Q 100 yr	71.60	23,79	26.67	20,00	1				1
					5E 46	25.50	0.013927	1,47	15,42	15.75	5
or Reach	1910.*	O 2 yr	24.10	23.66					·		
r Reach	1910.*	0591	34,50 43.30	23.66	<u> </u>	26.08	4				
Contract of the contract of th	1910.*	Q 10 yr	51.60	23.66	26.13	26.25				19.83	
	1910;*	Q 20 yr	51,60	23.66		26.52				20.83	
	1910.	Q 50 yr	71.60	23.66						21:7	il .
dason.	1910.1	Q 100 yr	71,001	20.00	1				1		
	error t	Q 2 yr	24,10	23.53	25.25	25.37	0.013937	1,47			
or Reach	1800.*	Q5yr	34.50	23.53	25.57		0.014380				
er Reach	1900.*	Q 10 yr	43.30	23,53	25.79		0.014616				
er Reach	1900.*	C 20 yr	51.60	23.53							
er,Reach	1900,*	Q 50 yr	52.50	23.53		25.37	0.014685				
or Reach or Reach	1900.	Q 100 yr	71.60	23.53			0.015027	1.92	37.28	21.69	4
ir Unight	1,000							1	ļ	1	1
or Reach	1890.*	ci 2 yr	24,10	23.40	25.11	25.2					
er Reach	1890.	Q 5 yr.	34.50	23.40	25.43						
ar Reach	1890.*	O 10 yr	43,30	23.40							
or Reach	1890.*	Q 20 yr	51.60	23.40							
r Reach	1890.*	Q 50 yr	62.50	23,40			~				
er Reach	1890.*	Q 100 yr	71.50	23.40	28.21	26,40	0.015211	1.94	36.94	21.5	'
							1	 	+	}	1
or Reach	1860.*	O 2 yr	24,10	23.27							
er Reach	1890.*	ОБУГ	34.50	23.27							
	1880,"	Q:10 yr	43.30	23.27							
	1880.*	Q 20 yr	51,60	23.27	25,58						
	1880.*	Q 50 yr.	62,50	23.27							
er Reach	1880,*	O 100 yr.	71,60	23.27	26.05	25,2	0.015072	1,96	36.6	21.6	-
er Reach er Reach							1		1	+	1
er Reach er Reach			,	25.45	24.63	24.9	0.014152				
er Reach ser Reach ser Reach ser Reach	1870.*	Q 2 VI	24,10	23,13	2.150						
er Reach er Reach er Reach ser Reach	1670.*	Q 2 yr. Q 5 yr.	24,10 34,50	23.13	25.13						
er Reach er Reach er Reach er Reach er Reach	1870.* 1870.*	02 yr 05 yr 010 yr		23.15 23.15	25.13 25.35	25.5	0.014731	1.73	25.10	18.7	5
er Reach er Reach er Reach	1870.*	Q 5 yr	34,50	23.15	25.13 25.35 25.53	25.5 25.6	0.014731 0.014865	1.73	25.10	18.7	5

EC-RAS: Plant S	Salvin-Final-09 River: Salvin C			nued)	Til more to to	laneà w e)	E.G. Elev	E.G. Stope	Vél,Chril	Flow Area	Top Width	Freude r Chl
Reach	River Sta	Profile	C Total (m3/s)	Min Ch EI	W.S. Elev (m)	Crit W.S. (m)	(m)	(m/m)	(m/s)	(m2)	(m)	Kermani Sacra
									1.50	16.10	15.63	0,47
Jpper Reach	1860.*	Q 2 yr	24,10	23.00	24.59 24.98		24.89	0.014181	1,64		17,60	0.48
Jpper Reach Jpper Reach	1860.* 1860.*	Q 5 yr	34,50 43,30	23.00	25.20		25.35	0.014724	1.74		18,74	0.48
Jpper Reach	1860,1	Q 20 yr	51.60	23.00	25.37		25.54	0.014873	1,82	28.34	19.70	0.48
Jpper Reach	1860,*	Q 50 yr	62.50 71.60	23.00	25.58 25.74		25.77 25.94	0.015391	1.99		21.58	0.49
Jpper Reach	1890.*	Q 100 yr	- 7.1.60	,23.00	1,37							0.46
Jpper Resch	1850;*	O 2 yr	24.10	22.87	24,54	<u> </u>	24.66	0,014404	1.51 1.65	16.51 20.90	15.87 17,58	0.48 0,48
Ipper Reach	1650.*	O 5 yr	34,50 43,30	22.87	24.84 25.05		25.20	0.014875	1.75		18:73	0.49
Ipper Reach Ipper Reach	1850,*	G 20 yr	51.60	22.87	25,22		25.39	0.015038	1.84	26.11	19,70	0.49 0.50
Joper Reach	1850,"	Q 50 yr	.62.50	22.87	25.43 25.58		25.62	0.015281	1,93 2.01	32.31	21.70	0.50
Jpper Reach	1850,*	Q 100 yr	71.60	22.87	23.36		1 25.10					
Jpper Reach	1840.*	Q 2 Yr	24.10	22.74	24,40		24,51	0.014509	1,51 1,66	15.91	15.90 17.56	0.49
Jpper Reach	1840.*	O 5 yr	34.50	22.74 22.74	24.69 24.89		24.83 25.05	0.014720	1.77		18.73	0.49
lpper Reach Ipper Reach	1840." 1840."	C) 10 yr	43.30 51.60	22.74	25,07]	25.24	0,015076	1.85	27.87	19,72	
Jpper Reach	1840."	Q 50 yr	62.50	22.74	25,27		25.47	0.015355	1,95		20,87 21,73	0.50
Joper Reach	1840.*	O 100 yr	71.60	22,74	25.42		25.63	0.015630	2.03	33,2.0	2.10.0	
Joper Reach	1830."	Q 2 yr	24,10	22,61	24.25		24.37	0.014690	1.53	15,80	15.89	0.49
Jpper Reach	1830.*	Q 5 yr	34.50	22.61	24,54		24.58	0.01506B	1,58	20.58	17.55	0,49 0.50
Joper Reach	1830,*	O 10 yr	43.30 51.60	22.61	24.74	ļ	25.09	0.015277	1:87	27.62	19.74	0.50
Joper Reach Joper Reach	1830;*	Q 20 yr	G2.50	22.61	25.71		25.31	0,015603	1.97	31.69	20.90	0.51
Jpper Reach	1830."	Q 100 yr	71,80	22.61	25.26	<u> </u>	25.48	0.015934	2.05	34,86	21.77	0.52
	1070 t	Q 2 yr	24,10	22.48	24,10	-	24,22	0.014714	1.54	15.66	15.88	0,49
Jpper Reach Jpper Reach	1820,1	Q 5 yr	34.50	22,48	24.28		24.53	0.014930	1.69		17.55	
Joper Reach	1820.*	0 10 yr	43.30	22.48	24.59		24.75	0,015150 0.015393	1.89		18.76 19.77	
Joper Reach	1820.*	D 20 yr	51.60 62.50	22,48 22,48	24,76 24,95		25.15	0.015786	2.00		20.34	0.52
Jpper Reach Jpper Reach	1820;"	O 100 yr	71.60	22.46	25,10		25,32	0.016124	2.08	34.41	21.77	0.53
,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,					20.00		24.07	0.014931	1.55	15.52	15.83	0,50
Joper Reach	1610."	Q 5 yr	24.10 34.50	22,35	23.95 24.23		24.38	0.015165	1.71	20.21	17,56	0.51
Jpper Reach Joper Reach	1810.*	Q 10 yr	43.30	22.35	24,43		24.50	0,015413	1.82		18,79 18,81	0.51
Jppor Reach	1810.7	Q 20 yr	51,60	22.35	24.60 24.79		24.76	0,015700 0.016188	1.91 2.02	27,04	20.98	0.52
Jpper Reach	1810,*	Q 50 yr Q 100 yr	62.50 71.60	22.35	24.79		25,15	0.016349	2.11	33.93	21,66	0.54
Jpper Reach	1810.	4 (4)								15.70	15.82	0.51
Jpper Reach	1600,1	O 2 yr	24,10	22.22	23.80 24.08		23.92	0,014754	1.57 1.72		17.58	
Jpper Reach Jpper Reach	1800;*	Q 5 yr.	34,50 43,30	22.22	24,27		24.45	0,015300	1.83	23.61	18.83	
Joper Reach	1800,*	Q 20 yr	51.50	22.22	24.44		24,63	0,015651	1.93		19,85	0.53 0.54
Jpper Reach	1800.7	D 50 yr	62.50	22.22 22.22	24,62		24.83	0.016052 0.016141	2.05		21.55	0.55
Jpper Reach	1800.*	Q 100 yr	71.60	22.22	25,72		1				11	
Joner Reach	1790.*	O 2 yr	24,10	22.09	23,65		23.78	0.014935	1,5B		15,83 17.83	0.51 0.52
Jpper Reach	1790."	Q 5 yr	34.50	22.09 22.09	23.92	:	24.08	0,015230	1,74		18.90	
Jpper Reach Jpper Reach	1790.* 1790.*	Q 10 yr Q 20 yr	43.30 51.60	22.09	24.27	-	24.47	0.016028	1,95	26.42	19.93	0.54
Joper Reach	1790.*	Q 50 yr	62,50	22.09	24,45		24.57	0.016216	2,08		20,81	
Jpper Reach	1790.*	O 100 yr	71,60	22.09	24,59	ļ.	24.83	0.016253	2.17	33.03	2047	
Jpper Reach	1780;*	O 2 yr	24,10	21.96	23.50	 	23.63	0.014962	1.59		15,85	
Јррег Неасп Јррег Явасп	1780.*	Q 5 yr	34.50	21.96	23,77		23.92	0.015324	1.75		17,69 18,97	
Jpper Reach	1780.*	Q 10 yr	43.30 51.60	21.96 21.96	23.95 24.11		Z4.13 24.31	0.015777	1:98		19.88	0.55
Upper Reach Upper Reach	1780.* 1780.*	Q 20 yr	62.50	21,96	24.28		24.51	0.016204	2.11	29,69	20.69	0.56
Joper Reach	1780,*	Q 100 yr	71,60	21.96	24,42	ļ	24.67	0.016256	2.20	32.58	21,32	0.57
		Q2yr	24.10	21.82	23.34		23.47	0.015196	1.51	15.01	15,88	0.53
Upper Reach Upper Reach	1770.* 1770.*	Q 5 yr	34.50	21,82	23.61	**.	23.77	0:015641	1.77		17,76	
Upper Reach	1770.*	O 10 yr	43.30	21.82	23.79		23,97				19.04 19.75	
Upper Reach	1770.*	O 20 yr O 50 yr	51,60 52,50	21.82	23,94		24.14		2,14	29.27	20.56	0.57
Upper Réach Upper Reach	1770.*	Q 100 yr	71,60	21.82	24.25		24,51	0.016382	2.23	32.12	21,18	0.56
				04.00	23.19		23.32	0.015307	1,52	14.57	15,84	0.54
Upper Reach Upper Reach	1760.*	Q 2 yr Q 5 yr	24.10 34.50	21.69 21.69	23.45		23,61	0.015894		19,23	17.85	
Upper Reach	1760.	Q 10 yr	43.30	21.69	23.62	1	23.81				18.92	
Upper Reach	1760,*	O 50 At	51.60	23.69	23.77		23,98				20,42	
Upper Reach	1760.	G 50 yr G 100 yr	52.50 71.60	21.69 21.69	23.95 24.08		24,34					
Upper Reach	1750.1				1	1:	1			17.70	15,01	0,54
Upper Pleach	1750.*	0.2 yr	24,10	21,56 21,56	23.03		23,45		1.64			
Upper Reach Upper Reach	1750.* 1750.*	Q 5 yr	34.50 43.30	21,56 21,56	23,45		23,65		1.95	22.09	18:76	0.58
Upper Heach Upper Reach	1750.	Q 20 yr	51,60	21,56	23.50		23.82		2.07		19.46	
Upper Reach	1750.1	O 50 yr	62.50	21.56			24.18					4
Upper Reach	1750."	O 100 yr	71,60	21.56	23,92	 	24,18	5,010,30				F 45 (4.7)
Upper Reach	1740.*	O Z yr	24,10	£1,43	22.87		23.01	0.015815			16.10	
Upper Reach	17407	O 5 yr.	24.50	21,43	23,11		23,29					
Upper Reach	1740,*	Q 10 yr Q 20 yr	43.30 51,60	21,43	23,25		23.66		2.09	24.64	19,31	0.59
Upper Reach Upper Reach	1740.	Q 50 yr	E2.50	21.43	23.61	<u> </u>	23:86	0.016097	2.22			
Upper Réach	1740.*	Q 100 yr	71,60	21.43	23.75	1	24,02	0.016028	2,31	30.96	20.75	0.50
	1730.*	Q 2 yr	24,10	21.30	22.71		22,85	0.016217				
Upper Reach				2		4	23,12		1,89	18.29	17.59	0:59

	1	I com cont	. C-2Z	0.007730	EE.15	T	21.08	18'63	05.55	O 10 M		E921 (1269H.):
29:0	£2.31	95.61	EZ Z	9E370G.0	11.15		00.00	19.63	34.50	34 2 0		देशकेर अध्यक्षकारी भ
910	62'71	07,01	5.00	205800.0	20.61	_	75.02	53.61	01.45	५८०।		CRET HOSAN A
3910	14,12	10.81	Se't	505800 D	11400	+	17700	1		725 July 200 10		
									Culver	10.000000000	Bayan St Culved	P031 1569A 1
										201223		
				Legitor	115077	82.12	87.55	ELEE	09.17	G-100 Yr		oret dassR1
2.0	25.24	h1.8a	3E.1	166100.p	78.55	21.11	65.55	19.73	62.50	A DS D		Otel hosaRi
6.0	44.83	0713	1.28	815100.0	22.71		22,44	ET.E1	09:15	10 20 Yr		C(81 1815
2.0	31.14	10.E2	91.1	01.5100.0	55,51	£6.0S	22.06	E7.61	02.52	G 10 Xc		CTREACH 1810
32.0	59.65	05.66	81.1	X38100.0	22.13	20.80	21,75	E7.61	34.50	G 5 yr		Of Br 1510
0.25	76.42	20,16	P1/1.	156100.0	19.15	35.05		E7.61	24,10	OSW		Ular dasath
6.0	18.32	22.45	70.1	828200.0	Ob. t.S.	95.05	21,34	PEC	10110			5555
				<u> </u>				98.61	09.12	Q 100 yr	1.5 (2) (2) (2) (2)	r. Nasarh 1620.
0 3	ZB.04	30.88	ፈቱ ነ	9981000	68.SZ		22.79		85.50	N OS D		(Reach (1620)
0.29	20,70	25,34	TE.I	1/L/100.0	ET.SS		22:64	98'61		OSU	A. C.	r Reach 1620.
Z'C	32.14	62.24	1.24	+k8:00.0	22.53		55.45	38.61	08.12	0.10 %		г Невси 1620.
£.0.	67.25	34.84	62.1	0.005200	22,15		70.SS	19.86		NeO.	CHILL TO COMMAND TO COMMON STORY OF THE PARTY OF THE PART	(Reach 1620.
E.G.	71,15	95.72	92,1	198200.0	12.15d		51.19	88.61	0976	77 E C		: ISBI NaceRa
E.O	18.82	60°0Z	1.20	183200.0	E7'LZ		58.13	38.21	24,10	34.6.0		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,
	1200			- 20						The second second		.0081 1630.°
5.0	33.49	98.03	99'1	0.002427	22.92		08.52	66,61	71.60	14.001 to		осат пасея.
0.33	46,06	61.34	201	EECZCO'G	97.SS		22.65	66'61	09'29	1K 05 D		DEBI RoseR1
0.31	17.75	09'07	1:34	012200.0	22.55		22.45	19.99	09.13	Nazol		. Reach 1630.
30'0	22.67	71,15	Dh.t	0.003239	31.52		80.52	19,99	06.65	1, 10 TO		.0531 dosell
0.3	18.81	4B.45	66,1	0.003952	88,15	1	87,1%	66'61	34.50	17 5 D		. 0591 1620.
70	£6'51	10.81	1.34	572400.0	31,15		21,39	66.61	24.10	36.2.0		. ULBI 4000 E
					-							.040t daceRr
100	\$1.85	89'57	491	822500.0	55'22		18.52	21,02	09.17	1/ Cat (D)		Star Section Asy Constant to Assessment Street
25.0	16.72	41.53	Z\$`1	Z\$1E00'0	22.79		7,9"ZZ	20,12	05.58	N 96 D		
35.0	68.45	05.80	Fe'L	0.003068	85.55		72,47	20,05	08.12	C 20 W		C 733 744 C 244 C 24 C 24 C 24 C 24 C 24 C 24
14.0	20.30	55.85	55,1	895+00'0	22.23		11.55	21,05	06.64	N 01 D		
		59.52	52.1	186200.0	E6.15		21:81	20.12	34.50	14.2.0		Cohai dodan
	#E'SI	16.22	61.1	878800,0	\$1'24		21,43	20.12	01.42	O SAI		1099F 1540.
97'0	12.51	CU 21		-		1			4			
(WO	Part Cons	47.62	823	0,004240	00.CS		59'62	SZ'OZ	09'1.4	37-001 D		. Ковси 1650.
14.0	08.85	97,78 58 th	1,68	0.004223	22.83	1	52.69	\$2:0Z	05.58	. ⊃y a≥ D		Daar daadA
010	24.74	\$2,26 87,76	95.1	0.004225	Z2.52		05.55	9Z:0Z	09,12	1 20 yr		.028f db.eA.
6E.0	22.32		9971	9009000	55,29		31'78	\$2:0Z	06.E#	14 at 0		.ozat foseR
97'0	11.21	20,85	95.1	1912000	22.00	7	21.85	20.25	05.46	3X 5 C)		. Везер цегов.
BY 0	177.34	B7.0S		0.009285	28.15		6712	52.02	54.10	77.5.0		. Вейсь 1650.
56.0	52.51	177.27	£9.1	SECUSO O	10070							
- 71	<u> </u>			937200.0	23.05	-	78.5Z	20.38	03,17	C 100 M		Ragch 1860,"
3Þ'0	24.24	38.22	68,f	9595000	22.69		27.52	20.38	05.29	14.02.D		Hosch 1660.
570	85,55	34.61	08.f		22,68		E5.52	BC.0S	09,18	OZOK		Haach leed.
V C		69.05	69,1	708200,0			22.20	86.05	06.50	G 10 K		. Rasch (680.7
	85'81	61°76	61.1	≯86¥00.0	55,38		56.12	86.68	05°1°E	O 2 Ac		. Gaat 1560A
ES'O	16.91	15.81	67.1	+09600.0	\$5,09		85,15	86.05	DLAS	054		. Deat 1200 H
89°D	15.27	08.51	87.1	628510.0	17,15		13314	10000				
25.50			· 1 5%	<u> </u>	1			15102	09.17	100 M		Rosch 1670.
05.0	22.35	07,86	10,2	ZS+200.0	21,65		Se,52		02.50	U SO Yr		.10291 1670.°
610	20.15	32.56	56:1	584700.0	22.96		177.55	15.02	09.12	O 20 Vr		COZEL 40eaH
55,0	+ 6161	28.63	08.3	EEETCO.0	22.75		. 85.55	1902	13.30	W01.0		1,0731 AscaH
75.0	61.81	22.36	06,1	1009934	22.46		15.25			17.20		Roach 1670.
99'0'	12.91	06.81	68.1	4(81)0.0	22.20		20.25	15.02	0572	0.277		1,0781 Asset
29'0	15.37	8E,ET	08,1	868410.0	78.15		17,15	12.02	01,4S	4.60		10201
	1 1 1 1									and and the		1.0881 dassH
0.54	21.32	33.84	212	\$85,600.0	12.62		32.99	20.65	0917	34 001 D		,0881 daeaA
65.0	\$0°24	30.02	2,03	0.009224	23,05		18.52	39.05	05.59	0.50 Yr		.1880; HaneA
25.0.	67'61	26.92	161	102600.0	22.84		28.5S	20,65	09115	C 20 yr		Reach 1560.
85.0	BC.TI	97,15	66"	9105000	72.52		7E.52	68,02	43.30	Noto		Maria and Anna and and an anna and an
0,50	17,31	17.72	95'1	0.013845	22.33		PURZ	59'02	05'78	M S O		A STATE OF THE PARTY OF THE PAR
£8,0	15,52	13.28	18.1	0.016041	55.03		88,15	20.65	01.12	ηςο		.0831 1589.
												In any Company
15.0	20.02	35,48	5.30	8\$8010.0	SE.CS		70.ES	20,76	09.17	37 001 0		Geach case?
25'0 85'0	12.02	23.18	2:12	678010.0	81.65	1	52,93	87.0S	62.50	N 02.0		Contract to the second contract to the second
	12.02	17.02	2,00	886010 0	\$6'22		22,74	87,05	03.12	N 02 O		. реат навая
55.0		81,12	2.04	£19E10.0	22,70		6\$'22'	87.02	43.30	7,01.0		1690 Teeft
0.60	25'11	8t 12	1.0.0	0.015138	84,55		22,26	87.05	OSTE	N 2.D		",Deat Appen
29'0			08.1	815810.0	\$2,19		£0,52	87,02	24,10	1/20		1,0981 naseAR
59,0	17.21	15,Et	U8 F	017414 N	+====			1		100000000000000000000000000000000000000		
		16015	12.2	124210.0	29.44	-	B1.cs	16.02	71,60	O 100 %		Heach 11700.
65.0	20.78	£9,16		0.012619	23.28		23.04	16'02	62.50	14 DS D		Reach 1700,
85.0	20,02	19,82	2.18		83:08		22.65	16.02	09'15	N 02 D		Нааст 1700.
820	90'61	54:94	20.2	0,014963 S47S10.0	33.02		22.63	16,0\$	00'51	W 01 D		Навси 1700.
19'0	95,71	Z6:0Z	70.3	610310.0	22.63		22,43	16.05	24.50	מפא		.10071 ftsebH
59,0	76.81	25'21	(6,1	083810.0	22,36		02,52	16.02	24.10	18.5.0		1,005f / risseR
19,0	05'91	Za.er	TLI	nanatri n	100 00			_				
	120		-1	0.038610.0	78.62		0E.ES	10,15	05.11	JA 001 D		Heach 1710.
09'0	79.05	E0.1E	12.3		14,65		B1,65	21.04	62.50	38 05 D		Neach 1710.
09.0	36.61	år.as	2.22	0.013723	23.20		78.55	1012	08.12	O SO M		1,011(1 dasaA
65'O	E0.61	24.50	11.5	\$66£10°0			87,55 59.05	21.04	4330	14.01.0		Reach 17710,"
18,0	80.81	20.93	70.5	656810.0	23.00		22.60	21.04	34.50	N S O		1710.º
19'0	71,77	17.77	56.1	0.016270	£7.52		76.5S	21,04	24.10	O 2 XL		Reach 1710.
65.0	01.81	78.61	\$£'1	012510.0	22.52		12.0 24		- 			
77	1 1. 1.				<u></u>	4	- Ithrea	21,12	09.17	N 001 D		Hoseh 1720,
19.0	59,02	30,76	2,33	168410.0	53,72		23.44		05.29	10 co At		Reach 1720.
09'0	96'61	19.75	5.24	753410.0	53,56		23,30	71,15		O 20 Vr		Heach 1720.
09'0	20.61	24.33	5.12	0.015090	23,35		23,12	23.12	03.13	W 67 D		105VI , dasaR
190	EZ.81	51,08	502	871310.0	23,16		25,94	71.15	05.64	0.5%		Hoach 1720.
09,0	86.71	16'21	ZG'I	684810,0	98.55	1	77,55	TI, ES	05't£			Heach 1720.
69'0	(8.28)	14,12	IL.	0.018870	22,69		22.54	21,12	24:10	0.2%		73.79
				1					ستبيل	1 77237		Heach 1730.
19'0	07.0Z	30,76	2,33	1+5510'0	¥8.65		89.69	21:30	09,17	N 001 D	and the second second	60°156000°00000 E0000000000000000000000000000
0.60	ND.02	27.93	2.24	699510.0	17.65		S4.82	21.30	62.50	0.50 %		55 C. D. C.
09'0	71.61	24.40	2.11	128210.0	d2.65		75.25	21,30	08.18	14.02.0		
		75.15	2.03	0.016472	\$3.32	1.	11.63	05.12	43.30	N OLD		Невси 1730г.
	[5'R1											
09'0	(m) (15.81				(m)	(m)	(m)	W (B40.6	M 1510 T.D. (216m)	95019 1	FIS 184H	чэев

Reach	Inal-09 River: Salvin Ck Reach: Uppo River Sta I Profile	C Total	Min Ch El	W.S. Elev	Crit W.S. E.G. Elev	E.G. Slope	Vel Chrl	Flow Area	Tep Width.	Froude # Cht
neach	1000	(a:Cm)	(m)		(m) (m)	(m/m)	(rt/s)	(m2)	(m)	36-34-36-3
er Reach 1595	Q 20 yr	51.60	19.63	21.25	21.51	0.007750	2.38 2.56	22.14		0.6
er Reach 1595	C 50 yr	52.50	19.63	21.40	21.73	0.007752	2.71	28.22		0.5
erReach 1595	Q 100 yr	71,60	19,63	. 21,331	21.00					
er Reach 1585.	[0 2 yr	. 54,10	19,44	20,56	20,73	0.007865	1.83	13,14		D.6
or Reach 1585.	0.5 yr	34.50	19.44	20.82	21,03	0.007474	2.04	16.92		0.6
er Roach 1585.	Олеуг	43.30	19.44	21.00	21.25	0.007431	2.21	19.73	16,50	.0.6
er Reach 1585:		51.60	19.44	21.15	21,44	0.007456	2,36 2,55	25.67	21.20	0.6
er Reach 1585.	Ο 50 γε	52.50	19.44	21.32	21.82	0.007615	2,70	28.51	23.46	0.0
or Reach 1585.	O 100 yr	71.60	13,441	71.401						
er Reach 1575.	QZyi	24,10	19.25	20.48	20.85	0.007558	1,82	13:27	13.85	0.5
er Reach 1575.		34.50	19.25	20,75	20.96	8.007195	2.02	17.09		0.5
er Reach 1575.	O 10 yr	43.30	19.25	20,93	21,18	0.007231	2.19 2.35	. 19.88 22.48		0.0
r Reach 1575.	O 20 yr	51,60	19.25	21.08	21,35 21,58	0.007251	2.55	25.94		D.1
r Reach 1575. r Reach 1575.		62.50 71.60	19.25	21.23	21.74	0,007505	2.70	28,85		D.
r Reach 1575.	9,14031		- V			2.25	35.25.	1000		
r Reach 1565,	Q2yr.	24,10	19:07	20,41	20.58	0.007285	1.60	13,42		0. 0.
(Reach 1565.	Q 5 yr	34.50	19.07	20.68	20,89	0.006983	2.00 2.18	17.25 20.02		
Reach 1565.		43.30	19.07	20.65	21.11	0.007076	2.34	22,68	19.61	0.
rReach 1565,		51.60 62.50	19,07	21.01	21.50	0.007270	2.54	26.26	23.22	0.
r Reach 1565. r Reach 1565.		71.60	19.07	21.30	21.67	0.007461	2.70	29.28	25,60	0.
Reach 1565.	(4,152)						ag Press	a		
Reach 1555.	0.2 yr	24.10	18.68	20,34	20.50	0.007099	1,78	13.53		0.
Reach 1595,		34.50	18.88	20:52	20.88	0,006869	1,99	17.38 20.13		
Reach 1555,		43.30	168.81	20,79	21,03	0.008978	2.17	22.89		D
Reach 1555,		51.60 62.50	18.88	20.94	21.43	0.007269	2,54	26,52	24,55	0
tench (1555) Reach (1555)		71:60	18.88	21.22	21.59	0.007513	2.70	29.74	27,49	0
,	3-1-16						2.00			σ
Reach 1545.		24,10	18.59	20.27	20.43	0.007000	1.77	13.61	13.45	σ.
Reach 1545.		34,50	18.59	20.55	20.75 20.96	0.006955	2.17	20.24	18.11	. 0
Reach 1545.		43:30 51,60	18.69	20,72	21.15	0.007088	2.33	23.11	22:01	, j O
Reach 1545; Reach 1545;	C 20 γr C 50 γr	62.50	18.69	21.03	21.36	0.007361	2.54	27.03	26.51	Ü,
Reach 1545. Reach 1545.		71,50	18.69	21.15	21.51	0.007646	2.71	30.51	30.08	. 0
								13,64	13,29	0
Reach 1935.	O.2 yr	24,10	18.50	20.20	20,36	0.007002	1.77	17,45		0
Reach 1535.	Q.5 yr	34.50	18.50	20,48	20,68	0.000960	2.17	20.31	19.22	0
36ach 1535,		43,30 51,60	18.50 18.50	20.79	21.07	0.007233	2.34	23.35	23.86	0
Reach 1535;	Q 20 yr Q 50 yr	52,50	18.50	20.95	21.28	0.007586	2,56	27.52	29.26	0
Reach 1535.	Q 100 yr	71.60	18.50	21.07	21,44	0.007844	2.72	31,19	34,44	. 0
							3.32	13.60	13,10	0
Reach 1525.		24.10	18.32	20.13	20.29	0,007123	1,77	17.38	14.79	0
éach 1525.		34,50	18.32	20.41	20,82	0.007307	2,19	20.36	20.76	0.
each 1525, each 1525.		43,30 51.50	18.32	20.72	21.00	0.007510	2.36	23,64	26.62	
leach 1525. leach 1525.	The second secon	52.50	15.32	20.67	21.20	0.007842	2,57	28,32	33.92	. 0
each 1525		71,60	18.32	20.99	21.35	0,008053	2.73	32.57	38.76	0
		ad his file					7.70	13,44	12.80	
Reach 1515.	Q 2 yr	24.10	18.13	20,05	20,22	0,007400 0,007532	1.79	17,21		Ū
leach 1515	O 5 yr	34.50	18.13	20.33	20,74	0.007772	2.02	20,35		
leach 1515 leach 1515	Q 10 yr Q 29 yr	43.30 51.60	18.13	20.53	20,92	0.007979	2.39	24.06	30.98	. 0
teach 1515 teach 1515	Q 50 yr	62.50	18.13	20,79	21,12	0.008261	2.60	29,40		
Reach 1515	Q 100 yr.	71.60	18,13	20.50	21.27	0.000474	2.75	34.05	42.78	0
			. 1.2				3.5	13.46	12.93	ō
Reach 1505.		24.10	16.06	19.98	20,14	0.007377	1.79	17.26		0
Reach 1505,	0.5 yr	34,50	18.08	20.25	20.67	0.007765		20.35	23,09	0
leach 1505,	an investment of the property	49,30 51,60	18.08	20,55	20.64	0.007916	2.38	24.02	30.66	
Reach 1505, Reach 1505,	C 20 yr	62.50	18.08	20.71	21,03	800900.0	2.56	29.37		. 0
Reach 1505.		71.60	18.08	20.83	21,18	0.008063	2.68	34.01	41,21	
						0.007028	1.79	13,49	13,07	
leach 1495,		24.10	18.02	19.91	20,07	0.007028		17,31		0
Reach 1495,		34.50 43.30	18,02	20,34	20,59	D,007428		20,35		
leach 1495. teach 1495.		51,60	18.02	20.48	20,76	0.007588	2.37	23.98	30.48	Ç
teach 1495. teach 1495.	And the second s	62.50	18.02	20,53	20.96	0.007695		29.19		0
each 1495,		71,80	18.02	20.75	21,10	0.007770	2,69	33.66	40,20	0
					20,00	0.007007	1.76	13.52	13,21	
leach 1485.		24.10	17,97 17.97	19.84	20,00	0,007197		17.36		
leach 1485.	The state of the s	34.50 43.33	17,97	20.11	20.51	0.007435		20.39	23,02	
leach 1485. leach 1485.	Commence of the commence of th	51.60	17.97	20,40	20.58	0.007800	2.37	23.93		
	. 0.50 W	62.50	17.97	20.56	20.88			29.10		
Reach 1485.	The second secon	71,60	17,97	20.67	21.02	0.007794	2.68	33,48	39.62	į c
					19.93	0.006866	1.78	13.56	13.35	0
Reach 1475.		24.10	17.92	19.7.7	19.93			17.42		
Reach 1475,	The state of the second	34,50	17.92 17.92	20.04	20.44			29.43		
Reach 1475		43,30 51,60	17.92	20.33	20.61			23,94	30,40	C
Reach 1475.		62.50	17.92	20,48	20.80	0.007397	2.54	29.06		
Reach 1475. Reach 1475.		71.60	17.92	20.60	20.95		2.68	23.37	39.33	. 1141
		3 1							13.52	
Reach 1465.		24,10	17.87	19.71	19.87		1.77	13:50 17:49		0
Reach 1465		34.50	17.87	19,97	20.17		2.18	20.49		
Reack 1495		43,30 51,60	17.87	20.13	20.54	4		23,97		
Reach 1465 Reach 1465		62.50	17.87	20.20	20.73		2.54	29.04	35,93	0
	Q 100 yr	71.60	17,87	20:52	20.67			33.32	39,27	0

EC-RAS Plant Reach	Salvin-Final-09 River, Salvin River Sta	Profile	o Total	Min Ch El	W.S. Elev (m)	.C/∉ W.S. (m)	E.G. Elev	E.G. Slope (m/m)	Vel Chril (m/s)	Flow Area (m2)	Top Width (m)	Froude # Chl
	1		[m3/s]	(m)	886-99/3612	1	A. V.					
pper Roach	1455.*	G 2 yr	24,10	17,82	19,64		19.80	0.008639	1.77	13.83 17.53	13.67	0,5 0,5
pper Reach	1455."	Ci 5 yr	34.50	17.82	19.90 20.06		20.10 20.30	0.005557	2.19	20.52	23,56	0,5
ppor Reach ppor Reach	1455.1	G 10 yr G 20 yr	43.30 51.60	17.62	25,19		20.48	0.007309	2,35	23.98	30.63	0.6 0.5
pper,Reach	1455.*	CI 50 yr	62.50	17.82	20.34		20,65	0.007451	2.53 2.67	29,02 33,28	36.12 39.34	0.6
pper Reach	1455.1	O 100 Yr	7,1.50	17.62	20.45		10,00	7.7				
pper Reach	1445.7	Q 2 yr	24,10	17,76	19.58		19.73	0.006337	1,77	13.65 17.57	13.83 16.60	0.5
pper Reach	1445.*	0.5 yr	34.50	17,76 17,76	19.84	<u> </u>	20.03	0.006843	2.17	20.55	23.63	0.8
pper Reach	1445.	O 10 yr	43,30 51.60	17.76	20,11		20.39	0,007018	2,34	23,99	30.85	0.6 0.6
pper Reach	1445.7	Q 50 yr	62.50	17.76	20,26		20,58	0.007168 0.007246	2.53 2.67	29.00 33.25	36,40 39,53	0.5
ppor Reach	1445.1	O 100 yr	71.60	17.76	20.37	 	20.72	0,007240	2,07	Cale		films and finite
oper Reach	1435.*	Q 2 yr	24,10	17.71	19.51		19.67	0.006346	1.76	13.68	13.99	9.5 0.5
pper Reach	1435.1	Q 5 yr	34,50	17.71	19.77		19.97	0.006554	1.96 2.17	17.61 20.59	16.81 24.17	0.1
per Reach	1435.1	O 10.yr	43,30 51,60	17.71 17.71	19.92		20.18	0.007060	2.34	24.03	31:07	0,6
per Roach per Roach	1435.*	O 20 yr	62.50	17.71	20.19		20.51		2,53	29.00	38,75 39,84	0.t
per Reach	1435.1	O 100 yr	71.60	17,71	20.30	<u> </u>	20,65	0.007265	2,56	33.27	29.04	1000
	1	Q 2 yr	24,10	17,66	19,45		19,51	0.006058	1.76	13.71	14,17	0.
operReach operReach	\$425;* 1425;*	Q 5 yr	34,50	17.66	19,71		19,90	0.006378	1.96	17.65 20.65	17,06	0.
per Reach	1425,*	Q 10 yr	43,30	17.66	15,85		20.09		2.16	24.53	31.35	
per Reach	1425.*	Q 50 yr	51,60 62,50	17.66			20.44	0.006934	2.52	29,03	37.20	
oper Reach oper Reach	1425.*	G 100 yr	71.60	17.66			20.58	0.008997	2.66	33,32	40.24	D.
			24.10	17.61	19,39	 	19.55	0.006063	1.75	13,75	14.35	
pper Reach oper Reach	1415."	Q 2 yr Q 5 yr	34.50	17.61	19,64		19.84	0.006408		17,69	17.35	
pper Reach	1415.7	Q 10.yr	43.30	17.61	19.79		20,03		2.16 2.33	20.73	25.12 31.72	
pper Reach	1415.7	Q 20 yr	51,60 62,50		19.91		20.37			29,12	37.53	0.
pper Reach pper Réach	1415.*	D 100 yr	71.60		20.16		20.51	0.007019	2.55	32,44	40,76	n interes and a
					19.33	1	19.49	0.005784	1.75	13.79	14.56	
per Reach	1405.1	O 2 yr	24,10 34,50				19.78		1.95	17,74	17.87	
oper Reach oper Reach	1405.*	Q 10 yr	43.30	17.56	19,73		19.95		2.15 2.32	20.81	25.70 32,12	
pper Ranch	1405,"	O-20 yr	.51.60				20.12			29.22		
pper Reach	1405.*	O 50 yr	82.50 71.50		- grand and the same		20.44	4	2.65	. 33,58	41.35	0.
pperReach	1405.	4,00,	11.2		14 1 44 1			200	1.74	13,83	14,77	D.
ppor Reach	1895.*	Q 2 yr	24.10 34.50	17.50			19,43 19,71					ο.
pper Reach pper Reach	1395.*	Q 10 yr	43.30	17.50			19,50	0.006369	2,15			
pper Reach	1395.*	CJ 20 yr	51.60				20,05			24.40		0.
pper Reach	1395,7	CJ 50 yr	62.50 71.60	17.50			20,23					4
pper Reach	1395.*	Q 100 yr	77,00			1	100			1000	14,98	0.00
pper Reach	1365,7	Q 2 yr	24.10				19.37			13,85		
pper.Reach	1385.7	Q 5 yr	34.50 43.30				19.83				27.08	0.
pper Reach pper Reach	1365."	Q 20 yr	51,80				19.98					
apat Reach	1385.*	Q 50 yr	62.50				20,17					
pper Reach	1385.*	Q 100 yr	71,60	17,43	13,31				1. 1. 1. 2. 2. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	1774		
pper Reach	1975	Q 2 yr	24,10				19.31					
pper Reach	1975,1	Q 5 yr	34,50				19.59	4	4			0
pper Reach	1375.*	Q 10 yr	43.30 51,60				19,92	0,096344	2.31	24.60		
pper Reach oper Reach	1375.1	Q 50 yr	62.50	17.4	19,7		20,10					
ppor Reach	1375.	Q 100 yr	71.60	17.41	19.5	0	20.24	. U.D.B.S.	2.00	1		
lpper Reach	1365;"	02 yr	24,10	17.3			19.26					
pper Reach	1365.*	□ 5 yc	34.50	17.3	19,3		19,53					
pper Reach	1365.	O 10 yr	43.30 51,60				19.88		2.31	24,75	34.2	0
pper Reach	1365,*	O 20 yr	62.50		19.7	2	20.03	0.00654	2.50			
pper Reach	1385.	O 100 yr	71,60	17.3	5 19.8	3	20.17	8.006530	2.62	34,41	43.6	
	1	□ 2 yr	24.10	17.3	19,0	5	19.20	0.00548				
pper Reach pper Reach	1355.*	Q 5 yr	34.50	17.3	19.2	8	19.47					
Ipper Reach	1355.*	Q 10 yr	.43.30				19.85					
pper Reach	4355.*	Q 20 yr	51.60 62.50				19.97		2.49	30.0	41.0	
pper Reach pper Reach	1955;* 1355;*	Q 100 yr	71.6				20.11	0.00624	2 2.53	2 34.8	7 47.8	2
			1	 	4 16.9		19.11	0.00559	7 1.7	4 13.8	6 15.9	
pper Reach	1345.1	0 2 yr	24.11 34.5				19.4	0.00587	8 1.93	3 17,9	5 21.8	6 (
ipper Reach ipper Reach	1345.	Q 10 yr	, 43,31	17.2	4 19,3	5	19.5					
oper Reach	1345.1	Q 20 yr	51,6				19.73					
Ipper Reach	1345.*	Q 50 yr Q 100 yr	62.5 71.6				20.0				1 49,5	7 - 1 - 1
Jpper Reach	1345,*	Q JUU YI	11121								0 16.1	2 (
lpper Reach	1335.*	C) 2 yr	24,1				19,0					
Jpper Reach	1335.1	O 5 yr	34.5 43.3				19.5		1 2.1	4 21,4	8 31.4	8 (
Jpper Reach Jpper Reach	1335,*	C) 20 yr	51.5	0 17.1	9 19.4	0	19.6	0.00633				
Upper Reach	1335,*	O 50 yr	€2.5	0 17.1			19.8					
Upper Reach	1335.	Q 100 yr	71.6	0 1.7.1	9 19.6	⊕ 16.7.3	19.3	9,90022	210			1 1 4 9 14
Upper Reach	1325.5	Огуг	24.1	0 17.1			19.0					
	and the second s	Q 5 yr	34.5			اه	19,2	9 0.00583	6 1.9	4 17.9	ž 23.4	, I

	Salvin-Final-09 River: Salv	in Ck Reach: Up: Profile	xer Reach (Conlin	ues) Win Ch El	W.S. Ekv	Crit W.S.	E.G. Elev	E.G. Slope	Vé Chrk	Flow Area	Top Width	Froude # Ch
Reach	River Sta	Linin	(m3/s)	(m)	(m)	(m)	(m)	(m/m)	(a\m)	(m2)	(m)	0.
r Reach	1325.*	G 10 yr	43,30	17.14	19.23		19.46	0.005960	2.14	21.55	37.25 37.58	0.
r Reach	1325.*	O 20 yr	51.50	17.14	19.34		19.61	0,006127	2.31	30.78	46.26	0
r Reach	1926.1	Q 50 yr	62.50	17.14	19.47		19,78	0.005881	2.57	35.84	53,77	0
r Reach	1325.*	C) 100 yr	71,60	17.14	19,59		(2.00.)	1				
		- In avia	24.10	17.09	18.61		15.97	0.005941	1.78	13.56	16.50	.0
r Reach	1315.*	Q 2 yr Q 5 yr	34.50	17.09	19.64		19,24	0,006028	1.95	17.86	24,19	0
r Heach r Heach	1315,*	Q 10 yr	43.30	17,09	19.17		19,40	0.006110	2.14	21.60	33.10	0.
r Reach	1315,*	" CJ 20 yr	51.60	17,09	19.27		19.54	0,006277	2.31	25.34	3E.57. 45,19	0
r Reach	1315.*	Q 50 yr	82.50	17.09	19,41		19.72	0.006242	2.48	37,51	56.80	0
r Roach	1315.	Q 100 yr	71.60	17.09	19,54		19.85	0.005611	2,30	01,011		
				47.00	18,75		18.92	0.005976	1.81	13,35	16.62	0
r Reach	1305."	Q 2 yr	24,10	17.03	18.98		19.18	0.005936	1,97	17,76	24.91	0
r Reach	1305.1	Q 5 yr	34.50 43.30	17.03	19.11		19.34	0.005949	2.15	21.64	34,07	0
r Reach	1305.1	Q: 10 yr Q: 20 yr	51.60	17.03	19.21		19.48	0.006114	2.32	25.43	40,25	0
r Reach r Reach	1305.*	Q 50 yr	62.50	17.03	19,35		19.55	0.005963	2.48	31.79	50.56	
r Reach	1305.*	Q 100 yr	71.60	17.03	19,49		19.60	0.005401	2.52	39.32	58.93	-
133001			printer and the				41 42		4.50	13.01	16.61	0
r Reach	1295.	O 2 yr	24.10	16.98	18.68		18.85	0.005495	1.85	17,55	25.37	0
r Reach	1295.*	Ω5 γτ	34,50	16,98	18.91		19.11	0.006280	2.17	21.61	35.15	0
r Reach	1295."	Q 10 yr	43.30	16.96	19.05		19,42	0.005341	2.34	25.49	42,42	C
Reach	1295.*	10 20 yr	51,50	18.98	19,15		19,59	0.005961	2.46	32.58	53,61	0
l Reach	1295.	(Q 50 yr	62.50	16,98	19.29		19,74	0.005232	2.48	41.12	61,84	
Reach	1295.*	Q 100 yr	71.60	10.38	(3,44							<u> </u>
	Agree	0.2 yr	24,10	15.93	18,59		18.75	0.007088	1,95	12.36	16.27	1315
Reach	1265.*	Q.5 yr	34.50	18.93	18.83		19.05	0.006779	2.05	16.88	24.33	
Reach Reach	1265.	Q 10 yr	43,30	16.93	18,95	18,76	19.22	0.006459	2,22	20.97	35,30 43,46	
Reach	1285.*	Q 20 YI	51.50	15.93	19.07	18.86	19.35	0.008559	2.39 2.45	24.90 33.60	43.46 56.66	
Reach	1285.1	Q 50 yr	62.50	16.93	19.24		19.53	0,005664	2.45	43.26	54,85	
Reach	1285."	Q 100 yr	71.60	16.93	19,40		19.59	0.004775	2,43	+5.20	04,00	
							18.68	0.011308	2.38	10,13	13.99	
Reach	1275	0.2 yr	24.10	15.86 16.86	18,40	18.56	18.94	0.012517	2.58	13.36	17.59	1 1 1 1 1 1
Réach	1275	Q 5 yr	34,50 43,30	16.86	18.74	18,71	19,11	0.012748	2.72	15.01	22,37	3,47,613
Reach	1275	Q 10 yr	51,60	16.88	18,65	18.83	19.26	0.011414	2.82	19.26	32.91	12. 12. 1
Reach	1275	O 20 yr	52,50	16.88	19.19		19.48	0.005518	2,43	35.00	59,42	
r Reach	1275	Q 100 yr	71.50	16.88	19.36		19,63	0,004505	2,37	46.12	68.00	4
Reach	1673										34,45	34 34
Reach	1265.*	Q2yr	24,10	16,80	16.25	18.22	18.57	0.013097	2,46	9,80 13:12	16.33	
Reach	1265.*	O.5 yr	34,50	16,80		18,45	18,81	D.D13812	2.63	15,53	19.36	
Reach	1265.7	O'10 yr	43.30	16.80	18.59	18.58	18.98	0.013372	2.79 2.67	29,35	32.12	-
Roach	1265.1	O 20 yr.	51.50	16.60	18,78	18,68	19.14	0.004176	2.22	39,13	60.35	
r Reach	1285,1	Q 50 yr	62.50	16,60	19,17		19.58	0:003426	2,18	50.85	69.03	
r Réach	1285/	Q 100 yr	71.60	16.80	19.33		1	. 73			- 140mg	4.50
		6.7.	24.10	19,70	18,17		18:43	D.011429	2.26	10,68	16,12	
Reach	1255.*	0 2 yr	34.50	16,70	18,34	18.30	18.65	0.012307	2.52	13.70	18.74	
r Peach r Reach	(1255.)	Q 10 yr	43,30	16.70	18.53	18.42	18,85	0.009412	2.51	17.25	19.91	
r Reach	1255.1	0 20 yr	51,60	15.70	18,75	18,53	19,04	0.006296	2.37	23,20	35.59	
r Reach	1255.*	Q 50 yr	62.50	16.70	19.19	Y	19.36	0.002588	1,89	45.24	63.28 70.42	
r Reach	1255.*	Q 100 yr	71.60	16.70	19.38	ļ	19,53	0.002101	1,84	57.65	1974	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
			0.44					a naran	2,28	10.58	17.07	1
r Reach	1245.*	02yr	24.10	16,60	18.05	18.00	18,51	0.012549 0.012089	2.50	13.77	16.65	
r Reach	1245.1	0 5 yr	34.50	16,60		18.17	18.75	0.007498	2.34	18.55	20.83	
rReach	1245."	Q 10 yr	43,39	15,60 16,60			18.97	0.004972	2.18	26.30	40,41	1 2 3 2 2
r Reach	1245,1	IQ 20 yr	51.60 62.50	16.60			19.33	0.002326	1.64	49.42	61.78	
r Reach	1245.1	Q 50 yr	71,60	16.60			19.51		1.65	60.82	57.8	1
r Reach	12452	O 100 yr	73,60	.0.08	1	1		9 2	5 7445		24.2	1
. m.	1025.1	C 2 yr	24,10	16,50	17.99	2.2	18,19	0.008770	2.01	12.51	17.92	
r Fleach r Fleach	1235.*	Q5yr	54:50	16.50			19,43		2.26	15.27	18.43	
r Heach	1235.	Q (0 yr	43,30	16.50	15,45		1B.67	0,005452	2,11	20.62	22,36	
r Reach	1235.*	O 20 yr	51,60	16.50			18.92		1,99	26.98 52,33	39,71 61,58	
r Reach	1235.	C) 50 yr		16.50			19,31		1,72			
r Heach	1235.*	© 100 yr	71.50	16.50	19,34	1	19.48	0,001652	1,/4	00.19		1
					17,80	17.76	18:07	0.013886	2.34	10,31	17.39	9
r Reach	1225.	Q2yr	24,10 34,50	16.50			18,34	0.007650	2.20		18.3	2
r Reach	1225.*	Q 5 yr	34.50 45.30	16.50			18.61	0,004766	2.01			
r Reach	1225.1	Q 10 yr	51.60	16.50			18.87	0.003089	1.86			
r Reach ir Reach	1225.1	Q 50 yr	62.50	16.50			19.28		1,62			
r Heach	1225	O 100 ýr	71.60	18,50			19.46	0.001442	1.65	68.54	68.7	1
e, rasimeli			\$ I				ļ	1		10:69	17.2	1
r Reach	1215.1	0.2 yr		16.40			17,94		2.21			
Reach	1215.1	Q 5 yr	34,50	16.40			18,26		1,62	- 	30.2	
ır Russch	1215.1	Q 10 yr	43.30	16.40			18,56 18,64		1,73			
r Reach	1215.*	10 20 yr		16.40			19,26		1.51			8
n Reach	1215.*	10 50 yr	62.50 71.60	16.40 16.40			19,44		1.55			3
er Reach	1215,*	Q 100 yr	71,00	10.40	12,03	1	1					
	and a second	0.50	24,10	16.30	17.63	1	17,83	0.008435	1.98			
or Reach	1205.	0.2 yr		16.30			18,20	0.004380				
or Reach		G 10 yr	43.30	16.30			18,52	0,003026				
er Reach	1205.*	G 20 yr		16.30			18.81					
er Reach er Reach	1205.	Q 50 yr	62.50	16,30			19,25					
er Heach er Reach	1205.*	G 100 yr	71.60	16.30		<u> </u>	19,43	0.001151	1.46	76.25	56.2	<u> </u>
wi-tre-dott						1		1			16.9	o i
er Reach	1195.*	Q 2 yr		16,20			17,75					
er Reach	4195.*	Q 5 yr	84.50	15.20			18.16					
er Reach	1195."	O 10 yr		15.20			18,49					
	1195.*	0.20 yr	51.60	16.20	9 18.67		18.79					

	Sahin-Final-09 River, Sahin C	k Reach! Upp	er Reach (Cont	inued)	W.S. Elev	Cri W.S.	E.G. Elev	E.G. Slope	Vel Chol	Flow Area	Top Width	Fraude # Chl
Reach	River Sta	Profile	(m3/s)	ms, Cit Ci (m)	(in)	(m)	(m)	(m/m)	(m/s)	(m2)	(m)	
		Q 100 yr	71.50	16.20	19.33		19.42	0.000892	-1.41	79.56	66.27	0.29
pper Reach	1195."	Q-100 yr	77.50	10.2.0		i						
	1.6P.	Q 2 yı	24,10	16.10	17.58		17,69	0.004448	1.56	15.45	17.13	
pper Reach	1185.	0.5 yr	34.50	16.10	18.02		18,13	0,002870	1.47	23.54	19,30	
pper Reach	1185.*	Q 10 yr	43,30	16.10	18.35		18,46	8.002165	1,43	35.24	35.64	0.36
pper Reach	1185;	Q 20 yr	51.60	16,10	18,57		18.77	0.001609	1,39	46.30	4E.84	0.32
pper Reach	1185.*	Q 50 yr	62,50	16.10	19,15		19.22	0,600985	1.26	72.12	61,90	
pper Reach pper Reach	1185."	O 100 yr	71,60	16,10	19.33		19,40	0.000984	1,31	83.52	66.18	0.26
pper now	7,025									47.00	17.12	0,45
ppor Reach	1175,	Q 2 yr	24,10	16.00	17.55		17.65	0,002563	1.40	17.23		0,37
pper Reach	1175.	Q 5 yr	34,50	15.00	18,00		18,10	0.001846	1.35	25.67	23.51 38.17	0.33
pper Reach	1175.	Q 10 yr	43.30	16.00	16,35		18,44	0,001335	1.34	35,59	47.19	
pper Reach	1175,	O 20 yr	51,E0	15.00	18,67		18.75	0.001025	1.31	49.97	60.65	0.25
pper Reach	1175.1	Q 50 yr	62.50	16.00	19,14		19.21	0.000563	1.22	75,77 85,69	64.56	0.25
	1175.*	Q 100 yr	71,60	16.00	19,32		19.39	0.000661	1.27	65.63	174,30	-
pa									1.28	18,79	17.24	0.39
per Roach	1165.1	O 2 yr	.24,10	15.90	17.53		17.65	0.002862	1.28	27.69	24.86	0.3
	1165.*	O.5 yr	34.50	15,90	17.99		18.07	0.002349	1.27	38,65	39.57	0.30
per Reach	1165.	O 10 yr	43.30	15.90	18.34		18.42	0.001766		52,42	47.92	0.27
per Reach	1165.	Q 20 yr	51.60	15.90	18.66		18,74	0.001366	1,24	78.45	59.80	
per Reach	1165.*	O 50 yr	62.50	15,90	19.14		19.20	0.000884	1.19	89.51	64,49	
oper Reach	1165,1	Q 100 yr	71.60	15.90	19.32		19,38	0,000881	1,19	03.31	0.04	l
								0.000,20	1.19	20.23	17.01	0.35
oper Reach	1:155.*	O 2 yr	- 24.10	15.90	17,51		17.58	0.002478	1,21	29.05	25.20	
per Reach	1155.*	O 5 yr	34.50	15,90	17.97		18.05		1.21	40.47	37,85	
per Reach	1165.1	מן פון בס	43.30	15.90			18.41	0.001627 0.001286	1,20			
per Reach	1155.*	C) 20 yr	51.60	15.90			16.72	0.000854	1.11	79.57	59.65	
pper Reach	1155.1	Q 50 yr	62.50	15.90	19.14			0,000856	1,16			
per Reach	1155.*	D 100 yr	. 71.60	15.90	19.31		19.37	0,000830	1,10			
						16.56	17.54	0.004493	0,98	24,49	17.28	0.2
pper Reach	1145	Q 2 yr	24,10	15,78		15.74	18.01	0,004184	1,05	34.07	-27,40	
per Reach	1145	Q 5 yr	34,50	15.78	17.05	10.88	18,38	0.003428	1.07	45,93		
oper Reach	1145	Q 10 yr	43.30	15.78		17.00	18.70	0.002865	1.07	59.50		
per Heach	1145	□ 20 yr	51.60	15.78	18.54	17.14	19.18	0.001983	1.01	85.47		0,1
oper Roach	1145	Q 50 yr	62.50	15.78		17.25	19.36	0.001989	1,05	97:30		0.19
pper Reach	1145	O 100 yr	71.60	15.78	19.31	17.55		3.20(0.20			1 1 1 1 1	
		4										
per Reach	1144 Ploc Mountain Rd		Gulven								1.5	0
			=	14,36	16.24	15.46	15.37	0.005499	1,57	15,56	13.63	0.3
pper Reach	1115	Q 2 yr	24.10	14,36		15.71	16.72	0.007565	1,87	20,17	14:29	
ppor Reach	1115	Q 5 yr	34.50 43.30			15,89	15.98	0.008406	2,08	23.43	14.78	0,4
pper Reach	1115	0.1	51,60			15.06	17.21	0.007641	2,12	33,05		
oper Reach	1115	Q 20 yr	62.50			16.31	17,45	0.008000	2.29	38.75		
per Reach	4115	Q 50 yr	71.60			15,48		9.006213	2,42	43.73	30.64	0.4
oper Reach	11.15	O 100 yr	71,00	-	i							
		O 2 vr	24.10	14.36	16.19	15.46	16,33	0,007204	1.62	15.26		
oper Reach	1109.*		34.50			15.71	16,67	0.008575	1.95	19,25		
pper Reach	11097	O 5 yr	43,30			15,89		0,009469	2.17	22.31		
pper Reach	1109,1	Q 10 yr Q 20 yr	51.60			16,06		0,008632	2:20			
pper Reach	1109.1	Q 50 yr	82.50	14.36			17.38	800000,0	2.38			0.4
oper Reach	1109.7	Q 100 yr	71.60	14,36			17.58	0.009198	2.51	41,36	29.37	0,4
oper:Reach	1109.7	- C (UU J)	,,,,,,	1		i -	I.	1	1		ļ	1
4	1100	QZyr	24.10	14,36	15,13	15.46	15.28					
per Reach	1103	Q 5 yr	34.50			15.71	15,61	0.009812				
opel Reach	1103	O 10 yr	43.30			15.89		0.010923	2.28			
pper Reach	[103 [103	O 20 Vf	51.60			15,05	17.09	0.011650	2.46			
pper Reach	1103		62.50			15.31	17:33	0.010430	2.50			
pper Reach	1103	Q 100 yr	71,60			15,48	17,52	0,010493	2,62	36,77	27,9	.0.
ppor Reach	1)103	G 100 y			1				1	1	<u> </u>	
	1095	Q 2 yr	24.10	14.38	16,13	1	16.24					
pper Reach		0.5 yr	34.50				16.56	0,002183	1,65			
pper Reach	1095	C 10 yr	43.30		16.64		16.80		1,78			
Ipper Reach	1095	C 20 yr	51.50				1.7.01	0,002309	1,87	31.86		
pper Reach	1095	Q 50 yr	62.50				17.27				26.58	
Ipper Reach	1095	Q 100 yr	71,50			T	17,46	0.092406	2.08	42.54	29.45	0.
lpper Reach	1000	- 100 Jr	1	1	1.						1	
	1035	O 2 yr	24:10	14.07	15.99		16.10					
Ipper Reach	1035	Q 5 yr	34.50			T	16.41					
pper Reach		G 10 yr	43.30	4			16.65					
pper Reach	1035	Q 20 yr	51.60				16,65					
Ipper Reach Ipper Reach	1035		62.50				17.12					
	1035	Q 50 yr	71.80				17.30		1.82	73.7	69.5	3 0.

Count Facility County	E.G. Slope Vel C	Clark Fow Area		Frouds # Chi
Beach 13	(m/m) (m/c		(m)	HUMBER
See Peach 973		3.11 15.30		0.9
West Peters 913		3.45 20.93 3.69 25.13	22.02	9.0
Very Part Very		3.69 25,13 3.67 30,51	29.95	0.5
TWO REACH 913 100 110	0.011574	4.03 37.94	33.43	0.9
West Peters 1918 1919	0.010268	4,15 46.54		0.9
rev Peach 655 0 0 9 y 167.10 11.50 11.50 11.50 15.00 0 9 w Peach 655 0 0 9 y 167.00 11.50 15.00 15.00 0 9 w Peach 75.00 15.00 0 9 y 167.10 11.50 15.50 14.50 15.00 0 9 w Peach 75.00 15.00 0 9 y 167.10 15.00 15.00 15.00 0 9 w Peach 75.00 15.00 0 9 y 167.10 15.00 15.00 15.00 0 9 w Peach 75.00 15.00 0 9 y 167.10 15.00 15.00 15.00 15.00 0 9 w Peach 75.00 15.00 15.00 15.00 15.00 15.00 0 9 w Peach 75.00 15				
The Page 19 Control of the Control o	0.002816	1,54 31,61		0,4
wer Peach 1605 0.76 pt 1.60 1	0,002088	1,63 44,30		0.4
American Continue	0.001755	1,69 54.26		0.4
March 1985	0.001621	1.78 63.94		0,3
March 1955	0.081216	1.76 E1.57		. 0,3
Perf Reach 805 0.2 yr 47.00 11.00 19.24 15.15 15.27 14.27 1.00 17.20 11.00 19.24 15.15 15.27 14.27 1.00 17.20 15.50 14.27 1.00 15.50 14.27 1.00 15.50 14.27 1.00 15.50 14.27 1.00 15.50 14.27 1.00 15.50 14.27 1.00 15.50 14.27 1.00 15.50 14.27 1.00 15.50 14.27 1.00 15.50 14.27 1.00 15.50 14.27 1.00 15.50 14.27 1.00 15.50 14.25 14.25 1.00 15.50 14.25 14.25 1.00 15.50 14.25 1.00 15.50 14.25 1.00 15.50 14.25 1.00 15.50 14.25 1.00 15.50 14.25 1.00 15.50	0.000596	1,09 104.12		
Per	0.016197	3,05 15.53	13.15	0.8
March Sto G. Striff Sto Sto G. Striff Sto St		3.15 21.98		0.8
of Papers 905 CREATY 118.00 14.00 14.85 O 14.00 14.85 O 14.00 14.85 O 14.00 14.85 O O PROSED OS OS </td <td>0.009299</td> <td>3.04 31.73</td> <td>34.22</td> <td>0.</td>	0.009299	3.04 31.73	34.22	0.
The Peach 155 0.59 yr 1976 11.00 15.00 14.31 15.27 0.00 1.00 15.00 14.31 15.27 0.00 1.00 15.00 14.31 15.27 0.00 1.00 15.00 14.31 15.28 1	0.006373	3.16 41.17	37.86	6.7
March 1956 1978 147-10 11.0 15.50 14.48 15.50 0	0,003953	2.63 74.03	54.23	0,:
MERIAND 757	0.002373	2.31 105.43	55.61	.0.4
in Peach 757		97.77	14.87	Q.
me Reach 767	0.003478	2.11 22.37 2.33 29.62		0.
66 Reach 767 G. 19 yr B8.30 11.19 14.08 13.22 17.35 1.4.6 1.4.	0.003419	2.33 29.62 2.35 35.68		0,
February 777 192 Style 101,09 11,19 12,35 12,76 15,27	0.002970	2.53 41.32		0
Financh 777	0.001661	2.12 80.46		0
	0.000716	1.58 202.41		0
Pasish 735 Creek Pload Biddy Bridge				
Final 725				
PRODUCT 735			J	0
Fleech 795	0.003949	1,75 26,99		
FRESCH 755	0.004450	2,08 33,19 2,13 40,59		9
FROMER 735	0.003762	2.13 40.59 2.43 42.96		
FRESCH 755	0.004655 0.005615	2,77 46.08		0
Place 735	0.005626	3.07 47.95		.0
Reach 870	0.0000EV			
Reach 670	0.001608	1.23 38.88	30.75	0
PRach 670	0.001442	1.38 52.25		Ó
Reach 579 Q20 yr 104.50 11.00 13.86 12.56 13.95 17.00 17.0	0.000884	1.28 74.57		
Finach S70	0.001007	1,42 82,30		.0
Reach 100 14,20 12,97 143,33 14,20 12,97 14,33 14,34	180100,0	1,55 93.09		0
PRact 488	0.001185	1,68 99.88	72.71	. 0
Pack 488		2.17 35.47	40.01	Ċ
Float 458	0.011623	2.17 35:47 1,14 80.51		0
Fig.	0.002578 0.001126	0.85 114,44		ť
Reach 488	0,001249	0.93 121,22		
Reach 488	0.001324	1.00 131,32		(
	0.001428	1.06 137.25		(
	0.002537	1:29 47.17		
Reach 430 Q 20 yr 191.20 8.98 13.49 10.64 13.54 10.65 13.66 13.67 13.66 13.66 13.67 13.66 13.67 13.66 13.67 13.66 13.67 13.66 13.67 13.66 13.67 13.66 13.67 13.6	0,001198	1,22 88.25		
Reach 430 Q20 128.50 8.88 13.61 11.02 13.66 13.68 13.67 13.68 13.68 13.67 13.68 13.68 13.67 13.68 13.68 13.67 13.68 13.68 13.67 13.68 13.68 13.67 13.68 13.68 13.68	0.000728	1.09 122.73		
Reach 450 Q 50 yr 153.20 8.86 13.81 11.23 12.86 Reach 430 Q 700 yr (71.70 6.38 13.97 11.39 14.02 14.	0.000863	1.21 128.77		
Reach 430 QHO yr 171.70 6.38 13.97 11.39 14.02	0.000992	1.34 137,95		
Reach 420 Q_2yr 65.40 6.90 11.71 10.24 11.81	0.000550	1.02 194.60	83.21	
Reach 420 0.59x 82.00 8.50 12.74 10.58 12.83 Reach 420 0.59x 82.00 8.50 12.74 10.58 12.83 Reach 420 0.50x 111.20 8.90 13.45 10.75 13.53 Reach 420 0.50x 153.20 8.90 13.83 10.83 13.07 Reach 420 0.50x 153.20 8.90 13.83 11.15 12.87 Reach 420 0.50x 153.20 8.90 13.83 11.15 12.87 Reach 420 0.50x 153.20 8.90 13.83 11.15 12.87 Reach 420 0.50x 153.20 8.90 13.97 11.52 14.01 Reach 420 0.50x 17.70 8.80 13.97 11.52 14.01 Reach 435 0.50x 65.40 8.00 11.19 10.05 11.35 Reach 385 0.2x 65.40 8.00 11.19 10.05 11.82 Reach 385 0.50x 32.00 6.00 11.59 10.35 11.82 Reach 385 0.2x 11.20 8.80 12.81 10.74 12.39 Reach 385 0.2x 12.50 13.20 6.00 12.32 10.60 12.71 Reach 385 0.50x 153.20 6.80 12.32 10.60 12.71 Reach 385 0.50x 153.20 6.80 12.32 10.60 12.71 Reach 385 0.50x 153.20 6.01 11.02 11.12 Reach 386 0.2x 65.40 6.01 11.02 11.12 Reach 348 0.2x 65.40 6.01 11.02 11.20 Reach 348 0.2x 65.40 6.01 11.65 11.93 Reach 348 0.2x 153.20 6.01 11.43 11.65 Reach 348 0.2x 153.20 6.01 11.92 11.20 Reach 348 0.2x 153.20 6.01 11.92 12.10 Reach 348 0.2x 153.20 6.01 11.20 12.40 12.85 Reach 348 0.2x 153.20 6.01 11.20 12.40 12.85 Reach 348 0.2x 153.20 6.01 12.20 12.44 Reach 348 0.2x 153.20 133.20 133.20 133.20 Reach 348 0	2.000215	1.35 48;1	22.65	
Reach 420 Q.5 yr 11.20 8.90 12.74 10.55 12.83 10.75 13.53 10.75 13.53 10.75 13.53 10.75 13.53 10.75 13.53 10.75 13.53 10.75 13.53 10.75 13.53 10.75 13.53 10.75 13.53 10.75 13.53 10.75 13.53 10.75 13.53 10.75 13.53 10.75 13.53 10.75 13.67 12.67 12.75 13.67	0.000848	1,30 70.78		
Figure F	0.000352	1,29 BG.38		
Reach 420 G.Sp yr 153.20 8.90 13.88 11.18 13.87 14.91 12.87 14.91 14.9	0.000388	0,94 168,17		
Reach 429 Q SUY SS.20 Resp 13.97 11.22 14.01	0,000417	1.01 184.10	26.58	
Reach 419.5 Dennique Sites Cutvert	0,008438	1:05 195.72	2 83.16	
Resch 385		*	1	
Resch 385			1	
Resch 395 Q 2 yr 65-40 5.89 11.59 10.30 11.62 Reach 385 Q 5 yr 92.06 6.00 11.59 10.35 11.62 Reach 385 Q 50 yr 112.00 8.80 11.85 10.74 12.39 Reach 385 Q 50 yr 123.20 6.80 12.32 10.96 12.71 Reach 385 Q 50 yr 153.20 6.80 12.50 11.13 12.94 Reach 386 Q 100 yr 171.70 6.80 12.50 11.13 12.94 Reach 348 Q 2 yr 65.40 8.01 11.02 11.12 11.65 Reach 348 Q 5 yr 92.00 8.01 11.43 11.65 Reach 348 Q 20 yr 122.50 6.01 11.92 12.10 Reach 348 Q 20 yr 125.20 6.01 11.92 12.10 Reach 348 Q 20 yr				
Rescrit 285 Q.5 yr 82.00 0.00 11.59 10.26 11.87 React 395 Q.10 yr 111.20 8.80 11.85 10.96 12.12 React 395 Q.20 yr 128.50 6.80 12.08 10.74 12.39 React 385 Q.50 yr 128.50 6.80 12.08 10.74 12.39 React 385 Q.50 yr 128.50 6.80 12.32 10.95 12.71 React 385 Q.50 yr 128.50 6.80 12.32 10.95 12.71 React 386 Q.2 yr 65.40 6.01 11.02 11.13 12.94 React 348 Q.5 yr 42.00 6.01 11.02 11.20 React 348 Q.70 yr 111.20 6.01 11.69 11.93 React 348 Q.70 yr 128.50 6.01 11.92 12.10 React 348 Q.70 yr 128.50 6.01 11.92 12.10 React 348 Q.70 yr 128.50 6.01 11.20 12.20 12.44 React 348 Q.70 yr 155.20 6.01 12.20 12.85 React 348 Q.70 yr 171.70 6.01 12.40 12.85 React 257 Q.72 yr 65.40 7.83 10.14 18.43 React 257 Q.72 yr 65.40 7.83 10.14 19.43 React 257 Q.72 yr 65.40 7.83 10.14 19.43 React 257 Q.72 yr 65.40 7.83 10.14 19.43 React 257 Q.72 yr 65.40 7.83 10.14 19.45 React 257 Q.72 yr 65.40 7.83 10.14 19.85	0.002002	1.74 37.50 2.10 43.9		
Reach 365 Q-10 yr 111.20 8.80 11.85 10.59 12.12	0.002341	2.32 48.00		
Reach S85 O.20 yr 122.50 E.80 12.08 10.74 122.59 Reach S85 O.50 yr 153.20 E.80 12.21 19.65 12.71 19.65 12.71 19.65 12.71 19.65 12.71 19.65 12.71 19.65 12.71 19.65 12.71 19.65 12.71 19.65 12.71 19.65 12.71 19.65 12.71 19.65 12.71 19.65 12.70 11.13 12.94 19.65 12.70 11.13 12.94 19.65 19.	0.002542	2.52 \$1.44 2.52 \$1.44		
Reach 985 O 50 yr 153.20 6.80 12.32 10.85 (6.71)	0.002730	2.75 55.8		
	0.003122	2.93 58.5		
Reach 348			1	
FREACH 348 Q12yr 55.40 5.07 11.43 11.65 FREACH 348 Q5yr 82.00 6.01 11.43 11.65 FREACH 348 Q10yr 111.20 6.01 11.69 11.93 FREACH 348 Q20yr 129.50 6.01 11.92 12.10 FREACH 348 Q5yr 155.20 6.01 12.20 12.44 FREACH 348 Q10yr 171.70 6.01 12.40 12.85 FREACH 348 Q10yr 171.70 6.01 12.40 12.85 FREACH 257 Q2yr 65.40 7.63 10.14 10.43 FREACH 257 Q5yr 82.00 7.83 10.48 19.85 FREACH 257 Q5yr 82.00 7.83 10.40 11.12 FREACH 257 Q5yr 82.00 7.83 10.14 10.43 FREACH 257 Q5yr 82.00 7.83 10.14 FREACH 257 Q5yr 82.00 7.83 10.14 10.43 FREACH	0.010721	1.92 39,7	8 25,92	
	0,011503	2.18 50.7	7 28.34	
Reach 348 Q 20 yr 172.50 E.01 11.92 12.15 Reach 348 Q 20 yr 152.50 E.01 11.92 12.15 Reach 348 Q 50 yr 155.20 E.01 12.20 12.44 Reach 348 Q 50 yr 155.20 E.01 12.40 12.65 Reach 348 Q 50 yr 171.70 E.01 12.40 12.65 Reach 357 Q 2 yr E5.40 7.83 10.14 10.43 Reach 257 Q 5 yr 92.00 7.83 10.48 10.85 Reach 257 Q 5 yr 92.00 7.83 10.48 10.85 Reach 257 Q 5 yr 92.00 7.83 10.48 10.85 Reach 257 Q 5 yr 92.00 7.83 10.48 10.85	0.0(1517	2,30 59.5		
	0.010955	2.35 88,3		
Freech 257 0.5 yr 92.00 7.63 10.14 10.45 Freech 257 0.5 yr 92.00 7.63 10.14 10.85 Freech 257 0.5 yr 92.00 7.63 10.14 10.85 Freech 257 0.5 yr 92.00 7.65 10.68 10.85 Freech 257 0.5 yr 92.00 7.65	0,010109	2.37 79.1		
CRESCH SSC	.339660,0	2,40 86,8	2 38.49	
Pleach 257 (22y) (22y) (234) (7.53) 10.48 10.66 (7.63c) 257 (25.9) (25.9				
(Neach 257) 0.5 yr 92.00 7.83 10.48 10.65 7.89 10.49 11.17	0.095642	2.44 33.5		
7.01 10.70	0,006737	2.78 43.3		
Reach 257 (Q10-y) (1120 /100	0.006809	2.99 49.7 3,19 55.3		
1 Resch 257 (Q'20 yr 129.50 7.83 10.86 11.65	0.006969	3,19 55.3 3.51 50.7		
O 50 ir 153 20 7.83 11.05 11.62	0.007685	3.74 64.7		

roude # C		Flow Area	Vel Chal	E.G. Slope	E.G. Ebv	Cri.W.S.	W.S. Elev	Min Ch El	Reach (Contin	n-Finat-09 River; Salvin Ck. Reach; Lowe River Sta. Profile	-RAS Plan: Salvin-F Reach
2079000190	(m)	(m2)	(m/s)	(mim)	(m)	(n)	(m)	(m)	(m3/s)	THE STA	Real
	37.24	54.24	1,39	0.005182	9.89						
	39,26	68.72	1,56	0,005155	10.29	i i	9.80	7.21 7.21	65.40		or Reach 175
	47.56	78.86	1,67	0.005150	10.55	i	10,42	7.21	92.00 111.20		er Reach 175
	66.60	91.24	1.73	0.004899	10.78		10.64	7.21	129.50		or Reach 1775 or Reach 1775
	68.03	103.15	1.73	0.004330	11:02		10.89	7.21	153.20		er Reach 175
	68,44	120.34	1,72	9,003957	11,20		11.07	7.21	171.70	The second of th	er Reach 175
	51.52	77.61	1.06	0.002658	9.59	2.50					0.000000414
	53.36	97.95	1.19	0.002849	9.99	8.75	9.55 9.93	7.25 7.25	55,40		er Reach 100
	54.54	111.35	1.27	0.002817	10.25	8.87	.10.18	7.25	92.00		er Reach 100
·	61.03	124.20	1,36	0.002855	10.48	8.97	10,41	7,25	129.50		er Reach 100 er Reach 100
	76,77	149.15	1,42	0.002744	10.75	9.10	10.57	7.25	153.20	The state of the s	of Reach 100
	77.75	163.68	1.45	0.002655	10.94	9.19	10.85	7,25	171.70	The second secon	er Reach 100
	32.67	58.15	1,12	0.004341	9.24						
	33.99	69.38	1.33	0.005449	9.60	8.01 8.23	9.17 9.51	6,42	- 65.40	O Zýr	er Reach 0
	34.85	77,05	3,44	0.006086	9.84	8.37	9.73	6.42 6.42	92,00	Q.5yr	er Reach 0
	35,66	64.20	1,54	8,006586	10,05	8.50	9.93	6,42	129.50	Q 18 yr Q 20 yr	r Reach 0 r Reach D
	37.29	93.32	1.54	0.096877	10.32	8.65	10.18	6,42	153.20	Q 50 yr	r Reach D r Reach D
	41.75	100,55	1.72	0.006895	10.52	€.77	10.37	6.42	171,70	Q 100 Yr	r Reach 0
	20.46	105.54									.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,
	29,46	35.54	1.64	0.009914	9.10		8.93	6.25	65.40	Q 2 yi	or Reach [-1]
	32.69	51.29	2.17	0.010071	9.44		9,22	6.25	92.00	Q.5 m	r Reach 1-1
	33.70	57.89	2.24	0.009711	9.67 9.89		9,43	6.25	111.20	Q 10 W	r Reach -1
	35.11	85.74	2,30	0.008401	10.16		9.63 9.69	6.25 8.25	129.50	Q 20.yr	r.Reach -1
	36,80	73.78	2.33	0,007643	10.36		10.08	6.25	153,2D 171,70	Q 50 yr	r Reach -1
								47.63	17100	IC TOUNT	r Reach -1
	52,68	47,69	1,47	0,006155	8.73	8,02	8,52	6.40	65,40	027	r Reach -2
	59.72	65.02 62.76	1,54	0.004727	9.10	8.24	8.99	6,40	92.00	Q 5 yr	Reach -2
	63.45	97.20	1,57 1,60	8.094048 0.093562	9.36	8.38	9.24	6,40	111,20	Q 10 yr	r Reach I-2
	67.61	116,52	1.62	0.003081	9.89	8,53	9,48	5.40	129.50	1C) 20 yr	Reach -2
	70.93	131.75	1.64	0.002799	10.12	8,55 8.75	9.77	6.40	153.20	O 50 yr	rReach -2
P				0.002.031	10.12.1	5.73	9,99	5.40	171,70	Q 100 Y	Reach -2
	37,38	61,00	1.07	0,002135	8.57		6.51	5.82	65,40	0.7%	
	39.72	75,48	1.23	0.002226	8.96		83,3	5.82	92.00	G Z yı	Reach -3
	41.25	85,90	1.32.	0.002220	9.23		9,14	5.82	111.20	Q 10 yr	Reach -3 Reach -3
	43.05	95.91	1.30	0,002165	9,48		9,38	5.82	129.50	G 20 yr	Reach 3
	45.80	109,08	1,45	0.002120	9.78		9,68	5.82	153,20	Q 50 yr	Reach -3
	59.48	121.11	1.50	0,002040	10,01		9.90	5.82	171,70	D 100 yr	Reach -3
	25,74	32.56	2.01	0.010975	8,40						
	27.15	41,71	2.21	0.010270	8.79		6.19 8.54	6.22 6.22	65.40		r Reach : 3.5
	28.19	48.80	2.28	0.009368	8.06		8.79	6.22	82.00 111.20		Reach -3.5
	29.18	55.74	2.32	0,008589	9.31		9.04	6.22	129.50		Reach -3.5
	30,43	64.88	2.36	0,007693	9.63		9,34	6.22	153.20	The barrier to respect to the period of the	Roach i-3.5 Roach i-3.5
	31,37	72,07	2,38	0.007113	9.66		9.58	6.22	171.70	worker to a control of the section o	r Reach [-3.5] r Reach [-3.5]
	ec 03										
	25.93 27.33	49.09 57,05	1,33	0.002485	8.33	7,01	8.24	5.96	65,40	Q 2 yr	Beach -4
	28,34	88,86	. 1,77	0.002980 0.003157	8,72 8,99	7.27	8,58	5.96	92.00	Q 5 yr	Reach 4
	29.29	58.24	1,90	0.003251	9.25	7.59	8,83 9.06	5.95 5.95	111.20	Q 10 yr.	r Beach : [-4
	30,49	75.06	2.04	0.003311	9.57	7,77	9.36	5.95	129.50 153.20		r Reach 4
	31,40	80.23	2.14	0,003332	9.81	7.89	9.58	5.96	171.70	Q 50 yr	Reach 4
									37 1.73	N 100 E	rReach -4
									Culvert	Donnington Stree	Reach 5
	20.00										
	25.03 25.75	51,45 56,91	1,27	0.001979	8.16	6.64	80.8	5.34	65.40	Q2yr	Reach 0
	25.25	59,77	1.86	0,003472	8.44 8.64	E.96	8.30	5.34	92,00		Reach 6
	25,89	62,91	2.05	0,003472	8.83	7.07	8.46 8.61	5.34	111.20	Q 10 yr	Reach -6
	27.77	65,60	8.30	0.004573	9.05	7.41	8,79	5.34 5.54	129.50	Q 20 yr	Roach -6
	28.36	69,36	2,48	0.005041	9.22	7,55	8.91	5.34	153.20 171.70		Reach 16
									47.117.91	10 no yr	Reach -5
	24:47	47.5D	1.38	0.003026	8.14		8.04	5.34	65.40	S CI 2 Vr	Reach -6.5
	25.97 26.03	52.83	1.74	0.004418	8.41		8,25	5.34	92.00		Reach -6.5
	26.65	56:69 60:71	1,95	0,005227	5.61		8,42		111,20		Hosch 1-6.5
:	27.54	65.56	2.13 2.34	0.005901	8,79 9.02		8,58	5.34	129,50		Reach -6.5
	28,19	E9.20	2,48	0.007235	9.02		8.74 8.87	5.34	153.20		Reach -6.5
				2,22,200	0.00		8.07	5,34	171,70	5 Q 100 yr	Reach 6.5
	29.36	44.76	1.48	0.004269	8.00		7,89	5.58	€5:40	027	
	33.28	48.60	1,91	0.006723	8.20		8.01		92.00		r Fleach -7
	35.77	52.05	2.18	0,008199	8.35		8.11	5,58	111.20		r Heach -7 r Heach -7
	37.57	55,47	2.40	0.009444	8.50		15.3	5.58	129.50		r Reach -7
	39.80	59.97	2.57	0.010870	8.68		£,32	5.58	153.20		r Heach -7
	41.37	63,45	2.85	0.011817	8.82		8.41	5.58	171.70		r Reach -7
	77,56	30 14									i i
	77,56	72.14 91.45	1,54	0.001658	7.85	6:44	7,80		65.40		r Reach -8
	78.51	96.80	1,30	0.008502	7.95	5,69	7.86	4.92	92.00		r Reach -8
	78,83	102.25	1.67	0.0031861	8,05 8,14	6,85 6.99		4,92	111.20		r Reacti -8
	79.26	109,54	1,86	0.003/67	8.26	7.17	8.02 8.11		129.50		r Roach -8
	79.50	115,34	1,99	0.004859	8.56	7.37			153,20		r Reach -5
						1,07	800	4.82	171,70	Q 100 yr	r Reach -8

	Salvin-Finel-09 River, Sak River Sta	Profile	D Tetal	Min On El	W.S. Floy	CR W.S.	EG ERY	E.G. Slope	Vel Cital	Flow Area	Tap Width	Froude # Chi
Reach	nine: Jia	and I state the	(m3/s)	(m)		(m)	. (m)	(hvm)	(m/s)	(m2)	(m)	
Lower Reach	i e	02%	65,40	5.06	7,76	6.50	7.78	0,000576	08.0	128.71	97.64	0.16
	173	Q5yt	92.00	5.06	7,51	6.81	7.85	0.001555	1,08	133.87	98,18	0,24
Lower Reach		Q 10 v7	111.20	5.06	7.86	7.02	7.91	0.952071	1,26	136.37	98.47	0.27
Lower Reach	-9 -0	Q 20 yr	129.50	5.06	7.91	7.13	7,98	0,002549	1.42	143.18	98,79	0.30
Lower Beach	9	Q 50 yr	153,20	5.05	7.97	7,25	6.06	0.003131	1,60	(49.90	99.23	0.34
Lower Beach	1-9		171.70	5.06	6.03	7,35		6,003542	1.73	155.50	99.59	0.39
Lower Reach		O 100 yr	171.70	3,00	0.021							
			55.40	4,50	7.73	6.20	7,75	0.000456	0.58	160.55	109,91	0.13
Lower Reach	-10	O 2 yr	65.40		7.75	6.40			0.80	163.95	110:31	0,17
Lower Reach	-10	1Q 5 yr	92.00	4.60		6.52			0.95	167,01	110.67	0.21
Lower Reach	-10	(0.10 yr	111.20	4,80	7,79		7.87		1.08	170.44	111,08	0.23
Lower Reach	2 P10	Q 20 yr	129.50	4.60	7.82	5.51	7,93		1,25	175.40	111.66	0.27
Lower Reach	J-10	Q 50 yr	153.20	4.60	7.87	6.77			1,37	179.76	115.87	0,29
Lower Reach	-10	Q 100 yr	171,70	4,80	7,91	6,84	7.98	0.002204	1.01	113,70	1	
Million follows							ļ	0.000234	0.45	239.00	137.48	0.05
Lower Roach	-11	Q 2 yı	65.40	4.39	7.72	6.01	7.73		0.48	242.25	137.57	0.13
Lower Reach	J -111	Q 5 yr	92.00	4.39	7.75	.E.32	7.76		0.75	245.22	137,65	0,19
Lower Reach	(411)	0 10 yr	111.20	4.39	7,77	6,45				245.26	137,75	0.18
Lower Reach	[411	Q 20 yr	129.50	4.39	7.79	6.54	7,82		0.87		137.88	0.20
Lower Roach	-31	Q 50 yr	153.20	4.39	7,83	6.69	7.86		1.00	253,56		0.22
Lower Reach	1-11	Q 100 yr	171.70	4.39	7.85	6,77	7.90	0.001279	1.11	257.95	138.01	0.22
							,					0,13
Lower Reach	-12	C Syr	69.40	4,33	7.70	5.95	7.71	0.000452	0.69	142.46	139,11	
Lower Reach	-12	O S ye	92,00	4,33	7.70	6.17	7.73	0.000894	0.82	142.46	139,11	81.0
Lower Reach	-12	IQ 10 yr	111.20	4.33	7.70	6.30	7.74	0.001306	1.00	142.46	139.11	0.22
Lower Reach	512 (C)	□ 20 yr	129.50	4,33	7.70	6.45			1,16	142.45	139.11	0.25
Lower Reach	-12	Q 50 yr	153.20	4.33	7,70	6.56	7,78	0.002460	1,37	142,46	139.11	0.30
THE R. CO. LEWIS CO. P. LEWIS CO.	cotor of the management of the process of the pro-	Constitution of the second					7.00	2 202416	< 54	727.46	130/15	0.34

	Galvin-Final-09		Ck Reacit: Gl	TOL ALCO	W.S. Elev	CHWS	E,G. Elev	E.G. Slape	Vel Chal	Flow Area	Top Width	Froude # Chl
Réach	River Sta	Profile	O Total	Min Ch El			(m)	(m/m)	(m/s)	(m2)	(m)	
	Logical	1 Steeling of	(m3/s)	(m)	(m)	(m) 23.41	24.04	0.007618	1.42	3.89	8.59	0.44
Glongariff Trib	910	Q 2 yr	12.80	22,20	23.93		24.04	0.011160	1,81	10.54	9.11	0.5
Glenganff Trib	910	Q 5 yr	19.10	22.20	24.11	23.64	24.44	0.0111676	2.14	11.42	9.39	0.62
Glengariff Trib	910	Q 10 yr	24.50	22.20	24.20		24.58	0.017568	2.41	12,18	9.62	0.68
Glengariff Trib	910	Q 20 yr	29.30	22.20	24.28	23.94	24.77	0.020811	2,71	13.32	9.96	0.75
Glengariff Trb	910	O 50 yr	.36.10	22.20	24,40	24.12		0,021465	2.85	14.60	10.33	0.77
Glengard (Trib	910	Q 100 yr	41.60	22,20	24.52	24.25	24,94	0,0214651	2.05	1111		<u> </u>
						~~	22,36	0.011232	1,47	16.20	40,45	0.5
Glengariff Trib	730	O 2 yr	12,80	20.66	22,28	22.11	22,56	0.007713	1,44	26.25	41.82	0.44
Glengarill Trib	730	O 5 yr	19.10	20.66	22,52	22.25		D.005949	1.42	34,70	42.94	0.40
Glengariff Trib	730	D 10 yr	24.50	20.66	22.72	22.33	22.78	0.005949	1.43	41,35	43.80	0.3
Glengarill Trib	730	Q 20 yr	29.30	20.66	22,87	22.39	22,93	0.003742	1.47	49.27	44.81	0,3
Giengariff Trib	730	Q 50 yr	36,10	20.66	23,05	22.48	23.11		1.56	53.63	45.35	0.38
Glengaritt Trib	730	Q 100 yr	41.60	20.66	23.15	22.54	23.22	0.004914	1,30	55.05	10.00	
									1.57	10.92	12,28	0.53
Glengarill Trib	510	Q 2 yr	17.10	17.99	20.05		20.17	0,009097	1.79	15,86	31.03	0.55
Glengarift Trib	510	Q 5 yr	25.50	17,99	20:28		20,44	0.011808		17.77	35.81	0.66
Gleogariff Trib	510	G 10 yr	32.60	17.99	20,34	20.05	20.56	0.016687	2,13	19,45	39,21	0.75
Glengaritt Trib	510	Q:20 yr	38.80	17.99	20,38	20.25	20.67	0,021014	2.40	23.59	46.56	
Glengariti Trib	510	Q 50 yr	48.10	17,99	20.48	20.44	20,82	0.024906	2.55	30.25	67.36	0.7
Glengarill Trib	510.	Q 100 yr	55.50	17,99	20,60	20.60	20.91	0.023597	2.53	30.23	00.00	5,7
								B All Berg	2.25	7.76	10.00	0.6
Glengariff Trib	410	Q 2 yr	17,10	17,21	18.92	18.61	19,18	0.010595		20.03	63.02	0.6
Glengariff Trib	410	Q5 yr	25.50	17.21	19.23		19.45	0.008291	2.26		71,87	0,5
Glengariff Trib	410	Q 10 yr	32,60	17.21	19.43		19.59	0.006215	2,09	33.33	77,56	0.4
Glengariif Trib	410	Q 20 yr	38,60	17.21	19.57		19.70	0.005162	1.99	43.84	80,15	0,4
Glengariff Trib	410	Q 50 yr	48,10	17.21	19,71		19.83	0.004746	1.99	55.44	B1.85	
Glengarill Trib	410	Q 100 yr	55.50	17.21	19.81		19.92	8,004630	2,02	63.25	. 81.85	1 ,0,4.
			i .							7.70	7.04	0.6
Glengariff Trib	330,1	Q 2 yr	17.10	16.33	18,07		18,32	0.010952	2.21	7.73	7.61	0.7
Glengarili Trib	330.*	Q 5 yr	25,50	15.33	15.36		18.68	0.011116		10.62	12.58	
Glengariff Trib.	330.*	Q 10 yr	32.60	16,33	18,56	18.35	18,92	0.011078	2,74	13.89	23,40	
Glongarif Trib	330.*	G 20 yr	38.60	16.33	.18.71	18,55	19.09	0.010759	2.84	18.55	38.98	0.7
Glengarilf Trib	330.*	Q 50 yr	48,10	16.33	18.90		19.28	0.009830	2,90	27.20		
Glerganif Trib	330.5	Q 100 yr	55.50	16.33	19.06		19.40	0,008658	2,88	35,11	53,53	0.6
Cloring and Co	-										L	
Glengariff Trib	250.*	Q 2 yr	17.10	15,45	17.28		17,49	0.009497	2.05	8.34		
Glengarilf Trib	250.*	Q.5 yr	25,50	15.45	17,60		17,87	0,008909	2.29	11,58		
Glengarill Trib	250.*	Q10 yr	32.60	15,45	17.83	17,44	18.13	0.008553	2.45	14,72		
Glengariff Trib	250.*	O 20 yr	38.80	15.45	17,98	17.63	18.31	0.008487	2.60	17,59		
Glengariff Trib	250.*	O 50 yr	48,10	15.45	18,18	17.83	18.55	0.008274	2.78	22.24	23,13	
Glengarilf Trib	250.	Q 100 yr	55.50	15,45	18.33	18.01	18.73	0.008086	2.90	26.12	31,07	0.6
Grengani na	1								<u> </u>			
Glengarif Trib	170.*	Q 2 yr	17.10	14.57	16:32		18,58	0.013747	2.28	7.48		
Glenganif Trib	170.*	Q 5 yr	25.50	14,57	16,53	16,40	15.91	0.016762	2.73	9.35	9,12	
Glenganii Trib	170.1	Q10 yr	32.60	14,57	16.69	16.60	17.15	0,018031	3:01	10.86	10.55	
Glengarii Trib	170,	G 20 yr	38.80	14.57	16.82	16.76	17.94	0.017947	3.20			0.9
Glenganti Trib	170.	Q 50 yr	48,10	14.57	16:09	16,95	17,60	0.017704	3.47	14.70		
Glengariff Trib	1170.*	Q 100 yr	55,50	14.57	17.11	17.10	17.78	0.017551	3.65	16.70	17.15	0.9
calengarin HIIC	170.	- coc 1c	1									
or water	90	Q 2 yr	17.10	13,69	15,93		16.02	0.003624	1.36	16.48	32.88	
Glengariff Trib	90	Q5yr	25,50	13.69	16.27		16.37	0.002829	1.44	28.78		
Glengarilf Trib	90	0 10 yr	32.60	13:69	16.52		16.61	0.002503	1.49			
Glengariff Trib		Q 20 yr	38.80	13.69	16.72		16,82	0.002222	1,52	47,97		
Glengarilf Trib	90	Q 50 yr	48.10	13.69	16.98		17.08	0.002030	1.58	60,73	50,98	
Glengarilf Trib	90		55:50	13.69	17.16		17.26	0.001944	1,63	69.98	52,86	ε,0
Glengariti Trib	90	O 100 yr	33.50	15.08	12.10			1	1	T ·		
		100	17.17	13,66	15.69	15.17	15.82	0.004270	1,61	10.60	9.98	0.5
Glengariff Trib	40		17,10		16.02	15.44	15.19	0.004368	1.80	14,17	11,58	0.5
Glengariff Trib	40		25.50	13.65	16,26	15.64	16,44					
Glangarilf Trib	40	Q 10 yr	32,50	13,65	16,26 15.48	15.54	16,44	0.003674				
Glengarill Trib	40	C 50 M	38.80	13,65		15.98	16.94		2.00			
Glengariff Trib	40.	Q 50 yr	48.10 55.50	13.65 13.65	15,75 16,93	15.98	17,13				4	

city design



Dedicated to a better Brisbane

Appendix J Flood Inundation Plots



Branch name & Cross section	Chainage	& AMTD	Ca	libration ever	Verification Events		
ID:	MIKE-11 Chainage	AMTD (m)	Mar-92	Jan-94	Mar-01	Мау-96	Nov-04
Mi13	2325		40.46	40.39	41.57	40.44	41.31
Mi12	2516		39.45	39.40	40.53	39.44	40.26
Mi11	2635		38.68	38.63	39.83	38.69	39.53
Parkway St	2648		Parkway St	reet bridge a	nd weir	Construction of the Constr	· · · · · · · · · · · · · · · · · · ·
Mi10-2	2664	<u> </u>	38.61	38.57	39.64	38.60	39.38
Mi9	2718		38.43	38.39	39.40	38.42	39.14
Vii8	2828		37.74	37.64	38.93	37.69	38.60
Mi7	2955		37.35	37.14	38.64	37.24	38.28
VII /	3069		37.07	36.87	38.23	36.96	37.93
Mi5	3221		36.52	36.35	37.63	36:42	> 37.31
Mi4	3388		35,74	35.51	37.06	35.62 🤇	36.69
Mi3	3496		35.36	35.14	36.63	35,26	36.25
Mi2	3585		35,03	34.82	36.16	34.93	35.82
Mi1	3801		33.95	33.71	35.10	34.03\	34.82
Mi2	3890		33.22	32.99	34.47	33.59	34,28
Minnippi BypassBranch							<u>,,, ,, ,, ,, ,, ,, ,, ,, ,, ,, ,, ,, ,,</u>
	80		3.21	2.62	\3.52 \	3.20	2.99
Minnippi_new1	125		3.10	2.62	3,51	3.19	2.97
Minnippi_new2	230		3.07	2.62	3.47	3.16	2.95
Minnippi_new3	400		∠3,01 \	2.62	3.42	3.09	2.91
Minnippi_new4 Minnippi_new5	542	\	2.97	2.62	3.39	3.04	2.89
Stanton RD	€650	+++	2.95	2.62	3,37	3.02	2.88
new_A	720		2.85	1.77	3:30	2.99	2.65
new_B	730		2,84	2.00	3.28	2.98	2.55
Minnippi new6-US	745	+/	2.84	1.20	3.27	2.98	2.55
Gateway culverts	748		Gateway C	ulverts	<u></u>	A	
Minnippi new7-DS	810		2.84	1.14	3.26	2.97	2.55
new_E	825		2.83	1.30	3.25	2.96	2.54
new G	860	<u> </u>	2.81	2.20	3.22	2.94	2.52
new_7a	870		2.78	1.58	3.20	2.92	2.49
Minnippi new8	945		2.50	1.68	2.88	2.66	2.15
BM31GHD_modified	1015	 	2.34	1.67	2.74	2.51	1.98
Minnippil-6 ALS	1115		2.25	1,67	2.64	2.41	1.89
Wynnum Road bridge	1125		Wynnum R	load bridge a	nd weir	I	
V	1150		2.17	1.66	2.39	2.28	1.88
BM 31GHD-copy	1310		2.13	1,66	2.32	2.22	1.84
BM36_GHD	1560		2.08	1.66	2.23	2.17	1.81
Minnippi_newl1	1850	-	2.06	1.66	2.17	2.12	1.79
BM 42B_GHD BM42BGHD	2004	-	2.04	1.66	2.13	2.10	1.78
	2001				<u> </u>		····
Murarrie Bypass Branch	7.0		2.49	2.04	2.63	2.50	2.26
MU1_ALS	20 35	<u> </u>	2.48	2.03	2.62	2,49	2,25
New MU1_ALS	35 160		2.47	2.02	2.62	2.48	2.24
New_MU2_ALS	275		2,47	2.02	2,61	2.48	2.24
New_MU3_ALS			2.46	2.01	2.61	2.48	2.23
Copy_new_MU3	310 390	<u> </u>	2.46	2.00	2.60	2.47	2,23
New_MU5_ALS	<u> </u>	<u> </u>	2.45	1.99	2.60	2.47	2.21
Mu_6_ALS	470		۷.۳۰	1	2.00		1 - 2 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -
Gateway culverts			0.00	1.02	2.40	2.32	2.10
MU_7_ALS	545		2.28	1.93	2.40	1 4.34	5.10

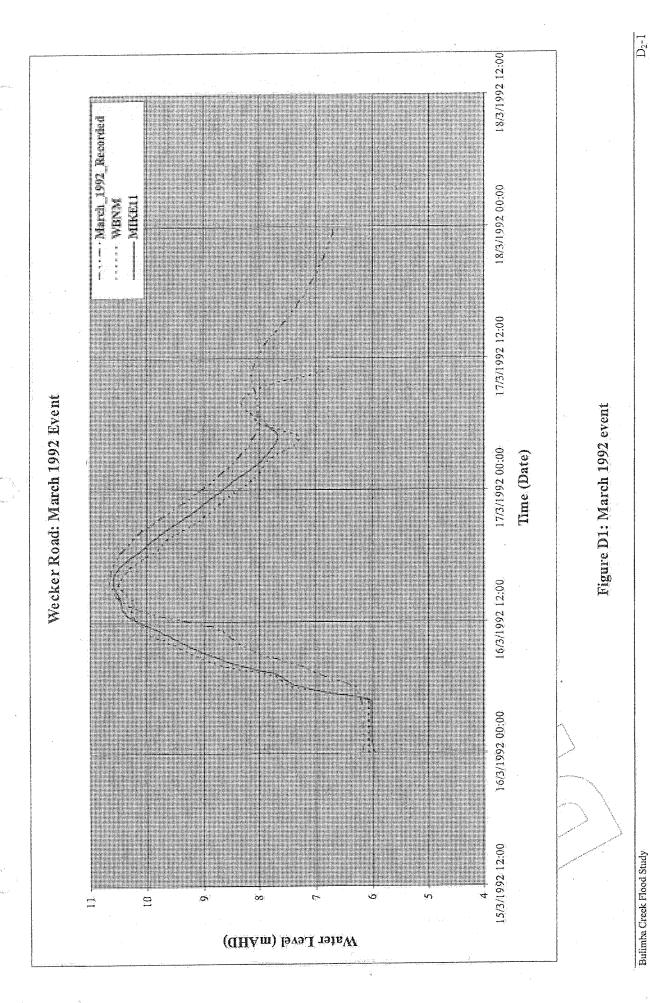
Bulimba Creek Flood Study

D-12

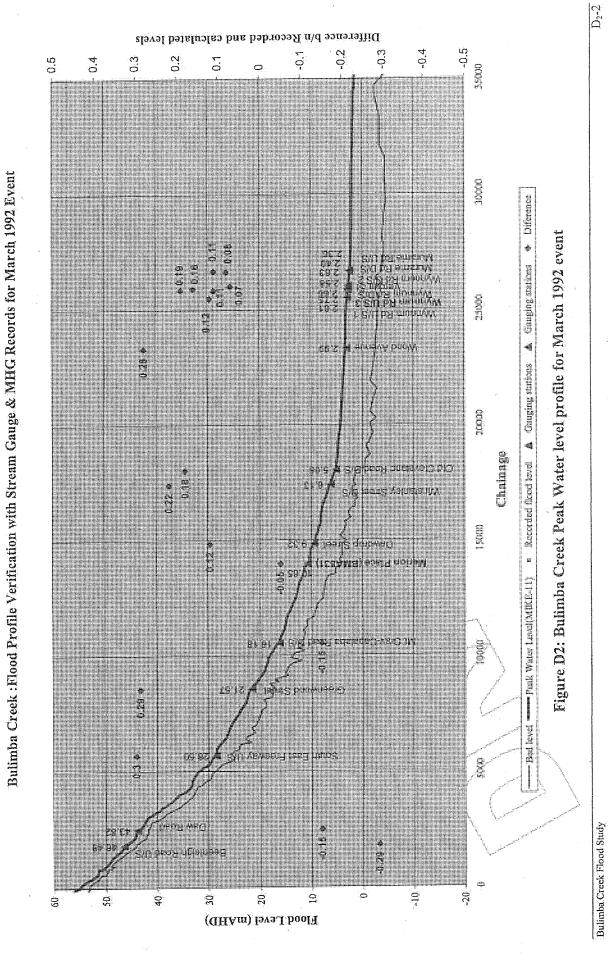
Branch name & Cross section ID	Chainage d	& AMTD	Calibration	ı events		Verification events		
	MIKE-11 Chainage	AMTD (m)	Mar-92	Jan-94	Mar-01	May-96	Nov-04	
MU_9_ALS	595	######################################	2.27	1.92	2.40	2.31	2.09	
MU5_ALS	640		2.26	1.91	2.38	2.30	2.08	
	650		2.26	1.90	2.38	2.30	2.08	
Bulimba East Leftarm								
BE276	0		48.19	47.78	48,46	48.02	48.39	
BE276	33		48.11	47.62	48.39	47.87	\ 48.29	
BE275	144	· · · · · · · · · · · · · · · · · · ·	47.80	47.80	47.80	47.80	47.80	
BE274	226		46.97	46.95	47.39	46.95	47.23	
BE273 US	347		46.88	46.87	47.31	46.87	47.14	
BE273 DS	443		46.56	46.56\	46.88	46.56	\46.76	
BE273A	488		46.40	√ 46.39 \	46.64	46.39	46.57	
BE273A	520		46.40	46,11	46.61	46.27	46.55	
Cleveland Rail	1	ang ang ang ang ang ang ang ang ang ang 		M. A.	1 1			
CLEV RAIL	0		\1.71	1,22	\ 1.71_>	1.74	1,20	
CLEV RAIL	939		1.36	0.91	1.48	1.54	0.91	

D2 Peak water level plots for calibration/verification events





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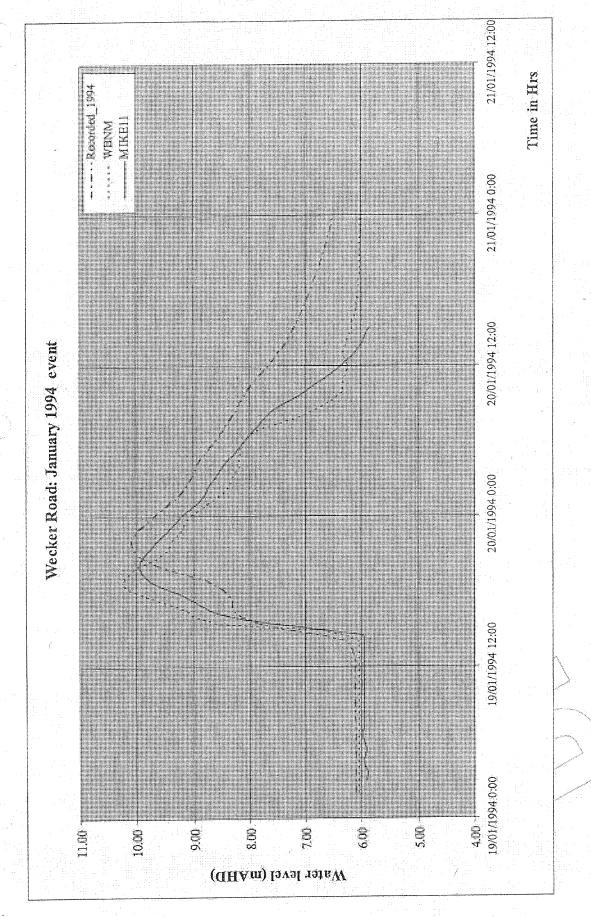
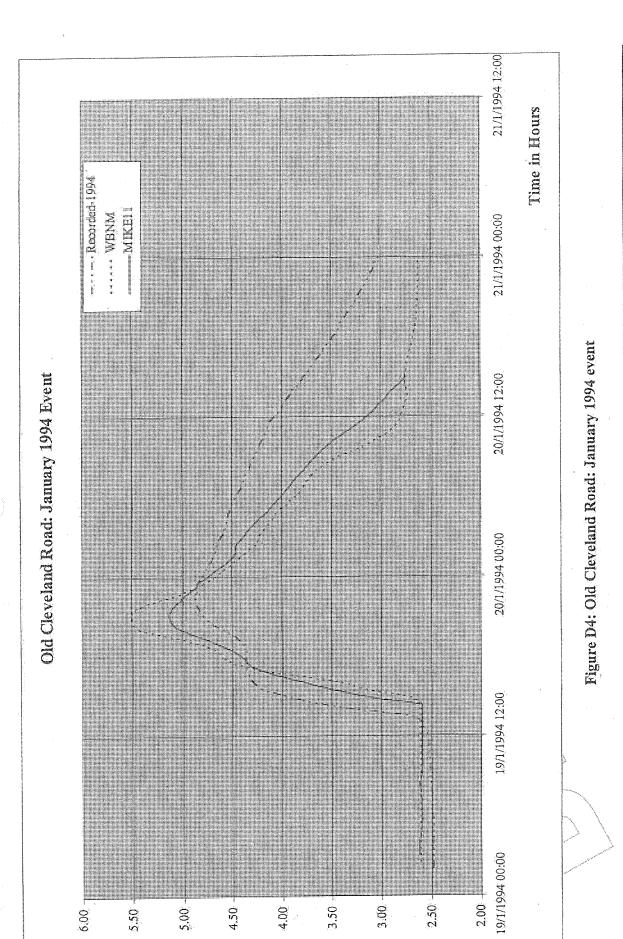


Figure D3: Wecker Road Gauging Station-January 1994 Event



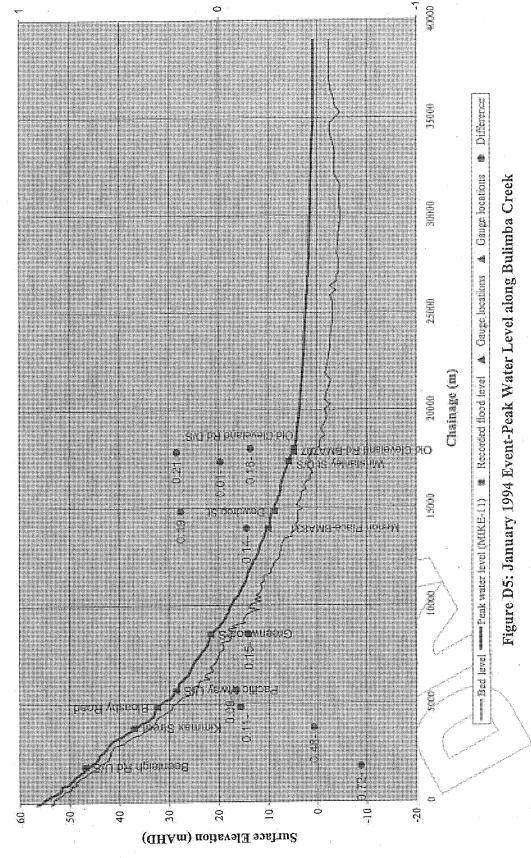
Watr level in mAHD

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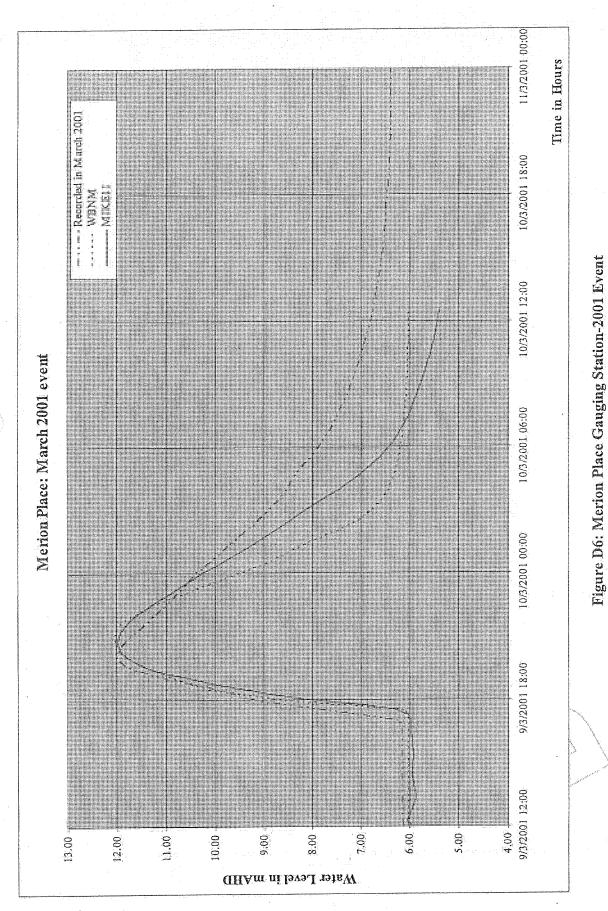
Bulimba Creek Flood Study

D₂-4



Bulimba Creek: Flood Profile Verification with Stream Gauge & MHG Records for January 1994 Event

Difference b/n Recorded and calculated levels





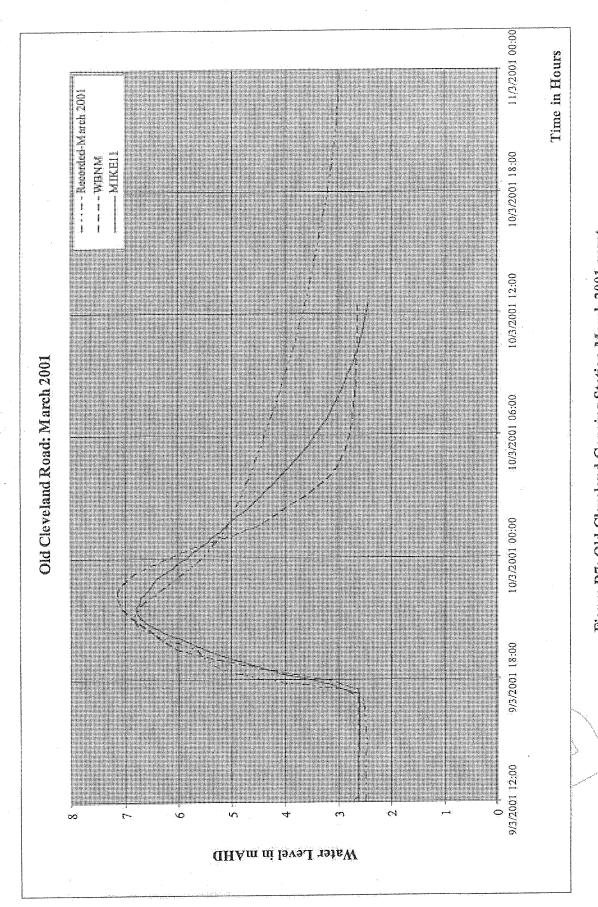


Figure D7: Old Cleveland Gauging Station-March 2001 event

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D₂-8



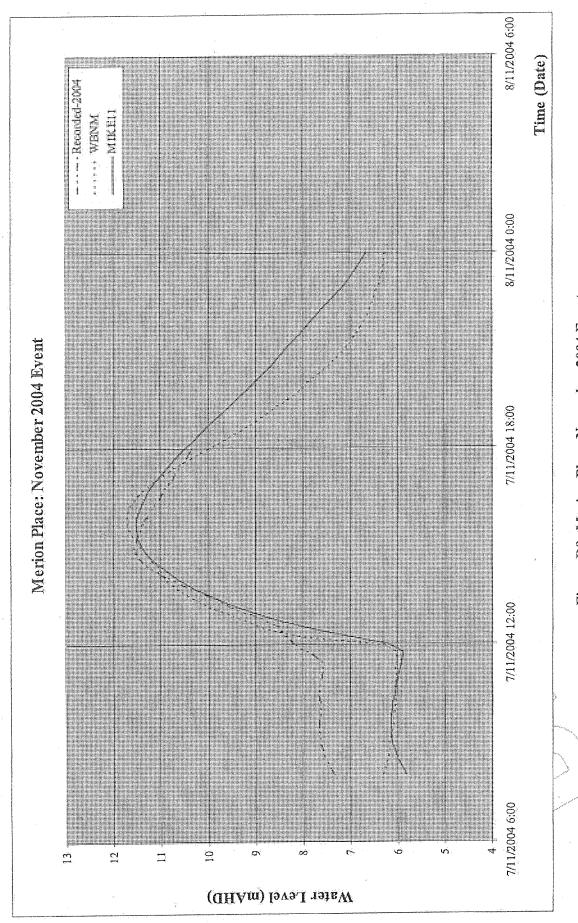
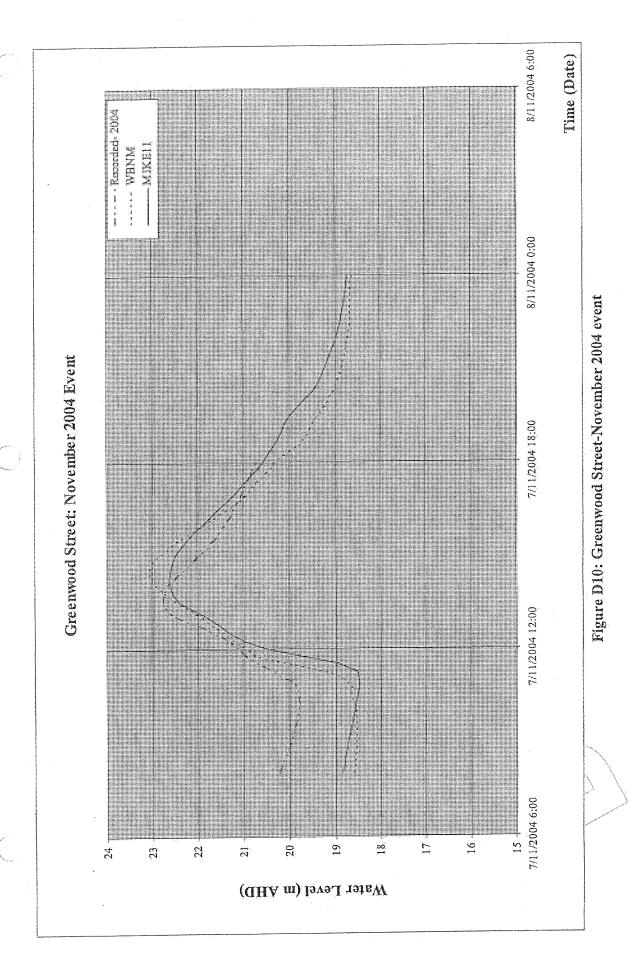
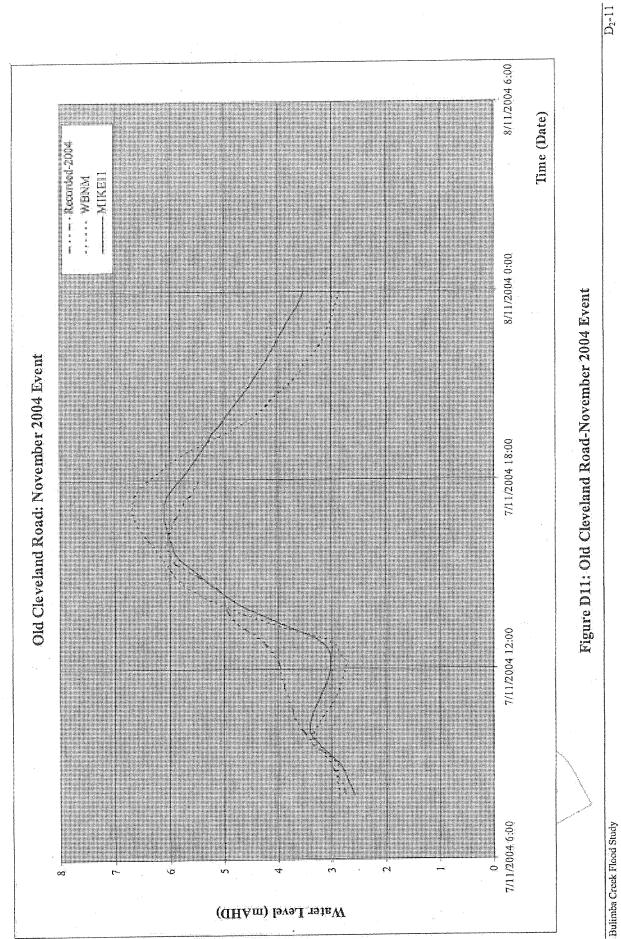


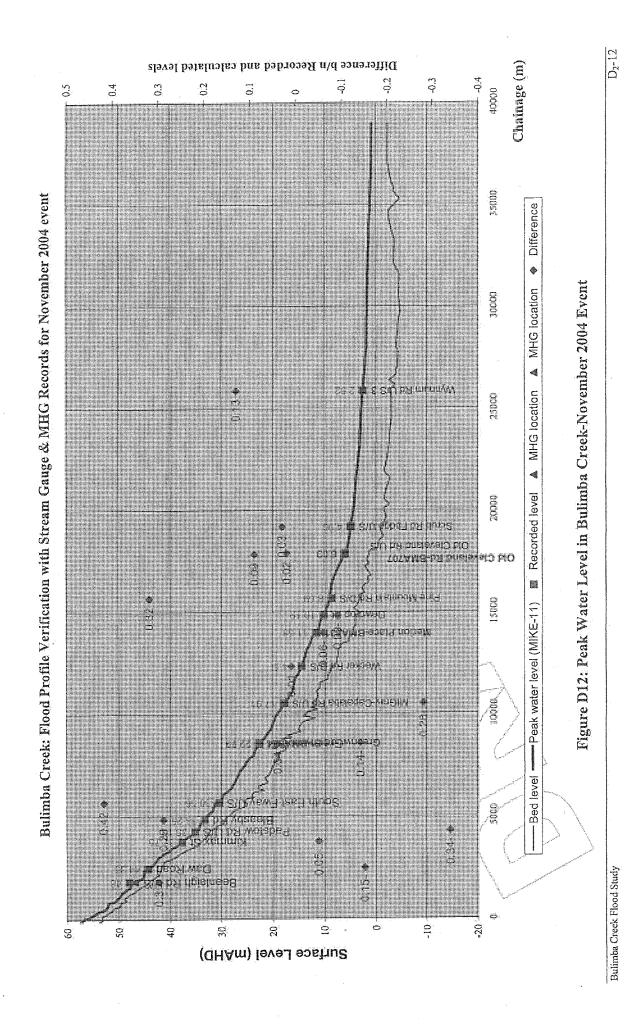
Figure D9: Merion Place-November 2004 Event

Bulimba Creek Flood Study











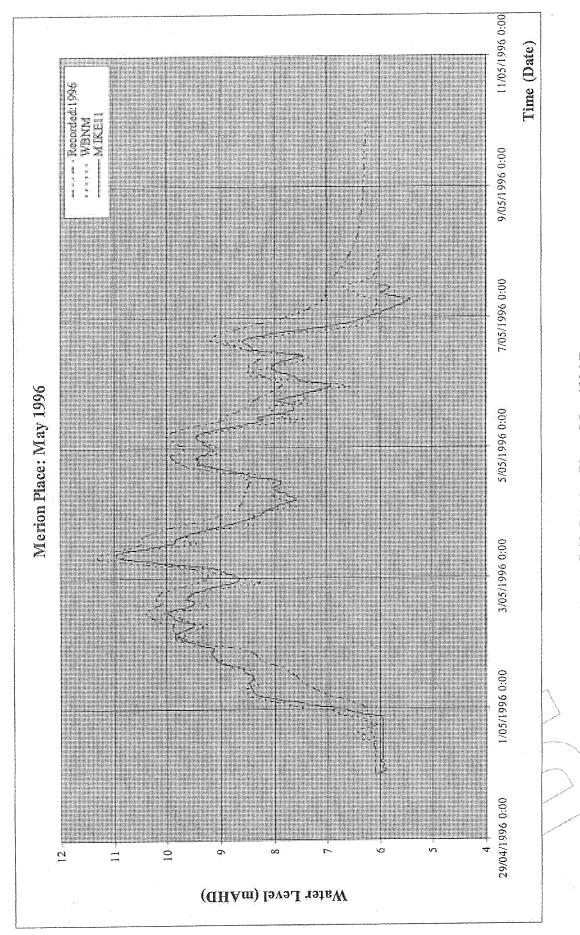
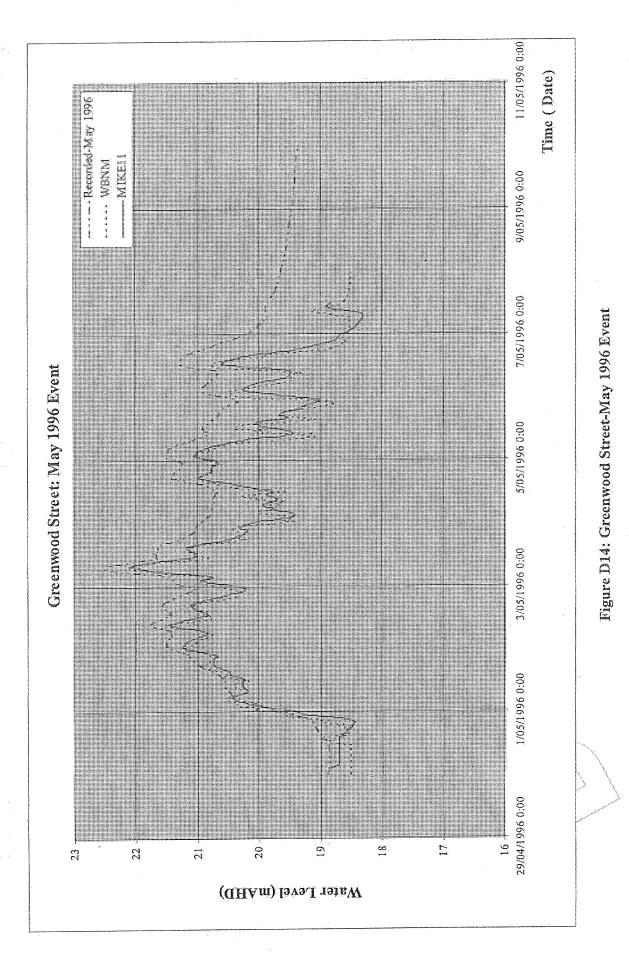
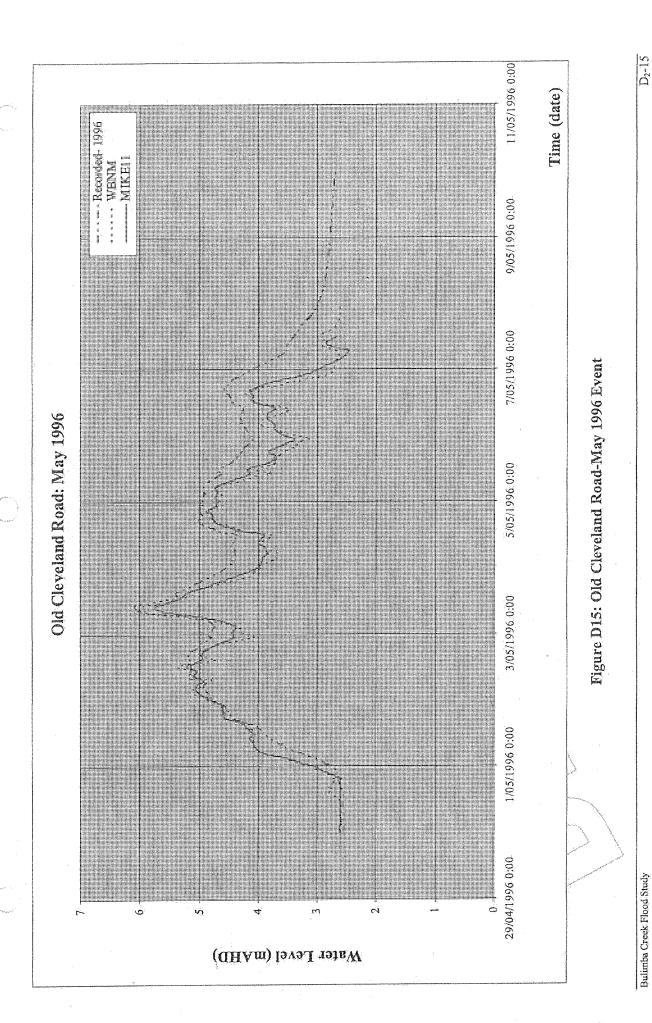


Figure D13: Merion Place- May 1996 Event







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Appendix E Downstream Boundary Levels Adopted for Calibration/Verification Events



TIDAL TAILWATER LEVEL March 1992 - Brisbane River at Pinkenba

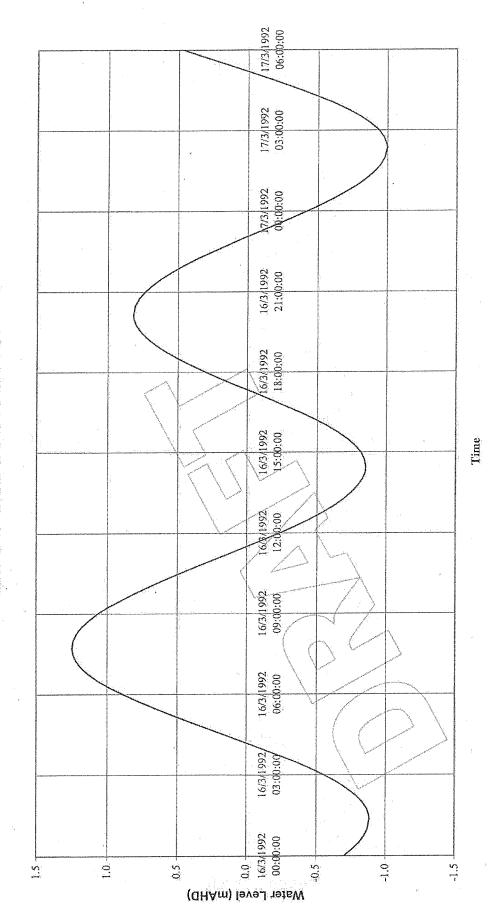


Figure E1: Tidal tail water level at Pinkenba for March 1992 event

E-2



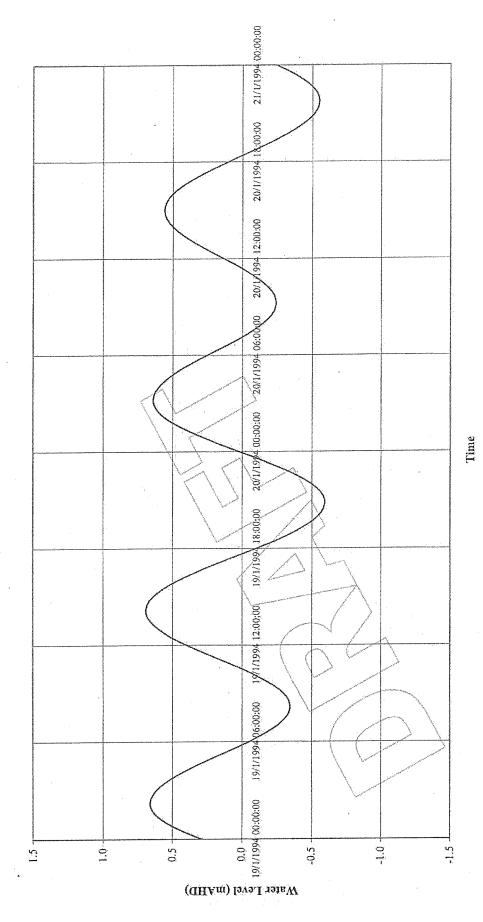


Figure E2: Tidal tail water level at Pinkenba for January 1994 Event

TIDAL TAILWATER LEVEL May 1996 - Brisbane River at Pinkenba

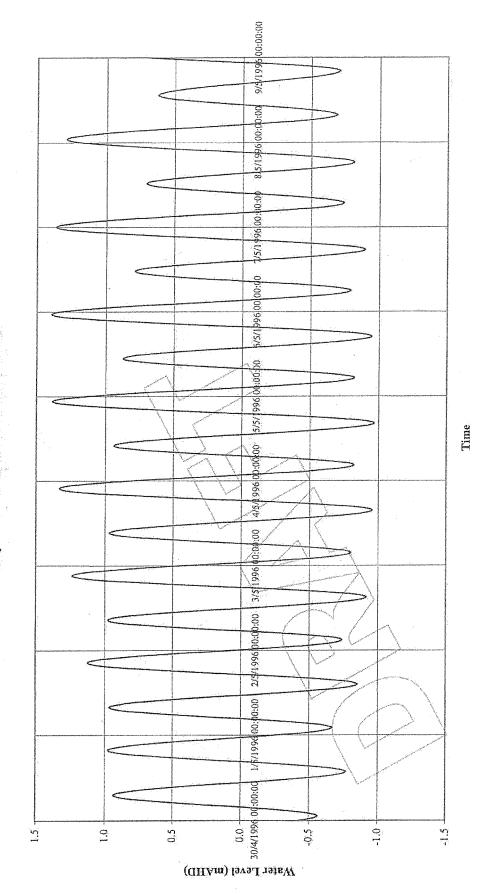


Figure E3: Tidal tail water level at Pinkenba - May 1996 Event

TIDAL TAILWATER LEVEL March 2001 - Brisbane River at Pinkenba

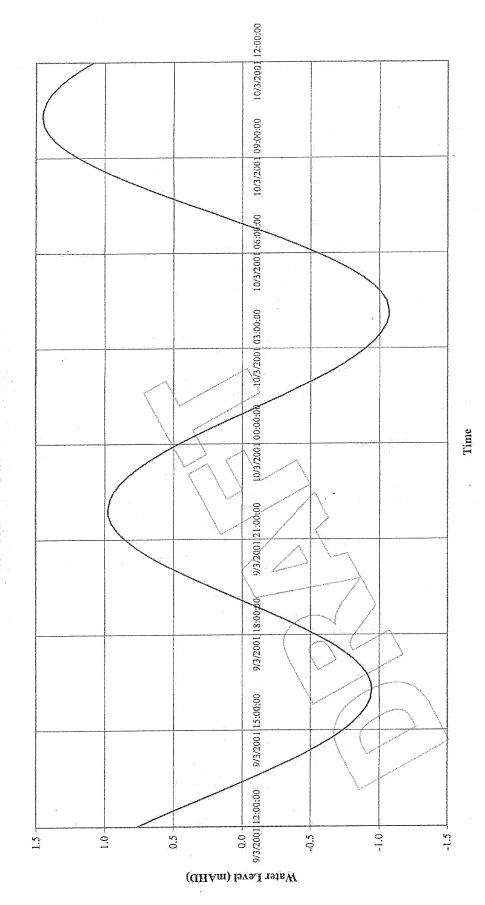
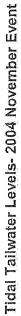


Figure E4: Tidal tail water level at Pinkenba - March 2001 Event

Bulimba Creek Flood Study



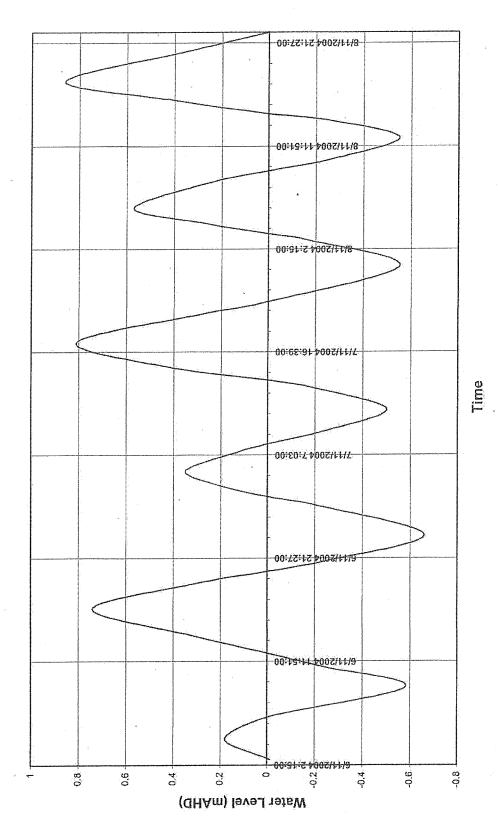


Figure E5: Tidal tail water level: November 2004 event

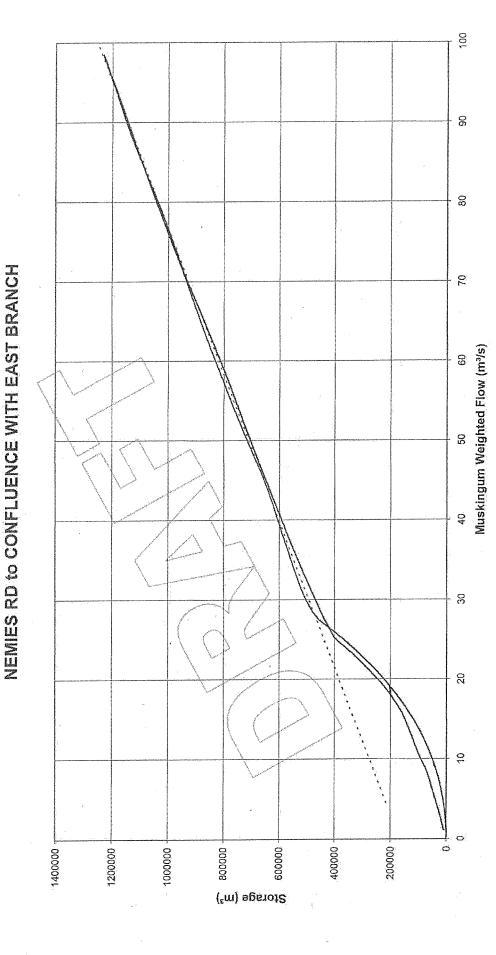
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Appendix F Muskingum Analysis





MUSKINGUM ANALYSIS

Figure F1: Muskingam analysis for Bulimba Creek: Nemies Road to confluence with East Arm

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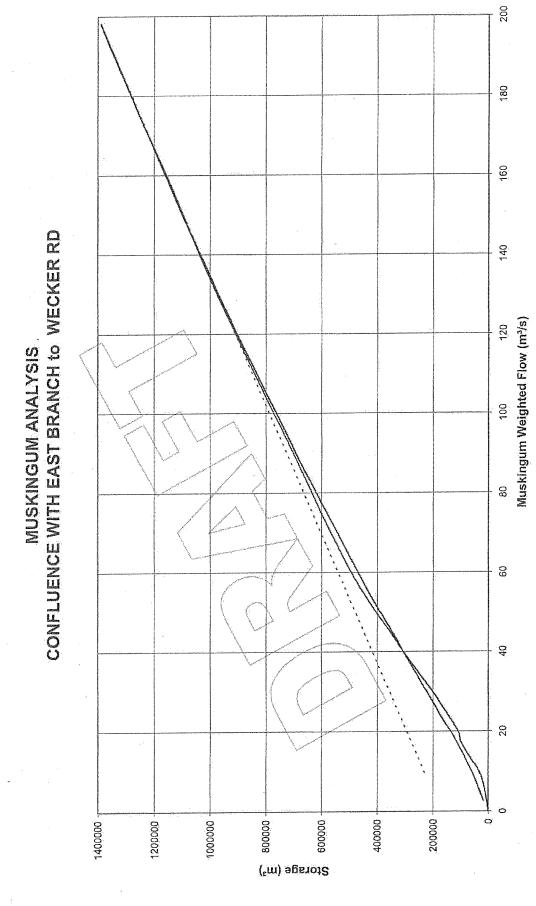


Figure F2: Muskingam Analysis-Bulimba Creek from East arm confluence to Weeker Road

BCC.079.1179

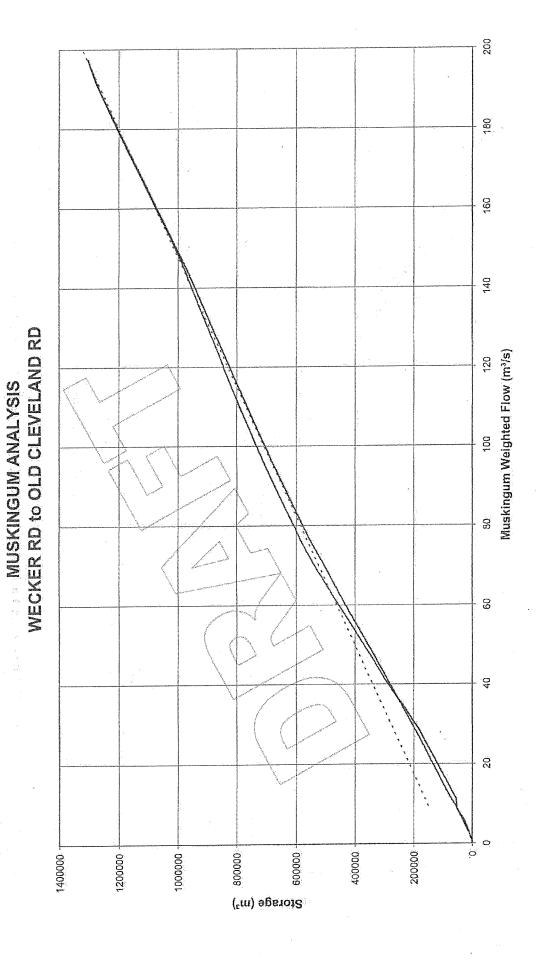
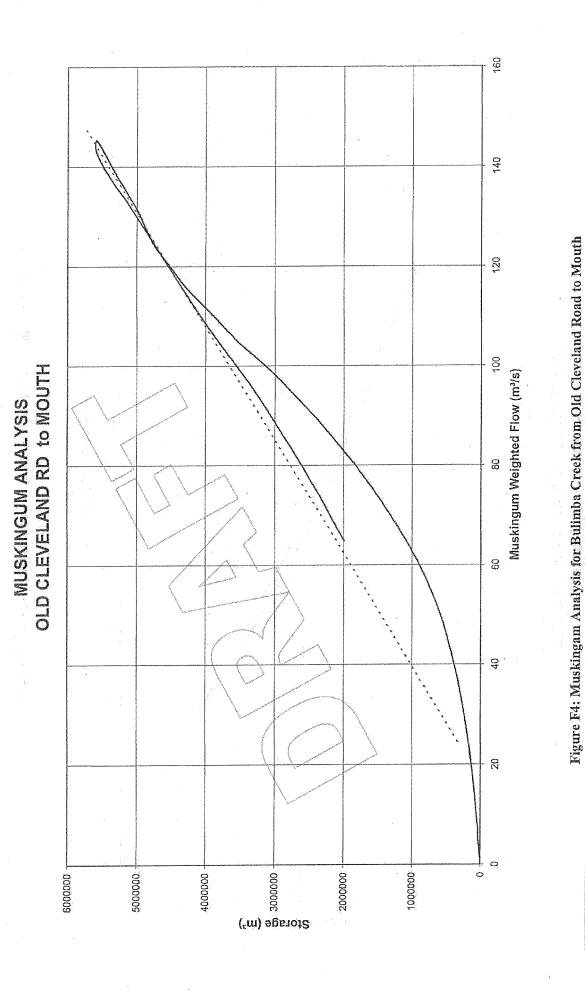


Figure F3: Muskingam Analysis-Bulimba Creek from Wecker Road to Old Cleveland Road

F-3

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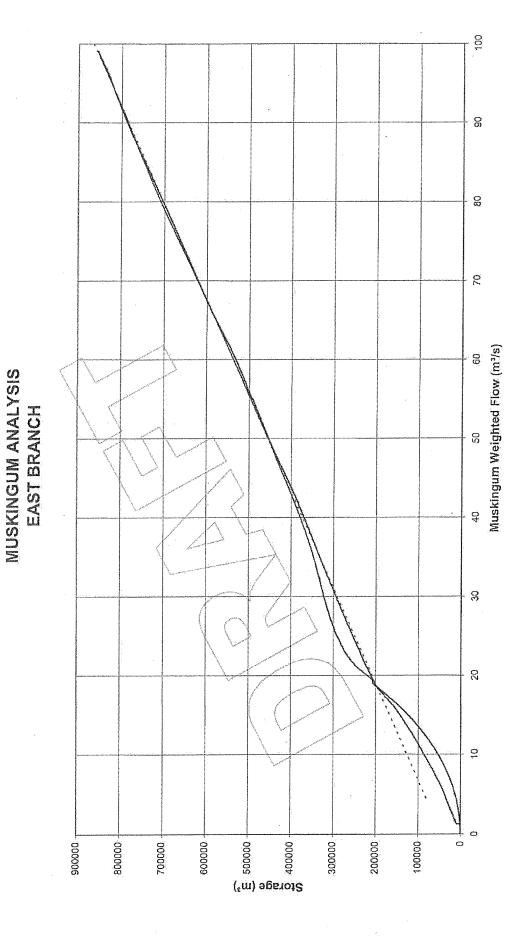


Figure F5: Muskingam Analysis-Bulimba Creek East Branch

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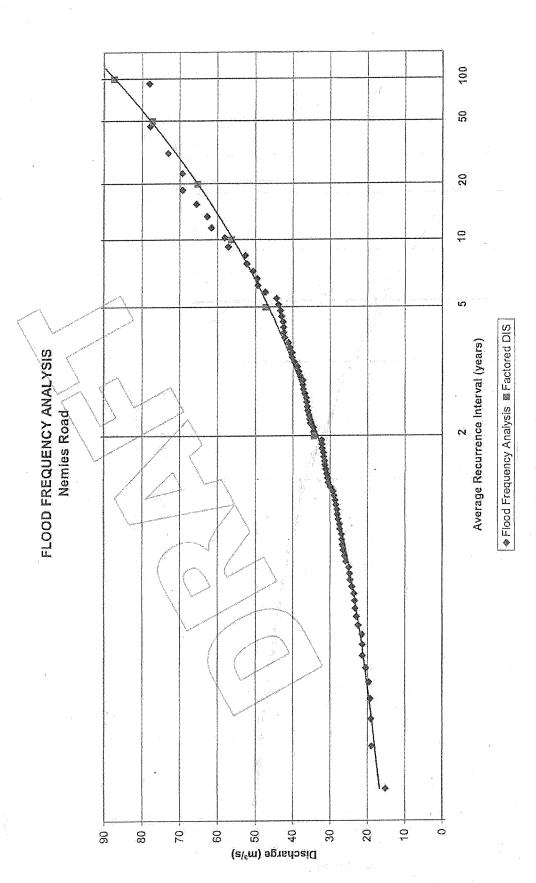


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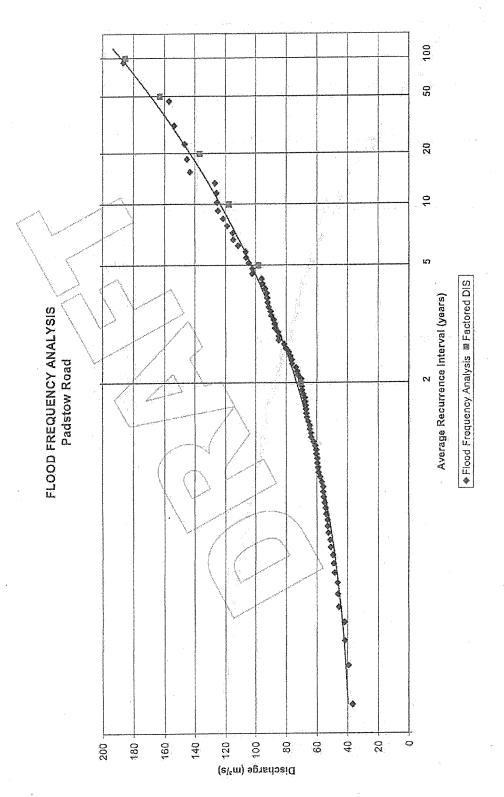
Appendix G Flood Frequency Analysis

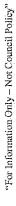


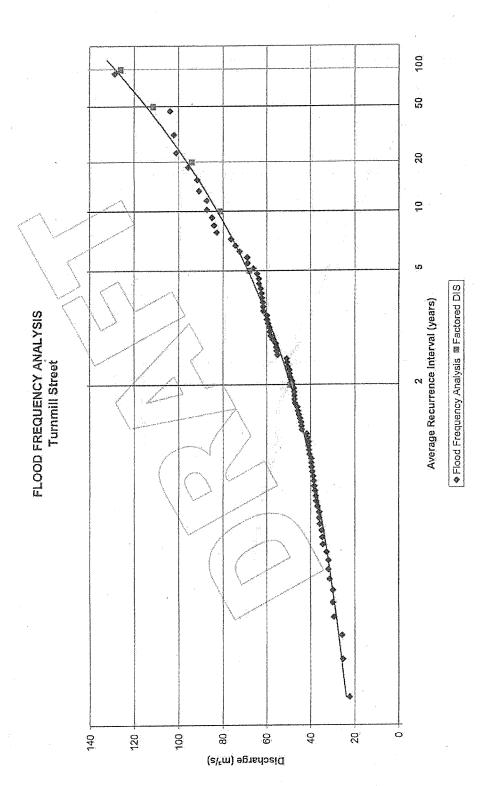




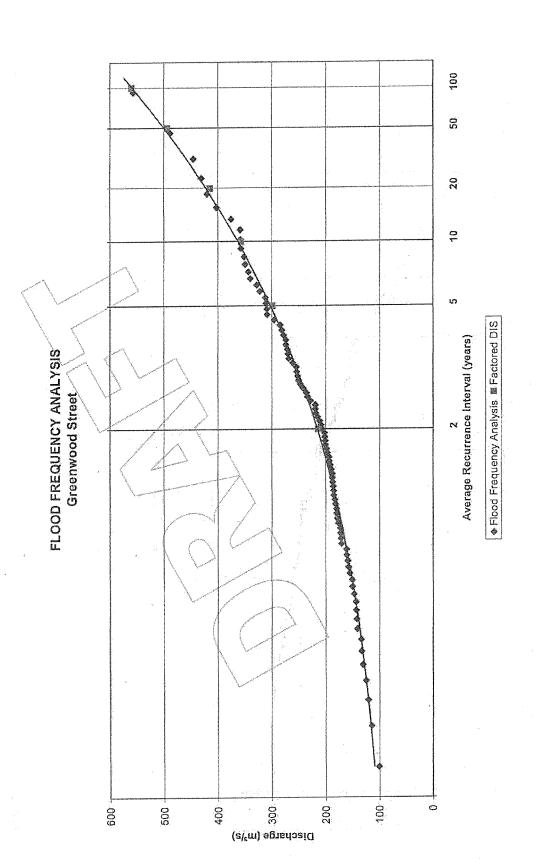
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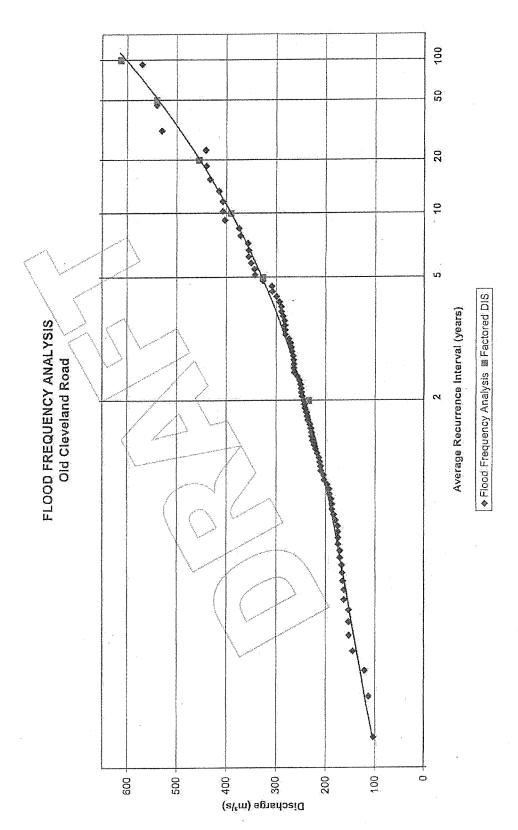








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Appendix H Design Peak Flood Discharges at Sub- catchment Outlets



Table H1: Peak flow discharges at each sub-catchment outlet for design events (from WBNM hydrology model)

Sub-catchment ID		Peak flood Dis	charge at each	sub-catchment	outlet (m3./sec)	
	100yr	50yr	20yr	10yr	5yr	2yr
Ala	60.3	56.5	47.7	41.4	34.8	24.2
Alb	86.6	77.6	65.5	56.6	47.5	33.9
A2	103.4	92.4	77.9	67.1	56.2	39.8
A3	115.5	101.7	85.7	73.8	61.7	44.4
В	121.5	106.6	89.6	77.2	64.5	46.5
Cla	39.5	36.9	31.2	27.1	22.8	15.9
C2b	78.1	67.7	57.2	49.3	41.2	30.2
D	88.3	83.0	70.1	60.8	51.1	35.3
Е	109.9	94.6	80.0	69.0	57.8	42.9
F	125.2	109.0	92.0	79.3	66.4	48.6
G	183.7	160.0	134.4	1,15.5	96.3	69.3
H	307.0	266.7	224.1	192.8	160.9	116.7
<u> </u>	316.3	276.1	231.7	199.5	166.5	120.0
<u> 12</u>	322.0	282.4	237.0	204.1	170.3	122.2
Ji	21.7	20.2	17.1	14.9	12.6	8.9
	48.8	41:5	35.1	30,3	25.5	19.2
KI.	65.9	57.4	48.5	41.6	34.8	25.3
K2 \	21.8	20.3	17.1	14.8	12.5	8.7
K3 \	30.2	27.0	22.8	19.6	16.4	11.6
LI	98.8	86.6	73.0	62.7	52.5	37.8
L2	120.3	105.9	89.1	76.5	63.9	45.7
M1	124.0	109.3	92.0	79.0	66.0	47.2
M2	41.7	38.9	33.1	28.8	24.4	17.2
M3	46.6	43.0	36.5	31.6	26.6	18.6
M4	11.2	10.4	8.7	7.5	6.3	4.3
M5a	34.1	31.8	26.8	23.2	19,4	13.4
M5b	49.3	44.6	37.5	32.4	27.1	19.1
M6	17.8	16.6	14.0	12.1	10.1	7.1
M7	66.4	59.7	50.3	43.3	36.2	25.5
M8	114.1	102.0	86.1	74,2	62.2	44.3
NI	230.7	201.8	169.9	146.1	122.1	88.1
N2a	33,2	31.0	25.7	22.1	18.3	12.2
N2b	52.5	45.0	37.5	31.9	26.3	18.7
N2c	267.5	234.8	197.3	169.7	141.8	102.0
0	557.7	488.7	410.4	353.4	295.1	212.0
P	97.2	91.1	76.2	65.6	54.6	36.9
Q	581.0	510.7	429.0	369.2	308.3	220.9
R	119,4	112.4	95.1	82.6	69.5	48.1
S	587.2	516.3	434.0	373.3	312.1	223.4
Tl	61.2	57.3	48.3	41.9	35.2	24.3
T2	583.8	513.4	431.7	371.4	310.5	222.0

Sub-catchment ID		Peak flood Dis	charge at each	sub-catchment	outlet (m³./sec)	10 A.
PARTITION OF THE PROPERTY OF THE PARTITION OF THE PARTITI	100yr	50yr	20yr	10yr	5yr	2yr
UI .	61.3	57.4	48.5	42.0	35.3	24.4
U2	74.5	66.3	56.0	48.3	40.5	29.0
U3	90.4	78.8	66.5	57.1	47.8	34.6
V	586.3	516.2	434.0	373.1	311.8	222.4
W1	52.1	48.7	40.8	35.1	29.3	19.9
W2	63.0	54.7	45.7	39.1	32.4	23.0
W3	80.3	70.1	58.6	50,1	\41.5	29.4
X1	50.3	47.1	39.7	34.5	29.0	20.1
X2	54.0	در 47.5	40.1	34,5	28.9	20.7
X3	42.9	40.0	33.5	₹28.8	24.0	16.3
X4	46.2	39.7	33,2	28.5	23.7	17.0
X5	99.0	86.7	>72.7	62.4	52.0	37.1
Y1	€600.6€	528.8	444.9	382.5	319.8	228.5
Y2	611.1	538.6	453.1	389.3	325.4	232.2
Z	120,7	113.5	95.8	83.0	69.7	47.9
AA (606.8	534.7	449.6	386.4	322.9	230.4
BB1	593.5	522,6	439.3	377.6	315.5	224.7
BB2	69.6	65.2	54.9	47.5	39.8	27.4
BB3	589.3	518.9	436.3	374.9	313.3	223,1
BB4	586.8	516.6	434.4	373.3	311.9	222.1
CC	64.8	60.7	51.1	44.2	37.0	25.4
DD	584.2	514,3	432.6	371.6	310.4	221.0
EE	565,3	497.5	418.4	359.3	300.1	213.6
FF	71.5	62.5	51.7	44.0	36.2	24.5
GG	89.7	78.0	64.7	54.8	45.1	31,3
HH1	60.0	56.1	46.9	40.4	33.6	22.8
HH2	89.7	78.5	65.2	55.7	46.2	32.1
HH3	119.3	104.5	87.0	74.5	61.7	43.4
II.	559.7	492.5	414.7	355.9	297.3	211.7
11	98.1	92.2	77.8	67.5	56.7	39.1
KK	109.0	94.6	79.5	68.3	57.0	41.4
LL	558.6	491.5	414.1	355.3	296.7	211.4
MM	155.2	146.5	124.0	107.8	90.9	62.9
NN	547.6	481.9	406.1	348.4	291.0	207.3

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Appendix I Anticipated Peak Design Flood Levels & Flood Discharges



Table I1: Estimated Peak Design Flood Levels for Bulimba Creek

Branch name & cross section	MIKE11	AMTD(m)	Design Eve	nt flood lev	els (Ultimat	e) in mAH	D	<u> </u>
ID	Chainage (m)	wirin(m)	2 yr	5 yr	10yr	20 yr	50 yr	100 yr
Bulimba Creek;Compton Road		Road						
Start	1 0	39900	60.86	61.07	61.18	61.28	61.40	61.45
BM222	65	39835	60.63	60.82	60.91	61.00	61.11	61.14
Bm221	175	39725	60.23	60.41	60.50	60.58	60.68	60.71
BM220	270	39630	59.72	59.85	59.94	60.02	60.12	60.19
BM219	415	39485	58.94	59.11	59.24	59.36	59.51	59.66
BM218	560	39340	58.02	58.23	58.38	58.52	58.67	58.86
BM217	736	39164	57.19	57.50	57.69	57.86	58.05	58.23
BM216	900	39000	56.45	56.96	57.21	57.4 1	67.64	57.86
End	935	38965	56.17	56.79	57.05	57.26	∖57.50	57.73
Bulimba Creek-Main Branch			Creek-Mai					7 F
BM214	0	38965	56.17	56.79	57.05	57.26	57.50	57.73
BM 214	10	38955	56.1,5	56.77	57.04	^{-/-} 57.25	57.49	57.71
Nemies Road	17	38948		ad Culverts				
BM214 copy	40	38925	55.69	55.97	56.14	56.29	56.48	56.66
ВM213	120	38845	55.33	55.54	55.68	55.79	55.94	56.08
BM212	215	38750	/54.80∖	55.00	5 5.11	55.22	55.35	55.47
BM211	355	38610	53,64	53.84	53.93	54.00	54.09	54.17
Brandon Road	370	38595	Brandon F	toad Culver	ts .			
BM211 copy	385	38580	53.40	53,65	53.76	53.84	53.94	54.03
BM 209	470	38495	52.60	52.78	52.89	52.98	53.09	53.17
BM 208	540	38425	52.20	52.36	52,47	52.61	52. 7 7	52.86
BM 207	600	38365	52.05	52.23	52.35	52.45	52.63	52.74
BM 206	740	38225	51.88	52.06	52.18	52.28	52.44	52.58
BR 1	800	38165	51.79	51.96	52.07	52.17	52.32	52.45
Brandon Road	805	38160	Brandon F	load downst	ream weir			
BR 2	825	38140	51.03	51.21	51.32	51.41	51.51	51.63
BM 205	840	38125	50.82	51.02	51.14	51.23	51.35	51.47
BR 3	890	38075	50.60	50.80	50.91	51.00	51.12	51.25
BR 4	905	38060	50.52	50,71	50.81	50.90	51.01	51.14
BR 5	942	38023	50.36	50.54	50.63	50.72	50.82	50.93
BR 5 copy	960	38005	50.26	50.43	50.53	50.61	50.71	50.81
BM 204 copy	990	3 <i>7</i> 975	50.09	50.26	50.34	50.42	50.52	50.62
BM 203	1075	37890	49.66	49,84	49.95	50.06	50.18	50.28
BM 202	1160	37805	49.40	49.59	49.73	49.85	49.98	50.09
BM 201	1300	37665	49.00	49.19	49.34	49.47	49.61	49.71
BM 200	1365	37600	48.61	48.79	48.92	49.05	49.20	49.31
BM 199	1545	37420	47.55	47.72	47.80	47.89	48.03	48.14
BM 198	1670	37295	46.95	47.23	47.40	47.55	47.71	47,86
BM340-MHG	1800	37165	46.60	46.99	47.22	47.39	47.58	47.74
BM 197	1830	37135	46.57	46.97	47,21	47.38	47.57	47.72
Beenleigh Road	1845	37120	Beenleigh	Road Weir				
ВМ 197 Сору	1860	37105	46.12	46.30	46.44	46.55	46.69	46.81
BM195-I	1900	37065	45.78	45.97	46.13	46.26	46.42	46.56
BM 194	1940	37025	45.74	45.91	46.05	46.18	46.34	46,49

Bulimba Creek Flood Study

I-1

Branch name & cross section	MIKE!1		Design Eve	nt flood lev	els (Ultima	te) in mAH	D	
ID	Chainage (m)	AMTD(m)	2 yr	5 yr	10yr	20 yr	50 yr	100 yr
	I(m)	1	1 - 7				<u> </u>	
Distract	1960	37005	45.54	45.62	45.68	45.74	45.81	45.88
BM 194 copy BM 192	2045	36920	44,88	45.01	45.14	45.29	45.49	45.63
BM 191 copy	2115	36850	44.62	44.89	45.07	45.24	45.47	45.62
St Lawrence Foot Bridge	2117	36848		NAME OF THE OWNER, WHEN PERSONS ASSESSED.	dge and We	Licenson Company of the Company of t	<u> </u>	AND DESCRIPTION OF THE PROPERTY OF THE PROPERT
	2125	36840	44.60	44.88	45.06	45,24	45.46	45.61
Bm 191 BM190	2123	36710	44.47	44.83	45.02	45.20	45.44	45.58
BM188-6 copy	2370	36595	44.36	44.76	44.96	45.14	45.38	45.52
Altandi Street Foot Bridge	2375	36590	<u> </u>		ridge and W			
	2380	36585	44.12	44.34	44.49	44.61	44.80	44.98
BM188-6	2470	36495	43.84	44.04	44.1.7 <	44.29	44.47	44.64
BM188-2 ALS BM188-1 ALS	2500	36465	43.60	43.79	43.91	44.02	44.20	44.37
Fig.	1	36295	42.88	43.05	43.18	43.30	43.45	43.61
BM187		36180	42.64	42.80	42.93	43.04	43.17	43.31
BM186	2785 2985	35980	42.04	42.16	42.27	42.37	42.49	42.59
BM185		35800	40.96	41.11	41.21	41.30	41.41	41.51
BM184	3165	35670	39.84	40.04	40.16	40.26	40.41	40.54
BM183	3295	<u> </u>	39.04	39.24	39:37	39.48	39.63	39.77
BM182	3435	35530 35340	37.61	39.24 37.83	37.99	38.11	38.27	38.41
BM181	3625	<u> </u>	36.79	37.06	37.25	37.40	37.57	37.72
BM320-MHG	3765	35200	36.64	36.92	37.12	37.40	37.46	37.61
BM180	3800 \ 3960	35165 35005	35.90	36.14	36.31	36.46	36.61	36.73
BM179 Malbon Street Foot Bridge	3965	35000		la construction of	ridge and W			
	3970 /	34995	35.77	36.04	36.23	36.41	36.55	36,68
BM179 copy	4150	34815	34.27	34.52	34.71	34.92	35.17	35.35
BM178	4260	34705	33.84	34.15	34.36	34.60	34.91	35.13
BM177-MHG310	4320	34645	33.48	33.87	34.08	34.32	34.65	34.92
ALŠ	1	34590	33.29	33.76	33.97	34,21	34.56	34.84
LC BM176modified with ALS	43.75 43.85	34580	33.29	33.75	33.97	34.20	34.55	34.84
Padstow Road	4390	34575	· ·		s and Weir	La companion de	&	
	4415	34550	33.28	33.74	33.96	34.18	34,49	34.72
BM176 DS	4460	34505	33.25	33.72	33.94	34.15	34.45	34.68
BM 175	4515	34450	33.24	33.71	33.93	34.14	34.44	34.67
BM175-174 Mimosa Merge	4555	34410	33.23	33,71	33.92	34.14	34.43	34.66
	4575	34390	33.21	33.68	33.89	34.11	34.39	34.62
Padstow Merge	4590	34375	33.14	33.60	33.81	34.02	34.30	34.52
BM 174	4700	34265	32.83	33.28	33.49	33.70	33.98	34,21
BM174A	4765	34200	32.65	33.08	33.28	33.48	33.75	33.97
BM174B BM173- MHG300	4780	34185	32.61	33.04	33.24	33.45	33.73	33.96
Blesby Road Foot Bridge	4785	34180		d Footbrid				
	***************************************	34175	32.59	33.03	33.23	33.44	33,71	33.93
BM 173 copy	4790	34060	32.21	32.65	32.86	33.09	33,38	33.63
BM172	4905 4995	33970	31.79	32.03	32,45	32.69	33.01	33.30
BM171	5120	33970	31.79	31.55	31.76	32.02	32.45	32.85
BM170	4		29.94	30.45	30.75	31.16	31.81	32.34
Garden City connection	5280 5285	33685 33680	29.94	30.43	30.73	31.15	31.80	32.33
BM169	2602	33000	1 47.71	ال د ۱۷۰۰	20.12		1.00	

Branch name & cross section	MIKE11		Design Eve	nt flood lev	els (Ultima	te) in mAH	D	
ID	Chainage	AMTD(m)	2 yr	5 yr	10yr	20 yr	50 yr	100 yr
	(m)	225.60	29.54	30.14	30.52	30.99	31.70	32.25
BM168	5405	33560	29.34	29.94	30.35	30.87	31.62	32.19
BMI 67	5520	33445	28.99	29.94	30.15	30.74	31.54	32.13
CopyBM 167-MHG290	5615	33350 33340	-	Freeway cu		30.74	21.3	
South-East Freeway	5625	la construence de la		E-months and a second	29.79	30.24	30.72	30.98
BM 165 copy	5715	33250	28.74	29.39			30.72	30.97
BM165	5730	33235	28.72	29.38 29.26	29.77 29.70	30.23 30.18	30.70	30.94
SurveyXs-5	5785	33180	28.58	d Culverts		30.10	20.07	1 20.21
Logan Road	5790	33175	ស្ទឹកការការការការការការការការការការការការការ	Park transfer and the second s	CONTRACTOR OF THE PROPERTY OF	20.56	△ 29.88	30.12
SurveyXs-4	5845	33120	28.46	29.02	29.30	29.56		30.12
SurveyXs-3	5902	33063	28.41	28.96	29.25	29.51	29.84	Salaran management and the salar
SurveyXs-2	5918	33047	28.40	28.95	29.23 <	29.50	29.83	30.08
BM158 Xs-1	5935	33030	28.38	28.93	<u> 29.22</u>	29,48	29.82	30.07
Garden City Branch start	5938	33027	28.38	28.93	29.22	29.48	29,82	30.07
HEC2937-MHG280	5985	32980	28.30	28.85	29:14	29.40	29.73	29.99
BM157	6050	32915	28(13	28.66	28.94	29.20	29.55	29.81
BM156	6160	32805	27.68	28.20	28.47	28.71	29.04	29.30
BM155	6240	32725	27.34	27.84	28.11	28.35	28.68	28.94
BM154	6340/	32625	26.94	27.44	27:71	27.95	28.28	28.55
BM153 ALS	6450	32515	26.48	₹27.03	27.31	27.56	27.90	28.18
BM151	6650	32315	26.09	26.63	26.91	27.16	27.49	27.77
BM149	6860	32105	25.69	26.20	26.47	26.71	27,04	27.30
BM148-BM147	6930	32035	25.48	25.96	26.24	26.47	26.80	27.07
CraigStreet Foot Bridge \	6935	32030		et Foot Bric	************	_		
BM148 copy	6945	32020	25.44	25.92	26.19	26.43	26.75	27.02
BM148	6985	31980	25.39	25.87	26.14	26.38	26.70	26.97
BM146	7185	31780	24.97	25.44	25.72	25.97	26.31	26.59
BM144	7420	31545	24.26	24.81	25.14	25.41	25.77	26.05
BM143	7490	31475	24.09	24.66	24.99	25.27	25.63	25.91
ALS-142	7600	31365	23.81	24.42	24.77	25.05	25.42	25,71
BM141	7735	31230	23.42	24.04	24.41	24.70	25.07	25.38
BM139	7915	31050	22.85	23.35	23.68	23.94	24.26	24.53
BM138	7985	30980	22.67	23.15	23.47	23.72	24.03	24,29
BM137	8070	30895	22.62	23.10	23.41	23.66	23.97	24.23
BM136	8200	30765	22.42	22.90	23.21	23.45	23.76	24.02
BM135	8325	30640	22.28	22.74	23.04	23.26	23.56	23.80
BM134	8475	30490	22.04	22.46	22:74	22.95	23.21	23.44
MHG-BM260	8555	30410	21.83	22.23	22.50	22.69	22.94	23.16
BM132	8570	30395	21.79	22.19	22.45	22.65	22.89	23.10
BM131	8780	30185	20.91	21.29	21.54	21.73	21.98	22.19
BM130	8840	30125	20.57	20.99	21.28	21.50	21.78	22.02
BM129	8950	30015	20.31	20.75	21.04	21.27	21.58	21.83
BM127	9115	29850	19.75	20.21	20.52	20.77	21.09	21.35
BM126	9215	29750	19.38	19.85	20.17	20,43	20.77	21.03
BM126a	93 65	29600	19.09	19.58	19.91	20.18	20.52	20.79
BM126b	9530	29435	18.85	19.38	19.73	20.00	20.36	20.64
BM122	9670	29295	18.61	. 19.16	19.51	19.79	20.16	20.45

Branch name & cross section	MIKEII	Livences	Design Eve	ent flood lev	els (Ultima	te) in mAH	D	
ID .	Chainage (m)	AMTD(m)	2 yr	5 yr	10yr	20 yr	50 yr	100 yr
BM121	9765	29200	18.48	19.01	19.35	19.63	19.98	20.26
BM119	9890	29075	18.36	18.87	19.20	19.46	19.80	20.07
BM118	9920	29045	18.29	18.79	19.11	19.37	19.71	19.98
BM117	10100	28865	17.72	18.22	18.54	18.81	19.15	19,43
BM116	10205	28760	17.45	17.96	18.29	18.56	18.91	19.19
BMI 15	10315	28650	17.27	17.76	18.09	18.35	18.71	18.98
BMI 14	10400	28565	16.93	17.46	17.81	18.10	18.47	18.76
BM112	10510	28455	16.51	17.05	17.41	17.72	18.11	18.43
BM111-MHG250	10575	28390	16.36	16.91	17.27	17.58	△ 17.98	18.31
BM110	10685	28280	16.23	16.78	17.14	17:45	17.85	- 18.17
Mt Gravatt Capalaba Road	10702	28263	Mt Gravat	t Capalaba	Road Bridg	ge S		
ВМ110 сору	10725	28240	16.09	16.59	/16.92	~ 17.19	17.54	17.81
BM108	10875	28090	15.84	16.32	16.64	16.90	17.24	17.51
BM107	10965	28000	15.62	16.09	16:40	16.65	16,99	17.27
BM106	11095	27870	15,19	15.69	16.02	16.30	√16.66	16.96
BM104	11255	27710	15.00	15.53	15.88	16.17	16.55	16.86
BM102	11515	27450	14.75	15.33	15.69	16.00	16.40	16.72
BM10I	11620	27345	14.69	15.27	15.64	15.95	16.34	16.67
BM100	11695	27270	/ 14.62	(15.19	15.55	15.86	16.25	16.56
BM99	11820	27145	14:35	14.91	15.26	15.55	15.94	16.24
BM98	11910	27055	\ 14.09 ³	14.62	14.97	15.26	15.63	15.93
BM97	12035	26930	13.80	14.33	14.68	14.97	15.34	15.65
ВМ97сору	12135	26830	13.65	14.19	14.54	14.83	15.20	15.51
Wecker Road Bridge	12139	26826	Wecker Ro	ad Bridge	and Weir		_	
ВМ97сору	12155	26810	13.60	14.12	14.47	14.76	15.13	15.44
BM94	12215	26750	13.50	14.04	14.38	14.68	15.05	15.36
BM94-93	12320	26645	13.30	13.88	14.24	14.54	14,93	15.24
BM93	12385	26580	13.12	13.72	14.09	14.40	14.80	15.11
ВМ90 сору	12505	26460	12.83	13.45	13.83	14.14	14.54	14.86
ВМ90	12690	26275	12.55	13.21	13.60	13.92	14.32	14.65
BM88	12820	26145	12.41	13.06	13.45	13.77	14.17	14.49
BM87	13140	25825	12.06	12.70	13.07	13.38	13.76	14.07
BM84	13440	25525	11.40	12.09	12.48	12.80	13.19	13.49
BM83	13530	25435	11.29	11.97	12.35	12.67	13.05	13.35
BM81	13670	25295	11.16	11.81	12.18	12.48	12.85	13.13
BM80	13765	25200	11.05	11.69	12.06	12.34	12.70	12.97
BM78	13910	25055	10.69	11.32	11.68	11.96	12.31	12.58
ВМ78 сору	13965	25000	10.36	10.96	11.31	11.61	11.98	12.27
BM77	14115	24850	10.11	10.66	11.00	11.29	11.66	11.95
ВМ76	14360	24605	10.01	10,57	10.90	11.20	11.57	11.86
BM75	14460	24505	9.96	10.52	10.86	11.15	11.52	11.81
BM74-BM72	14625	24340	9.85	10.40	10.73	11.02	11.37	11,66
BM72	14785	24180	9.48	9.98	10.28	10.55	10.89	11.16
BM71-MHG-230	14845	24120	9.35	9.85	10.16	10.43	10.78	11.06
BM70	14960	24005	9.20	9.70	10.01	10.28	10.63	10.93

	MIKEII	<u> </u>	Dacion F.	out flood los	els (Ultima	te) in mAH	n	
Branch name & Cross section	Chainage	AMTD(m)		i i		•	Name and Associated Street, St	100
	(m)		2 yr	5 yr	10yr	20 yr	50 yr	100 yr
BM69	15160	23805	8.88	9.33	9.62	9.89	10.24	10.54 10.31
BM67	15340	23625	8.51	8.99	9.32	9.61	9.99	10.31
BM66	15460	23505	8.38	8.89	9.23	9.54	9.93	10.23
ВМ66 сору	15540	23425	8.32	8.84	9.19	9.50	9.90	10.22
Pine Mountain Road	15555	23410	\$:::::::::::::::::::::::::::::::::::::		Bridge and			1
BM64 copy	15570	23395	8.24	8.76	9,10	9,41	9.82	10.14
BM64-MHG250	15600	23365	8.18	8.70	9.05	9.36	9.77	10.09
BM64	15660	23305	8:09	8.64	9.01	9,32	9.73	10.06
BM63	15790	23175	7.98	8.56	8.94	9.27	<u>\ 9.68</u>	10.01
BM62	15965	23000	7,88	8,49	8.88	9:21	>9.63	9.96
BM61	16015	22950	7.85	8.47	8.86	9.19	9.61	9.95
BM60	16190	22775	7.69	8.34	<u>/ (</u> 8.75	9.10	9.54	9.88
BM59	16390	22575	7.45	8.13	8,55	8.92	9.37	9.72
BM59 mod	16435	22530	7.38	8.06	8.48	8,85	9.30	9.65
Meadow Sreett Foot Bridge	16445	22520	Meadow S	treet Foot B	ridge and \	Veir		
Bm55-mod	16455	22510	7.37	8.04	8.46	8.83	9.28	9.63
BM57-mod	16680	22285	7.06	7.72	8,13	8.50	8.93	9.27
BM56	16785	22180	6.91	7.56	7.97	8.33	8.77	9.11
Bm55-mod	17080	21885	6,45	7.08	7.48	7.84	8.26	8.59
BM55-54	17240	21725	6:19	6.83	7.23	7.58	7.99	8.32
BM54 C	17300	21665	6.14	6.77	7.16	7.51	7.92	8.25
CD10	17325	21640	6.10	6.72	7.12	7.47	7.88	8.20
Winstaly Street Bridge	17338	21627	Winstanly	Street Foot	Bridge and	Weir		
CD09	17355 /	21610	6.08	6.66	7.03	7.37	7.79	8.13
BM52	17540	21425	5.82	6.35	6.71	7.03	7.44	7.76
CD07	17765	21200	5.46	5.98	6.34	6,66	7.09	7.39
BM50-49-ALS	17850	21115	5.28	5.83	6.19	6.49	6.88	7.22
CD06	17920	21045	5.04	5.56	5.93	6.26	6.65	6.95
Old Cleveland Road	17935	21030	Old Clevel	and Road b	ridge and V	Veir	Service and an experience of the second	
CD05	17960	21005	5.04	5.55	5.94	6.26	6.63	6.92
CD04	18025	20940	4.86	5.46	5:83	6.17	6.58	6.90
BM47-mod	18065	20900	4.78	5,41	5.79	6.13	6.54	6.87
BM46-mod	18110	20855	4.75	5.37	5.76	6,10	6.49	6.84
CD02	18320	20645	4.64	5.25	5,62	5.96	6.36	6.70
BM44 mod	18495	20470	4.53	5.13	5.51	5.84	6.25	6.57
BM43-mod	18690	20275	4.44	5.03	5.39	5.72	6.12	6.44
BM42-mod	18995	19970	4.32	4.89	5.25	5.56	5.95	6.26
	19165	19800	4.24	4.81	5.16	5.48	5.86	6.17
BM41-mod BM41 copy	19105	19770	4.22	4.79	5.14	5,45	5.83	6.14
Scrub Road Foot Bridge	19193	19760	-	AND DESCRIPTION OF THE PARTY OF	ge and Wei		32 4 2 F.	
**************************************		***************************************	4.21	4.78	5.13	5.45	5.82	6.14
BM41	19215	19750	1	4.70	5,04	5.35	5.72	6.03
BM5GHD	19375	19590	4.14			<u> </u>	5.43	5.72
BM6GHD	19640	19325	3.97	4.48	4.80	5.09	4	
Bm7GHD	20050	18915	3.78	4.27	4,56	4,82	5,13 5.03	5.40 5.30
BM8GHD copy	20260	18705	3.72	4.19	4.47	4.72	- 2.03	0.30

Branch name & Cross section	MIKE11		Design Eve	ent flood lev	els (Ultima	te) in mAH	D .	
ID	Chainage (m)	AMTD(m)	2 yr	5 yr	10yr	20 yr	50 yr	100 yr
Meadowlands Road Bridge	20270	18695	A	nds Road bi		Salaran managaritan ni		
	20290	18675	3.71	4.17	4.44	4.67	4.93	5.15
Bm8GHD BM9GHD	20510	18455	3.68	4.14	4.40	4.62	4.87	5.08
BM37	20850	18115	3.58	4.04	4.29	4.50	4.75	4.96
	21090	17875	3.50	3.95	4.21	4.42	4.68	4.88
BM17GHD	21555	17410	3,35	3.80	4.06	4.29	4.56	4.78
BM18GHD BM19GHDcopy	21335	17090	3.22	3.67	3,93	4.17	4.46	4.69
Preston Road Foot Bridge	21885	17080		ad Foot bri		<u> </u>	E	<u></u>
BM19 GHD	21895	17070	3.21	3.66	3.92	4.16	4.45	4.68
MHG170	22305	16660	3.09	3.52	3.77	4:01	4.31	4.54
	22775	16190	2.95	3.37	3.62 <	3.86	4.16	4.40
BM23GHD	23165	15800	2.85	3.26	3.52	3.76	4.07	4.32
MHG160	23105	15680	2.84	3.25	3:51	3.75	4.06	4.31
BM10GHD	23285	15365	2.81	3.22	3.48	3.72	4.03	4.27
BM11GHD	23900	15065	2.79	3.20	3,45	3.69	4.00	4.25
ALS23900	24000	14965	2.78	3.19	3.45	3.69	4,00	4.25
Minnippi connection	24695	14270	2.69	3.11	3.37	3.61	3.92	4.17
BM13a	24890	14075	2.64	3.05	3.30	3.54	3.85	4.10
BM13GHD MHG19-old	25515	13450	2.49	2.88	3,12	3.35	3.65	3.88
MHG20-old	25565	13400	2:49	2.87	3.11	3.34	3.64	3.87
BM26 MHG150	25865	13100	2.43	2.81	3.05	3.28	3.58	3.81
Wymnum Road Weir	25885	13080	Samuelan sucantificament and a	Road bridge	la announce de la company			
	25905	13060	2.37	2.71	2.92	3.11	3.37	3.57
BM 26 copy MHG-140	26015	12950	2.33	2.66	2.87	3.06	3.32	3.52
	26145	12930	2.29	2.60	2.80	2.98	3.23	3.42
BM24	26365	12600	2.23	2.52	2.71	2.89	3.13	3.31
BM23 Murrarie connection	26550	12415	2.19	2.47	2.66	2.84	3.08	3.26
	26620	12345	2.18	2.47	2.65	2.83	3.07	3.25
BM22 BM22 copy	26710	12255	2.17	2.45	2.63	2.81	3.05	3.23
Murarrie Road Weir	26730	12235	Same and the same	Road bridge	haracean mineral			£
	26750	12215	2.12	2.38	2,54	2.71	2.94	3.13
BM22 copy MHG-120	26780	12185	2.11	2.37	2.54	2.70	2.93	3.12
BM22 copy	26940	12025	2.09	2.35	2.51	2.67	2.89	3.08
Gateway Motorway	26950	12015	Gateway N				<u> </u>	Recipion de la company de la c
	26990	11975	2.07	2:31	2.48	2.64	2.87	3.07
BM42AGHD copy BM42A-mod	27100	11975	2.06	2.31	2.47	2.63	2.85	3.05
	27300	11665	2.04	2.27	2.43	2.58	2.79	2.98
BM42AGHD copy	27305	11660	2.04	2.27	2.43	2.58	2.79	2.98
Murrarie connection	27355	11610	2.03	2.26	2.43	2.56	2.77	2.96
BM42AGHD	1	11010	1.93	2.14	2.29	2.44	2.65	2.85
BM43AGHD	27755	11053	1,90	2.11	2.26	2.41	2.62	2.82
LC	27912		1	2.11	2.25	2.40	2.62	2.81
BM44AGHD	28025	10940 10150	1.89	2.08	2.23	2.39	2.60	2.80
BM44BGHD	28815		1.85	2.08	2.23	2.39	2.60	2.80
LC	28855	10110	1.85	2.08	2.24	2.40	2.61	2.80
LC DYWARCHD	28930	10035 9890	1.85 1.84	2.08	2.24	2.40	2.62	2.82
BM43BGHD	29075	2020	I I.UT	4.00				B

Branch name & Cross section	MIKE11	LAMBER	Design Eve	nt flood lev	els (Ultima	te) in mAH	D	
ID	Chainage (m)	AMTD(m)	2 yr	5 yr	10yr	20 yr	50 yr	100 yr
LC	29150	9815	1.84	2.08	2.24	2.40	2.62	2.82
LC	29325	9640	1.84	2.08	2.24	2.40	2.62	2.83
LC	29420	9545	1.84	2.08	2.24	2.40	2.62	2.83
LC	29652	9313	1.82	2.07	2.23	2.40	2.62	2.82
BM43CGHD	29730	9235	1.82	2.07	2.23	2.39	2.61	2.82
BM43CGHD	30635	8330	1.75	2.02	2.18	2.35	2,57	2.78
ĹC	30800	8165	1.73	1.99	2.15	2.32	2.55	2.75
BM45GHD	31600	7365	1.65	1.92	2.09	2.27	2.50	2.71
ĹĊ	31740	7225	1.64	1.90	2.08	2.26	2.49	2.71
BM46CGHD	32110	6855	1.57	1.83	2.01	, 2:20	>2.45	2.67
BM46BGHD	32355	6610	1.54	1.82	2.00 <	2.19	2.44	2.66
LC	32650	6315	1.55	1.82	2.01	2.19	2.44	2.66
BM46AGHD	33330	5635	1.48	1.77	1:97	2.16	2.42	2.64
BM52 GHD copy	34300	4665	1.40	1.72	1.92	2.12	2:38	2.61
BM52 GHD copy	34490	4475	1.40	1.70	1.91	2.11	2.37	2.60
Cleveland Rail Bridge	34500	4465		Road Bridg	e and Weir	<u> </u>	<u> </u>	B
BM52 GHD	34510	4455	1,34	1.62	1.80	1.99	2.22	2,43
BM52 GHD copy	34700	4265	1.28	1.57	1.76	1.95	2.20	2.41
BM52 GHD шру	35260	3705	1.26	1.49	1.66	1.84	2.08	2.29
BM52 GHD copy	35670	3295	1.22	1,42	1.57	1.73	1.94	2.13
Lytton Road	35680 \	3285	Lytton Roz	d Bridge a	nd Weir	2	<u> </u>	
BM6 copy	35690	3275	1.19	1.36	1.50	1.64	1.83	2.00
BM48	35785	3180	1.17	1.33	1.46	1.59	1.77	1.94
Bm4	36370	2595	1.14	1.27	1.37	1.48	1.64	1.79
BM3	37040	1925	1.09	1.19	1.27	1.35	1.47	1.59
BM2 copy	37465	1500	1.08	1.14	1.20	1.26	1.36	1.46
<u>Б</u> М2	38070	895	1.04	1.07	1.11	1.15	1.21	1.27
BM1	38610	355	1.02	1.03	1.05	1.06	1.09	1.12
Brisbane River Boundry	38965	0	1.00	1.00	1.00	1.00	1.00	1.00
Bulimba-East Branch				3				
BE289	0	6280	55.58	55.71	55.77	55.83	55.90	55.93
BE289	60	6220	55.50	55.62	55.69	55.75	55.82	55.85
BE288	170	6110	54,48	54.64	54.70	54.76	54.83	54.84
BE287	250	6030	53.58	53.64	53.70	53.76	53.84	53.93
BE286	388	5892	52.91	53.09	53.19	53.27	53.38	53.39
BE285	525	5755	52.01	52.11	52.19	52.27	52.35	52,47
BE284	612	5668	51.07	51.16	51.23	51.29	51.35	51.44
HEC2146	660	5620	50.43	50.51	50.56	50.61	50.67	50.74
BE283	708	5572	50.13	50.22	50.27	50.32	50.38	50.44
HEC2030	755	5525	49,95	50.10	50.17	50.22	50.29	50.34
p		-	40.00	50.00	50.15	50.20	50.27	50.32
BE283 copy	799	5481	49.93	50.08	30.13	30.20	30.21	

Branch name & Cross section	MIKE11		Design Eve	ent flood lev	els (Ultima	te) in mAH	D	
ID	Chainage	AMTD(m)	2 yr	5 yr	10yr	20 yr	50 yr	100 yr
	(m) 820	5460		Road culver	Accessoration and the second		1 30,1	2007
Beenleigh Road Culverts BE281DS	835	5445	49.49	49.80	49.95	50.07	50.22	50.27
BE281DS BE280	840	5440	49.52	49.80	49.95	50.07	50.22	50.27
Beenleigh Rail Culverts	040	3440	Anna Carlo C	Rail Culver	2	Leanne		
	0.11	5436	49.52	49.80	49.95	50.07	50.22	50.27
BE279HEC	844	······································	49.14	49.44	49.65	49.88	50.12	50.20
BE278	852 875	5428 5405	49.14	49.44	49.64	49.87	50.11	50.19
BE277-HEC	876	5404	Annual Committee of the	Road Pipe (Language and the second second second second	Esperantia de la companya della companya della companya de la companya della comp		
Beenleigh Road Culvert-2	\$			48.29	48.39	48.48	48.57	48.68
BE Rail bypass	930	5350	48.09	48.27	48.37	48.45	48.55	48.66
BE277-HEC DS	946	5334	48.07	A STATE OF	48.38	48.47 48.47	48.56	48.67
DE2/1-A	956	5324	48.08	48.28 48.26	48.36	48:45	\\\ 48.54	48.65
BE277-A copy	978	5302	48.07		<u> </u>	48.45	48.55	48.66
XS-7450	981	5299 5299	48.06	48.26	48.37 48.34	48.43	48.53 48.53	48.64
XS-7400	991	5289	48.04	48.24		48.43 48.39	48.33	48.60
Xs-7480	1011	52 69	48,00	48.20	48.31	48.39 48.36	48.49	48.57
XS-7500	1031	5249 5330	47.96	48.16	48.27		48.42	48.53
XS-7520	1051	52.29	47.92	48.13		48.32	48.42	48.53 48.50
XS-7540	1071	5209	47.89	48.10	48:20	48.29	8	48.47
XS-7560	1091	5189	47.86	48,07	48.17	48.26	48.36	48.44
Xs-7580	1111	5169	47.84	48.04	48.15	48.23	48.33	
Xs-7600	1131	5149	47.81	48.01	48.11	48.20	48.29	48.40
Xs-7620	1151	5129	47:76	47.97	48.07	48.15	48.25	48.36
XS-7640	1171	5109	47.70	47.90	48.00	48.09	48.19	48.29
XS-7660	1191	5089	47.57	47.76	47.86	47.94	48.03	48.14
XS-7680 \	1211/	5069	47.33	47.54	47.64	47.73	47.83	47.94
Xs-7700	1231	5049	47.22	47.43	47.53	47.61	47.71	47.81
XS-7720	1251	5029	47.09	47.28	47.37	47.45	47.54	47.64
XS-7740	1271	5009	46.89	47.06	47.14	47.21	47.30	47.39
XS-7760	1291	4989	46,66	46.82	46.91	46.98	47.07	47.16
Xs-7780	1311	4969	46.46	46.65	46,74	46.81	46.91	47.00
XS-7800 (154) 11 (175)	1331	4949	46.38	46,55	46.64	46.72	46.82	46.90
Xs-7810	1341	4939	46.36	46,54	46.63	46,71	46.81	46.90
BE273	1355	4925	46.34	46.51	46.60	46.68	46.78	46.87
BE Rail Bypass	1380	4900	46.29	46.44	46.53	46.61	46.71	46.80
BE272	1498	4782	45.85	45.95	46.01	46.08	46.17	46.23
BE272	1565	4715	45.38	45.49	45.56	45.63	45.71	45.77
BE271_ALS	1600	4680	45.23	45.35	45.42	45.49	45.56	45.64
BE270	1730	4550	44.40	44.61	44.72	44.81	44.93	45.03
BE269	1915	4365	43.64	43.89	44.03	44.15	44.31	44.43
BE268	2020	4260	43.01	43.30	43.46	43.59	43.77	43.91
BE267	2145	4135	42.38	42.61	42,75	42.87	43.02	43.14
BE266	2245	4035	41.77	41,92	42.02	42.11	42.23	42.32
BE265	2410	3870	40,56	40.70	40.78	40.87	40.97	41.06
BE264	2500	3780	40.00	40.14	40.20	40.27	40.35	40.42
BE263	2605	3675	38.78	38,99	39.10	39.20	39.42	39.53
BE262	2765	3515	37.25	37.63	37.89	38.15	38.59	38.73
Underwood Road Culverts	2767	3513	Underwoo	d Road Cub	verts and W	'eir		
BE261	2785	3495	37.22	37.56	37.78	37.98	38,43	38.59

Bulimba Creek Flood Study

Branch name & Cross section	MIKEI1		Design Eve	ent flood lev	els (Ultima	te) in mAH	D	
ID	Chainage (m)	AMTD(m)	2 yr	5 yr	10yr	20 yr	50 yr	100 yr
DEGGO	2990	3290	36.56	36.86	37.04	37.20	37.38	37.56
BE259	3200	3080	35.30	35.64	35.82	35.97	36.12	36.29
BE258 BE257	3320	2960	34.59	34.93	35.11	35.24	35.36	35.50
Gateway Motorway Culverts	3330	2950	<u> </u>	Iotorway C	L.	<u> </u>	<u></u>	
BE257 copy	3425	2855	34.58	34.91	35.09	35.22	35.35:	35.49
BE256	3490	2790	34.28	34.58	34.76	34.89	35.01	35.13
BE255	3670	2610	32.75	32.97	33.12	33.24	33.41	33.60
BE255 copy	3695	2585	32.41	32.63	32.79	32.94	33.15	33.38
BE255 copy -mod	3725	2555	31.76	32.06	32.32	32,57	∖ 32,88	33.19
Trib B start	3726	2554	31.75	32,08	32.35	32.59	32.89	33.20
BE254 copy	3735	2545	31.69	32.08	32.37	32.66	32.96	33.23
BE254 COPY	3745	2535	31.68	32.08	/32.36	32,67	32.98	33.26
Logan Road Culvert	3748	2532	Salara de la companya del companya de la companya del companya de la companya de	d Culvert a	nd Weir	Barrier Commence	Mariante	
BE253	3785	2495	31.15	31.43	31.62	31.81	32.04	32.22
Interpolated	3810	2470	31(14	31.43	31.62	31.80	√32.02	32.21
Trib B end	3888	2392	31.11	31.39	31.58	31.77	31,99	32.18
BE251	3925	2355	31.06	31.34	31.53	31.73	31.96	32.14
Be250	4020	2260	30.76	31.06	31:30	31.53	31.80	32.00
BE249	4110	2170	Z 30.26	₹30.70	31.05	31.35	31.65	31.85
BE248	4230	2050	30.08	30.59	30.97	31.30	31.60	31.81
Trib A DS	4284	1996	√ 30.07	30.58	30.97	31.29	31.60	31.80
BE247	4300	1980	30.04	30.56	30.96	31.28	31.59	31.80
Pacific Motorway Culverts	4305	1975	Pacific Mo	torway Cul	verts		÷	
BE247 copy	4360	1920	29.74	30.04	30.21	30.39	30.64	30.86
BE246	4419	1861	29.45	29.79	29.98	30.17	30.42	30.66
BE246A-ALS	4507	1773	28.99	29.34	29.53	29.73	30.01	30,26
Old4612	4602	1678	28.51	28.86	29.04	29.28	29.63	29,92
Eight Mile Plains Bridge	4608	1672	Eight Mile	Plains Bus	way Access	Road Brid	ge and Weir	_
Copy Old 4612	4638	1642	28.15	28.57	28,81	29.06	29.39	29.69
BE244	4656	1624	28,09	28.51	28.75	28.99	29.33	29.63
Miles Platting Road Bridge	4660	1620	Miles Plati	ing Road B	ridge and \	Veir	Quantum management	
Old 4665	4695	1585	28.04	28.43	28.65	28.87	29.17	29.44
Old 4685	4730	1550	27.90	28.27	28.47	28.68	28.96	29.22
Old 4705	4750	1530	27.89	28.27	28.49	28.70	28.99	29.25
BE241	4870	1410	27.65	28.02	28.23	28.45	28.74	29.00
BE240	4980	1300	27.33	27.72	27.95	28.18	28.48	28.76
Gateway Off-ramp	5010	1270	Gateway C	off-ramp Br	idge and W	[/] elr		
BE239	5050	1230	27.09	27.42	27.60	27.79	28.03	28.24
BE238.	51.75	1105	26.76	27.08	27.26	27.45	27.69	27.90
BE236	5330	950	25.97	26.35	26.55	26.74	27.02	27.24
BE235	5470	810	24.98	25.47	25.73	25.95	26.27	26.53
BE232	5712	568	24.08	24.50	24.74	24.96	25.26	25.52
BE231	5810	470	23.79	24.20	24.44	24.66	24.95	25.21
BE230	5895	385	23.45	23.85	24.10	24.32	24.63	24.88
BE229	5975	305	23.14	23.58	23.85	24.09	24.40	24.66

Branch name & Cross section	MIKEII		Design Evo	ent flood lev	els (Ultima	te) in mAH	D	
ID	Chainage	AMTD(m)	2 yr	5 yr	10yr	20 yr	50 yr	100 yr
BE228	(m) 6055	225	22.91	23.39	23.68	23.93	24.24	24.51
BE227	6135	145	22.75	23.23	23.54	23.79	24.10	24.36
BE227	6280	0	22.62	23.10	23.41	23.66	23.97	24.23
Tributary A	UL OU		Tributary		L		Approximate the contract of th	COMPANIES CONTRACTOR OF THE PARTY OF THE PAR
The same of the sa	0		51.96	52.32	52.47	52.60	52.76	52.82
ALS1-copy	100		51.71	52.06	52.20	52.31	52,45	52.65
ALS1-copy	320		50.81	51.07	51.18	51.33	51.48	51.67
ALS1	600		46.69	46.88	47.03	47.16	47.35	47.58
AL\$2	950		44.85	45.02	45.08	45.13	△ 45.19	45.27
BE-1060	1400		41.05	41.19	41.28	41:37	41.46	41.52
BE-1040	1770		37.23	37.45	37.58 <	37.71	37.87	38.04
BE-1030 BE-1020	2070		34.79	35.16	_35.45\	×35.75	36,09	36.54
School Road	2072		P	Santa and American Street, Spirit and Spirit	ay Culverts			
	2125		34.71	35.00∖	35.48	35.33	35.52	35.68
interpolated	2163		34.66	34.95	35.13	35.28	35.47	35.62
Interpolated Dr. 1010	2235		34.20	34,52	34.72	34.89	35.09	35.25
BE-1010 BE-1005	2535	A STATE OF THE STA	32.19	32.60	32.90	33.19	33.57	33.77
Freeway Off-ramp	2545		A	· · · · · · · · · · · · · · · · · · ·	liverts and			L
BE-1005	2555		32.12	32.51	32.74	32.96	33.25	33.45
	2735		31.17	31.52	31.76	32.04	32.38	32.66
BE1005 copy BE1000	2765		30.47	30.98	31.38	31.78	32.19	32.50
Gateway Motor way	2805		<u> </u>	AND DESCRIPTION OF THE PARTY OF	ulverts and			
BE1000 modified	2935		30.42	30.92	31.30	31.65	31.98	32.19
BE1000 modified	3015	ľ.	30.09	30.60	30.99	31.32	31.64	31.84
BE1000 modified	3021		30.07	30.58	30.97	31.29	31.60	31.80
Tributary A1			Tributary	annen market sammen sen sen sen sen sen sen sen sen sen s	Lanineranomenen	MANAGEMENT OF THE PROPERTY OF		
A1-1050	0		49.72	50.01	50.16	50.28	50.42	50.47
A1-1050	280		48.91	49.11	49.21	49.30	49.42	49.43
ALS	500	<u> </u>	44,50	44.65	44.74	44.83	44.94	44.96
ALS	720	<u> </u>	41.06	41.20	41.30	41.38	41.48	41,54
ALS	750	g in r	41.05	41.19	41.28	41.37	41.46	41.52
Tributary A2			Tributary	A2				
TRIB A2	0		44,93	45.07	45.13	45.18	45.25	45.27
SMP	7 80		44.55	44.66	44.72	44.76	44.82	44.83
SMP	475	1	40.27	40.36	40.44	40.51	40.59	40.71
SMP	690		38.69	38.80	38.87	38.92	38.99	39.08
SMP	1035		34.66	34.96	35.13	35.29	35.47	35.63
SMP	1042		34.66	34.95	35.13	35.28	35.47	35.62
Tributary B			Tributary	В				
BE2030	1000		36.12	36.37	36.51	36.80	36.88	36.91
BE2030	1055		35.09	35.44	35.63	35.71	35.99	36.04
Dance Court 1	1062	<u> </u>		rt Culvert :	and Weir	amananan katan kat		
BE2030 copy	1075		34.56	34.85	34.98	35.07	35.21	35,24
BE2020	1215		34.33	34.51	34.61	34.69	34.78	34.83
BE2020 copy	1340		33.36	33.51	33.64	33.74	33.84	33.96
Interpolated	1360		33.27	33.41	33.52	33.62	33.72	33.84
Truck bonness	I			la construence de la	Lancon de la companya		Secretary and included the	·

Branch name & Cross section	MIKE11		Design Eve	ent flood lev	els (Ultima	te) in mAH	D	
	Chainage (m)	AMTD(m)	2 yr	5 yr	10yr	20 yr	50 yr	100 yr
Logan Road Culverts	1361			ad Culvert	SAME AND ADDRESS OF THE PARTY O	Service manufacture concerns when		
BE2010	1394	en yan en	32.92	33.02	33.09	33.15	33.23	33.35
BE2000	1432		31.16	31.43	31.61	31.79	32.01	32.19
BE2000	1492		31.11	31.39	31.58	31,77	31.99	32.18
Tributary C			Tributary	<u> Annon anno anno anno anno anno anno ann</u>	nga 242 bili 1993	r gaz Arindar		S
BE-3050	0		49.14	49.23	49.27	49.31	49.36	49.37
BE-3050	10		49.09	49.15	49.19	49.23	49.28	49.34
	390		46.73	46.86	46.94	47.00	47.08	47.13
BE-3040	545		45.48	45.57	45.64	45.70	^ 45.77	45.80
BE-3030	665		44.29	44.41	44.49	44.57	44.66	44.74
BE-3020			42.62	42.75	42.84	42.92	43.02	43.10
BE-3010	810		39.21	39,37	39.47	×39.56	39,65	39.73
BE3000	1000 1005		38.50	38.50	38:50	38.55	38.95	39.11
ВЕ-3000 сору	Leanung and a second		- Commence of the Commence of	Pipe Culve	population and the second		1 . 20.55	27.11
Gateway Culvert	1008	***************************************		· · · · · · · · · · · · · · · · · · ·	***************************************	**************************************	38.90	39.04
BE3000 copy	1100		37,58	37.97	38.22	38.48	38.91	39.04
ALS	11.10		37.58	37.98	38.22 38.22	38.49 38.48	38.91	39.03
ALS	1120		37.58	37.97	30.22	30.40	30.71	3.2.04
Tributary B1			Tributary			45.24	1 32 30	33.04
ALS	1000	-\/_	/ 33.27	33.41	33.52	33.62	33.72	33.84
ALS	1002		33.17	33.30	33.42	33.51	33.61	33.74
ALS	1020		31.99	32.19	32.37	32.62	32.92	33.23
ALS	1055		31.75	32.08	32.35	32.60	32.90	33.21
ALS	1140		31.75	32.08	32.35	32.59	32.89	33.22
ALS	1145		31.75	32.08	32.35	32.59	32.89	33,20
Padstow Branch		e de la composición dela composición de la composición de la composición de la composición dela composición de la composición dela composición dela composición de la composición dela composición de la composición dela c	Padstow J	3ranch				year a final and
BM177	0	Tr.	34.27	34.52	34.71	34.92	35.17	35,35
BM177	32		34.21	34.47	34.66	34.88	35,14	35.32
BM177-176ALS	105		33.89	34.25	34.52	34.79	35.08	35.26
BM176-US-ALS	175		33.52	34.10	34.43	34.74	35.04	35.23
Padstow Road			Padstow I	Road Culve	erts and W	eir	ar i yari k	
BM176-DS-ALS	205	- 1 - 1	33.42	33.82	34.01	34.20	34.46	34.68
BM175	258	i i i i i i i i i i i i i i i i i i i	33.37	33.79	33.97	34.17	34.44	34.67
BM175-174ALS	325	y en ĝ Ligi dengan li	33.27	33.72	33.92	34,13	34.41	34.64
BM174	352		33.23	33.70	33.91	34.12	34.40	34.63
BM175	375	an in the	33,21	33.68	33.89	34.11	34.39	34.62
Garden City	4844		Garden C	ity Brancl	1		-	
BM169	5280		29.94	30.45	30.75	31.16	31.81	32.34
BM169	5285		29.94	30.44	30.74	31.16	31.81	32.34
BM168	5405		29.78	30.26	30.54	30.99	31,70	32.25
BM167	5510		29.43	29.99	30.35	30.86	31.61	32,19
BM165 copy	5615		29.09	29.81	30.24	30.80	-31.57	32.16
BM165 copy	5715		28.80	29.37	29.78	30.24	30.72	30.98
Bm165	5730	THE PARTY OF THE 	28.76	29.35	29.77	30.23	30.72	30.97
XS5-Logan Road survey	5785		28.51	29.18	29.66	30.16	30.67	30.92
AND TANKER INDUSERVEY	1 2/03	***************************************	20,31	L			L	

Branch name & Cross section	MIKE11	Ī	Design Eve	nt flood lev	els (Ultimat	e) in mAH]	D	
ID	Chainage	AMTD(m)	2 yr	5 yr	10yr	20 yr	50 yr	100 yr
	(nı) 5790			ad culvert	Language and the second	20 J.		
Logan Road	5850		28.43	28.98	29.27	29.54	29.90	30.20
XS4-logan-survey XS4 copy	5935		28.38	28.93	29.22	29.48	29.82	30.08
XS4 copy	5938		28.38	28.93	29.22	29.48	29.82	30.07
Mimosa Creek	. 7		Mimosa C					
Start of model	l 0	58880	54.81	55.08	55.22	55.35	55.51	55.56
Mi 40 Hecras	5	58875	54.79	55.06	55.20	55.32	55.47	55.53
Mi 40a	96	58784	54.32	54.55	54.67	54.77	54.91	54.95
	200	58680	53.60	53.75	53.88	54.00	54.14	54.25
Mi39	330	58550	52.68	52.89	53.03	53.15	53.29	53.44
MI38 Mi37	484	58396	51.23	51.63	51.57	51.69	51.83	52.01
Mi36	506	58374	50.98	51.33	51:30	51\42	51.57	51.74
	558	58322	50.55	50.93	50,90	51.02	51.17	51.32
Mi35	660	58220	49.88	50.30	50,27	50.38	50.52	50.64
Mi34	696	58184	49,64	50.10	50.07	50.18	50.31	50.45
Mi33 Mi32	811	58069	48.95	49.56	49,49	49.65	49.83	49.97
	952	57928	48.33	\48.85\	48.77	48.94	49.14	49.24
Mi31	1037	57843	47.88	48.33	48.27	48.42	48.61	48.71
Mi31-copy	1186	57694	46.79	47:31	47.26	47.41	47.60	47.76
Mi29 Mi28	1302	57578	46.02	46.71	46.63	46.83	47.07	47.28
	1302	57558	45.88	46.62	46.54	46.75	46.99	47.21
Mi27	1366	57514	45.78	46.54	46.45	46.67	46.91	47.13
Mi26	1439	57441	45.58	46.32	46.24	46.45	46.69	46.89
Mi25	1549	57331	44.86	45.64	45.53	45.78	46.01	46.19
Mi24	1588	57292	44.68	45.48	45.37	45.62	45.86	46.04
Mi23 Mi22	1719	57161	44.11	44.82	44.75	44.97	45.21	45.36
Wi21-2	1738	57142	43.95	44,64	44.57	44.82	45.11	45.27
	1739	57141	_E	et Bridge a	B			
Nagel Street Bridge	1752	57128	43.85	44.49	44.44	44.61	44.92	45.11
Mi21-1	1762	57118	43.74	44,40	44.35	44.53	44.82	45.02 -
Mi20	1882	56998	43.10	43.77	43.71	43.92	44.23	44.48
Mi19	1892	56988	43.10	43.75	43.68	43.89	44.20	44.45
Mi19-4	1895	56985		torway Cul	<u> </u>			
Pacific Motorway Culverts		56916	42.67	43.21	43.24	43.42	43.65	43.85
Mi19-1	1964		42.42	42.85	42.93	43.10	43.31	43.51
Mi18	2023	56857	41.96	42.40	42.48	42.67	42.89	43.08
Mi17	2086	56794	41.59	42.12	42.21	42.43	42.68	42.89
Mi16	2133	56747	-1	£	41.54	41.78	42.06	42.26
Mi15	2224	56656	40.95	41.46 41.34	41,43	41.70	41.99	42.19
Mi13-3	2248	56632 E663E		ad Bridge	Action to the second se	41.70	14.22	
Kessels Road Bridge	2255	56625	and the same of th	Žinii varani kalenti kalenti kalenti	41.35	41.54	41.75	41.93
Mi13-2	22.84	56596	40.77	41.27	<u> </u>	41.34	41.60	41.77
Mi13	2325	56555	40.65	41.13	41.21		40.55	41.77
Mi12	2516	56364	39.62	40.05	40.13 39.42	40,32 39.62	40.55 39.87	40.74
Mil1	2635	56245	38.87	39.33	Marson variation that the same of the same	37.04	39,01	TO. 0.7
Parkway Street Bridge	2648	56232		treet bridg		39.45	39.67	39.84
Mi10-2	2664	56216	38.79	39.19	39.28	37.43	27,01	37.07

Branch name & Cross section	MIKEII		Design Eve	nt flood lev	els (Ultima	te) in mAH	D	
ID	Chainage (m)	AMTD(m)	2 yr	5 yr	10yr	20 yr	50 yr	100 yr
Mi9	2718	56162	38.59	38.95	39.03	39,20	39.40	39.57
Mi8	2828	56052	37.88	38.29	38.39	38.59	38.81	38.97
Mi7	2955	55925	37.40	37.90	38.03	38.23	38.47	38,62
Mi6	3069	55811	37.06	37.56	37.68	37.86	38.08	38.24
Mi5	3221	55659	36.49	36.97	37.09	37.26	37.44	37.61
Mi4	3388	55492	35.79	36.29	36.44	36.64	36.88	37.07
Mi3	3496	55384	35.41	35.86	36.01	36.22	36.46	36.65
Mi2	3585	55295	35.08	35.48	35.61	35.80	36.02	36.19
	3801	55079	33.96	34.38	34.52	34.70	34.94	35.12
Mil	3880	55000	33,23	33.71	33.92	34.14	34.43	34.66
Bulimba Main merge	2000	33000		ypass Brai				
Minnippi Bypass Branch					3:45	3.69	4.00	4.25
Start	0		2.78	3.19		3.64	3.96	4.22
Minnippi_new1	80		2.78	3,16	3,40		*	4.22
Minnippi_new2	125		2.78	3,15	3,40	3.64	3,96	
Minnippi_new3	230	1	2.77	3.12	3.36//	3.61	3.94	4.19
Minnippi_new4	400		2.77	3.05	3.31	3.58	3.92	4.18
Minnippi_new5	542	and the second	2.76	3.00	3.27	3.55	3.90	4.17
ALS	650		2.76	2.97	3.26	3.54	3.89	4,16
Stanton Road	710		Stanton Ro	ad overfloy	V.			
New A	720	<u> </u>	2,56	2.95	3.22	3.47	3.77	3.98
New B	730 \		2,24	2.93	3.20	3.45	3.75	3.96
Minnippi_new6-US	745		2.24	2.93	3.20	3.45	3.76	3.97
Gateway Motorway	748		Gateway N	Iotorway C	ulverts			
Minnippi new7-DS	₹ 810		2.24	2,93	3.19	3.41	3.66	3.85
New E	825		2,24	2.92	3.18	3.40	3,65	3,83
New G	860		2.23	2.90	3.15	3.38	3.62	3,81
New 7a	870		2.01	2.88	3.14	3.36	3.62	3.80
Minnippi new8	945		1.92	2.61	2.88	3.13	3,42	3.62
BM31GHD-mod	1015		1.87	2.43	2.71	2.99	3.32	3,53
BM31GHD-mod	1115	art to the	1.85	2.31	2.60	2.89	3.25	3.47
Wynnum Road			<u> </u>	Road Bridge	 	S	A	
	1150		1.85	2.22	2.41	2.58	2,78	2.96
BM31-GHD copy	·		1.84	2.16	2.34	2.51	2,72	2.91
BM36GHD copy	1310		1.84	2.10	2.28	2.45	2.67	2.86
Minnippi_newl1	1560	ļ	1.84	2.09	2.25	2.41	2.64	2.84
BM42BGHD	1850	<u>.</u>	1.84	2.08	2.24	2.40	2.62	2.83
BM42BGHD	2004			den management and the contract of the contrac	B	ム、コリ	g 4.034	,
Murrarie Bypass				Bypass Bra	**************************************	204	3.08	3.26
ALS	0	<u> </u>	2.19	2.47	2.66	2.84		§
MUI ALS	20	1	2.19	2.47	2.65	2.83	3.08	3.26
ALS	35	<u> </u>	2.18	2,46	2.65	2.82	3.07	3.24
New_MU2_ALS	160		2.17	2,46	2.64	2.82	3.06	3.24
New_MU3_ALS	275		2.16	2.45	2.64	2,82	3.06	3.24
Murrarie Road	280		Murarrie	Road Bridg	e		1	
Copy_new_MU3	310		2.16	2.45	2.63	2,81	3.06	3,23
New MU5 ALS	390		2.15	2.44	2.63	2.81	3.05	3.23

Branch name & Cross section	MIKEII Chainage	AMTD(m)	Design Eve	ent flood lev	els (Ultimat	e) in mAH	D	
ID	(m)	Ziti i ziti	2 yr	5 yr	10yr	20 yr	50 yr	100 yr
Mu 6 ALS	470		2.13	2.43	2.62	2.80	3.05	3.23
Gateway M'way	475		Gateway N	I'way ME (Culverts	· · · · · ·		
MU 7 ALS	545		2.06	2.29	2.44	2.59	2.80	2.99
MU_9_ALS	595		2.05	2.29	2.44	2.59	2.80	2.99
MU5_ALS	640		2,04	2.27	2.43	2.58	2.79	2.98
End of branch	650	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	2.04	2.27	2.43	2.58	2.79	2.98
Bulimba East Rail Bypass		Maria de la Compania del Compania de la Compania de la Compania del Compania de la Compania de l	Bulimba E	ast Rail By	pass			
BE276	0		48.09	48.29	48.39	48.48	^\ 48. 57	48.68
BE276	33		48.00	48.22	48.32	48,41	48.50	48.60
BE275	144		47.80	47.80	47.80 🤇	47.80	47.84	47.94
BE274	226		46.94	47.05	∠′47.21\	47.36	47.53	47.70
BE273 US	347		46.86	46.95	47.13	47.28	47.46	47.62
BE273 DS	443		46.56	46.61	46:75	46.86	46.98	47.10
BE273 A	488	1 D. 1	46.39	46.44	46.53	46.61	√46.73	46.82
BE273 A	520		46.29	46.44	46.53	46.61	46.71	46.80
Kianawah Park Branch			Kianawah	Park Branc	h\			
	0 <		2.67	2.81	2.89	3,09	3.33	3.50
WY-1 ALS	48		2.65	₹2.77	2.87	3.09	3.33	3.50
WY-2 ALS	210		2.56	2.66	2.87	3.09	3.33	3.50
WY-3 ALS	260	X	2.55	2.65	2.87	3.09	3.33	3.50
WY4 ALS	340		2.51	2.63	2.87	3.09	3.33	3.50
WY-5 ALS	430		2.48	2.63	2.87	3.09	3.33	3.50
WY-6 ALS	530		2.47	2.63	2.87	3.09	3.33	3.50
WY-7 ALS	660		2.44	2.63	2.87	3.09	3.33	3.50
WY-8 ALS	780		2.40	2.63	2.87	3.09	3.33	3.50
WY-9 ALS	860		2.27	2.63	2.87	3.09	3.33	3.50
WY-10 ALS	945	1	2.13	2.62	2.87	3.09	3.33	3.50
	985		1.99	2.62	2.89	3.13	3.42	3.63
WY-11 ALS	1006	1	1.94	2.62	2.89	3.13	3.42	3.63
End	TOOO	<u> </u>	1.77	1 -102		71,57	<u> </u>	

Table I2: Estimated Peak Design Flood Discharges

Chainage	AMTD(m)	ID					- Vinness de la constant	10000000000000000000000000000000000000
			2 year	5 year	10 year	20 year	50 year	100 year
Bulimba C	reek:Compt	on Road to Ne	mies Road					
0	39900	Start	25.8	37.1	44.0	50.6	59.7	63.7
65	39835	BM222	25.0	36.2	43.0	49.5	58.5	62.2
175	39725	Bm221	22.9	34.2	40.9	47.3	56.1	59.2
270	39630	ВМ220	20.3	31.5	37.8	43.9	52.3	54.6
415	39485	BM219	29.2	38.3	46.5	54.5	65.2	73.3
560	39340	BM218	38.0	48.5	57.4	66.2	77,8	94.9
736	39164	BM217	38.9	51,2	60.4	69.4	× 81.5	97.4
900	39000	BM216	39.1	53.3	63.3	72.9	85.8	99.9
935	38965	End	47.5	64.9	77.8	,√89.8 _	105.3	124.2
	eek-Main Bra	nch				<u> </u>	\ \	
0	38965	Start	47.5	64.9	77.8	89.8	105.3	124.2
10	38955	BM 214	46.0	62.6	74,5	86.1	101.4	118.8
17	38948		Nemies Road					
40	38925	BM214 copy	46.6	63.60 ₁	75.7	87.5	103.2	120.7
120	38845	BM213	45:4	62.65	74.6	86.3	101.8	118.5
215	38750	BM212	45.7	63.78	76.0	88.0	104.0	120.7
355	38610	BM211	⟨38,8⟩	57.66	×69.1×	80.3	95.4	108.3
370	38595	LITALETT	Brandon Ro					·····
	38580	BM211-copy	44.9	65,9	79.1	92.1	109.4	125.7
385	<u> </u>	<u> </u>	40.3	60.3	73.0	85.7	102.3	115.1
470	38495	BM 209	41.5	57.9	70.5	83.5	100.4	111.6
540	38425	BM 208	43.9	58.5	70.5	85.3	103.4	114.5
600	38365	BM 207 BM 206	41.4	55.3	65.0	73.8	86.8	100.4
740	38225	BR 1	41.4	55.4	65.2	74.1	85.9	100.9
800	38165	BK\1		ream of Bra	www.commencensorial	/3.2	03.7	100,5
805	38160		Semination and services are services and services and services and services and services and services are services and services and services and services are services and ser	ypeyranacayana markananananananananananananing	AND THE PERSON NAMED IN COLUMN TWO IS NOT THE OWNER.	or a	87.8	103.I
825	38140	BR 2	41.8	56.5	66.5	75.7 82.3	95.6	112.1
840	38125	BM 205	45.1 46.0	61.1	72,1	75.2	93.8 87.3	102.2
890	38075	BR 3	40.8	55.9	66.0 72.1	73.2 82.4	95.9	112,2
905	38060	BR 4	44.4	61.0			90.0	105,1
942	38023	BR 5	41.3	57.3	67.7	77.4	95.5	111,4
960	38005	BR 5copy	43.4	60.5	71.5	81.9	93.3 97.9	114.1
990	37975	BM204	44.0	61.8	73.2	83.9		110.1
1075	37890	BM 203	40.6	59.0	70.2	80.8	94,8 97.5	110.1
1160	37805	BM 202	40.6	58.5	70.6	82.2		106.3
1300	37665	BM 201	40.2	53.0	63.8	76.1	92.4	
1365	37600	BM 200	44.0	58.7	71.0	85.2	104.2	120.1
1545	37420	BM 199	46.1	63.8	74.8	88.3	109.4	125.4
1670	37295	BM 198	45.0	63.7	75.8	87.3	103.7	118.7
1800	37165	BM340-MHG	41.8	57.7	71.7	84.7	100.5	116.4
1830	37135	BM 197	43.1	58.7	73.9	87.7	104.6	121.0
1845	37120		Beenleigh R	<u> </u>				
1860	37105	ВМ 197 Сору	43,4	58.9	74.1	88.4	105.8	122.4
1900	37065	BM195-I	43.1	58.9	72.9	87.6	105.3	121.9
1940	37025	BM 194	42.4	58.4	70,6	85.8	103.8	120.2
1960	37005	ВМ194 сору	44.3	61.3	74.2	90,3	109.3	126.4

MIKE11 Chainage	AMTD(m)	Cross section ID	IVERENIZEE IV	goder i caix i	Discussion (<u></u>
Chamage	**************************************		2 year	5 year	10 year	20 year	50 year	100 year
1960	37005	ВМ 194 сору	44.3	61.3	74.2	90.3	109.3	126.4
2045	36920	BM 192	42.6	59.3	69.9	84.7	102.1	117.6
2115	36850	BM 191 copy	40.6	55.4	65.9	75.5	91.5	105.4
2117	36848		St Lawrence	es Foot Bridg	e			
2125	36840	BM 191	43.9	59.8	71.3	82.4	100.0	115.2
2255	36710	BM190	40.5	53.2	64.4	75,7	91.0	107.8
2370	36595	BM188-6 copy	38.4	51.9	62.2	71.8	87.1	104.4
2375	36590			et. Foot Bric	ge & Weir	J. 19	<u> </u>	
2380	36585	BM188-6	40.8	55.4	66.3	<i>77</i> .2	< 94.7	113.2
2470	36495	BM188-2	42.2	57.8	69.4	<\ 80.5 /√	99.2	118.8
2500	36465	BM188-1	45.2	62.0	74:5	87.9	108.3	129.4
2670	36295	BM187	43.6	59.8	72.5	84.4	102.5	123.2
2785	36180	BM186	44.3	60.3	73.6	86.1	103.0	123.5
2985	35980	BM185	43.8	59,4	72.3	₹ 85.5	103.1	119.2
3165	35800	BM184	43.1	59.5	√71.2	84.9	103.3	120.6
3295	35670	BM183	/43.3	60.0	72.1	84.9	104.0	122.3
3435	35530	BM182	43.8	60.0	72.7	84.3	104.0	123.1
3625	35340	BM181	43.6	59.1	72.3	84.3	102.1	121.5
3765	35200	MHG320	43.1	√ 58.5	71.2	83.8	100.3	118.8
3800	35165	BM180 \	45.5	62.0	76.0	89.4	107.4	127.6
3960	35005\	BM179\\	48.9	67.5	82.7	97.9	118.5	140.5
3970	34995	ВМ179 сору	50.7	70.0	86.4	102.2	124.4	147.3
4150	34815	BM178	50.4	70.5	85.9	102.3	125.1	145.6
4150	34815	BM179	21,4	29.6	37.2	46.4	57.6	63.7
4260	34705	BM177	21.3	29.7	37.5	46.3	58.0	64.5
4320	34645	BM177A	21.3	29.8	37.7	46.3	58.1	64.9
4375	34590	LC	21.5	29.9	37.8	46.3	58.3	65.2
4385	34580	BM176 US	21.5	30.0	37.9	49.2	71.5	87.3
4415	34550	BM176 DS	21.6	30.1	38.0	49,3	71.6	87.5
4460	34505	BM 175	35.5	51.1	60.4	70.8	84.2	99.9
4515	34450	BM175-174	33.3	47.9	56.6	66.3	82.1	65.3
4555	34410	LC	32.0	45.2	53.6	62.8	82.6	87.1
4555	34410	LC	66.7	100.2	117.5	142.1	181.6	87.3
4575	34390	LC	66.6	100.1	117.4	142.0	181.5	99.7
4575	34390	LC	89.3	134.5	160.0	189.1	232.7	97.9
4590	34375	BM 174	89.3	134.5	160.0	189.1	232.7	98.5
4700	34265	BM173-BM174	89.3	134.1	159.9	189.2	232.6	214.2
4765	34200	Interpolated	89.3	134.1	159.9	189.2	232.6	214.1
4780	34185	BM173	89.3	134.1	159.9	189.2	232.6	270.3
4785	34180		Blesby Road	l Foot Bridge	e & Weir			
4790	34175	ВМ 173 сору	89.3	134.1	159.9	189.2	232.6	270.2
4905	34060	BM172	89.3	134.3	159.9	189.2	232.5	270.0
4995	33970	BM171	89.2	134.4	159.8	189.1	232.3	269.7
5120	33845	ВМ170	90.6	136.5	162.6	192.3	235.9	273.5
5280	33685	LC	92.4	139.1	166.0	195.9	239.6	277.7

MIKE11 Chainage	AMTD(m)	Cross section ID	MIKE11 N	Iodel Peak I	Discharges ((m³/s)		
and the second			2 year	5 year	10 year	20 year	50 year	100 year
5280	33685	LC	70.0	99.0	112.3	130.9	156.8	178.9
5285	33680	BM169	70.0	99.0	112.3	130.9	156.8	178.8
5405	33560	LC.	69.8	98.7	111.8	130.0	155.3	177.2
5405	33560	LC	69.8	102.6	121.7	138.9	162.3	181.9
5520	33445	BM167	69.8	102.2	121.3	138.1	161.1	180.7
5520	33445	LC	69.8	102.2	121.3	134.3	151.3	168.2
5615	33350	LC	69.8	101.9	121.2	133.6	151.0	168.1
5615	33350	LC	69.8	101.9	121.2	140.4	171.7	199.1
5715	33250	LC	69.8	101.4	121.1	140.1	√171.5	199.0
5715	33250	LC	69.8	100.1	119.2	139.9~	174.4	196.3
5730	33235	BM165	69.8	100.1	1.19.1	//139.9	174,3	196.2
5785	33180	LC	69.7	100.1	1,19.0	/139.7	174.2	196.1
5785	33180	LC	69.7	100.1	119.0	136.0	147.6	150.1
5845	33120	Xsec4	69.7	100.0	118.8	₹ 135.7	147.2	148.9
5902	33063	Xsec3	69.7	99.9	1,18.7	135.7	147.0	148.6
5918	33047	Xsec2	69.7	99.8	118.7	135.7	147.0	148.6
5935	33030	Xsec1	69.6	99.8	118.8	135.7	147.1	148.7
5938	33027	Garden City	69.6	99.8	118.8	135.7	147.1	148.8
5938	33027	Garden City	91.8	136.4	163.3	191.4	233.0	271.4
5985	32980	HEC2937	91.8	136.3	163.3	191.5	233.2	271.3
6050	32915\	BM157	₹ 91.8	136.3	163.4	191.5	233.4	271.0
6160	32805	BMI56	₹94,3	139.9	168.0	196.8	239.7	279.2
6240	32725	BM155	96.2	142.5	171.7	200.7	244.6	285.1
6340	32625	BM154	96.2	142.4	171.5	200.7	244.5	284.6
6450	32515	BM153 ALS	96.1	142.2	171.4	200.7	244.6	284.0
6650	32315	BM151	96.0	141.7	171.4	200.6	244.4	284.0
6860	32105	BM149	96.0	141.6	171.2	200.6	242.2	282.4
6930	32035	BM148-BM147	98.0	141.1	171.2	199.1	250.4	298.1
6935	32030		Craig Street	Foot Bridge	&Weir			
6945	32020	ВМ148 сору	97.4	141.3	171.2	199.3	248.2	295.0
6985	31980	BM148	96.2	141.8	171.1	200,2	246.3	284.0
7185	31780	BM146	95.8	141,5	170.9	199.8	243.5	283.7
7420	31545	BM144	95.9	141.3	170.8	200.0	243.4	283.4
7490	31475	BM143	95.9	141.3	170.9	200.1	243.3	283.3
7600	31365	ALS-142	97.5	143.4	173.9	203.6	247.1	287.8
7735	31230	BM141	99.4	146.1	177.6	207.9	252.3	293.4
7915	31050	BM139	99.8	146.6	178.2	208.5	253,1	293.7
7985	30980	BM138	100.0	147.1	178.7	209.0	253.6	294.3
8070	30895	ВМ137	100.9	148.3	179.8	210.1	254.7	295.6
8070	30895	Bulimba East	181.5	255,4	313.2	362.9	434.3	500.6
8200	30765	BM136	181.1	255.2	312.8	362.7	434.2	500.5
8325	30640	BM135	180.6	254.9	312.4	362.5	434.1	500.3
8475	30490	BM134	179.9	254.4	311.8	362.2	433.8	500.0
8555	30410	MHG 260	179.5	254.2	311.5	362.0	433.6	499.8
8570	30395	BM132	179.5	254.1	311.4	362.0	433.5	499.8

MIKE11	AMTD(m)		MIKEII M	lodel Peak I	Jischarges (m /s)		
Chainage		<u> </u>	1 yraisa	5 year	10 year	20 year	50 year	100 year
			2 year		310.2	361.1	432.7	498.8
8780	30185	BM131	179.1	253.1	310.3	360.7	432.3	498.3
8840	30125	BM130	179.1	252.9	310.3	359.9	431.1	496.9
8950	30015	BM129	179.1	253.0	310.3	364.9	436.7	502.7
9115	29850	BM127	181.4	256.5		367.7	440.1	506.8
9215	29750	BM126	182.5	258.4	316.7	366.9	439.7	506.5
9365	29600	BM126a	181.3	257.5	315.7	365.5	438.8	505.9
9530	29435	BM126b	180.1	256.1	314.0		438.1	505.2
9670	29295	BM122	180.0	255,4	313.0	364.3	436.1 -437.6	504.7
9765	29200	BM121	179.9	255.5	313.1	363.8	437.0	503.8
9890	29075	BM119	179.7	255.6	313.3	△ 363.9 △		507.4
9920	29045	BM118	181.0	257,4	315.5	>366.5	440.1	<u> </u>
10100	28865	BM117	188.2	268.1	328.5	382.0	458.4	528.4
10205	28760	BM116	187.6	267.9	328.3	382.0	\457.2\	527.2
10315	28650	BM115	186.9	267.6	328.0	381.8	457.3	526.5
10400	28565	BM114	188.1	269.2	330.1	384.4	460.6	529.9
10510	28455	BM112	189.7	271.2	332.7	387.8	464.7	534.2
10575	28390	BM111	189.7	271.0	332.5	387.6	464.6	534.3
10685	28280	BM110	189.7	270.5	332:0	387.2	464.4	534.2
10702	28263		Mt Gravat	t Capalaba	Road			gunnamumumumumumumumumumumumumumumumumumu
10725	28240	BM110 copy	189.7	27.0:4	331.8	387.1	464.3	534.2
10875	28090\	BM108\\	189.6	[™] 269.8	331.0	386.4	463.9	533.8
10965	28000 \	вм107	189.4	269.9	330.5	386.0	463.6	533.5
11095	27870	ВМ106	189.1	269.7	330.1	385.0	462.8	532.8
11255	27710	BM104	189.9	271.9	333.1	388.2	466.8	537.5
11515	27450	BM102	192.9	277.2	340.0	397.2	476.6	549.3
11620	27345	BM101	193.2	277.3	340.4	398.1	477.2	549.8
11695	27270	BM100	193.0	276.9	340.1	397.9	477.2	548.9
11820	27145	BM99	192.7	276.2	339.6	397.5	477.1	548.2
11910	27055	BM98	192.5	276.2	339,2	397.2	477.0	548.2
12035	26930	ВМ97	191.9	276.1	338.2	396.5	476.5	547.9
12135	26830	ВМ97сору	191.3	275.8	337.6	395.6	475.9	547.4
12139	26826		Wecker Roa	d Bridge	Section of the sectio			
12155	26810	ВМ97сору	191.2	275.7	337.6	395.4	475.8	547.3
12215	26750	ВМ94	191.2	275.5	337.5	394.8	475.3	547.0
12320	26645	ВМ94-93	191.0	274.9	337.1	394.0	474.5	546.3
12320	26580	BM93	190.8	274.5	336.9	393.8	473.9	545.7
12505	26460	ВМ90 сору	190.2	273.6	336.2	393.5	472.7	544.6
12690	26275	ВМ90	188.8	272.4	334.9	392.6	471.5	542.5
12820	26275 26145	BM88	188.8	273.1	335.3	393.6	473.1	543.5
	.g	BM87	190.3	275.5	338.0	396,9	478.3	549.8
13 140	25825	BM84	189.4	274.5	338.0	396.8	478.2	550.6
13440	25525		189.3	274.4	337.5	396.6	477.6	550.2
13530	25435	BM83	107.2	1. 4/7.7		396.4	476.9	549.7

25200 25055 25000 24850 24605 24505 24340	BM80 BM78 BM78 copy BM77 BM76 BM75	2 year 189.0 188.8 188.7 187.9 190.1	5 year 274.1 273.7 273.6	10 year 336.6	20 year 396.2	50 year	100 year
25055 25000 24850 24605 24505 24340	BM78 BM78 copy BM77 BM76	189.0 188,8 188.7 187.9	274.1 273.7	336.6			
25055 25000 24850 24605 24505 24340	BM78 BM78 copy BM77 BM76	188,8 188.7 187.9	273,7		396.2		***************************************
25055 25000 24850 24605 24505 24340	BM78 BM78 copy BM77 BM76	188,8 188.7 187.9	273,7			476.4	549.3
25000 24850 24605 24505 24340	BM78 copy BM77 BM76	188.7 187.9	***************************************	335.8	395.6	476.4	548.3
24850 24605 24505 24340	BM77 BM76	187.9	2,510	335.8	395.3	476.3	547.8
24605 24505 24340	BM76		272.4	335.2	393.8	475.5	546.6
24505 24340			276.2	339.9	400.3	483.5	556.7
24340	DIVI/3 *	191.1	278.0	342.0	403.3	486.9	560.9
		190.9	277.8	341.4	403.0	486.1	560.4
	BM74-BM72	190.9	277.6	340.9	402.8	485\5	560.0
24180	BM72	190.7	277.4	340.8	402.6	485.1	559.7
24120	BM71			***************************************	Annual Control of the	<u> </u>	559.2
ACCOUNTS AND ADDRESS OF THE PARTY OF THE PAR				······································	Townson and the second	CONTRACTOR DESCRIPTION OF THE PROPERTY OF THE	560.5
THE RESERVE OF THE PERSON NAMED IN COLUMN TWO IS NOT THE PERSON NAMED IN COLUMN TWO IS NOT THE PERSON NAMED IN	<u></u>					3	561.3
	The same of the sa			***************************************	Samuel and the second second	<u></u>	560.7
					<u> </u>	<u> </u>	560.6
STATE OF THE PARTY			A	and the second second second	102.7	10,110	
NAME OF TAXABLE PARTY.			CHARLES AND SERVICE OF THE PARTY OF THE PART	A CONTRACTOR OF THE PROPERTY OF THE PARTY OF	3026	486.8	560.5
	Barranian	Commence of the Commence of th				8	560.4
	g arana an arang a	ORIENTAL TOTAL CONTRACTOR OF THE PROPERTY OF T	The same of the sa	and the control of th	Commence of the Commence of th	Service and the service and th	560.2
			Samuel and the same of the sam	Commission was a second discount of the secon	THE RESERVE OF THE PERSON NAMED IN COLUMN TWO		559.7
****	<u></u>					Same and the same	559.1
	Zantonia de la compania de la compa	AND DESCRIPTION OF THE PROPERTY OF THE PROPERT				Quantification and the contraction of the contracti	558.9
			E		<u></u>	<u> </u>	568.7
		and the second s	Maria			<u> </u>	580.2
							580.1
CONTRACTOR				£		302.3	700.1
22520							1 - co 1
22510	Bm55-mod	MANAGEMENT CONTRACTOR OF THE PROPERTY OF THE P	***************************************			&	580.1
22285	BM57-mod	***************************************	§		&	Carrier Contract Cont	579.4
22180	BM56		8		<u></u>	8	579.4
21885	Bm55-mod			I	S	<u> </u>	594.2
21725	BM55-54	200.6	<u> </u>	<u></u>	<u></u>	<u> </u>	601.6
21665	BM54	200.6		<u> </u>	B		601.4
21 640	CD10	200.6	<u> </u>	360.8	430.2	521.3	601.3
21627		Winstanly S	Street Weir		Sales and the sa		-
21610	CD09	200.6	293.0	360.8	8	<u> </u>	601.4
21425	BM52	200.7	293.6	360.9	<u> </u>	<u> </u>	602.1
21200	CD07	200,4	291.5	367.1	436.5		602.8
AND DESCRIPTION OF THE PROPERTY OF THE PROPERT	BM50-49-ALS	204.2	292,1	369.0	446.8	533,3	601.8
21045	CD06	251.1	359.7	454.5	440.1	573.3	598.3
	CD05	241.7	343.9	434.3	421.5	541.9	598.0
***************************************	CD04	199.4	290.6	366.8	433.4	539.9	602.9
	BM47-mod	199.1	295.6	372.2	444.6	528.5	603.8
		199.0	297.0	373.4	443.3	523.0	602.0
			297.3	363.3	436.5	526.0	607.9
	24005 23805 23625 23505 23425 23410 23395 23365 23305 23175 23000 22775 22575 22575 22575 22530 22510 22285 22180 21885 21725 21665 21640 21627 21610 21425 21200 21115	24005 BM70 23805 BM69 23625 BM67 23505 BM66 23425 BM66 copy 23410 23395 23395 BM64 copy 23365 BM64-MHG25 23305 BM64 23175 BM63 23000 BM62 22950 BM61 22775 BM69 22575 BM59 22530 BM59 mod 22520 22510 22180 BM55-mod 22180 BM56 21885 Bm55-mod 21725 BM55-54 21665 BM54 21640 CD10 21627 21610 CD09 21425 BM52 21200 CD07 21115 BM50-49-ALS 21045 CD06 21005 CD05 20940 CD04 20855 BM46-mod	24005 BM70 190.3 23805 BM69 191.0 23625 BM67 191.5 23505 BM66 191.2 23425 BM66 copy 191.0 23410 Pine Mount 23395 BM64 copy 190.9 23365 BM64-MHG25 190.9 23305 BM64 190.7 23175 BM63 190.1 23000 BM62 189.9 22950 BM61 189.8 22775 BM60 192.4 22575 BM59 195.3 22530 BM59 mod 195.2 22530 BM59 mod 195.2 22510 Bm55-mod 194.8 22180 BM56 194.9 21885 Bm55-mod 198.8 21725 BM55-54 200.6 21665 BM54 200.6 21640 CD10 200.6 21627 Winstanly 21610 <td< td=""><td>24005 BM70 190.3 277.1 23805 BM69 191.0 277.6 23625 BM67 191.5 278.2 23505 BM66 191.2 277.9 23425 BM66 copy 191.0 277.6 23410 Pine Mountain Road Bridge State Sta</td><td>24005 BM70 190.3 277.1 340.8 23805 BM69 191.0 277.6 341.9 23625 BM67 191.5 278.2 342.6 23505 BM66 191.2 277.9 341.9 23425 BM66 copy 191.0 277.6 341.4 23410 Pine Mountain Road Bridge 23395 BM64 copy 190.9 277.5 341.3 23305 BM64 MHG25 190.9 277.5 341.2 23305 BM64 MHG25 190.9 277.5 341.2 23305 BM64 MG2 189.9 275.8 339.2 23175 BM63 MG2 189.9 275.8 339.2 22950 BM61 MG2 189.9 275.8 339.2 22775 BM60 MG0 192.4 279.6 344.3 22575 BM59 mod 195.2 284.4 350.1 22520 Meadowbank Stree Foot Bridge and Meadowbank S</td><td>24005 BM70 190.3 277.1 340.8 402.2 23805 BM69 191.0 277.6 341.9 403.3 23625 BM67 191.5 278.2 342.6 403.8 23505 BM66 191.2 277.9 341.9 402.9 23425 BM66 copy 191.0 277.6 341.4 402.7 23410 Pine Mountain Road Bridge 23395 BM64 copy 190.9 277.5 341.3 492.6 23365 BM64 copy 190.9 277.5 341.2 402.6 23305 BM64 190.7 277.3 340.9 402.4 23175 BM63 190.1 276.7 339.9 401.9 23000 BM62 189.9 275.8 339.2 401.1 22950 BM60 192.4 279.6 344.3 407.1 22575 BM59 195.3 284.4 350.1 414.5 22530 BM59 mod 195.2 <t< td=""><td> 24005 BM70 190.3 277.1 340.8 402.2 484.9 23805 BM69 191.0 277.6 341.9 403.3 486.8 23625 BM67 191.5 278.2 342.6 403.8 488.1 23505 BM66 191.2 277.9 341.9 402.9 487.4 23425 BM66 copy 191.0 277.6 341.4 402.7 487.0 23425 BM66 copy 191.0 277.6 341.4 402.7 487.0 23435 BM64 copy 190.9 277.5 341.3 402.6 486.8 23395 BM64 copy 190.9 277.5 341.2 402.6 486.6 23305 BM64 190.7 277.3 340.9 402.4 486.3 23175 BM63 190.1 276.7 339.9 401.9 485.4 23000 BM62 189.9 275.8 339.2 401.1 484.1 22950 BM61 189.8 275.5 339.2 401.1 484.1 22975 BM69 192.4 279.6 344.3 407.1 492.7 22575 BM59 195.3 284.4 350.2 414.5 502.3 22530 BM59 mod 195.2 284.4 350.1 414.3 502.3 22520 Meadowbank Stree Foot Bridge and Weir 22510 Bm55-mod 194.8 284.1 349.7 413.7 502.3 22180 BM56 194.9 284.1 349.6 414.1 502.7 21885 Bm55-mod 198.8 290.0 357.1 424.3 514.9 21725 BM59 200.6 293.0 360.8 430.1 521.2 21605 BM54 200.6 293.0 360.8 430.1 521.2 21610 CD09 200.6 293.0 360.8 430.1 521.2 21610 CD09 200.6 293.0 360.8 430.1 521.2 21610 CD09 200.6 293.0 360.8 430.3 521.5 21627 Winstanly Street Weir 21610 CD09 200.6 293.0 360.8 430.3 521.5 21627 SM55-54 200.7 293.6 360.9 431.5 522.0 2163 BM54 200.6 293.0 360.8 430.3 521.5 21640 CD10 200.6 293.0 360.8 430.3 521.5 21650 CD05 241.7 343.9 434.3 421.5 541.9 20940 CD04 199.4 290.6 366.8 433.4 539.9 20940 CD04 199.4 290.6 366.8 433.4 539.9 20940 CD04 199.4 290.6 366.8 433.4 539.9 20950 BM47-mod 199.1 295.6 372.2 444.6 528.5 20855 BM46-mod 199.0 297.0 373.4 443.3 539.0 20855 BM46-mod 199.0 297.0 37</td></t<></td></td<>	24005 BM70 190.3 277.1 23805 BM69 191.0 277.6 23625 BM67 191.5 278.2 23505 BM66 191.2 277.9 23425 BM66 copy 191.0 277.6 23410 Pine Mountain Road Bridge State Sta	24005 BM70 190.3 277.1 340.8 23805 BM69 191.0 277.6 341.9 23625 BM67 191.5 278.2 342.6 23505 BM66 191.2 277.9 341.9 23425 BM66 copy 191.0 277.6 341.4 23410 Pine Mountain Road Bridge 23395 BM64 copy 190.9 277.5 341.3 23305 BM64 MHG25 190.9 277.5 341.2 23305 BM64 MHG25 190.9 277.5 341.2 23305 BM64 MG2 189.9 275.8 339.2 23175 BM63 MG2 189.9 275.8 339.2 22950 BM61 MG2 189.9 275.8 339.2 22775 BM60 MG0 192.4 279.6 344.3 22575 BM59 mod 195.2 284.4 350.1 22520 Meadowbank Stree Foot Bridge and Meadowbank S	24005 BM70 190.3 277.1 340.8 402.2 23805 BM69 191.0 277.6 341.9 403.3 23625 BM67 191.5 278.2 342.6 403.8 23505 BM66 191.2 277.9 341.9 402.9 23425 BM66 copy 191.0 277.6 341.4 402.7 23410 Pine Mountain Road Bridge 23395 BM64 copy 190.9 277.5 341.3 492.6 23365 BM64 copy 190.9 277.5 341.2 402.6 23305 BM64 190.7 277.3 340.9 402.4 23175 BM63 190.1 276.7 339.9 401.9 23000 BM62 189.9 275.8 339.2 401.1 22950 BM60 192.4 279.6 344.3 407.1 22575 BM59 195.3 284.4 350.1 414.5 22530 BM59 mod 195.2 <t< td=""><td> 24005 BM70 190.3 277.1 340.8 402.2 484.9 23805 BM69 191.0 277.6 341.9 403.3 486.8 23625 BM67 191.5 278.2 342.6 403.8 488.1 23505 BM66 191.2 277.9 341.9 402.9 487.4 23425 BM66 copy 191.0 277.6 341.4 402.7 487.0 23425 BM66 copy 191.0 277.6 341.4 402.7 487.0 23435 BM64 copy 190.9 277.5 341.3 402.6 486.8 23395 BM64 copy 190.9 277.5 341.2 402.6 486.6 23305 BM64 190.7 277.3 340.9 402.4 486.3 23175 BM63 190.1 276.7 339.9 401.9 485.4 23000 BM62 189.9 275.8 339.2 401.1 484.1 22950 BM61 189.8 275.5 339.2 401.1 484.1 22975 BM69 192.4 279.6 344.3 407.1 492.7 22575 BM59 195.3 284.4 350.2 414.5 502.3 22530 BM59 mod 195.2 284.4 350.1 414.3 502.3 22520 Meadowbank Stree Foot Bridge and Weir 22510 Bm55-mod 194.8 284.1 349.7 413.7 502.3 22180 BM56 194.9 284.1 349.6 414.1 502.7 21885 Bm55-mod 198.8 290.0 357.1 424.3 514.9 21725 BM59 200.6 293.0 360.8 430.1 521.2 21605 BM54 200.6 293.0 360.8 430.1 521.2 21610 CD09 200.6 293.0 360.8 430.1 521.2 21610 CD09 200.6 293.0 360.8 430.1 521.2 21610 CD09 200.6 293.0 360.8 430.3 521.5 21627 Winstanly Street Weir 21610 CD09 200.6 293.0 360.8 430.3 521.5 21627 SM55-54 200.7 293.6 360.9 431.5 522.0 2163 BM54 200.6 293.0 360.8 430.3 521.5 21640 CD10 200.6 293.0 360.8 430.3 521.5 21650 CD05 241.7 343.9 434.3 421.5 541.9 20940 CD04 199.4 290.6 366.8 433.4 539.9 20940 CD04 199.4 290.6 366.8 433.4 539.9 20940 CD04 199.4 290.6 366.8 433.4 539.9 20950 BM47-mod 199.1 295.6 372.2 444.6 528.5 20855 BM46-mod 199.0 297.0 373.4 443.3 539.0 20855 BM46-mod 199.0 297.0 37</td></t<>	24005 BM70 190.3 277.1 340.8 402.2 484.9 23805 BM69 191.0 277.6 341.9 403.3 486.8 23625 BM67 191.5 278.2 342.6 403.8 488.1 23505 BM66 191.2 277.9 341.9 402.9 487.4 23425 BM66 copy 191.0 277.6 341.4 402.7 487.0 23425 BM66 copy 191.0 277.6 341.4 402.7 487.0 23435 BM64 copy 190.9 277.5 341.3 402.6 486.8 23395 BM64 copy 190.9 277.5 341.2 402.6 486.6 23305 BM64 190.7 277.3 340.9 402.4 486.3 23175 BM63 190.1 276.7 339.9 401.9 485.4 23000 BM62 189.9 275.8 339.2 401.1 484.1 22950 BM61 189.8 275.5 339.2 401.1 484.1 22975 BM69 192.4 279.6 344.3 407.1 492.7 22575 BM59 195.3 284.4 350.2 414.5 502.3 22530 BM59 mod 195.2 284.4 350.1 414.3 502.3 22520 Meadowbank Stree Foot Bridge and Weir 22510 Bm55-mod 194.8 284.1 349.7 413.7 502.3 22180 BM56 194.9 284.1 349.6 414.1 502.7 21885 Bm55-mod 198.8 290.0 357.1 424.3 514.9 21725 BM59 200.6 293.0 360.8 430.1 521.2 21605 BM54 200.6 293.0 360.8 430.1 521.2 21610 CD09 200.6 293.0 360.8 430.1 521.2 21610 CD09 200.6 293.0 360.8 430.1 521.2 21610 CD09 200.6 293.0 360.8 430.3 521.5 21627 Winstanly Street Weir 21610 CD09 200.6 293.0 360.8 430.3 521.5 21627 SM55-54 200.7 293.6 360.9 431.5 522.0 2163 BM54 200.6 293.0 360.8 430.3 521.5 21640 CD10 200.6 293.0 360.8 430.3 521.5 21650 CD05 241.7 343.9 434.3 421.5 541.9 20940 CD04 199.4 290.6 366.8 433.4 539.9 20940 CD04 199.4 290.6 366.8 433.4 539.9 20940 CD04 199.4 290.6 366.8 433.4 539.9 20950 BM47-mod 199.1 295.6 372.2 444.6 528.5 20855 BM46-mod 199.0 297.0 373.4 443.3 539.0 20855 BM46-mod 199.0 297.0 37

MIKE11	AMTD(m)	Cross section	MIKE11 M	Iodel Peak I)ischarges (m ³ /s)		
Chainage		ID .				30	<i>CO</i> ov	100 year
	g		2 year	5 year	10 year	20 year	50 year	613.8
18495	20470	BM44 mod	203.6	296.9	366.5	439.7	534.8	613.5
18690	20275	BM43-mod	203.3	295.5	366.0	438.4	530.9	611.4
18995	19970	BM42-mod	202.2	294.8	364.7	435.3	527.4	<u></u>
19165	19800	BM42-mod	204.0	298.0	367.9	439.2	534.3	618.0
19195	19770	ВМ41 сору	204.3	298.6	368.7	439.9	535.4	619.2
19205	19760		Scrub Road					4400
19215	19750	BM41-mod	204.2	298.5	368.6	439.8	535.3	619.0
19375	19590	BM5GHD	203.5	298.0	368.1	438.1	533.3	617.9
19640	19325	Bm5GHD	202.7	297.2	367.1	436.8	532.5	616.8
20050	18915	BM7GHD	200.7	295.0	364.7	435,0	530.8	613.9
20260	18705	BM8GHD copy	199,8	293.8	363.6	433.8	529.4	611.9
20270	18695		Meadowland	ls Road Brid			American de la composition della composition del	***************************************
20290	18675	Bm8GHD	199.8	293.7	√363.5	433.6	529.2	611.6
20510	18455	BM9GHD	198.5	292.2	361.8	431.8	<u>\ 527.1</u>	608.9
20850	18115	BM37	195.2	287.3	356.4	427.0	521:1	602.5
21090	17875	BM17GHD	193.0	284.0	352\9	423.7	516.9	597.6
21555	17410	BM18GHD	189.2	278.3	346.4	<u>\416.3</u>	508.8	587.6
21875	17090	BM18GHDcopy	188.4	276.5	344.5	//414.5	506.0	585.3
21885	17080		Preston Roa	d Foot Bridg	CONTRACTOR OF THE PROPERTY OF	***************************************		
21895	17070	BM19_GHD	188.4 ←	276.4	344.4	414.3	505.9	585.1
22305	16660	ALS mod	185.8	271,9	338.9	407.3	496.9	574.1
. 22775	16190	⟨BM23GHD\	183,8,	<u>√268.6</u>	334.0	401.4	488.4	564.8
23165	15800 🔪	ALS mod	\180.9	264.6	328.8	394.8	480.1	554.6
23285	15680	BM10GHD /	179.3	262.7	326.2	391.9	475.9	549.9
23600	15365	\BM11GHD'	176.2	258.8	321.5	385.8	469.0	541.7
23900	15065	ALS-23900	173.4	255.7	317.7	381.2	463.2	535.4
24000	14965	Minnippi merge	172.4	254.7	316.4	379.3	461.0	532.9
24000	14965	Minnippi merge	166.3	231.8	277.4	324.5	390.5	451.1
24695	14270	BM13GHD-mod	163.5	227.6	272.7	318.9	384.8	446.2
24890	14075	BM13GHD	163.6	227.7	273.0	319.2	385.3	446.9
25515	13450	MHG19-old	164.0	228.3	273.7	320.2	386.6	449.3
25565	13400	MHG20-old	163.9	228.2	273.6	320.1	386.4	449.1
25865	13100	BM26	163.4	227.4	272.8	318.9	385.1	447.9
25885	13080		Wynnum Ro	ad Bridge &	Weir			
25905	13060	BM 26 copy	163.3	227.3	272.7	318.8	384.9	447.7
26015	12950	MHG-140	163.1	227.1	272.3	318.5	384.4	447.2
26145	12820	BM24	163.0	226.9	272.0	318.1	383.9	446.6
26365	12600	BM23	162.8	226.3	271.3	317.2	382.8	445.4
26550	12415	Murrarie connec	163.2	226.9	272.0	317.7	383.8	446.9
26550	12415	Murrarie connec	135.6	182.9	217.5	254.6	316.2	371.7
26620	12345	BM22	135.8	183.1	217.7	254.9	316.6	372.1
26710	12255	ВМ22 сору	135.6	182.9	217.4	254.5	316.1	371.3
26730	12235		Murarrie R	oad Bridge &	& Weir			
26750	12215	ВМ22 сору	135.6	182.8	217.3	254.4	316.0	371.0

MIKE11	AMTD(m)	Cross section ID	MIKE11 N	[odel Peak]	Discharges	(m ³ /s)		
Chainage	<u> </u>	W	2 year	5 year	10 year	20 year	50 year	100 year
26780	12185	MHG-120	135.4	182.8	216.7	253.9	314.9	370.3
26940	12 105	BM22 copy	135.2	182.6	216.4	253.6	314.3	369.6
		BM42 AGHD cop	135.2	182.5	216.3	253.5	314.1	369.3
26990	<u> </u>	BM42A-mod	135.1	182.4	216.1	253.2	313.7	368.8
27100	11865	BM42AGHD cop	135.0	182.2	215.8	252.8	313.1	367.9
27300	11665		135.0	182.2	215.8	252.8	313.1	367.9
27305	11660	Murrarie connec	161.7	224.9	268.5	313.5	377.3	439.8
27305	11660	Murrarie_connec		224.9	268.5	313.4	377.1	439.5
27355	11610	BM42AGHD	161.7	178.4	201.2	223.8	253.9	283.3
27355	11610	LC	142.0	178.4	200.7	222.9	252.7	281.2
27755	11210	BM43AGHD	141.8	146.2	158.0	169.8	186.5	203.1
27755	11210	LC	125.5	146.2	157.7	169.5	186.0	202.5
27912	11053	BM44AGHD	125.4	76.2	77.2	80.9	90.3	103.0
27912	11053	LC	78.3	76.2	77.0	/80.7	\90.0\	102.7
28025	10940	BM44AGHD	78.2	73.1	72,4	21.7	70.4	69.5
28815	10150	BM44BGHD	73.7		72.5	78.6	76.8	75.3
29075	9890	BM43BGHD	81.5	80.3	101.0	108.9	123.9	139.3
29730	9235	BM43CGHD	92.7	96.0	121.1	133.5	154.7	176.6
30635	8330	BM44CGHD	102,1	111.9 \\ 208.2	244.8	281.0	331.5	378.4
30635	8330	I.C.	152,4		210.3	233.8	266.1	296.5
31600	7365	BM45GHD	145:2	185.8	<u> </u>	232.7	264.6	294.5
31740	7225	45GHD_US2\	145.2	185.4	209.6		319.I	362.3
31740	7225	LC	150.7	204.2	238.9	272.6	249.5	266.2
32110	6855	вм46СGHD∖	161.2	198,2	216.2	230.8	249.3	228.6
32110	6855 \	BM46CGHD	153.6	177.5	189.5	201.3	130.2	129.6
32355	6610	BM46BGHD	142.8	141.0	135.1	130.9	<u> </u>	
32355	6610	BM46BGHD	147.9	150.9	145.6	136.1	134.3	134.0
32650	6315	45GHD_D\$1	147.4	149.7	144.1	136.2	135.6	135.3 291.1
32650	6315	45GHD_DS1	155.3	193.2	215.8	234.7	263.4	
33330	5635	BM46AGHD	154.4	189.9	210.8	227.3	253.4	279.8 326.6
33330	5635	BM46AGHD	156.4	201.4	230.3	254.7	290,9	<u> </u>
34300	4665	BM52 GHD copy	155.7	195.9	220.8	241.4	271.7	299.5
34300	4665	BM52 GHD copy	168,7	244.8	296.1	345.8	413.8	474.1 484.6
34490	4475	BM52 GHD copy	172.7	250.1	302.3	353,4	422.8	1 404.0
34500	4465		Cleveland R			200.5	431.5	405.0
34510	4455	BM52 GHD	176.3	255.1	308.4	360.7	431.5	495.0
34700	4265	BM52 GHD	175.5	253.7	306.7	358.6	428.8	491.7
35260	3705	BM7	173.5	252.0	306.5	360,5	434.2	500.7
35670	3295	BM6	173.5	252.1	306.5	360.4	434.2	500.6
35690	3275	ВМ6-сору	173.5	252.1	306.5	360.4	434.2	500.6
35785	3180	BM48	173.5	252.1	306.5	360.4	434.2	500.6
36370	2595	Bm4	173.5	252.1	306.5	360.4	434.2	500.6
37040	1925	ВМ3	175.5	254.8	309.8	364.3	438:6	505.7
37465	1500	BM2_copy	176.9	256.7	312.1	367.1	441.8	509.4
38070	895	BM2	176.9	256.7	312.1	367.1	441.8	509.4
38340	625		176.9	256.7	312.1	367.1	441.8	509.4
38610	355	BM1	176,9	256.7	312.1	367,1	441.8	509.4
38965	0	End of branch	176.9	256.7	312.1	367.1	441.8	509.4

MIKE11 Chainage	AMILDIN	Cross section ID	IVIII IND EI IVI	touer reak I	machai ges (111.13)		
CALCARITY			2 year	5 year	10 year	20 year	50 year	100 year
ulimba Cre	ek East		<u>annon maria de la compania del compania del compania de la compania del compania del compania de la compania del compania de</u>					
0	and the second s	BE289	9.4	13.1	15.5	17.8	20.9	22.6
60.		BE289	8.4	12.2	14.4	16.6	19.6	20.9
170	6110	BE288	6.7	10.5	12.6	14.6	17.4	17.9
250	6030	BE287	7.0	9.3	11.2	13.1	15,6	16.9
388	5892	BE286	13.6	18.0	21.7	25.4	30.3	33.2
525	5755	BE285	20.6	25.9	30.5	35.2	42.4	50.2
612	5668	BE284	21.2	27.2	32.1	36.8	42.7	52.0
660	5620	HEC2146	21.4	27.8	32,7	37.5	43,6	52,7
		BE283	21.5	28.2	33.2	38.1	44.2	52.9
708		HEC2030	20.7	28.0	33.3	38.4	44.5	52.4
755 766		BE283 copy	18.9	27.3	33.2	38.5	44.5	51.3
799		BE282US	18.1	27.0	33.1	38.5	44.5	50.7
815	5465			oad East Cul				
820	5460	THE RESERVE OF THE PROPERTY OF THE PERSON NAMED IN	17.9	26.4	32.6	37.3	44.2	49.8
835	5445	BE281DS	17.6	26.2	32.5	36.9	44.0	49.5
840	5440	BE280	17.0	25.9	32.3	36.6	44.0	49.4
844	5436	BE279HEC		ail Culverts	22.3			
845	5435				210	35.4	43.5	48.8
852	5428	BE278	17.6	24.8	31.0	32.7	42.5	47.3
875	5405	BE277-HEC	(18.2)	23.8	CONTRACTOR	32,1	72.3	17.2
876	5404		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	oad Pipe Cul	THE REAL PROPERTY AND ADDRESS OF THE PARTY O	1 200	410	46.6
930	5350	Bulima_East_Ra		23,9	28.0	32.2	41.9	
930	5350 🔪	Bulima East Ra	17.9	22.9	26.4	29.8	37.2	40.7
946	5334 🔪	BE277-HEC DS	17.9	22.9	26.4	29.7	37.0	40.5
956	5324	BE277-A	17.9	22.9	26.4	29.6	36.9	40,3
978	5302	BE277-A copy/	17.9	23.0	26.5	29.3	36.6	39.9
981	5299	XS-7450	17.9	23.0	26.5	29.3	36.6	39.9
991	5289	XS-7460	17.9	23.0	26.5	29.4	36.3	39.6
1011	5269	Xs-7480	17.9	23.1	26.6	29.5	35.8	38.9
1031	5249	XS-7500	17.9	23.2	26.7	29.6	35.2	38.3
1051	5229	XS-7520	17.8	23.2	26.7	29.7	34.6	37.7
1071	5209	XS-7540	17.8	23.3	26.8	29.8	34.0	37.9
1091	5189	XS-7560	17.7	23.3	26.9	29.9	33.4	38.1
1111	5169	Xs-7580	17.7	23.3	26.9	30.0	33.5	38.3
1131	5149	Xs-7600	17.6	23.4	27.0	30.1	33.7	38.5
1151	5129	Xs-7620	17.5	23.4	27.0	30.1	33.9	38.6
1171	5109	XS-7640	17.5	23.4	27.1	30.2	34.0	38.8
1191	5089	XS-7660	17.4	23.5	27.1	30.3	34.2	39.0
1211	5069	XS-7680	17.4	23.5	27.1	30.4	34.3	39.1
1231	5049	Xs-7700	17.3	23.5	27.2	30.4	34.4	39,2
1251	5029	XS-7720	17.3	23.5	27.2	30.4	34.5	39.3
1271	5009	XS-7740	17.2	23.5	27.2	30.5	34.5	39.3
1291	4989	XS-7760	17.2	23.5	27.2	30.5	34.6	39.4
1311	4969	Xs-7780	17.1	23.4	27.2	30.5	34.7	39.4
1331	4949	XS-7800	16.9	23.4	27.1	30.5	34.7	39.5

MIKEII	AMTD(m)	Cross section	MIKEII N	Iodel Peak	Discharges	(m ³ /s)		(1) (1) (1) (1) (1) (1) (1) (1) (1) (1)
Chainage		l D						I don
	_	·	2 year	5 year	10 year	20 year	50 year	100 year
1341	4939	Xs-7810	16.8	23.3	27.1	30.5	34.7	39.4
1355	4925	BE273	16.6	23.2	27.0	30,4	34.7	39.4
1380	4900	Bulima East Ra	•	23.0	26.9	30.4	34.7	39.4
1380	4900	Bulimba East Le		22.9	26.9	30.9	36.7	42.3
1498	4782	BE272	16.4	21,6	25.9	30.0	36.2	41.4
1565	4715	BE272	16.6	21.9	25.6	29.2	35.5	40.4
1600	4680	BE271_ALS	16.6	22.0	25.7	29.3	34.9	39.6
1730	4550	BE270	16.1	22.2	26.0	29.7	34.4	39.6
1915	4365	BE269	19.8	28,5	33.9	39.1	46.4	53.5
2020	4260	BE268	22.0	32.1	38.4	44.5	53.2	61.3
2145	4135	BE267	22.4	31.8	38.2	44.5	53:5	61:7
2245	4035	BE266	22.6	31.5	38.0	44.4	53.6	61.8
2410	3870	BE265	22.7	31.2	37.4	44.0	53.6	61.8
2500	3780	BE264	22.6	31.5	37.2	43.7	53.4	61.6
2605	3675	BE263	22.4	31.7	37.6	43.2	53.0	61.2
2696	3584	Trib_C	22.3	31.9	37.9	_43.8	52.7	60.9
2696	3584	Trib_C	29.6	41.2	49.8	∖57.6	69.3	80,4
2765	3515	BE262	29.7	40.6	48.9	57.6	69.2	80.4
2767	3513		Underwood	Road Culver	ts \	_/		
2785	3495	BE261 \	(29.7)	40.7	/49.0 //	57.6	69.2	80.4
2990	3290	BE259 \	29.8	41.2	49.6	58.0	68.8	80.1
3200	3080	BE258	31:4	44.2	53.3	61.9	71.6	83.5
3320	2960\	BE257 \	∖ 32.0∖	45.6	55.1	63.9	73.5	87.6
3330	2950	1	Gateway Mo	otorway Culv	erts			
3425	2855	BE257 copy	31.4	45.4	55.0	63.7	73.2	85.1
3490	2790	BE256 /	30.9	45.1	54.8	63.4	73.2	85.4
3670	2610	BE255	31.3	44.2	54.0	62.3	73.5	85.8
3695	2585	BE255 copy	31.3	44.1	53.9	62.2	73.5	85.9
3725	2555	BE255 copy -mo	31.4	44.0	53.7	62.0	73.6	85.9
3726	2554	Trib Bl	31.4	44.0	53.7	62.1	72.7	85.5
3726	2554	Trib B2	32.8	48.1	59.4	69.7	98.5	92,4
3735	2545	BE254 copy	32.9	47.9	59.2	69.5	92.4	90.4
3745		BE254	33.0	47.6	58.9	69.2	75.4	90.5
3748	2532		Logan Road	annergy continued the second			kaasaanaanaanaanaanaanaanaanaanaanaanaana	
3785	2495	BE253	33.0	47.5	58.4	68.7	82.1	95.2
3810		interpolated	33.1	47.6	58.2	68.3	81.0	95.3
3888	2392	Trib B	33.2	48.0	58.2	68.2	80.3	93.4
3888	2392	Trib B	40.2	56.3	67.8	78.4	91.2	104.8
	2355	BE251	40.3	56.5	67.5	78.0	90.8	104.3
3925 4020	2355	Be250	40.3	57.9	68.7	78.9	91.7	106.2
4020		BE249	41.8	58.6	69.1	79.2	94.1	109.0
4110	2170		41.0		70.3	81.1	96.7	111.5
4230	2050	BE248	41.0	58.0	70.3 74.3	84.8	99.5	113.1
4284		Trib_A		60.5 100.1	128.1	148.3	177.2	205.5
4284	1996	Trib_A	80.3 79.9	109.1 108.8	126.1	147.5	176.6	205.0
4300	1980	BE247	17.7	100.0	12/.7	177.0	110.0	

, į	AMTD(m)	Cross section	MIKE11 N	Iodel Peak I)ischarges ((m ³ /s)		
Chainage	· · · · · · · · · · · · · · · · · · ·	<u>D</u>	2 year	5 year	10 year	20 year	50 year	100 year
4360	1920	BE247 copy	78.7	108.6	126.6	146.0	174.0	201.8
4300	1861	BE247 copy	79.0	108.5	126.9	146.4	173.6	199.9
		BE246A-ALS	79.2	108.3	127.0	146.6	173.9	200.1
4507 4602	1773 1678	Old 4612	79.4	108.5	127.2	146.7	174.3	200.6
4608	1672	010_4012	8	lains Bridge	AND DESCRIPTION OF THE PARTY OF	L	***************************************	
CONTRACTOR OF THE PARTY OF THE	1642	Copy Old 4612	danament dan	108.6	127.2	146.7	174.3	200.7
4638 4656	1624	BE244	79.5	108.6	127.2	146.7	174.3	200.8
4660	1620		13	ng Road Brid			<u></u>	Lentela (12.54 to 10.000) (10.000)
4695	1585	Old 4665	79.5	108.6	127.2	146.7	174.3	200.8
4730	1550	Old 4685	79.5	108.6	127.2	146.7	174.3	200.8
4750	1530	Old 4705	79.5	108.6	127.2	146.7	174.3	200.8
4870	1410	BE241	80.6	110.2	129.0	148.5	17,6.7	203.6
4980	1300	BE240	81.5	111.7	130.5	150.0	178.7	206.1
5010	1270	DLZ-TV	Gateway Of				-	
5050	1230	BE239	81.3	111.6	130.3	149.6	178.4	205.8
5175	1105	BE238	80.9	111.4	129.9	₹148.8	177.7	205.1
	950	BE236	80.2	111.1	129.3	147.8	176.6	203.9
5330	810	BE235	84.0	116.6	1.35.8	155.1	185.2	213.9
5470		BE232	90.0	125.8	146.8	167.4	199.5	230.2
5712	568 470	BE231	89.8	125.2	146:1	166.6	198.3	228.8
5810	470	BE230	90,9	126.4	147.6	168.3	200.2	230.8
5895	385 >-	BE229	91.8	127.3	148.8	169.7	201.9	232.5
5975	305	<u> </u>	\\ 91.6\\\	126.3	147.8	169.4	201.7	231.7
6055	225 \	BE228	91.0	125.8	147.4	169.0	201.3	231.3
6135	145	BE227 BE227	90.3	125.0	146.4	168.1	200.3	230.1
6280	0	BESS1.	90.3	123.0	170.7	100.1	200.5	
Fributary A			1/0	23.8	28.2	32.4	38.2	40.9
0		ALSI-copy	16.8	21.2	24.7	28.1	32.9	34.4
100		ALS1-copy	14.8		21.2	23.7	27.3	32.9
320		ALS1	12.7	18.4	CONTRACTOR OF STREET	24.3	28.5	33.3
600		ALS2	13.6	17.4 22.2	21.0 26.6	30.5	35.6	40.9
950		BE-1060	16.4	A	31.3	36.7	43.8	48.9
1400		BE-1040	18.0	25.4	31. <i>3</i> 39.4	46.5	55.8	63.3
1400		Trib_A1	22.3	32.0		49.1	59.7	66.9
1770		BE-1030	25.8	34.8	41.3	50.1	59.3	67.7
2070		BE-1020	25.4	35.4	42.8	JU, I	33.3	07.7
2072		: 2	School Road		411	F 510	61.5	70.1
2125		interpolated	26.1	36.6	44.4	51.9	61.5	73.7
2163	<u> </u>	Trib_A2	27.3	38.4	46.6	54.5	64.7	109.3
2163		Trib_A2	42.4	57.6	69.1	80,4	95.0	<u> </u>
2235		BE-1010	40.4	55.3	66.4	77.3	90.9	104.9
2535		BE-1005	43.2	60.0	72.2	84.1	99.7	115.5
2545		•	Freeway Of				1000	11170
2555		BE-1005	43.3	60.2	72.5	84.4	100.1	116.0

MIKE11	AMTD(m)	Cross section	MIKE11 N	1odel Peak	Discharges	(m³/s)		
Chainage	88	ID					q	
			2 year	5 year	10 year	20 year	50 year	100 year
2735		BE1005 copy	42.3	59.0	71.1	82.5	97.2	112.8
2765		BE1000	42.2	58.8	70.8	82.0	96.5	112.0
2805			Gateway Mo	otor way				
2935	:	BE1000 modifie	41.8	57.9	69.3	78.6	92.8	108.2
3015		BE1000 modified	41.8	57.4	68.6	77.3	91.3	106.5
3021		BE1000 modified	41.7	57.4	68.5	77.3	91.2	106.3
Tributary A	1		and the second contract was a second state of the second state of					
0		A1-1050	7.9	11.2	13.3	15.3	18.1	19.5
280		Å1-1050	5.8	9.1	11.0	12.8	15,3	15.8
500	:	ALS	6.0	8.1	9.8	11.5	13.8	15.0
720		ALS	5.3	6.8	8.3	9.9	1,2.0	14.6
750	<u> </u>	ALS	5.0	6.6	8.1	>√9.8	12.0	14.4
Tributary A	2			<u> </u>			Salaman da s	
0		TRIB A2	17.2	24.4	28.8	33.0	38.9	41.6
80		SMP	15.1	22.4	26.6	√30.7 ₅	36.3	38.3
475		SMP	17.8	22.4	26.3	30.5	36.9	43.6
690		SMP	20.2	26.8	31.7	36.4	42.3	51.1
1035		SMP	15:9	23.6	28.8	33.7	40.2	44.4
1042		SMP.	15.6	23,0	28.2	33.0	39.4	43.3
Tributary B								ĺ
1000		BE2030	22.6	32.3	38.3	44.0	52.0	55.5
1055		BE2030	21.6	31.2	37.0	39.9	49.9	53.3
1062			Dance Cour	Santana de la constanta de la				
1075		BE2030 copy	21.1	30.7	36.5	39.2	49.2	52.4
1215		BE2020	17.4	26.7	32.5	37.1	44.4	46.3
1340		BE2020 copy	18.1	23.9	29.0	33.6	39.5	45.6
1360		Interpolated	18.3	23.4	28.4	32.9	38.7	45.9
1360		BE2010	10.7	12.4	13.7	15.0	17.0	20.3
1361		DLLOTO	Logan Road				***************************************	
		BE2000	10.9	12.2	13.3	14.8	16.8	20.8
1394 1432	toda i more un un terri-	BE2000 BE2001	10.9	12.3	13.5	15.0	17.0	20.9
		BE2001	10.7	12.1	13.2	14.7	16.7	20.5
1492	Commission of the Commission o		10.7	12.1	یک، ل. ۱.	7 7.4	4.00.7	
Tributary C		DE 2000	0.7	12.7	16.3	18.7	22.1	23.8
0.		BE-3050	9.7 9.4	13.7 13.4	16.0	18.3	21.7	23.3
.10		BE-3050		9.6	11.6	13.5	16.0	18.3
390		BE-3040	6.8		}	13.0	15.6	17.3
545		BE-3030	6.5	9.1	11.0		<u> </u>	<u> </u>
665,	_	BE-3020	8.2	11.3	13.8	16.4	19.7	22.3
810		BE-3010	10.1	14.3	17.4	20.6	24.8	
1000		BE3000	10.2	14.1	17.2	20.3	24.4 24.4	28.1 28.0
1005		BE-3000 copy	10.2	14.1	17.2	20.3	24.4	Z 0.U
1008			AND DESCRIPTION OF THE PERSONS ASSESSED.	otorway Culv			22.	36.0
1100		ВЕ3000 сору	10.3	14.3	16.9	19.6	23.4	26.9
1110		ALS	10.3	14.3	17.0	19.7	23.0	26.7
1120		End Trib C	10.4	14.3	17.0	19.8	22.8	26.8

ž.	AMTD(m)	Cross section	MIKE11 N	Iodel Peak I)ischarges	(m ³ /s)		
Chainage		ID	2 year	5 year	10 year	20 year	50 year	100 year
D. 10	•		Z year	3 year	IO YEAT	20 / CA1	DO YEAR	200 / 000
Fributary B	L	1.7.0	7.6	11.1	14.7	18.0	21.6	25.6
1000		ALS	7.5	11.1	14.7	18.0	21.6	25.6
1002		ALS	7.5	11.1	14.5	17.8	21.0	25.5
1020		ALS	7.6				20.4	24.9
1055		ALS	7.6	11.3	14.5	17.6	16.5	19.7
1140		ALS	7.0	10.4	12.9	15.0		19.7
1145		ALS	6.9	10.3	12.8	14.7	16.1	19.4
Padstow Bra	nch	T. Carlotte	*****					
0		BM177	29.0	41.0	48.8	55.9	67.6	82.2
32		BM177	28.9	41.0	48.6	55.8	67.7	81.9
105		BM177-176ALS	28.7	41.2	48.5	55,5	68.1	82.6
140		LC	28.8	41.3	48.8	√′55.4	68.2	82.9
140		LC	28.8	41.3	48.8	.52.9	55.2	60.9
175		BM176-US-ALS	28.9	41.4	49.1	53.4	55.3	61.2
177			Padstow Ro	ad culverts				
205		BM176-DS-ALS	29.0	41.5	49.3	€53.7	55.6	61.6
205		LC	29.0	41.5	49.3	53.7	55.6	61.6
258		BM175	29.2	41.8	49.7	\$4.4	56.5	62.3
258	***************************************	LC /	29.2	41.8	49.7	√54.4	56.5	65.2
325		BM175-174ALS	29.6	42.1	50.2	55.1	57.5	66.0
352		BM174	29.8	42.3	50.4	55.4	57.9	66.2
375		BM175	29.9	42.4	50.5	55.6	58.2	66.4
Garden City	Branch							
5280		BM169	23.2	40.1	55.1	66.7	84.7	101.2
5285		BM169	23.1	40.1	55.1	66.6	84.6	101.1
5405		BM168 /	23.1	39.9	54.9	65.4	82.8	98.8
5405		LC\	23.1	36.0	44.6	56.9	76.4	94.7
5510	7	BM167	23.1	35.8	44.2	56.3	75.9	94.4
5510		LC	23.1	35.8	44.4	60.9	86.1	107.2
5615		ВМ167 сору	23.1	35.7	43.8	60.0	85.4	106.8
5615		LC	23.1	35.7	43.6	52.8	64.1	75.0
5715		Bm165 copy	22.9	35.5	43.6	52.5	63.7	74.8
5715		LC	22.8	36.8	45.2	52.6	61.1	77.9
5730		Bm165	22.9	36.8	45.2	52.5	61.0	77.9
5785		XS5	22.9	36.8	45.2	52.4	60.8	77.8
5850		XS4	22.9	36.7	45.2	52,3	60.8	77.5
5850 5850	<u> </u>	LC	22.9	36.7	45.2	57.0	88.5	125.6
5935		XS4 copy	22.9	36.6	45.2	57.0	88.7	125.3
5938		End	22.9	36.7	45.2	57.0	88.7	125.3

MIKE11 Chainage	TATE TATE	Cross section ID	IVILAND I I (V)				-	
			2 year	5 year	10 year	20 year	50 year	100 year
Aimosa Cre	ek							2
0	I	Mi 40 Hecras	35.3	51.1	60.7	70.0	82.9	88.2
5		Mi 40_Hecras	35.2	51.0	60.6	69,9	82.7	88.0
96		Mi 40a	32.3	48.3	57.7	66.8	79.3	83.9
200		Mi39	29.2	43.1	52.1	60.8	73.0	76.2
330		MI38	30.6	39.2	46.7	53.9	64,6	77.5
484		Mi37	42.5	69.8	65.3	75.9	91.4	109.1
506		Mi36	44.3	74.3	68.0	78.9	95,2	113.6
558		Mi35	44.8	71.8	69.3	80.3	95.2	114.7
660		Mi34	45.3	74.1	71.4	82.7	97.7	116.2
696		Mi33	45.1	74.7	71.8	83.2	98.3	116.4
811		Mi32	42.3	75.6	71.8	×^\83.9 _. √	99,4	115.5
952		Mi31	38.9	73.1	68.0	80.6	96,5	108.7
1037		Mi31-copy	39.6	70.3	64.6	77.3	93.3	103.2
1186		Mi29	39.6	66.5	63.8	73.3	86.0	101.3
1302		Mi28	38.4	67.0	63.9	₹ 73.9	87.3	102.1
1322		Mi27	38.0	67.0	√63.7∖	73.9	87.4	102.1
1366	<u> </u>	Mi26	×36.7	66.8	63:2	73.7	87.6	102.0
1439	1	Mi25	36.0	66.4	62.3	73.3	87.7	101.8
1549		Mi24	36,4	65.4	₹61.0 €	72.6	87.5	101.4
1588		Mi23	36.5	64.9	60.3	72.2	87.4	101.1
1719		Mi22	36,7	63.1	58.4	70.9	86.7	100.3
1738		Mi21-2	36.7	√62.8	58.5	70.5	86.5	100.0
1739			Nagel Street	Bridge				1 1102
1752		Mi21-1	36.7	62.7	58.6	70.2	86.1	99.6
1762		Mi20	36.7	62.6	58.6	70.1	85.9	99.3
1882		Mil9	36.6	62.3	59.6	68.5	83.2	95.8
1892	Egre in or in a Steps	Mi19-4	36.6	62.4	59.7	68.7	83.0	95,5
1895			Pacific Moto	rway		u de regerçación de a y Haza e Halfill		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
1964		Mi19-1	36.4	62.8	60.0	69.2	81.7	94.4
2023		Mi18	38.4	63.0	63.8	73.7	87.9	100.7
2086		Mi17	40.5	63.2	67.8	78.4	94,4	108.3
2133		Mi16	40.3	63.4	67,9	78.7	93.2	107.7
	Mark to the state of the state	Mil5	39.9	63.5	68.0	79.1	93.7	108.5
2224		Mi13-3	39.8	63.5	68.1	79.2	94.0	108.8
2248		IMITO-D	Kessels Roa					1
2255		Mi13-2	39.6	63.4	68.0	79.3	94.4	109.2
2284		Mi13-2	39.3	63.4	68.0	79.4	94.7	109.6
2325		Mi12	39.1	62.9	67.7	79.3	95.3	110.5
2516		Mill	39.4	62.3	67.2	78.8	95.3	110.6
2635		IATIT	Parkway Sti		<u> </u>			
2648		8 X 3 1 (0 1)	39.5	62.1	67.1	78.7	95.3	110.6
2664	<u> </u>	Mi10-2	39.5 39.6	61.9	66.9	78,6	95.3	110.5
2718		Mi9		<u> </u>	66.0	77.9	94.8	110.1
2828		Mi8	39.6	60.7	<u></u>	84.9	104.0	121.0
2955		Mi7	43.0	65.3	71.7	§	112.3	130.8
3069		Mi6	45.8	70.3	77.2	91.3	11,4,5	120.0

MIKE11 Chainage	AMTD(m)	Cross section ID	MIKE11 N	Iodel Peak l	Discharges ((m /s)		en e
Chamage	<u></u>	<u> </u>	2 year	5 year	10 year	20 year	50 year	100 year
3221		Mi5	44.8	70.4	77.8	90.6	110.8	129.4
3388		Mi4	44.0	69.5	77.7	91.1	108.9	125.9
3496		Mi3	44.2	68.5	77.3	91.2	109.7	126.1
3585		Mi2	44.3	67.7	77.0	91.1	110.0	126.7
3801		Mi1	44.2	67.5	75.5	90.2	110.0	127.3
3890		Mi2	44.0	67.5	75.0	89.8	109.6	127.0
	pass Branch							
0	İ	ALS-1	6.5	23,6	39.5	54.3	72.4	84.4
80		Minnippi new1	6.3	23.5	39.3	53.8	7).5	83.2
125	21 A A A A A A A A A A A A A A A A A A A	Minnippi new2	6.2	23.4	39.1	53.5	71.0	82.6
230		Minnippi new3	5.8	23.2	38.5	52.3	69.4	80.6
400		Minnippi new4	4.5	22.8	37.1	√ 50.0	66.1	76.5
542	Barrier de la companya de la company	Minnippi new5	2.9	22.5	36.2	48.8	64.3	74.7
650		Stanton RD	2.8	22.3	35.8	48.3	63.7	74.0
			2.8	22.2	35.7	48.1	63.4	73.8
720		new_A	2.8	22.2	35.7	48.1	63.4	73.8
730		new_B		22.2	35.7	48.1	63.4	73.8
745		Minnippi_new6-	2.8			740.1	05.4	75.0
748			AND DESCRIPTION OF THE PARTY OF	otorway Culv	CALL CONTRACTOR STORY AND ADDRESS OF THE PARTY OF THE PAR	40.1	62.7	73.7
810	S	Minnippi_new7-	2.8	22.2	35.7	48.1	63.3	73.7
825		new E	\ 2,8′	22.2	35:7″	48.1	63.3	<u> </u>
860		new G	4.1	22.2	35.7	48.1	63.3	73.7 73.7
870		new_7a	4.6	22,2/	35.7	48.1	63,3	<u> </u>
945	\ \ \	Mînnippi∖new8∖	5.3	~	32.2	43.2	57.2	67.3
1015		BM31GHD_mod	5.3	20.2	32.1	43,2	57.2	67.3
1115		Minnippi16_AL8	5.2	20.2	32.1	43.1	57.1	67.2
1125		3. November 2	Wynnum Re	oad Bridge			10 10 10 10 10 10 10 10 10 10 10 10 10 1	_
1150		BM 31GHD-cop	5.2	20.2	32.0	43.0	57.0	67.1
1310		BM36_GHD	5.0	20.1	31.8	42.7	56.5	66.4
1560		Minnippi_new11	4.4	20.1	31.5	42.1	55.4	64.9
1850		BM 42B_GHD	3,5	20.2	31.1	41.4	54.1	63.0
2004		BM42BGHD	3.7	20.4	31.2	41.0	53.5	62.1
		3				2.5		Territoria La Articología de Caracteria La Articología de Caracteria
o 0	pass Branch		27.6	44.2	54.5	64.9	71.0	75.6
20		MU1 ALS	27.6	44.2	54.5	64.9	70.9	75.5
20 35		New MU1	27.6	44.2	54.5	64.8	70.8	75.3
***************************************		New MU1 ALS	27.4	43.8	54.0	64.1	69.2	74.3
160 275		New MU2 ALS	27.1	43.3	53.5	63.1	67.5	73.6
310		Copy new MU3	27.0	43.2	53.4	62.8	66.9	73,3
390		New MU5 ALS	26.9	43.1	53.1	62.1	65.9	73.0
470	<u>.</u>	Mu 6 ALS	26.9	42.9	53.0	61.5	65.2	72.7
	torway Culve							<u> Kaisannassiannimuu</u>
545		MU 7 ALS	26.8	42.9	52.9	61.2	64.8	72.3
		MU 9 ALS	26.8	42.8	52.9	61.0	64.6	72.1
595 640		MU5 ALS	26.8	42.8	52.8	60.9	64.4	72.0
640 650	<u> </u>	INION WITH	26.8	42.8	52.8	60.9	64.4	72.0

MIKE11 AV Chainage	ITD(m) Cross section ID	MIKELL	Aodel Peak l	Discharges ((m /s)		
		2 year	5 year	10 year	20 year	50 year	100 year
Bulimba East Ra	il Bypass				***		gyasan tarist territory (the colored to the
0	Start	0.28	1.03	1.67	2.40	4.71	5.97
33 .	BE276	0.25	1.09	1.76	2.54	3.88	5.33
144	BE275	0.11	1.07	1.90	2.85	4,21	5.85
226	BE274	0.21	0.76	1.50	2.39	3.72	5.14
347	BE273 US	0.32	0.58	1.12	1.77	2.81	4.08
443	BE273 DS	0.33	0.51	1.09	1.78	2.90	4.19
488	BE273A	0.32	0.55	1.13	1.84	3.00	4.31
520	End	0.32	0.64	1.23	1.95	3.13	4.48
Cianawah Park I	3r an ch		<u> </u>				
0		18.07	25.98	30.90	35.59	42.13	45,06
48	WY-1 ALS	16.28	24.44	29.22	√3 4 .12	40.49	43.02
210	WY-2 ALS	11.92	15.93	18.66	22.46	27.22	32.01
260	WY-3 ALS	11.25	14.99	18.02	21.34	25.40	30.89
340	WY-4 ALS	10.10	13.88	16,77	20.01	24.09	28.84
430	WY-5 ALS	8.76	12:47	15.15	17.98	21\71	25.42
530	WY-6 ALS	7.97	10.50	12.71	\14.81	17.81	20.30
. 660	WY-7 ALS	6.19	8.36	9:75	10.87	12.34	13.65
780	WY-8 ALS	5.48	7.05	> 7.87	_8 ² .75	9.84	10.72
860	WY-9 ALS	<5.35 ₀	6.72	7,49	8.12	8.84	9.49
945	WY-10 ALS	5:34	6.69	7.43	8.02	8.82	9,30
985	WY-11 ALS	5.33	6.69	7.43	8.01	8.81	9.29
1006	End \	5.33	6.68	7.42	8.01	8.81	9.28
ink Canals	Ind.						
	42GHD AB	19.98	46.97	67.92	90.52	124.34	157.87
0	42GHD AB	19.98	46.97	67.92	90.52	124.34	157.87
175	43GHD AB	16.66	32.41	43.29	53.57	66.55	78.88
0	43GHD AB	16.66	32.41	43.29	53.57	66.55	78.88
186	43GHD BC	9.37	15.75	17.10	18.15	18.76	20.00
0	43GHD_BC	9.37	15.75	17.10	18.15	18.76	20.00
191	44GHD AB	48.93	70.81	81.14	88.63	95.70	100.83
	44GHD AB	48.93	70.81	81.14	88.63	95.70	100.83
74 0	44GHD_AB	51.83	98.16	125.11	148.58	177.29	202.24
		51.83	98.16	125.11	148.58	177.29	202.24
58	44GHD BC	19.89	48.87	70.73	93.03	123.60	151.64
0	45GHD US1 45GHD USI	19.89	48.87	70.73	93.03	123.60	151.64
465	45GHD US2	5.54	19.07	29.52	40.07	54.63	67.87
0	45GHD_US2	5,54	19.07	29.52	40.07	54.63	67.87
5,60		9.62	56.55	96.06	137.94	196.70	250.42
0	45GHD_DS1 45GHD_DS1	9.62	56.55	96.06	137.94	196.70	250.42
190	46GHD AB	2.01	12,57	20.18	28.10	38.33	47.27
0			12.57	20.18	28.10	38.33	47.27
621	46GHD AB	2.01 8.26	21.27	27.56	30.84	32.66	37.74
0.	46GHD_BC	<u> </u>	&	27.56	30.84	32.66	37.74
99	46GHD BC	8,26	21.27		104.47	142.19	174.67
0	46GHD_DS	13.04	48.98	75.34 75.34	104.47	142.19	174.67
294	46GHD_DS	13.04	48.98		7.05	142.19	16.77
0.	CLEV_RAIL	0.30	1.87	4.12		§	
939	CLEV_RAIL	0.30	1.87	4.12	7.05	11.80	16.77

Appendix I2

HECRAS Model Results for Newnham Road Tributary



-RAS Plant Plan 05 River: Newnha Beach River Sta	m Reach: Lower Profite	O Total 1	Min Ch El	W.S. Elev	Col W.S.	E.G. Elev	E.G. Slope	Vel Chini	Flow Area	Top Width	Froude # Ch
Reach River Sta	1,0.00	(m3/s)	(m)		(m)	(m).	(ការវារា)	(m/s)	(m2)	(m)	0
er 1880.00	100yr	60.60	22.75	24.88	24.58	25.02	0,003228	1,90	45.15 29.96	54.67	.0.
rer 1880.00	50yr	48.30	22,75	24.62	24,40	24.81	0,004937 0,005898	2.11	24.08	40.52	0.
er 1880.00	20yr	42.00	22,75	24,49	24,28	24.70 24.64	0.005148	2,16	21.68	37.21	0.
r 1880.00	10yr	38,70	22.75	24,43	24.08	24.57	0.006239	2,11	19.42	33.75	0.
1880.00	5yr	35,00 26,20	22.75	24.14	23.88	24.35	0.007546	2.05	13.29	21.11	
r 1880.00	2ут	20.20	EL.10		1						
(1873.00	190yr	60.60	22.71	24.82		25.00	0.003662	2.03	39,48	49,15	. 0
r 1873.00 r 1873.00	50yr	48.30	22.71	24,57		24,78	0.005004	2.13	27,79	43,33	0
1873,00	20уг.	42.00	22.71	24,45	-	24.66	0.005517	2,12	23.03	33.55	0
1873.00	10yr	38.70	22.71	24.39		24,60	0.005534	2.07	21.25	31.24 28.78	0
r 1873.00	5уг	35.00	22.71	24.34		24,53	0.005420	1,99	19.50 14.25	19.14	7 0
r 1873.00	2yt	25.20	22,71	24.12		24.30	0.006125	1,57	171,241	1 1400	
						24,97	0.004033	2,13	36,73	44.53	
r 1866.00	100yr	60,60	22.50	24.77		24,74	0.006283	2.33	24.75	37.44	
r 1866.00	50yr	48,30	22.50	24.48 24.33	24.14	24.61	0.007991	2.42	19.37	31.18	· C
r 1866.00	20yr	42.00 38.70	22.50 22.50	24.27	24.07	24.55	0.008201	2.37	17.71	28.97	C
r 1866.00	10yr	35.00	22.50	24,23	24,00	24.48	0.007762	2.25	16,53	27.30	
r 1866.00	5yr 2yr	26,20	22.50	24.01	-	24.24	0.009279	2,15	12,19	14,28	
r. 1866.00	2,1	20/09		35						- <u>Villago</u>	
r 1860.00	100yr	60.60	22.26	24.77		24.94	0.003259	2.12	40.71	47.42	
r 1860,00	50yr	48,30	22.28	24.46		24.70	0.005048	2,36	27.28	39.63	0
1860.00	20yr	42.00	22.28	24.27		24.56	0.005843	2.53	20.56	32.18	0
1860.00	10yr	38.70	22.28	24.15	24,09	24.49	0.008538	2.67 2.84	17.03 13.64	26.92 20.50	
r 1860,00	5yr	35,00	22.28	24,01	24,01	24,41	0,011224	2,84	9.06	9.24	
r 1860,00	2yr	26,20	22,28	23,72	23,57	24.15	0,013084	2,09	3.33		4.
				01.77		24,91	0.002506	1,90	45,38	51,20	(
r 1854.00	100yr	60.50	22.25	24,77		24.65		2.07	31.08	42.89	(
r 1854.00	50yr	48.30 42.00	22.25 22.25	24.29		24.50	0.004915	2.21	23.95	34,66	
r 1854.00	20yr	38.70	22,25	24.17		24,42		2.33	20.06	30.16	
1854.00	10yr 5yr	35.00	22,25	23.99	23.83	24,32		2.59	15,25	24.39	
r 1854.00 r 1854.00	2yr	26.20	22.25	23.68	23.56	24.04		2.68	9.78	9.71	
-r 1854,00	E-31									2.0	
1847.00	100yr	60.60	22.20	24.78		24,89	0.001685	1,54	41.05	58.71	
r 1847.00	50yr	48.30	22.20	24.46		24.63	0,002601	1.70	27,37	33.41 25.73	
r 1847.00	20yr	42.00	22.20	24.28		24.47	0,003579	1.84	22.15 19.68	21,09	
1847.00	10yr	38.70	22,20	24.17		24.37	0.004337	1.95 2.20	16.25	19,59	
r 1847.00	5yr	35,00	22.20	24.00		24.24 23.95	0.006198	2,40	10.93	10.51	id (
r 1847.00	2yr	26.20	22,20	23.66		23.57	4.5/02/454				-
						24.88	0.001197	1,41	43,40	52.07	
er 1841.00	100yr	60,60	22.14	24.78 24.47		24.60		1.49	30.90	31.64	- 4
er 1841.00	50yr	48.30	22.14	24.30		24.43		1,58		26.59	
r 1841.00	20yr	42.00 38.70	22.14	24,18		24,33	0,002502	1.66		24,43	
r 1841.00	1Dyr	35.00	22.14	24,01		24.19		1.87	19.03	22.34	
r 1841.00	5yr 2yr	26.20	22.14	23,54		23.88		2,19	11.94	10.98	
er 1841.00	2)						36 36				
er 1834.00	100yr	50.60	22.08	24.74	24,01	24,86		1.66		42.91	
er 1834,00	50yr	48.30	22.08	24.42	23.72	24,59		1,87		27.30	
1834.00	20yr	42.00	22.06	24.25	23.59	24.42		1,88		22.19	
er 1834,00	10уг	38,70	22.08	24.13	23,52	24.31		1.92	4	20.17	ş
1 1834.00	5yr	35.00	22.08	23.98	23,44	24.16		2.00		17.28	<u> </u>
er 1834.00	2yr	26,20	22.08	23.62	23.23	23.82	0.005762	1.99	10,10	1	1
				 		3 10	1 1 1 1 1			565	
ar 1831.00 Z15 Creek Road	F	Bridge				-	1000			150	
	152	66.66	22.03	24.64		24.80	0.002165	1,81	34.90	29.63	
pt 1828.00	100yr	60,60 48,30	22.03	24.37	·	24,54	0.002703	1.84	·	27.98	
er 1828.00	50yr 20yr	42.00	22.03		7.64	24.37	4	1.83	23.67	16.76	
er 1626.00	10yr	38.70	22.03	24.10		24.27					
er 1828.00	5yr	35.00	22.03			24.12		1,88			
er 1828.00	2yr	26.20	22.03			23.78	÷	1.83	14.34	12.47	
			1,34%			100	7.0	2.04		22.90	
ir 1821.00	100yr	60.60	21.99		<u> </u>	24.78		2.01		22.18	
er 1821.00	50yr	48,30	21.99			24,52					
er 1821.00	20yr	42.00	21,99			24.35 24.24					
er 1821:00	10уг	38.70	21.99		<u> </u>	24.24	***************************************	4			
r 1821.00	5ут	35.00	21.99		36 1	23,75		4		4	
r 1821.00	2ут	26.20	21,99	£3.30		1	1				
100000	100yr	60.60	21.94	24,60		24,78	0.001970	1,75	34.84		
er 1615.00	50yr	48.30	21.94			24,48	·····	1,80			
Br 1815.00 er 1815.00	20yr	42.00	21.94	4		24.32					
er 1815.00 er 1815.00	10yr	38.70	21,94			24.22					***************************************
1815.00	5yr	35.00	21.94	23,90		24.06					
er 1815.00	27	26.20	21.94		. 34	23.71	0.003778	1.70	15.44		1
1,515.05	T I							<u> </u>	1-1	94.00	1
er 1808,00	100yr	60.60	21.89			24,73					Name and Address of the Owner, where
er 1808 00	50yr	48.30	21,89			24.48					4
er 1808.00	20w	42.00	21.89			24,30					~
er 1808.00	10yr	38,70	21.89		. 24	24.19					
or 1808.00	5yr	35.00	21.85		3	24.03					
et 1808.00	2yr	26.20	21.89	23.56		23,65	2 0,004072	9,00	1 12.40	1 3 3 3	
		1				24.72	0.00091	1.3	43.52	31,2	1
er 1802.00	100yr	60.60	21.84			24.44					
rer 1802.00	50yr	48.30 42.00	21.84			24,28					
rer 1802.00	20yr 10yr	38.70	21.84			24.17	***************************************		8 27.34		
er 1802:00				,			0.00175				- 4

Reach	en: Plan 05 River: Newnham River Sta	Reach: Lower (Profile	Continued) Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chol	Flow Area	Top Width	Froude # Chi
			(៣3/៩)	(m)	(m) 23.55	(m)	(m) 23,66	(m/m) 868200,0	(m/s) 1.51	(m2) 17.60	(m) 17,29	0,42
ower:	1802.00	2yr	26,23	21.84	23,35		23,00	0,002.003				
ower	1795.00	100yr	60.60	21.79	24.60		24.72	0.001141	1.48	.40.54 32.26	29.43 28,35	0.30
ower	1795.00	50yr	48.30	21,79	24.32 24.15		24.43 24.27	0.001482 0.001570	1,55		21,12	0.34
GWer	1795.00	2Dyr 10yr	42.00 \$8.70	21.79 21.79	24.15		24.16	0.001598	1,48	26,18	18,14	0,34
ower	1795.00 1795.00	5yr	35.00	21.79	23,69		24.00	0.001883	1.51	23.29	17,10	0.37
ower	1795.00	2yr	26,20	21.79	23.53	:	23.65	0.002489	1,49	17.68	14.86	9,41
	47ag go	100yr	68.70	21,76	24,22		24.67	0.006973	2.98	23.21	11.33	0.65
ower	1790.00 1790.00	50yr	58.40	21.76	23.97		24.39	0.007335	.2.87	20,33	10.93	0.67
ower	1790.00	20yr	52.00	21.76	23.84		24,22	0.007084	2.74 2.86	18.98	10.73	0.66
ower	1790.00	10уг	48.20	21.76 21.76	23.76 23.63		24,12 23,96	0.006963	2.54	16.79	10.41	0.54
DIVET	1790.00	Syr 2yr	42,60 31.30	21.76	23.35		23.61	0.006279	2.25	13,93	9.98	0,61
Ulyas.	1700.00	Ti e						0.00000	3.37	20.39	11,39	0.80
ower	1789.00	100yr	68.70	21.75	24.07 23.67	23.62	24.85 24.35	0.010250 0.014947	3.56	<u> </u>	10.63	0.95
ower.	1789.00 1789.00	50yr 20yr	58.40 52.00	21,75 21,75	23.49	23.49	24,18	0.016860	3,68		10,30	1.00
ower	1789.00	10yr	48.20	21.75	23.42	23.42	24,08	0.016856	3.59		10.17	1.00
wer	1789.00	5ут	42.60	21,75	23,31	23.31	23.92	0.017001	3,47	12.29 9.83	9.96 9.49	1.00
wer	1789.00	2yr	31.30	21.75	23.56	23.06	23.58	0,017751	3,12	3.001		
	1788.80	100yr	68.70	21.05	24.33	22.80	24.54	0.002323	1.99	34,51	11,92	0.37
ywer ywer	1788.80	50yr	58.40	21.05	24.01	22.62	24.20	0.002325	1,95	30.75	11.64	0.37
owe!	1788.80	20yr	52.00	21,05	23.79	22.51	23.96	0.002373	1.85 1.91	28,15 25.28	11.45 11.23	0.28
we:	1788.80	10yr	48.20 42.60	21.05 21.05	23.54 23.29	22,44	23.72 23.47	0.003023	1.89	22.54	11.02	0.42
we:	1788.80 1788.80	Syr 2yr	31.30	21.05	22.83	22,10	23.00	~~~~~~~~~~~~	1.78	17.61	10.63	0.44
+61	-	L'										<u> </u>
ywer .	1785,40, 215 Creek Road A		Bridge				<u> </u>					
or	178200	100yr	69.70	20.99	23,97		24.25	0,003569	2.32		10.76	0.45
wer wer	1782.00 1782.00	50yr	58.40	20.99	23.75		23.98	0.003276	2.15		10:64	0.43
wer	1782.00	20yr	52.00	20.99	23.57		23,79	0.003188	2.05		10,54	0.42
war :	1782.00	10yr	48,20	20.99	23.32 23.10		23.55 23.32	0.003748	2.09	The second secon	10.27	
SMB(1762.00 1762.00	Syr 2yr	42.60 31.30	20.99	22.69		22.88	0.004233	1,93		10,05	
W.R.C	1702.00	-7,										0.00
ower	1777.00	100yr	68,70	20.94	24,07		24.19	0.001407	1.51		20.49	0.32
ower	1777.00	50yr	58.40 52,00	20.94	23,83 23,64	·	23.93 23.74	0.001467	1,40		19.28	
awet.	1777.00	20yr 10yr	48.20	29.94	23.39		23.50		1,49		18.57	
ower ower	1777.00	5yr	42.60	20.94	23.15		23.27		1,52		17.92	·
ower.	1777.00	2yr	31.30	20,94	22.72		22,84	0.003049	1.53	20.47	15.59	0.44
		200 -	68.70	20.88	24.07		24.17	0.001218	1,41	48.59	21.52	0.30
WBF	1771.00 1771.00	100yr 50yr	58,40	20.88	23.83		23.92		1.34	43.43	20.91	
wer wer	1771.00	20yr	52.00	20.88	23.64		23.73		1.32		20.43	
JW91	1771.00	10yr	48.20	20.88	23,39		23.49		1,40		19.80 19.20	
wet	1771.00	5yr	42.60	20.88	23.15		23.26 22.82	0.002823	1,45		18.09	
rwes .	1771.00	2yr	31,30	20.05	42,77				100		. 134.4	
29981	1765.00	100yr	68.70	20.82	24.07		24.17		1.40		24,05	
wer.	1765.00	50yr	56,40	20.82	23.82		23.51	0,001152	1,34		22,59 21,45	·
ower	1765,00	20yr	52,00 48,20	20.82 20.82	23.53		23,48		1,41		19.92	
ower	1765.00 1765.00	10yr 5yr	42.60	20.82	23,14		23.24	0.001887	1,44		18,50	
ower	1785.00	2ут	31,30	20,82	22.70		22.80	0.002214	1.42	22.10	15.86	0.38
			200	00.70	24.07		24,15	0.000798	1,29	55.35	28.03	0.25
ower	1759.00	100yr	68.70 58.40	20.76	24.07	<u> </u>	23.90				27.73	0.26
ower ower	1759.00 1759.00	50yr 20yr	52.00	20.76	23.63	: .	23.71	0.000935	1.28		27,49	
ower	1759.00	10yr	48.20	20.75	23.37		23.47				26.14 17.97	
wat	1759.00	5yr	42.50	20.76 20.76	23,13		23.23 22.78	·	1.37		16,48	
ower	1759.00	2yr	31,38	20.76	20.00		1					
Taw	1753.00	100yr	80.65	20,18	23.35	23.11					14.45	
pwer	1753.00	50yr	69.60	20,18		22,90	23.84		3.53	<u>.</u>	12.90 11.71	
)Wef	1753.00	20yr	51.60 52.05	20,16 20.16			23.58				9:59	
ower ower	1753.00 1753.00	10yr 5yr	43.65	20,16	·		23.20	0.001110	2.75	15.85	9,28	
wet	1753.00	2yr	31.30	20.15	22.44		22.75	0.001099	2.50	12.53	8,54	0.66
				30.00	23,61	<u> </u>	23.97	0.000519	2.71	32.75	15,13	0,50
wer	1752,90 Dropstructure 3	100yr 50yr	80.65 69.60	19,62			23.75		·	30,09	15.02	0.46
ower ower	1752.90 Dropstructure 3 1752.90 Dropstructure 3	20yr	61,50	19.62	23.30		23.57	0,000451	2.35	28.09	14,51	
wer	1752.90 Dropstructure 3	10yr	52.05	19.62	23.12		23.35				13.65 12.85	
19Wit	1752,90 Dropstructure 3	Syr.	43,65	19.62		1	23.14				11.00	
)W81	1752.90 Dropstructure 3	2yr	31,30	19.62	26:56	<u> </u>	22.10	1 0,000000				
ower	1690:10	100yr	80.65	19.53	23.12	23.13					18,63	
ower	1690,10	50уг	69.60	19.53	22.98						17.98 17.44	
ower	1690.10	20уг	61.60	19,53							16.73	
ower	1690.10	10yr	52.05 43,65					·			15.81	
ower ower	1690.10 1690.10	5yr 2yr	31,30	19,53							6.22	1.90
U451	(530,10		0						ļ			
	The second of th	AND THE PERSON OF THE PERSON O	80.65	18,43	21.25	22.01	23.70	0.128608			9.1	
ower	1690.00	100yr 50yr				21,84	23.49	0.149266	6.91	10.07	6.70	1.80

Fraude # Chl	Top Width (m)	Flow Area (m2)	Vel Chril (m/s)	E.G. Slope	E.G. Elev	Crit W.S.	W.S. Elev (m)	Min Ch El	Continued) Q Total (m3/s)	Newsham Reach: Lower (a Profile	Pian: Plan 05 River: River S	Reach
1.91	5.88	7,50	6,94	0.185477	23,10	21.52	20.65	18.43	52,05	10yr	1690.00	ower
2.00	5.46 4.81	5.30 4.63	6.93	0,210066	22.88	21,33	20.43	18.43	43.55	5ут	1690.00	ower
	4,027	4,63	0.70	B.252358	22.44	20.82	20.11	18,43	31.39	2 ут	1690.00	DW8F
0.20	40.93	52.67	1.58	0.002423	22.97	21.63	22.85	18,46	80.65	100yr	1680.00	ower
0.2	40.40 30.87	46.15 38.21	1.61	0.002707	22,80	21,23	22.68	18,46	69.60	50yr	1650,00	ower
0.30	26.84	33,93	1.66	0.003215	22.58	21.08	22,45	18,45 18,45	61.60 52.05	20yr 10yr	1650.00	OWBC
0.39	16,02	24.52	1.81	0.005404	21,95	20.66	21.60	18.48	43.65	5yr	1660.00 1650.00	ower newo.
0,4	11.24	18.12	1.73	0.006684	21.50	20.36	21.35	18.45	31.30	2ут	1660.00	ower
0.5	24.87	38.49	3.04	0.000692	22.93	21,92	22.55	18,35	80.65	100.0	120202	
0,50	23,86	35.33	2.74	0.000584	22.77	21.78	22,46	18.35	69.60	100yr 50yr	1643,10	ower
0.5	22.93	30.22	2.81	0.000697	22,55	21,65	25.20	18:35	51.60	20yr	1643,10	ower
0.81	22,62	28.30 12.96	2.50 3.65	0.000574	22.40	21.44	22.12	18.35 18.35	52,05	10yr	1643.10	ower
1.00	6,22	8.53	3.67	0.002963	21.42	20.73	20.73	18.35	43.65 31.30	5yr 2yr	1843.10 1843.10	DWBC
0.2	26.09										, , , , , , , , , , , , , , , , , , ,	
0.23	25.22	49.67	1.45	0.001806	22.86	21,29	22,72	17.64	80.65		1543.00 Dropstro	ower
0.23	23.49	40.80	1.39	0.001899	22.48	20.94	22.36	17.64 17.64	69,60 61,60	The second section of the second seco	1643.00 Dropstru 1643.00 Dropstru	OWER
0.2	23.08	38.13	1.29	0.001683	22.34	20.73	22,25	17.54	52.05		1643.00 Dropstru	newor
0.3	14.58	22.76 14,69	2.16	0.005179	21,62	20.51	21,43	17.54	43.65		1643.00 Dropstru	OWE
		33,000	*.13	U.COECO.	21,013	20.03	20.76	17.64	31,30	ure 1 2yr	1643.00 Dropstru	.cwer
0.2	30.58	54.63	1,24	0.001313	22.83	21,23	22,70	17.59	80.65	topyr	1625.69	.awer
0.11	29.24 26.33	51.31	1.16	0.001196	22.69	21.04	22.59	17.59	69.60	50yr	1625.66	ower
0.19	25.60	41,43	1.13	0,001432	22.45	20,88	22.34	17.59 17.59	61,60 52,05	20yr	1625.68	ower
0.3	15.21	22.69	1.87	0,005174	21,53	20.47	21,34	17.59	43,65	10yr 5yr	1625.65	ower .ower
0.50	8.71	11.47	2.75	0.020546	20,77	19,97	20,38	17.59	31,30	2yr	1625.65	.ower
0.3	57.13	74.30	2.06	0,000222	22.78	21,31	22.64	4-7-16	00.00	120		
0.3	56.58	67.50	1.94	0,000222	22.65	21,13	22.52	17.48 17.48	92.60 80.80	100yr 50yr	1591.00 1591.00	awer awer
0.2	47,72	55,97	1,75	0,000180	22.41	20.84	22.30	17,48	.63,60	20yr	1591.00	ower.
0.4	42,80 19,33	50.80 22.47	1.64 2.25	0.000166	22.29	20,65	22.18	17.48	55.90	10yr	1591.00	awer
0,78	7.85	10.31	3.04	0.001760	20.61	20.32 19.87	20.14	17,48 17,48	44,70 31.30	5yr 2yr	1591,00	ower
											1551,00	ower)
									Bridge	Road B	1583.50 285 Cres	nswo
0.5	54,71	45,24	3.28	0.000796	22,14	21,72	21.72	17.45	92.60	100yr	1578,00	
0.8	17.64	24.39	4.05	0.001559	21.92	21,18	21,18	17.45	60.80	50yr	1576.00	iewo.
0.B 0.B	16.04	19.36	3.82	0.001543	21:58	20.88	20.88	17,45	63.60	20yr	1576.00	1ewo.
1.2	6.40	9,26	4,63	0.001841	21,39	20.68 20,30	20.68	17,45 17,45	55.90 44.70	10yr	1576.00	Oyer
1,19	5.81	7,42	4.22	0,004313	20.57	19,84	19.66	17.45	31.30	5уг 2ут	1576.00 1576.00	ower Temp
0.00	00.20											
0.3	85.30 76.19	69.91 60.02	1.73	0.001479	21,06		20.95	17.30	92.60	100yr	1526.60	76WO.
0.3	55.50	41,71	1.90	0.007357	20,70		20,83	17,30	63.60	50yr 20yr	1526,60	16WO.
0.43	46.20	33.78	1.99	0.002624	20.57		20.39	17,30	55.90	10yr	1526.50	ower ower
0.4	28.50	22.54	2,12	0.003608	20.32		20,10	17,30	44.70	5yr	1526,60	DYYBE
A	3,731	15.30	2.05	0.004412	19.80		19,58	17.30	31.30	2ут	1526.60	ower
0.39	79.89	57,09	1,92	0.002036	20.75		20.58	16,87	92.60	100yr	1411.00	ower
0,4	56.95 24.78	47.12	1,92	0,002188	20,61		20,43	16.87	80.80	50ут	1411,00	ower
0.3	18.11	35,79 33,66	1.50	0.002156	20.33		20.06	16.87 16.87	63.60 55.90	20yr	1411,00	ower
0,3	15.13	30.34	1.47	0.001591	19.97	7	19.85	16.87	44,70	10yr 5yr	1411,00	19wo.
0.3	13,41]	22,16	1.41	0.001866	19,39		19,29	16.87	31,30	5A.	1411.00	owar
0.1	99,02	129.84	0.61	0,000175	20.67	19.65	20.63	30.00	401 -			
0.1	94,58	115.88	28.0	0.000118	20.52	19,60	20.63	16.63 16.63	104.47 91,10	100yr 50yr	1365.00	.ower
0.1	58.37	.89.52	0.69	0.000275	20.23	18.68	20.19	16.63	71.80	20yr	1369.00	.ower .ower
0.1	85,47 76.24	78.33 60.18	0.72 0.84	0.000325	20.10	18.53	20.07	16.63	63.03	10yr	1366.00	awer
0.3	11,48	22.51	1.57	0.002069	19.87	18.29 17.97	19.83 19.15	16.63 16.63	50.40 35.27	5yi 2yi	1365.00	awer
									, , , , , , , , , , , , , , , , , , ,	-71	1000.00	18WQL
		, +							Culvert	Road.	1345.00 Newnhar	-ower
0.4	37.87	49.53	2.48	0.001899	20,37		20,09	16,11	104.47	100yr	1217.00	
0.6	31,79	33.43	2.97	0.003147	20.09		19.66	15,11	91,10	50yr	1317.00	ower Lower
5,8 3.6	10.60	20.12	3.57	0.006168	19,45		18.80	16,11	71.80	20yr	1317.00	Lower
8.0	9,85	15.02	3.50 3.35	0,006458	19.23		18.60	16.11 16.11	63.03 50,40	10yr	1317.00	Lower
9.7	9.15	12,58	2,80	0.005580	18.44	17.79	18.04	16.11	35.27	5yr 2yr	1317:00	Lower Lower
9.4												
0.4	21:40	49.98 43.75	2.49	0.000404	20,29 19,98		20.01	16.09	104,47	100yr	1282.00	Lower
0.5	17.79	28.79	2.72	0.000444	19.22		19.58	16.09 16.09	91,10 71,80	50yr 20yr	1282.00	Lower
0.5	17,75	25,06	2,64	0.000767	18.99		18.64	16:09	63.83	10yr	1282.00	Lower Lower
0.5 0.5	9,71 9,50	20.66	2.44	0,000748	18.63		18.33	16.09	50.40	5yr	1282.00	Lawer
9.3	8.00	15,76	2.24	0.000810	18.07		17.82	16.09	35.27	2yr	1282.00	Lower
0.2	50.72	72.69	1.67	0.000149	20.21	17.98	20.08	15,90	104,47	100yr	1253.00	- Court
0.3	. 34.98	57,49	1.69	0.000174	19.88	17.80	19.74	15,90	91,10	50ýr	1253.00	Lower Lower
0.3	16.20 15.59	39,78 36,42	1.81	0.000274	19.10	17.53	18.94	15,90	71.80	20yr	1253.00	Lower
کنۍ ن	15.02	36,421	1.73	0.000269	18.88	17.41 17.21	18.72	15.90 15.90	63.03 50.40	1Dyr 5yr	1253.00 1253.00	Lower
0,3												Lower

HEC-RAS PI Reach	lan; Plan 05 Hiver; Newnham River Sta	Reach: Lower (Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev (m)	E.G. Slope (m/m)	Vel Chnt (m/s)	Flow Area (m2)	Top Width (m)	Froude # Chi
			(m3/s)	(m)	007		2000 Q P 7 (200)					
Lower	1248.00 Bunnings Warehou	+	Bridge									
Lower	1243.00	100yr	104.47	15,89	19.69	18.29	20.05	0.000527 0.000586	2.68 2.67	39.03 34.10	11.74 11.73	0.47 0.50
Lawer	1243.00 1243.00	50yr 20yr	91.10 71.80	15.69 15.89	19.27	18.09 17.78	19.63 19.04		2.52	27,44	11.44	0.54
Lower Lower	1243.00	10yr	63.03	15.89	18.51	17,63	18.82	0.000642	2,48		11,10	0.52 0.50
Lower	1243.00	5yr	50.40 35.27	15.89 15.89	18,23 17,73	17.40 17.08	18.49 17.95		2.26 2.06	22.31 17.10	10.81 10.28	0.51
Lower	1243.00	2yr	33.27	(4,53								
Lawer	1219.00	100yr	104.47	15.72	19.73 19.22	18.12 17,92	20,01 19,51	0.000421	2.45 2.78	51.43 32.89	36,00 12.25	0.40 0.49
Lower Lower	1219.00 1219.00	50yr 20yr	91.10 71.80	15.72 15,72	18.67	17.61	19.02		2.63	27,30	9.81	0.50
Lower.	1219.00	10yr	63.03	15,72	18.49	17,45	18.80	0.000633	2,46	25.59 22.95	9.75 9.66	0.49 0.45
Lower	1219.00 1219.00	5yr 2yr	50.40 35.27	15.72 15.72	18,22 17,74	17,22 16,90	18,47 17,93	0,000552	1.53	18.31	9,49	0.44
Lower .	12 19,00	-yı									95.04	.0,37
Lower	1190.00	100yr	91.19	15.60 15.60	19.75 19.23		59.91 88.91	0.000354	2.29	55.48 36.92	35.01 33.35	0.37
Lower	1190.00	50yr 20yr	71,80	15.60	18.67		18.99	0.000602	2.51	28.58	9,84	0,47
Lower	1190,00	10yr	63.03	15,60	18.50		18,78		2.35	26.86	9.78 9.68	0.45 0.42
Lower	1190.00 1190.00	5yr 2yr	50.40 35.27	15.60 15.60	18.22 17.74		18,45 17,91		1.80		9.52	0.40
CONE	115460	1							4.70	00.00	30.07	0.31
Lower	1164,00	100yr	194.47	15.44	19.79 19.30	17.82 17.62	19.95 19.53		1,98 2.23	66.69 48.63	36.67 36,66	0.37
Lower Lower	1164,00 1164,00	50yr 20yr	91.10 71.80	15,44	18.70	17.82	18.96	0.000451	2.29	32,23	12,91	0,42
Lower	1164,00	10yr	63.03	15,44	18.52	17.15	18,75		2.15 1.92	29.88	12.88 11.52	0.40
Lower	1164.00 1164.00	5yr 2yr	50.40 35.27	15.44 15.44	18.24 17,75	16,92	18.42 17.89	0.000376	1.64	21.48	9,75	0.35
Lower	1184.00	2,91										, in the second
Lower	1160.00 Bunnings Warehou		Bridge									
Lower	1156.00	100yr	104.47	15.44	19,49		19.73		2.30	55.68	36.68	0.37
Lower	1156.00	50yr	91.10	15,44	19,25		19.50		2.29		36.66 12.90	0.38 0.42
Lower	1156.00	20yr	71.80 63.03	15,44 15,44	18.66 13.49		18.93 18,73		2,17	29.54	12.88	D.41
Lower	1156,00 1156,00	10yr 5yr	50.40	15.44	18.22		18,41	0,000383	1,93	26.13	10.82	0.38
Lower	1156.00	2yr	35.27	15.44	17.74	.,	17.88	0,000334	1,65	21.38	9,75	0.36
Lower	1147.00	100yr	104.47	15.39	19.29		19,68	0,000621	2,87	43.58	36.00	0.48
Lower	1147.00	50yr	91.10	15.39	19,02		19.44		2.90		31.41 9.07	0.51 0.51
Lower	1147,00	20yr	71,80	15.39 15.39	18.52 18.37		18.90		2.74	25,24 24,98	9.01	0.48
Lower	1147.00 1147.00	10yr 5yr	63.03 50.40	15.39	18.14		18.39		2.20	22.89	8,92	
Lower	1147,00	2yr	35.27	15,39	17.68		17.86	0.000452	1.67	18.85	8.72	.0.41
	2407.00	1000	104.47	15,33	19,33	17,73	19,63	0.000452	2,55	48.54	36.00	0.42
Lower	1135.00 1135.00	100yr 50yr	91.10	15.33	19.06	17,52	19.38	0.000499	2,55	38,93	35.21	8.43
Lower	1135.00	20yr	71,80	15.33	18,55	17.21	16.84		2.39	30.06 28.62	9.89 9.84	0,44
Lower	1135.00	10yr	50,40	15,33 15,33	18.41 18.17	17,05 16,82	18.95 18.35		2.20 1.92	25.27	9.76	0.37
Lower	1135,00 1135,00	5yr 2yr	35,27	15.33	17,70	15,50	17.84		1,62	- 21,77	9,50	0,34
			Bridge							<u> </u>		
Lower	1130,00 Bunnings Warehou		3,34									2 years
Lower	1127.00	100yr	104,47	15.33	19.02		19,47 19,22	0,000698	2.99 2.78	35.80 32.98	15.38 13,21	0,51
Lower	1127.00 1127.00	50yr 20yr	91,10	15,33 15,33	18,82	:	18,84	0.000525	2,39	30.01	88.0	0.44
Lower	1127,00	10yr	63.03	15,33	18.40		18,65	0.000464	2.21	28.58	9,84	0.41
Lower	1127,00	5yr	50,40	15.33 15.33	18.16		18.35 17.83	0,000378	1,92	26.23 21.75	9.75 9.60	0.34
Lower	1127.00	2yr	35.27	13,30	17.70		17,200	1.46.3				
Lower	1125.00	100yr	104.47	15.24	19.06	18.01	19.43	0.003631	2.74		31.02 25.62	0.51
Lower	1125.00	50yr	91,10 71,80	15.24 15.24	18.84 18.55	17.82 17.52	19.19 18.83	(2.33		15.95	0.48
Lower	1125.00 1125.00	20yr 10yr	63.03	15.24	18.40	17,37	18.65		2.19	29.53	15.59	0,46
Lower	1125.00	5yr	50.40	15.24	18,14	17.14			1.99		14,98 11.38	0.44
Lower	1125,00	2yr	35.27	15.24	17,65	15,82	17,82	0.003000	1.50	1 10.01	11.00	
Lower	1099,00	100yr	104.47	14.60		18.24	19.18		3.75		15.18	0.84
Lower	1099.00	50yr.	91.10	14.80		18,05	18,98	***************************************	3.41 2.95	26.82 24.24	14.66	0.78
Lower	1099.00	20yr 10yr	71.80 53.03	14.80 14.80	18.20 18.10	17.76	18.65 18.48		2.77		13,15	0.67
Lower	1099.00	5yr	50.40	14.80	17.87	17.35	18,20	0.005718	2.53	19.94	12,53	0.64
Lower	1099,00	2yr	35,27	14,80	17,14	17,03	17.60	0,013958	3,01	11.73	9,62	0.88
Lower	1066.00	100yr	104.47	14.52	18.49	17.44	18.75					
Lower	1065.00	50yr	91.10	14.52	18.39	17:28	18.61		- 2.07		31.27	
Lower	1065.00	20yr	71.80	14.52 14.52		17.03 16.89	18.35		1,80		25.34 20.99	
Lower	1066.00	10yr 5yr	63.03 50.40	14.52	·	16.66	17.95	0.001878	1,51	33.30	18.24	0.36
Lower	1066,00	2y:	35.27	14.52		16.33	17.13	0.004515	1,58	18.77	14.43	0,53
	4047.00	100yr	104.47	14,36	18.57	16,27	18.61	0,000412	1.05	114:83	109.06	0.18
Lower	1047.00	50yr	91.10	14.36		16,12	18,49	0,000396	1.01	105.71	103.20	0.17
Lower	1047.00	20yr	71.80	14,36	18.23	15.88	18.27		0.97		92.78 86.16	0.17
Lower	1047.00	10yr	63.03 50.40	14.36 14.36		15.76 15.58				+	73.58	
\$5, resters account growth	1047.00	5yr					17.02				15,71	
Lower	1047.00	2γτ	35.27	14.36	16.97	15.34	17.04	4.2001 OF	1,000	3 63,10		

Reach	River Sta	Reach: Lower (Profile	O Total (m3/s)	Min Ch El (m)	W.S. Elev (π)	Crit W.S. (m)	E.G. Elev (m)	E.G. Slope (m/m)	Vel Chnl (m/s)	Flow Area (m2)	Top Width (m)	Froude # Chl
Lower	1029,00 Devlan Street		Culven				4					
				40.03	17,47	15.67	17.60	0.001045	1,64	69.85	48.79	0.29
Lower Lower	1013.00	100yr 50yr	104.47 91.10	13,37 13,37	17.36	15.52	17.47	0.000918	1,50	95.04	39.80	0.27
Lower	1013.00	20уг	71,80	13.37	17,16	15.29	17,24	0.000746	1.29	57.98	32.23	0.24
Lower	1013,00	10yr	63.03		17.05	15.18 15.01	17.12 16.90	0.000667 0.000564	1.19 1.04	.54,63 49,23	28.96 23.93	0.21
Lower Lower	1013.00	5уг 2уг	50.40 35.27	13.37 13.37	15.84 15.33	14.78	16.37	0,000581	0.92	38,44	18:73	
LUWEI	101925						1					
Lower	982.00	100yr	104,47	12.82	17,43	16.37	17.55 17.42	0.001202	1,65 1,59	71.01 64.81	83.48 71.21	0,31
Lower	982.00 982.00	50yr 20yr	91.10 71.80	12.62	17.31 17.11	15.97 15.69	17.21	0.001138	1,49	54.70	49.83	0.29
Lower Lower	982.00	10yr	63.03		17.00	15.51	17,09	0.001069	1,40	49,80	39.88	0.28
Lower	982.00	5yr	50,40		16.79	15.26	15.87	0.001021	1,35	42,27 27,10	32.87 21.70	0,27
Lower	982.00	2yr	35,27	12.82	16.24	14.91	16,33	0.001407	1.34	27.10	21.00	1
Lower	959,00 Access Road	+	Culvert									
				1			47.00	0,000368	1.00	98,10	64,51	0.16
Lawer	948.00	100yr 50yr	104,47 91,10	12.37 12.37	17,02 16.89	14.31	17.08 16.95	0.000355	0.96	91,18	58.22	0.15
Lower Lower	948.00 948.00	20yr	71.80	12.37	16.67	13.91	16,71	0.000339	0.90	79.78	51.06	0.15
Lower	948.00	10уг	63.03	12.37	16.54	13.80	16.58	0.000334	88.0	73.63	46.98 39.10	0.14
Lower	948.00	5уг	50,40	12.37	16.30 15.68	13.57 13.32	16.34 15.72	0.000322	0.82	63.39 45.25	19.36	0.15
Lower	948.DO	2yr	35.27	12.37	13.64	10.00	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,					
Lower	934.00 Secam Streat		Cuivert									<u> </u>
	240.00	100	11000	12.30	16.40	14.75	16.59	0,000203	2.11	76.58	36.04	6.34
Lower Lower	918.00 918.00	100yr 50yr	116,33 101,40		16.26	14.55	16.42	0,000181	1.94	71.50	35.05	0.32
Lower	918.00	20yr	79.90	12,35	16.03	14,27	16,15	0.000148	1.68	53.54	33,44	0.29
Lower	918.00	10yr	70.17	12.30 12.30	15.90 15.71	14,13	16.01 15.79	0.000133	1.55 1,35	59.49 53.17	32,60	0.27
Lower Lower	918.00 918.00	Syr 2yr	56.10 39.23	12.30	15,36	13,62	15.42	0.000086	1,11	43.03	27.78	0.21
LUNCI	31049	-7,									45.00	0.10
Lower	905,00	100yr	116.33	12,30	15,47	13.94 13.81	16.53 16.37	0.000055	1,20	129.87 123.11	45.20 44.31	0.19
Lower	905,00	50yr 20yr	101,40 79,90	12:30 12:30	16.31 15.07	13.59	16.11	0.000038	0,94	112.45	42.86	0.15
Lower Lower	905.00	1Dyr	70,17	12,30	15,94	13.48	15.97	0,000033	0.86	107.01	42,10	
Lower	905.90	5yr	56,10	12.30	15.74	13.29	15.76	0.000027	0,74	98,48 84,48	40.88 38.79	0.13 0.11
Lower	905.00	2γτ	39.23	12.30	15.38	13.08	15,40	0.000020	0,03	S-C-ND		•
Lower	904.90	100yr	116.33	10.60	16,49		16.52	0,000615	D.8G	217,45	64.20	0.11
Lower	904.90	50yr	101,40		16.34		16,36	0,000012	0,70	208.34 194.79	54.08 53.39	0.09
Lower	904.90	20yr	79.90 70.17		15.09 15.96		16,10 15,97	800000,0	0,58 0,53	187.90	52,34	0.07
Lower Lower	904.90	10yr 5yr	56,10	·	15.75		15.76	0.000006	0.44	177,09	51.02	0.00
Lower	904.90	2ут	39.23	10.60	15.39		15,40	0.000004	0.34	159,35	48.92	0.05
				10.40	16.44	12.62	16.51	0.000068	1,31	120.44	41.11	0.17
Lower	879.00 879.00	100yr 50yr	115.33 101.40			12.44	16.35	0.000058	1,19	114.46	40.22	0.16
Lower Lower	879.00	20yr	79.90	10.40		12.15	16,10	0.000044	1,01	105.07	38.75	
Lower	879,00	1Dyr.	70.17	10,40	15,93	12.01	15.96	0.000038	0.92	100.27 92.70	38.00 37.07	0.13
Lower	879.00	Syr 2yr	56,10 39,23	10.40 10.40	15.73 15.38	11.50	15.75 15.40	0.000019	0.61	80.11	35.39	0.09
Lower	879.00	Zyi	35,25	10.10	10.00							
Lower	871.00 SQID Trash Rack		Ini Struct							-		
		100yr	118.33	11.40	16,36		15,45	0.000216	2.09	98.93	40.64	0.32
Lower	870.00 870.00	50yr	101,40		16.22		16.31	0.000194	1.94	93.21	40.04	0.30
Lower	870.00	20уг	79,90				16.06	0,000150	1.70 1.58	84.12 79.52	39.12 38.73	0.27
Lower	870.00	10yr	70,17		15.87 15.67		15.93 15.72	0.000145	1.40	72.00	38:27	0.24
Lower	870,00 870,00	2yr	56,10 39.23	4	10,00		15.37	0.000104	1,21	58.95	37.03	0.21
~27.01									7 9.4	2272.20	20.20	D.18
Lower.	845.00	100yr	116,33		16.32 16.18		16.37 16.23	0.005282	1,08	117.42 111.05	46,1S 45.62	0.18
Lower Lower	845.00 845.00	50yr 20yr	101,40 79,90	·	15.16		15.99	0,003995	88.0	100,91	44,76	0.16
Lower	845.00	10yr	70.17	11.28	15.84		15.87	0.003622	0.81	95.76	44,32	
Lower	845.00	5ут	56.10				15.67 15.32	0.003066	0.72 0.61	87.35 72.65	43.59 42.28	
Lower	845,00	2yı	39.23	11.28	15.31		10,02	4.002003	0,01	12.00		
Lower	798.00	100yr	116,33				16,04	0.005421	1.06		62,42	
Lower	798.00	50yr	101,40		15.88		15.93 15.74	0.005902	1,00	112.04 101.19	62.19 61.77	
Lower	798.00 798.00	20yr 10yr	79.90 70.17				15.64	0.004746	0.84	95.44	61.53	0,16
Lower Lower	798.00	5yr	56.10		15,46		15,48	0.004242	0.77	85.82	61,12	
Lower	798.00	2ут	39.23		15,14		15.16	0.004337	0.71	56.65	58.61	0,15
	775.00	100yr	116,33	10.98	15.75	13.16	15,80	0.005699	1.10	120,83	104,49	0.18
Lower	759.00 759.00	50yr	101.40		15.67	12:97	15:71	0.004987	1.01	122,27	91,78	
Lower	759.00	20yr	79.90	10.98	15.53	12,69		0.003995	65,0	110.22	81.67	
Lower	759.00	10yr	70,17			12.56 12.34		0.003541	0.82 0.72	103,89 93,71	77.89 73.64	
Lower	759.00 759.00	5yr 2yr	56,10 39,23			12.07		0,002320	0.67	59,08	60.47	
Lower	, 33.60	-7										ļ
Lower	749.00 Unlarmed Road		Culven	ļ	<u> </u>		ļ	-				
	1735 nn	100yr	116.33	10.89	14,74		14,83	0.017294	1,36	89.91	69.02	0.30
	735.00		101,40				14,72	0.016947	1.33		67,26	
Lawer	735.00	50yr	101770				14.53	0.015390	1,24	70.95	62,43	0.28

	Plan: Plan 05 River: Newnhar Fiver Sta	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chril	Flow Area	Top Width	Froude # Chl
Reach	rimer ora	1 ,,,,,,,,,,,	(m3/s)	(m)	(m)	(m)	{m}	(m/m)	(m/s)	(m2)	(m)	
VA. 407434.000	707.00	5yr	56.10	10.89	14,19		14,25	0,012506	1.11	55.56	53.89	
OWer	735.00 735.00	2yr	39.23	10.89	13,90		13.94	0.009304	86.0	41,96	34,68	0.2
ovres .	1733.00	- 12										
ower	621.00	100yr	128,20	10.44	13.51		13.56	0.902764	0,60	142,28	84,90	
- N. C.	521.00	50yr	111.70	10,44	13.38		13.43	0.002648	0.57	131.31	84.09	0.13
ower :	621.00	20уг	88,00		13.18		13.22	0.002559	0.53	114,22	82.82	0.1
Lower	621.00	10vr	77.30		13.08		13.11	0.002529	0.51	105.64	81,98	0.1
_ower	621,00	5yr	61.80	10.44	12.91		12.94	0.002494	0.48	92.10	80.21	0.1
_ower	621.00	2yr	43.20	10.44	12.68		12.70	0,002469	0.44	73.82	77,75	0,1
Ziwej.	UZ.100											
Lower	498,00	100yr	128.20	9.52	12.62		12,90	0.009273	1.11	105.04	69.40	
_ower	498.00	50yr	111.79	9.52	12.70		12.76	0.009287	1,07	97.47	67.94	
Lower	498.00	20yr	00.88	9.52	12.51		12.56	0.009170				
Lower	498.00	10yr	77.30	9.52	12.41		12.46			78.41	64.21	
Lower	498.00	5ут	61.60	9,52	12.25		12.29	0.008948			61.63	
CWef	498.00	2yr	43.20	9.52	12.03		12.05	0.008856	0.85	55.11	57.93	0.2
												0.1
Lower	300.00	100yr	128.20	6.90	11,42	9,92		0.002093		157.09	76,90	
Lower	300.00	50yr	111.70	8.90	11.09	9.85	11,13	0.002711	0.63	132.13	74.54	<u></u>
Lawer	300.00	20yr	88.00	6,90	10,83			0.002742	0.59	112.95	72.84	
ower	300.00	10γε	77.30	6.90			10.50			93,54	71.07 67.29	0.1
ower	300.00	5yr	61,80	6.90	10.09				0.87	60.91		\$
		Commence of the Commence of th	4		40.00	0.40	1 12	6.004403	8.61	60.91	57.29	

Appendix I2

HECRAS Model Results for Philips Creek



HEC-RAS RESULTS

Reach	River Sta	River: Phillips Reach Profits	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chol	Flow Area		Froude # Ch
			(m3/s)	(m)	(m)	(m)	(m)	(m/m)	(m/s)	(m2)	(m)	
er	1580 1580	Q2	30.50	15.12	17,71	16,89	17.88	0;005288	1.82	16.80	10.25	0. 0.
er	1580 1580	O5	44,10	15,12	18.34	17.23	18,51	0.004117	1.84	24.83	29,13 47,86	0.
er .	1580 1580	Q10	53.50	15.12	18.70	17,44	16.68	0.003552	1,87	30.39	54,09	0.
er	1580 1580	C)20	65.40	15.12	19.03	17.67	19.23	0,003602	1,97	35.58 41.76	62.55	0.
Gt.	1580 1580	Q50	85,10	15,12	19,38	18.03	19.63	0.003919	2.23 2.41		68.63	0.
er	1580 1580	Q100	99,40	15.12	19.59	18.28	19,88	0,004172	2.41	42.40	66,001	
	1		62.50	16.17	17.50	16.69	17.62	0,003981	1,54	19.78	13.41	0
er.	1533 1533	Q2	30.50	15.17	18,24	16.98	18.34	0.002005	1.42	39,40	55,17	0
ar .	1533 1533	05	44.10	15.17 15.17	18.64	17,15	18,74	0.001549	1.40	53.81	59.36	0
er	1533 1533	Q10	53,50	15.17	18,99	17,35	19.09	0.001410	1.45	66.73	63.03	0
er	1533 1533	O20	65.40	15.17	19,36	17.64	19.47	0.001514	1,62	80.16	68.95	0
ec	1533 1533	Q50	85.10 99.40	15.17	19,57	17.87	19,71	0,001613	1,75	85.19	85.71	
96	1533 1533	Q100	99.401	(3,17	13,37	17.01	- Factor C	3,000,000			1 1 1 1 1 1	
		IO2	30.50	14,82	17.38	16,12	17.44	0.001324	1.05	38.94	39.31	
91	1464 1464 1464 1464	Q5	44.10	14.82	18.22	16.38	18.25	0,000581	0.87	82,76	83.39	
91	1464 1464 1464 1464	010	53.50	14.82	18.64	16.54	18.66	0.000440	0.83		90.51	
er .	1454 1464	Q20	65.40	14.82	19.00	16,74	19.02	0.000395	0.85	130,46	95.91	
er	1454 1464	Q50	85.10	14,82	19.37	17,12	19,40	0.000420	0.93	153.51	111.19	
er	1454 1464	Q100	99.40	14.62	19,59	17.34	19.62	0.000445	1.00	167.33	120,36	. (
अर	1404 1404	4766										
	1396	02	30.50	14.77	17.23	15.95	17,31	0.002105	1.28	24,02	14.40	
er er	1396	O5	44.10	14,77	18.12	18.24	18.19	0.001151	1.20		70.33	
er er	1396	010	52.50	14,77	18.54	15.42	18,61	0.000973	1.21		80.28	
r	1398	Q20	65.40	14.77	18.89	15.53	18.97	0.000967	1.30		89.39	
er	1399	Q50	85.10	14,77	19.24	15.95	19.34	8.001140	1,50		98.69	
9f	1398	Q100	99.40	14.77	19.44	17,17	19.56	0.001279	1,54	89.76	104.04	<u></u>
	1											يسبن
er.	1387 Anzac Road		Gulvert							<u> </u>		سنبسب
	13.											<u> </u>
er.	1377	C2	30.60	14.64	16.63	15.58	16.89	0,001584	1,11		15,21]	
ır	1377	Q5	45.20	14.64	17.27	15.85	17,35	0.002013	1,29	34,99	21.75	
r	1377	010	54,30	14,64	17.46	16.00	17.56	0,002200	1,41	39,06	53.75	
ır	1377	O20	66,00	14,64	17.66	16.17	17.78	0,002365	1,56	43.95	73.98	
r	1377	Q50	66.40	14.64	17,97	16,45	18,13	0.002500	1.78	52.77	94,30	
er .	1377	Q100	101.00	14.64	18.17	16,64	18,35	0.002724	1,91	59.30	100.58	
				1.						50.70	53.11	
r	1329 1329	02	30.60	13.89	16.70	15.56	16.78	0.002557	1.24	26.07 52.19	118.42	(
ď	1329 1329	Q5	45.20	13,89	17,17	15,89	17.23	0.001618	1.18	64.35	124.41	
91	1329 1329	Q10	54,30	13,89	17.37	16.06	17.42	0.001455	1.19	77.86	131.04	
er .	1329 1329	Q20	66.00	13,89	17,58	16.27	17.64	0.001333	1,26		140.25	
τ	1329 1329	Q50	85.40	13.69	17,91	16.84	17,97 18,18	0.001257	1,30		144,09	. : (
r	1329 1329	Q100	101.00	13.89	18.12	16.99	10,10	0,007 (27	1,00	11,12,70		
				1 1 2 2 2	40.40	15.27	16.27	0.004457	1.59	18.12	10.29	- (
er .	1246	CX	30,50	14.16	18.12	15.58	16.85	0.002286	1,40		93,34	(
er .	1246	Q5	45,20	14,16	15.77	15,75	17.07	0.001862	1.32		94.87	(
15	1246	Q1D	54.30	14.16	17.08	15,95	17.30	0,001619	1.29		97.44	(
ŗ.	1246	O20	86.00	14,15	17,24	16.68	17.67	0,001013	1.28	·	105.33	(
er .	1245	Q50	101,00	14,18	17.60 17.83	16.78	17.90	0.001220	1.29		110.37	. (
r	1245	Q100	101,00	14,10	11,63	10.10	77.20	0.231823				
	<u> </u>		Calcad									
r	1234 Gallipoli Ro	ad .	Culvert									49.1
		56	30.00	13.96	15.74	14.88	15.84	0.003315	1:42	21.49	13.42	
er .	1222	02	30.60 45.20	13.96	16.05	15.14	15.22	0.004165	1,74	25.97	13.97	
ir.	1222	Q5	54,30	13.96	16.24	15.29	15,43	0.004630	1,91	28,46	14,36	
ετ .	1222	Q10 Q20	66.00	13.96	15.46	15,47	16,68	0.005091	2.09		15.00	
ır	1222	Q20 Q50	86.40	13.96	16.87	15.75	17.09	0.004598	2.17		85,67	
ır	1222	Q100	101.00	13.96	17.14	15.94	17,37	0.004251	2.21	56,40	58,18	
<u>r</u>	1446	4.00		,0.00			6.4	30				
er	1130 1130	Q2	30.60	12.59	. 14.54	14.23	14,86	0.008797	1,79		44,88	
A	1130 1130	Q5	45,20	12.59	14,90	14,43	14.99	0.005970	1.67	42.91	53,13	
r r	1130 1130	010	54,30	12.59		14.52	15,13	0.005570	1,69		55,96	
i i	1130 1130	Q20	66.00	12.59		14.75	15.28	0,005501	1.74		58.53	
, T	1130 1130	Q50	86.40	12,59		14,88	15.50	0.005420	1:83		62.57	
r	1130 1130	0100	101.00	12.59	15.53	14,95	15.64	0.005359	1.88	80.44	64.11	
			11 3					1,5				
er.	1066 1086	Q2	30,60	11.63	13,99	13.23	14,08	0.003989	1.42		24,05	
er.	1066 1066	05	45.20	11.63		13.54	14,46	0.003992	1.59		42.40	
er	1066 1066	Q10	54.30	11.63		13.69	14,85	0.004403	<u> </u>		65:56	
er	1066 1066	Q20	56.00	11,63		13.85	14.65	0.003920			76,41	
er	1086 1086	Ω50	89,40	11.53		14.08	15,12	0.003430			89.19	
er:	1066 1066	0100	101,00	11.53	15.15	14.28	15,28	0.003306	1,89	.97,44	91,81	<u> </u>
										ļ		
er	966 966	022	30.60	11,20	13.44	.12.81	13.56	0.004657	1.53		15.62	
er	968 968	Q5	45.20	11.20	13,72	13.06		0,005529			45.47	1
er	965 969	010	54.30	11:20	13.86	13.20		0.006017			62.16	
er	966 986	Q20	66.00	11.20	14.00	13,37	14.23	0,006451	2.15		77.28	
er	966 956	Q50	85.40	11,20		13.67	14.48	0.006423			89.16	
a compression	965 966	Q100	101.00	11.20	14.39	14,00	14.64	0,005210	2,40	60.65	91.21	<u></u>
er												

HEC-RAS RESULTS (CONTINUED)

Reach	EUILMRC_WWC F	Profile	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Stope	Vel Chr.l	Flow Area	Top Width	Fraude # Ch
Heach	niyer dia	1,074	(m3/s)	(m)	(m)	(m)	(m)	(m/m)	(m/s)	(m2)	(m)	
	G1 861	Q5	45.20	10,57	13.41	12.32	13.44	0.001597	1.01	66.55	67.82	Ü.
		Q10	54.30	10.67	13.58	12.42	13.61	0.001559	1.07	80.12	70,19	0.
	51 851		65.00	10.67	13,76	12.53	13.80	0.001539	1.14	93.32	72.12	0.
	61 861	O20		10.67	14.04	12.62	14.09	0.001540	1.25	113.93	75,93	0.
The second second	61 861	O50	86,40	10.67	14.22	12.98	14.27	0.001559	1.32		76.77	0.
ipar 8	161 861	0100	101.00	10,07	19.55	12.00	4 1750				130 to 100	9.5
*					10.50	14.00	12.47	0.004849	1.89	24.05	45,08	0.
per 7	18 718	O2.	31,80	9.94	12.30	11.60		0,005556	2,22	35.19	50.28	0.
per 7	18 710	Q5	46.70	9.94	12.56	11.92	12.77		2,39	41,10	52.23	0.
	18 718	010	56.30	9.94	12.69	12.29	12.93	0.005970			54.48	0.
	18 718	C/20	68.60	9,94	12.84	12.53	13,11	0,006417	2.59	48.02		0.
	18 718	O50	89.90	9.94	13.07	12.77	13.33	0.007042	2.89	59.47	61.06	
The second second second	18 718	Q100	105,00	9.94	13.21	12.90	13.55	0.007314	3,06	67.68	66.05	0
per 7	10 710	47.7				1. 150	in the	3.55			/NW	
	54 554	02	31.80	9,49	11.42	10.90	11,59	0,006236	1.61	22.30	44.72	0
		OS	46.70	9,49	11.69	11.20	11,86	0.005872	1.97	36,74	54.29	0
	554 554					11.54	12.01	0,005629	2.05	44.72	55.58	0
	54 554	010	56.30	9,49		11.67	12.18	0.005368	2.13	54,24	57,07	
ier S	54 554	020	68.60	9.49	12.00			0.005160	2.26		59.33	0
ser 5	54 554	050	89,90	9,49	12.25	11.85	12.44		2.36	77,85	62,04	0
er 5	54 554	Q100	105.00	9,49	12,40	11,96	12.60	0,005147	2.30	(1,031	02.57	
i i			1 1 1					-يىنىنى			E3 F4	
er 4	117 417	O2	34.10	8.15	10.98	10.13	11,05	0.002578	1,43		57.51	
	117 417	O5	49.90	8.15	11.25	10.66	11,34	0.002855	1,64	61.04	62.52	
	117 417	010	60.20	8.15		10.79	11,50	0.002916	1.73	70.67	- 64.28	
A THE RESIDENCE OF THE PARTY OF		020	73.80	8.15		10.93	11.68	0.003079	1.86	81.40	66,13	1
	117 417	O50	96.80	8,15		11.13	11,93	0.003331	2.06	97.48	68.85	
	117 417		113.00	8.15		11.27	12.07	0.003614	2,21	106,32	70,30	
er 4	117 417	Q100	. 113,00	B. (5	11,00	11.2						
					ļ		10,72	0.021631	2.93	17,91	33.83	
er 3	174 374	02	34.10	8.20					3.10	***************************************	40.85	
	374 374	05	49.90	8.20			10,98				47.84	
	374 374	Q10	60.20	8.20		10.71	11,13	0.019048	3.28	,	57.63	2
	374 374	Q20	73.80	8.20	. 10.88		11.30		3.38			
	374 374	C50	95.80	8.20	11.08	11.08	11.53	0.017048	3.53		69,00	
	174 374	Q100	113.00	8.20	11.24		11.67	0,015152	3,63	66.00	77.70	1
er 2	274 374	u ioc										<u> </u>
		02	34.10	8.26	10.09	9.88	10.20	0,005635	1,72	34.58	64.02	
	128 328		49,90	8,26		10.05	10,45	0,004723	1,75	51.64	65.78]
A second control of	328 328		60.20	8.26			10,59	0.004436	1.80		66.85	
	328 325	010					10.78		1,83	73.92	68.13	
	328 328	C)20	73.80	8.26			11.09		1.86	95.14	70,76	
or 3	328 328	Q50	96.80	8.26		10.37			1.82	113.53	74.73	İ
er S	328 328	Q100	113.00	8.26	11.24	10,45	11.33	0.002037	1.04	73020		
			1 5 A		:	1		<u> </u>		00.00	21,92	
er 2	214 214	02	34,10	5.80	9.13	8.51	9.25					
	214 214	Q5	49,90	5.80	9.59	8.76	9,72			35.23	28.89	
	214 214	Q10	60.20	08.8	9.82	8.90	9,97	0.003288	1.76	42,55	33.20	
	214 214	020	73.80	6.80		9.07	10,25	0.003155	1.87	52.00	38,45	
,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		Q50	96.80	08.0	-		10.65	0.003051	2,03	67.53	43,51	
Accessed to the same of the	214 214			6.80		9.51	10.99		2.03	63,33	47.49	1.
er 2	214 214	Q100	113.00	1	10.01	1		1				
			1997		-		8.88	0.003415	1,50	37.22	44.58	
	125	Ω2	34,10								55.68	4
ier :	125	O5	49,90				9.45				59.16	*****
	125	Q10	60,20				9,72				61,51	
er :	125	G20	73.80				10.01			***************************************	64.71	<u> </u>
	125	Q50	96,80	6.34	10.36		10.42		1,43			
	125	Q100	113.00	6,34	10,74	9.07	10.79	0.001081	1,40	146.62	65.73	
)eı	160	- 1	.112	1,41 +		1	11.0	1 1	1	1		<u> </u>
	480 FIE		Bridge		1					41114		
901	122 Bikeway		37,036	1	1	1	I .	V., :	1			1
			34.10	6.34	8.72	8.14	8.62	0.004144	1.61	33,93	42,32	
	119	02					9,42				55,17	
	119	Q5	49.90								59.00	
	119	Q10	60.20							4	61,31	
er.	119	Q20	73.80								64.65	
	119	O50	96.80	6.34								
	119	Q100	113.00	6.34	10,72	9.07	10.78	0.001101	1,41	145.56	65.68	
					1	1		<u> </u>	1			1
		Q2	34.10	5.67	8.40	7.09	8,45	0.001214	0.98		23.32	
	4 4		49.90						0.97	64,16	49.50	
	4 4	Q5									.58.47	
	4 4	010	60.20								67.71	
per .	4 4	C)20	73.80			4	<u></u>		-		80.27	-
рег	4 4	Q50	96.80								92.25	
	4 4	Q100	113.00	5.67	10.60	80.8	10.67	0.00068	1,24	1: (-2.30	1 32.20	<u> </u>

Appendix I2

HECRAS Model Results for Salvin Creek



Reach	Salvin-Final 09 River, Sal River Sta	rin Ck Reach: Up; Profile	er Reach O Total	Min Gh El	W.S. Elev	Crit.W.S. E.G. Elev	E,G, Slope	VelChal		Top Width	Froude # C
			(m3/s)	(តា)	(m)	(m) (m)	(m/m)	[akm]	(m2)	(m) 22.27	
er Reach	2130	O 2 yr	15.90	24.88	26.42	26.49 26.77		0.81 0.84	20.91	27.63	
er Reach	2130	O 5 yr	23.90 30.00	24.88 24.86	26,74	27.01		0.87	35.81	34.23	
or Reach	2130	Q 10 yr	35.50	24.68	27.16	27.20		0.90	42.86	39.53	
er Reach er Reach	2130	0 50 yr	43.10	24.68	27.40	27.44		0.93	53.08	50.19	
r Reach	2130	O:100 yr	49.30	24.68	27.58	27.62	0,002337	0,94	53.51	63,75	
				A45							C
r Reach	2120.*	Q 2 yr	16.90	24.63	26.40	26,43	0.001376	0,83	20,45	21,43 24,48	
r Reach	2;20.	C 5 yr	23.90	24.83	26,72	26.75	0.001187	0.86	27.76 34.09	29.54	(
r Reach	2120.*	O 10 yr	30.00	24.83	26.95	26,99		0.89 0.92	40.21	34:04	
r Reach	2120,*	Q 20 yr	35.50	24.83	27,14	27.19		0.98	46.69	39.46	
r Reach	2120,"	Q 50 yr	43.10	24.63	27.38	27.43 27.61	0.000773	0,99	55.28	43.51	
r Reach	2120,*	O 100 M	49.30	24.83	27.56	127.00	0.000770		1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1		الأراث والموادي
			16.90	24,78	26.36	25,42	0.001515	0,83	20.30	20.84	41.12
r Reach	2110,"	Q 2 yr Q 5 yr	23.90	24,78	26.70	26.74		0.87	27,41	23.69	
r Reach r Reach	2110.1	Q 10 yr	30.00	24.78	26.94	26,98		0.90	33.31	26,61	
r Reach	2110.*	Q 20 yr	35.50	24:78	27,13	27.18		0.93	38.82	30.35	
Reach	2110.*	G 50 yr	43.10	24.78	27,37	27,42		0.97	46,57	35.07	
Reach	2110.1	Q 100 yr.	49.30	24,78	27.55	27,80	0,000897	1.00	53,12	38,53	
										20.00	- 100 - 11 W
Reach	2100,*	OSW	16.90	24.74	26,37	26,40		0.84	20.20	20,35	
Reach	2100.1	Q 5 yr	23.90	24.74	26.69	26.73	0.001465	83.0	27,16	25,03	
Reach	2100.1	Q 10 yr	30.00	24.74	26.93	26.97		12.0	32.87	27.74	
Reach	2100,*	Ø 20 yr	35.50	24,74	27.12	27.17		0.94 0.98	37.98 45.07	31.81	
r Reach	2100.*	Q 50 yr	43.10	24,74	27.36	27,41		1.01	51.63	34,87	
Reach	2100.*	O 100 yr	49.30	24,74	27.54	Z/,59	8201022	1,01	71.70	2-101	
		0.0	1000	24,69	26.35	26.39	0.001603	0,64	20.12	19.93	
Reach	2090,*	C 2 yr	16.90	24,69	28.67	26.71		0.89	26.97	22.48	
Reach	2090.*	Q 5 yr	23.90 30.00	24,69	26,91	26.95		0.92	32,55	24,36	
Reach	2090,*	Q 10 yr	35.50	24.69	27.11	27.15		0,95	37.47	25.90	
Reach Reach	2090.*	Q 50 yr	43.10	24.69	27.35	27.40		0.98	44:09	29.39	
Reach	2090.*	G 105 yr	49:30	24.69	27.53	27.58	0.001202	1.01	49,61	32,10	- 1581
1100041	12.000		i i			100		3.1			
Reach	2080.1	Q2yr	16.90	24.54	26.33	26.37		0.84	20.06	19,58	
Reach	2080.*	Q.5 yr	23.90	24.64	26.65	28,65		0.89	26.81	22.01	Sugernar Sugeralitz
Reach	2080.*	Q 10 yr	30.00	24.64	26.89	26.94		0.93	\$2,29	23.79	
Reach	2080.*	Q 20 yr	35,50	24,64	27,09	27.14		0.96	37.11 43.44	25.27 27.58	
Reach	2080,*	Q 50 yr	43.10	24.54	27,53	27:38		0.99	48.55	29.97	ALC: New York
Reach	2080,*	Q 100 yr	49,30	24.64	27.51	27.57	0.001417	1,02	40.55	23.01	
						26.35	0.002101	0.84	20.02	19,27	
Reach	2070.*	OZyr	16.90	24.59 24.59	26.31 26.64	26.55		0.90	26,59	21.59	
Reach	2070.*	O 5 yr	23.90 30,00	24.59	26.67	26.92		0.94	32.07	23,30	34.75.5
Reach	2070,*	Q 10 yr	35.50	24,59	27.07	27.12		0.95	36.60	24,71	
Reach	2070.*	Q 20 yr	43.10	24.59	27.31	27.39	4	1.00	42.98	86,43	1. 1.400
Reach Reach	2070.*	C 100 yr	49.30	24.59	27.50	27.55		1.03	47.96	28.34	-
REGUL	2010.	4 104 7					1	10.7			
Reach	2060.*	Q2yr	16.90	24:54	26.29	26.32		0.88	20,00	19,00	
Reach	2060.*	Q 5 yr	23.90	24.54	28.61	26,66	0.002097	0.90	26,60	21.24	
Reach	2060.*	Q 10 yr	30.00	24.54	.28.85	26.90		0,54	31,90	22.68	
Reach	2060.*	Q 20 yr	35.50	24.54	27.05	27.10		0.97	36.55	24.23	
Reach	2050.*	Q 50 yr,	43.10	24.54	27.29	27.35		1.01	42.51	25.88	301 1 No.
Reach	2060,*	Q 100 yr	49.30	24,54	27.48	27.59	0,001662	1,04	47,46	27,13	
			1 an 118 119						19.98	18,77	
Reach	2050.1	Q 2 yr	16.90	24,49	25.28	26,30		9,85	26.52	20,93	
Reach	2050.*	Q 5 yr	23.90	24.49	26.59	26.63	-	0.90 0.94	31.75	22.50	
Reach	2050.*	O10 yr	30.00	24.49	26,63	26,88		0.98	35.34	23.80	
Reach	2050.*	O 20 yr	35.50	24.49	27,03	27,86		1.02	42.29	25,39	
Reach	2050.*	Q 50 yr	43,10	24.49	27,27	27.93 27.51		1.05		26.59	3 1311
Reach	2050.*	C3 100 yr	49.30	24,49	61,40	27,31	1				
	00404	Dave.	16.90	24.45	26.24	26.27	0.002546	0.85	19.98	16.56	91.0
Reach	2040.*	O 2 yr O 5 yr	23.90	24.45	26,57	26.61			26,46	20,65	
Reach Reach	2040.	Q 10 yr	30.00	24.45	26.81	26,86	0.002386	0.95	31.62	22.17	1,194,
Reach	2040."	O 20 yr	35,50	24,45	27.01	27.09	0.002331	0,98		23,42	حدث بنيب غنج
Reach	2040.*	Q 50 yr	43,10	24.45	27.25	27.30			42.01	24,95	Q., 18, 87, 17
Reach	2040.1	Q 100 yr	49,30	24.45	27,43	27.49	0,002263	1.06	4E.69	2£.10	
										40.00	
Reach	2030,	Q 2 yr	16.90	24,40	26.21	26.25			19.94	18.37	
Reach	2030.*	Q 5 yr	23.90	24,40	26:54	26.56		0.91	25.39	20.39 21.86	
Reach	2030."	Q 10 yr	30,00	24.40	26.78	26.83		0.95 0.99	31.50 35.97	23,07	
Reach	2030.*	0.20 yr	35.50	24.40	25,98	27.00 27.20		1.03	41.74	24.55	بسيست
r Reach	2030.*	O 50 yr	43.10	24.40	27.22	27,61		1,06		25.66	
r Reach	2030,*	O 100 yr	49.30	24.40	27.41	21,41	V.006402	1	1 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3		
		0.7	3 ****	24.35	26.16	25.22	0.002965	0.85	19.91	18.20	
Reach	2020.	C 2 yr	16,90 23,90	24.35	26.10	26.5		0.91		20,17	
Reach	2020.	0.5 yr 0.10 yr	30,00	24.35	26.78	26.86		0,96		21.59	
Reach	2020.*	Q 20 yr	35.50	24.35	26.98	27.0				22.77	
Reach	2020,*	O 50 yr	43.10	24.35	27.20	27.2			41,49	24.19	
r Reach	2020.*	D 100 yr	49.30	24.35	27.38	27.4		1.07		25.27	
Reach	EJEG.			1	1						
rReach	2010.*	Q 2 yr	16,90	24.30	26,15	26.11				18.04	
r Reach	2010.*	G 5 yr	23.90	24.30	25.49	26.5				19.95	<u> </u>
r Reach	2010.*	Q 10 yr	30,00	24,30	26.73	26.7				21.35	
r Reach	2010.*	Q 20 yr	35.50	24,30	26.93	26.99				22.48	
r Reach	2010.1	Q 50 yr	43,10	24.30	27.17	27.2				23.87	<u> </u>
r Roach	2010,*	Ο 100 γτ	49.30	24,30	27.35	27,4	0.002873	1.08	45,73	24,91	2500
							0.003360	0.85	19.52	17.90	
	energia ar ar arrah sententro energia (CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC	Q Z yr	16,90	24.26	25.12	26.1			13:02		
r Reach r Reach	2000.*	Q 5 yr	23.90	24.26	25,45	26.5	0.003162	0.91	26.20	19.78	1

	River Sta	in Ck Reach: Upp Profile	er Reach (Conli Q Total	Min Ch El	W.S. Elev	Crk W.5,	E,G, Elev	E.G. Skope	Vel Chri (m/s)	Flow Area. (m2)	Top Width	Froude # Ch
300000	-1-2-2	0.00	(m3/s)	(m) 24.25	(m) 26.95	(m)	(m) 25,95	(m/m) 0.003098	1.00	35.49	22.23	O.
Reach Reach	2000.*	Q 20 yr	35.50 43.10	24.25	27,14		27,19	0.003105	1,95	41.03	23.57	0.
Reach	2000.	Q 100 yr	49.30	24.26			27,38	0.003097	1.08	45.45	24.59	0.
					00.00		26,12	0,003514	0.85	19.74	17.77	0.
Reach	1990.*	Q 2 yr Q 5 yr	16.90 23.90	24.21	26,08 26,42		25,45	0.003402	0.92	26,10	19.60	0
Reach Reach	1990.	Q 10 yr	35.50	24.21	26,66		26.71	0.003375	0.97	31,02	20.91	
Reach	1990.	O 20 yr	35.50	24.21	25.86		26.91	0,003351	1.01	35.31	21.59	
Reach	1990,*	Q 50 yr	43.10	24.21	27.11		27.16 27.35	0.003370	1.06	40.78 45.14	24.28	
Reach	1990.*	O 100 yr	49,30	24.21	21.29		27.33	0.00000			1. 1.	244,11.00
Reach	1980.*	Q 2 yr	16.90	24,16	25.04		26.08	0.003840	0.86	19,54	17.64	0.
Reach	1980."	Q.5 yr	23.90	24.16	26,39		25,43	0.903509	0,92	25 99	19,44	0.
Reach	1980.*	O 10 yr	30,00	24,16	26,63		26,58 26,68	0.003592	0.97	30.87 35,12	20.72	0.
Reach	1980.*	Q 20 yr	35.50 43.10	24.16 24.16	26.83 27.07	<u>L</u>	27.13	0,003602	1.06	40.52	23.03	0.
Reach Reach	1980,	Q 100 yr	49.30	24.16			27.31	0.003608	1,10	44.83	23.93	0.
									0.07	19.52	17.44	0.
Reach	1970.*	Q 2 yr	16.90	24.11	26.00 26.35		26.04 26.39	0.004037 0.003640	0.87 0.92	25,86	19.28	0
Réach	1970.*	Q S yr	23.90 30.00	24.11 24.11	26.59		26.64	0.003832	0.98	30.70	20,53	0
Reach Reach	1970.	O 20 yr	35,50	24.11	26.79		26,84	0.003817	1.02	34,90	21.55	
Reach	1970.*	Q 50 yr	43.10	24.11	27.03		27.09	0.003863	1.07	40.24	22,76 23.72	0
Reach	1970,1	O 100 yr	49.30	24.11	27.21		27.28	0.003878	1:11	44.50	23.72	[
		0.835	1600	24.06	25.98		26.00	0.004238	0.87	19.39	17.23	0
Reach Reach	1960.*	Q 2 yr Q 5 yr	16.90 23.90	24.06	25,31		26,35	0.004092	0.93	25.70	19,13	0
Reach	1960.*	Q 10 yr	30.00	24,08	28,55		26,60	0.004092	0,98	30,49	20.35	0
Reach	1960.1	Q 20 yr	35.50	24.65	28.75		26.60	0.004982	1.02	34.66	21.35 22.55	
Reach	1960.*	Q 50 yr	43.10	24.06 24.05	25.99 27.17		27,05 27,24	0.004145	7,12	44.13	23.46	
Reach	1960,*	O 100 yr	49.30	24.05	21.17		2,	7.62				. 14
Reach	1950.*	Q 2 yr	16.90	24.02			25,95	0,004495	0.88	19.24	17.02	c
Reach	1950.*	Q 5 yr	23,90	24.02			26.31	0.004415	0.94	25.51	18.99 20.18	
Reach	1950.*	Q 10 yr	30.00	24,02 24,02	26.51 25.71		25,58 25,76	0,004418	1.03	34,39	21.16	
Reach	1950.*	Q 20 yr Q 50 yr	35.50 43,10	24,02	25.94		27.01	0.004489	1,09	:39.59	22,33	
Reach Reach	1950.	Q 100 yr	49.30	24.02	27.13		27,19	0,004520	1.13	43,74	23.22	
										40.6%	40.04	0
Reach	1940.*	0.2 yr	16.90	23.97	25.87		25.91 25.26	0.004899	0,89 0,95	19.08 25.27	16.81 18.85	
Reach	1940,*	Q 5 yr	23,90 30,50	23.97 23.97	25,22 26,45		26.51	0.004720	1.00	29.99	20.01	
leach leach	1940,*	Q 20 yr	35.50	23.97	26.68		26.71	0,004714	1.04	34.08	20.97	7
Reach	1940.*	Q 50 yr	43.10	23.97	25,90		26.96	0,004607	1,10	39.21	22,10	
Reach	1940.*	Ci 100 yr	49.30	23.97	27.08	***************************************	27,15	0.004845	1,14	43.31	22.98	
			7140	27.03	25,70		25.81	0.019559	1,42	17.01	15.94	C
Reach Reach	1930	Q 2 yr Q 5 yr	24.10 34.50	23.92 23.92	26.04		25.16	0.020247	1,52	22.66	17.87	0
Heach	1930	Q.10.yr	43,30	23.92	26.27		26,40	0.020924	1,61	26.98	19.19	
Teach	1930	O 20 yr	51,60	23.92	26,46		26,61	0,021316	1.68	30.71	20.08 21.14	
Reach	1930	Q 50 yr	62.50	23.92	26.69		26.65 27.03	0.021779	1.77	39.09	21.95	
Reach	1930	Q 100 yr	71.60	23.92	26.86		27,03	0.022.104	122		1.346.3	
Reach	1920.*	Q 2 yr	24,10	23.79	25.53		25.64	0.013785	1.46	16.47	15.75	
Reach	1920."	Q5 yr	34.50	23,79	25.86		25,99	0.014112	1.57	21.96	17.69 18.97	
leach .	1920.*	C) 10 yr	43.30	23.79	26,09		26,23 26,43	0,014496	1,66 1,73	26.11 29,75	19.86	
Reach	1920.*	Q 20 yr	51.60 62.50	23,79 23,79	26.28 26.50	/11 1	26.67	0,014725	1.82	34.29	20.92	
Reach Reach	1920.*	Q 100 yr	71.60	23.79	26.67	***************************************	26.85	0.014847	1,89	37.91	21.74	
	104.00	1 7										
leach	1910.*	Q2 yr	24,10	23.66			25.50	0.013927	1,47 1,58	15:42 21.85	15.75 17.69	
Reach	1910.1	Q5yr	34,50 43.30	23.65 23.65			25.85 26.08	0.014613	1,67	25.92	18.91	
leach leach	1910.*	Q 10 yr Q 20 yr	51.60	23.66	26.13		26.25	0.014714	1,75	29.52	19.62	
leach leach	1910.1	Q 50 yr	.62.50	23.55			26.52	0,014860	1.84	34.01	25,89	
Reach	1910.*	Q 100 yr	71,60	23.66	26.52		26,70	0,014590	1,90	37.60	21,71	
	lyana t	0.0.7	24,10	23.53	25.25		25,37	0,013937	1,47	16,26	15.78	
Reach Reach	1900.*	Q 2 yr Q 5 yr	34.50	23.53			25.70	0.014350	1.59	21.71	17,71	
leach	1900.*	O 10 yr	49,30	23,53	25.79		25,94	0.014618	1,58	25,71	18.86	
Reach	1900.*	Q 20 yr	51,60	23.53	25.98		26.14	0.014728	1,76	29.28	19.78 20.86	
Reach	1900.*	Q 50 yr	62.50 71.60	23,53 23.53			26.37 28.55	0.014866 0.015027	1.92	37.28	21.69	
Resch	1900.*	D 100 yr	100.11	20.03	******				1111111		100	
Reach	1890.*	0.2 yr	24,10	23.40			25,23	0,514137	1,48	16:29	15.76	
Reach	1890.*	Q 5 yr	34.50	23.40			25.56	0.014658	1.60	21.54 25.49	17.72	
Reach	1890.*	0 10 yr	43.30	23.40			25.79 25.99	6,014779 6,014894	1.78	29,03	19.74	
Reach Reach	1890.*	0.20 yr 0.50 yr	51,60 62,50	23.40			26,22	0.015061	1.87	33,43	20.84	
Reach Reach	1890."	Q 100 yr	71,50	23.40			25.40	0,015211	1.94	36.94	21.67	
										1000	(1.79.5
Reach	1860."	0'2 yr	24.10	23.27			25.08 25.41	0,013999 0,014497	1,49	16,22 21.37	15,78	
Reach	1880.*	Q5y	34.50 43.30	23.27	4		25.64	0.014497	1.71	25.29	18.78	
Reach Reach	1880.* 1880.*	Q 10 yr Q 20 yr	51,60	23.27			25,84	0,014792	1,79	28.79	19,72	
Reach Reach	1880.*	0.50 yr	62,50	23.27			26.07	0.014910	1,83	33.15	20,82	
Fleach	1880,*	Q 100 yr	71,60	23.27		<u> </u>	26,25	0.015072	1,96	36.61	21.66	
				<u> </u>				0.014152	1,49	16.17	15.80	
Reach	1870,*	02yr	24,10 34,50	23.13 23.13			24.94 25.27	0.014605	1,63	21.22	17.63	
Reach	1870.*	Q 5 yr Q 10 yr	43.30	23.13			25.50	0.014731	1,73	25.10	18.75	
				23.13			25,69	0.014865	1.81	28.57	19.70	le san C
Reach Reach	1870,	Q 20 yr	51,60	20,10	25.74		25.92		1,90	32.88	20.82	(

EC-RAS Plan Reach	n: Salvin-Final-09 River: Salv River Sia	in Ck Reach: Upp Profile	G Total	Min Ch El		Crit W.S. E.G. Elev	E.G. Slope	VelChrl	Flow Area (m2)	Top Width (m)	Freude # Ghl
			(m3/s)	(m)	(970)	(m) (m)	(m/m)	(m/s)	(mz)	(HI)	
pper Reach	1860.*	O 2 yr	24,10	23.00	24.59	24,80	0,014181	1.50	15:10	15.83	0.47 0.48
pper Reach	1860,*	Q 5.yr	34,50	23.00	24.98 25.20	25,12 25,35	0.014582	1.64	21,05 24,91	17,60 18,74	0.48
pper Reach pper Reach	1860.*	Q 10 yr Q 20 yr	43.30 51.60	23.00 23.00	25.20	25.54	0.014873	1,82	28,34	19.70	0.48
pper Reach	1850.*	G 50 yr	82.50	23,00	25.58	25,77	0,015091	1.92	32.60	20.83 21.68	0.49 0.49
pper Reach	1850.*	Q 100 yr	71.60	23.00	25.74	25.94	0.015295	1.99	35,97	21.00	0.13
pper Réach	1850.	O 2 yr	24.10	22.87	24.54	24.58	0,014404	1.51	* 16_01	15.67	0,48
pper Reach	1950.1	Q 5 yr	34,50	22.87	24.84	24.97	0.014722	1,65	20,90 24,72	17.58	0.48 0.49
pper Reach	1850.1	Q 10 yr Q 20 yr	43.30 51.60	22.87 22.87	25.06 25.22	25.20 25.39	0.015038	1.84	28.11	19,70	0.49
pper Reach pper Reach	1650.*	Q 50 yr	62.50	22.87	25.43	25,62	0.015281	1.93	32.31	20,85	0.50
pper Reach	1850,	Q 100 yr	71.60	22.67	25.58	25.79	0.015514	2.01	35.63	21,70	0.50
pper Reach	1840.*	Q 2 yr	24,10	22.74	24,40	24.51	0.014509	1.51	15.91	15.90	0.48
pper Reach	1840.*	Q 5 yr	34.50	22.74	24.69	24.83	0.014728	1,66	20.74 24.52	17.56 18.73	0.49 0.49
pper Reach	1840.1	Q 10 yr	43.30	22.74	24,89 25,07	25.05 25.24	0.014892 0.015076	1.77	27.87	19.72	0.50
pper Reach pper Reach	1840,*	Q 20 yr	51,60 £2,50	22.74	25,27	25.47	0.015355	1.95	32.01	20,87	9,50
pper Reach	1840."	O 100 yr	71,60	22.74	25:42	25.63	0.015630	2.03	35,26	21,73	0.51
				22.61	24.25	24,37	0.014690	1.53	15.80	15.89	0.49
ppor Reach	1830,* 1830,*	Q2 yr Q5 yr	24.10 34.50	22.61	24,54	24,68	0.014875	1,68	20,58	17,55	0,49
lpper Reach Ipper Reach	1830.*	Ca 10 yr	43.30	22.61	24.74	24,90	0,015068	1.78	24.31	18,74	0.50
pper Reach	1830.1	Q 20 yr	51,60	22.61	24,91 25,11	25.09 25.31	0.015277 0.015603	1.87 1.97	27.62 31.69	29,90	0.51
pper Reach pper Reach	1830.* 1830.*	Q 100 yr	62.50 71.60	22.61	25.26	25.48	0.015934	2.05	34.86	21.77	0.52
Abbut Mason	34504	,							70.00	42.00	0,49
pper Reach	1820,	Q 2 yr	24,10	22.48	24.10 24.38	24,22 24,53	0.014714 0.014930	1.54	15,66 20,40	15.86 17.55	
pper Reach pper Reach	1820,*	Q 5 yr	34.50 43.30	22.48 22.48	24.58	24.75	0.015150	1.80	24,08	18.78	0.51
pper Heach pper Reach	1820.*	O 20 yr	51.60	. 22.48	24,76	24,94	0.015393	1,89	27.34	19.77	0.51
doseR requ	1820.*	Q 50 yr	62.50	22.46 22.46	24.95 25.10	25,15 25,32	0.015786	2.90 2.08	31,33 34,41	20,94	0.52 0.53
oper Reach	1620.*	O 100 yr	71.60	22.45	25.10		0.07012		* * * * * * * * * * * * * * * * * * *		Y Y
pper Reach	1810.1	O 2 yr	24,10	22,35	23.95	24.07	0.014931	1.55		15.83	0,50
pper Heach	1810."	Q 5 yr	34,50	22.35	24.23 24.43	24.38 24.50	0.015165	1.71	20.21	17,56 18,79	
oper Reach ppor Reach	1810."	Q 10 yr	43,30 51,60	22.35 22.35	24.60	24.78	0,015700	1,91	27.04	19.81	0.52
pper Reach	1810.1	C) 50 yr	62.50	22.35	24.79	24,95	0,016188	2.02	30,92	20.98	
pper Reach	1810.1	Q 100 yr.	71,60	22.35	24.93	25,15	0,016349	2.11	33.93	21,66	0.34
0 - 1	4500.4	Q 2 yr	24,10	22.22	23.80	23.92	0.014754	1.57	15.39	15.82	
pper Reach pper Reach	1600."	QSyr	34,50	22.22	24.08	24.23	0,015015	1.72		17,58	
pper Reach	1800.*	Q 10 yr	43.20	22.22	24,27	24.45 24.53	0.015000	1,63 1,93	23.81 26.74	16.63	
pper Reach	1850.*	Q 20 yr	51.60 62.50	22.22	24.44 24.62	24.83	0.015052	2.05	30.51	20.92	0.54
pper Reach pper Reach	1800.*	Q 190 yr	71.60	22.22		24,99	0.015141	2,14	33,47	21.55	0.55
					****	29.78	0.014930	1.58	15.27	15,83	0.51
pper Reach	1790.	02yr	24,10 34,50	22.09	23,65 23.92	24.08	0.015230	1.74	19.86	17.63	
pper Reach pper Reach	1790.* 1790.*	Q 10 yr	43,30	22.09	24.12	24.29	0.015579	1,85	23.38	18.90	
pper Reach	1790.*	Q 20 yr	51,60	22.09	24.27	24.47	0.016028	1,95 2,08		19.93 20.81	
oper Reach	1790.*	O 50 yr	62.50 71.60	22.09 22.09	24,45 24.59	24.57 24.83	0.016263	2,17		21,44	
lpper Reach	1790.*	(0 100 yr	77.00		7. 7		J 11, 1				
pper Roach	1780.*	Q 2 yr	24.10	21.96	23.50	23.63 23.92	0.014962 0.015324	1.59 1.75	15,14 19,67	15.85 17.69	
Ipper Reach	1780.*	Q 5 yr	34.50 43.30	21.96	23.77	24.13	0.015777	1.87	23.11	18,97	
pper Reach pper Reach	1780.*	Q 20 yr	51.60	21.98	24,11	24,31	0.016134	1,98	26.05	19.86	
pper Reach	1780.*	Q 50 yr	62.50	21,96	24.28	24.51 24.57	0.016204 0.816256	2.11 2.20	29.69 32.58	20.59	
pper Reach	1780.*	Q 100 yr	71.60	21,96	24.42	24.57	0.0182.20	4.20	32.50		
Ipper Reach	1770.	Q 2 yr	24.10	21.82		23.47	0.015196	1,61	15,01	15.88	
oper Reach	1770.	Q 5.yr	34,50	21,82	23.61	23.77 23.97	0:015641 0:016250	1.77 1.90	19.47 22,80	17.76 19.04	
pper Reach pper Reach	1770.	Q 10 yr Q 20 yr	43.30 51,60	21.82		24,14	0.016301	2.01	25.69	19,75	0.50
pper Heach pper Reach	1770.*	Q 50 yr	62.59	21.82	24.12	24,35		2.14		20.56	
Ipper Reach	1770.*	G 100 yr	71:60	21,82	24.25	24.51	0.016382	2.23	32.12	21.18	Mary.
	1760.*	Q 2 yr	24.10	21.69	23.19	23.32	0.015307	1.82		15,94	0.5
pper Reach	1760.*	Q 5 yr	34,50	21.69	23,45	23,61	0.015894	1,79		17.85	
Ipper Poach	1760.	Q 10 yr	43.30	21.69		23.81 23.98	0.015312 0.015279	1.93 2.04		18.92 19.61	
lpper Reach	1760.1	Q 20 yr	51,60 52,50	21.69		24,19		2.17		20,42	0.5
lpper Reach Ipper Reach		Q 100 yr	71.60	23.69		24,34	0.015298	2,26	31,68	21,05	0.5
					07.25	23,17	0.015437	1.64	14,73	15,01	0,5
pper Reach	1750.7	Q 2 yr	24,10 34,50	21,56 21,56		23.45		1,82		17,84	0,5
ipper Reach Ipper Roach	1750.* 1750.*	O 10 yr	43.30	21,56	23,45	23.55	0.016318	1.95	.22.09	18.76	
Ipper Reach	1750.	O 20 yr	51,60	21.56	23.59	23.82		2,07		19.48	
Jpper Reach		Q 50 yr	62.50	21.58 21.56		24.02 24.18	0.016156		4	20.92	
Jpper Reach	1750."	O 100 yr	71,60	21.35	24.78		Ai a. Z				1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
Jpper Reach	1740.*	Qzyr	24,10	21,43		25.91	0.015815	1,85			
Jpper Reach	1740.	Q 5 yr	24.50	21,43		23.29	0.016517 0.016489	1,85		18.59	
Jopes Reach Joses Reach	1745.* 1740.*	Q 10 yr Q 20 yr	43.30 51.60	21,43 21,43	ļ	23.66		2.09	24.64	19,31	0.5
Jpper Reach Jpper Reach	1740.	Q 50 yr	£2.50	21.43	23.51	23:85		2.22		20,15	
Jpper Reach	1740.*	Q 100 yr	71,60	21.43	23.75	24,02	0,016028	2:31	30.96	20,75	3.0
	1730."	Q 2 yr	24,10	21.30	22.71	22.65	0.016217	1,68			
Joper Reach			34,50	21.30		23.12		1.89	18.29	17.59	0.5

							Þ.					
29.0	£91	95,61	2.23	0.007730	21,33	1	80.12	19.63	43,30	14.01 (2)	5651	
90	64,21	97,81	2.06	968100,0	11.15		\$0.90	19.63	34,50	\ \A ≥ O	9691	
9'0	14,12	10.61	1,85	202800.0	20.61	<u> </u>	79.0Z	19.63	24,10	74.2 D	Seet	doseR te
	- 1 - 1				1							L
			-		1		T		hovino		1609 Bayan St Culvert	doseR te
					1							<u> </u>
5.0	Z*'9>	\$1.5g	96.1	166100,0	78.55	21.25	37.SS	EL 61	0914	G 100 Yr	0151	
92.0	68.44	0719	82.1	815100.0	22.71	21.11	22,63	19,73	05.50	M 69 D	otet	
32.0	81,14	23'01	81.1	0.001210	15.55	26.0S	12.54	EZ'61	91.60	7 02 D	CLO	
85.0	59.65	98.50	51.1	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	22,13	08.0S	22.05	E7.61	43.30	N 01 D	0191	
0.29	24.57	31.05	\$LL	159100.0	19'12	30.02	21,75	E7.61	34.50	1/20	0191	
10.0	18.32	20.05	20"1	855.500.0	21,40	94,05	21'34	£7.61	24,10	927	ofai	dasaR 19
12.0	06.01	137.00	129	1,,,,,,,	1	1						
	COOK	30.82	75.1	898100.0	55.69	1	55'39	19861	09°1E	Q 100 Yr	1,0531	ст Яваси
00.0	40.85		75.1	1777100.0	22,73		P8.55	98'61	05.28	# DS D	. D29	ек Вевси
0.29	20,1¢	42.69	1.24	7721000	22.53		55,45	98'61	09.12	O 20 M	1950.	от Неасћ
72.0	32,14		62.1	0,05500.0	22,15	4	32.07	98.61	06.EA	1601.0	.10291	तंत्रहास १६
r E.G.	67.2g	18.46		198200.0	21.84		21.76	38.61	05.48	NSD	850:	дэван зо
ve.0	51,15	22.56	92.1	0.003261	21.83		55.13	38.61	54.10	0.2.9%	.029	er Reach
56.0	16.62	50.0Z	02.1	1982000	EFFE			-1				
	<u>. 1</u>						22.80	66'61	71.60	7 100 %	£30°.	or Reach
65.0	EA.EE	38.02	82.f	\$24200.0	22.92		55.55	86.81	0978	C 20 %	.009	
0.35	96.0E	61.8¥	25'1	£EEZ0076	22.76		53.05 53.05	66'61	03.12	O SO AL	.009	
16'0	TTTZ	09'01	1,34	0.002210	22.55				06.64	Yar O	.'009	
96.0	19,95	71,1E	071	0.003239	32,15		25.08	19,99		7 de 0	, DC9	
6£°0	18,81	78.45	96.t	\$26200°B	21.85		87.15	6661	34.50	N20	. 009	
07'0	26'51	10.81	134	\$72400.0	9\$°12		21.39	66'61	24,10	100	.023	1 4
and a comme	15. Physic 1	. 4 55. 11	1 1 2 2 2							- 1/20/20	.*079	er Roach
ZE 0	21.62	89'57	£9,1	825.00.0	56.52	1	18.55	20.12	09.17	14 CG (D)		S. Service Co. Charles Co.
98.0	18.72	ES'1.1	13.1	121500.0	22.79	<u> </u>	1,972	S1.0S	02.50	N 05.0	640°.	
60.35	54.89	09'98	pp's.	890500.0	95'22	1	2772	20.12	03.12	0 20 W	.1019	
140	20.30	26,82	ES'L	899+00′0	22,23	1	22.11	20.12	43.30	סוסא .	2019	3
Et 0	Z5'Z1	\$2,65	1.52	186200.8	E8.15		21.81	20.12	34.50	M S D	2407	
9) 0	15.24	16.22	65.1	872800.0	\$1.54		21'43	20.12	01 tZ	n s yr	.19401.	daseR 19
17.56	- T. V.				1							Nan
17'Q	05.8%	55.14	87.1	0,004240	23.00	1.	22,64	52.02	09'17	7K 001 D	.'059	dasoft to
0/0	24.74	97,76	89'1	0.004223	22.83	1	89,55	S2.02	05.29	7 00 pt	. 099	
039	25.32	33.24	99'1	0,004225	25.52	1	22.50	20.25	09'15	17 OS D	. 059	or Roach
95.0 95.0	\71.6f	50.85	99"1	900900'0	52.29	1	5572	52:02	00°E#	36 O 10	e20°.	er Reach
81,0	17.34	87.0S	99'1	191700.0	22.00		21.85	20.25	34.50	W2.D	.1059	er Reach
ES 0		14.01	69'1	0.009285	51'85	-	65.15	52'02	24,10	77.50	.059	f daseR to
630						1		1				
SP'0	54.24	38.22	66.1	997800.0	53.05		78.95	86.02	09.17	7√ 0a1 D	.*099	
	84.52	18.15	1.80	959500.0	22.89	1	22.32	80.05	05'79	74 05 C	.1099	
50'0 90'0		20.53	88.1	Z08900'0	\$5,68	1	25.53	8C.0S	08,12	O 20 K	. 099	
	85'91	24.19	97,f	486700.0	52,38	1	22.20	20.38	93,50	MOLO	.7099	Азавя за
	*6'91	15.61	62'1	109600 0	22,09	-	21,93	20.38	05°#£	O.5 V:	. 099	f Hosen 1s
ES'D		13.80	S21	0,012559	17.74		85,15	20.38	24'10	uzo	.095	i daseR to
89'0	16.27	14.80	94.1	632010 0	172.44							I
		0.000	10.3	S2+500.0	23,52		25.92	15:08	09°12	JA 001 D	.029	्रा सङ्ख्या । ।
05.0	22.38	02.88			96.55		77,55	1502	62.50	N o≥ O	:029	пакон з
5¥°0	20,15	32,55	Z61k	0.007339	22.75		22.58	15.02	51.60	0.20 Vi	.'029	
8>0	18:61	29,63	08.1				72,25	12.02	43.30	1,010	.'029	исеан 10
75.0	e.t.8t	22,75	06'1	\$66600.0	22.46		22.02	15.02	84.50	ik s D	.'019	
25.0	15.74	OE.81	68,1	118110.0	22.20	4			24.10	720	.029	
Z9'0	\\ \teal	3E,Et	08.1	668410.0	78.15		17.15	15.02	(Ut Pa		· ·	1
	4 t. (10)									Q 100 W		н давай 19
¢9′0	26.15	>8.EE	SIZ	\$85,600.0	12.65		55.99	20.65	09114	O 20 M	.'099	
£5.0	20°24	S8.0£	2.03	0.009224	23,05		48.SZ	20.65	05.58	G 20 M	.1099	
S\$.0	61'61	76.92	161	102600.0	22.84		28.85	59'02	09,18		.099	
85.6	B6.71	87,15	66'1	91021070	22.57		72.37	29,02	05.64	Q 10 yr		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
69,0	12.31	57.71	36'1	249210,0	22.33		41,52	20.65	34.50	n a o	690.°	
6,63	16,52	82,£t	18.1	1000100	22.03		88,15	20.65	24.10	OZY	, U639	4254634
	1.0										ince.	taseR14
/5'0	26.02	32.48	5.20	8>8010,0	56.65		23.07	37,02	09.17	1 00 tO	.069	7,300
95'0	12.02	59.51	21.2	478010.0	91.ES		22.93	87.02	05.56	V 05.0	.069	A X 200000000000000000000000000000000000
55'0	15.21	P2'92	2.00	886010.0	22.94		45,55	87,02	05.18	N 02.0	690.	
09'0	26,71	81:12	\$0.5	E18E10.0	22.70		22.49	81.0\$	02.54	70,01.0	. 069	
55,0	16,80	6×21	76,1	9815100	84,55		55,29	20.78	05.45	14.50	.069	
23.0	17.21	I.P.E.I	68.1	815810,0	22,19		22,53	87.02	24.10	7,20	.069	i daseA se
	1 1 2			Lan	1		1.					
69'0	20.76	45,15	12.2	0.012421	23,44		81,85	16,05	69,15	N 001 D	7007	
82.0	20.03	1978	2.18	0.012519	23.28	1	\$3'04	16'02	62.50	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	700.	
85.0	190.81	24.94	20.5	0.012742	53.08	1	22.65	1E'0Z	09715	17.02.0	.002	
18.0	99.71	25°02	40.5	6,014963	28.25	1	\$2.63	16.02	43.30	7010	.007	
59.0	78,81	59,77	16'1	61091070	22.63		22,43	20,91	34.59	ηSD	700.	
18.0	06'51	13,62	177.1	0.016660	55,36	1	DZ,SZ	16.03	24,10	0.2 yr	.1001.	f dasaRite
,, u	0731	12200			1	1		-1		1		
C9'8	78,05	31.03	15.5	0.013580	75.52	1	05.ES	80.TS	71.80	O 100 M	.1012	
			3.22	0.013720	23,41	+	91,65	21.04	62.50	JA OS D	.1012	
09.0	96'61	27.85	11.5	P66E1070	23.20		78.92	10,15	08.18	O 20 At	. 017	
69'0	19.03	20.83	20.2	0.013994	23.00	+	87.25	21.04	43.30	O 10 Yr	.101.	
19'0	80.81	20.93			67.25		02,52	21.04	34.50	μso	710.7	
19'0	21.77	17,71	\$6°1	0.016270	25.55	-	72.55	21.04	24.10	0.2 %	710.7	-
09:0	01.81	78.8t	72.1	012810.0	P2 CE	-	1 44	112.10		-		
<i>A</i> 1 7	1		سسييات		1200	أسنساك	53.44	71,12	09'12	74 001 O	150.	F doesel 1s
9.0	20.65	97.05	2.33	(69)10'0	23,72	-				16 co At	150.	
090	96'61	16,75	5.24	0.014637	83,55	1	53'30	21.12	05.58	G 20 Vr	720.	
09'0	ZC'61	24,33	212	060210.0	28,85	4	23,12	21.12	51,60		.027	
1976	18.23	21,08	\$02	8718,10,0	23,18		22,94	\$1,12	43.30	W 61.0		
d9'0	86,71	16,71	26.1	681810.0	96°22	1	27,55	71,15	05.45	, બદ્ર	720.	
65°0	16.28	14,12	i£1	072910.0	22.69		72.54	41,12	01.4Z	Ozyr	120,1	f Reach 1
					12	1						1
9'0.	07.02	97,06	\$33	1955100	78.85		\$3.58	2130	03,17	1,001.0	730.7	
09'0	\$0.0S	27.93	224	6999100	23.71	1	53 12	21.30	62.50	3 ce D	730.	
08.0	71,21	24.40	231	158510'0	02.65	1	72.25	81,30	09.18	Nozo	730.7	
09'0	14,81	25.13	2.03	0.016472	55.55	1	11.25	21.30	43.30	7,010	1301.	r Reach 1
UZV	(m)	(57)	(8/31)		(m)	(m)	(w)	(m)	(e)E(n)			
	verson sommerces de la Silva		omana samok ki ki ki ki k	CONSTRUCTION OF THE PROPERTY OF THE PARTY OF	an a said an an an an an an an an an an an an an						EIC 1941A	Hasch 1

Peach	Satvin-Finat-09 River: Sa River Sta	Profile	Q Total	Min Ch El	W.S. Eley Crit Y		E.G. Slope			Top Width	Froude # C
_	i name	0.00	(m3/s)	(m):	(m) (m	(m) 21.51	(m/m) 0.007750	(m/s) 2.38	(m2) 22.14	18.07	
per Reach per Reach	1595 1595	C 50 yr	51.60 62.50	19.63	21.23	21.73	0.007752	2.58	25.45	20.54	1. 17 . . .
per Reach	1595	Q 100 yr	71,60	19,63	21.53	21.90	0.007822	2.71	28.22	22.62	1
							5.007005	1,83	13.14	13.98	- (
per Reach	1585.1	024	24.10 34.50	19,44	20.58	20.73 21.03	0.007865 0.007474	2,04	16.92	14,51	
per Reach iper Reach	1585.* 1585.*	0.5 yr	43.30	19,44	21.00	21.25	5.007431	2.21	19.73	16,50	S 1. 10 10 10 10 10 10 10 10 10 10 10 10 10
per Reach	1585."	0.20 yr	51.00	19.44	21.15	21,44	0.007456	2.38	22.30	18,41	
per Reach	1585.*	Q 50 yr	62.50	19,44	21.32	21,65	9,007507	2.55	25.67 28.51	21.20	
per Reach	1585.	O 100 yr	71.60	19,44	21,45	21.82	0.007615	6.73	20.31	23.40	1.00
per Reach	1575.1	QZYI	24.10	19.25	20.48	20.65	0.007558	1,82	13.27	13.85	72.00.00
per Reach	1575.*	Q.5 yr	34.50	19.25	20.75	20.98	0.007195	2.02	17.09	14.50	30 00 0
per Reach	1575.*	O 10 yr	43.30	19.25	20.93	21,18 21,35	0.007231	2.19 2.35	19.68	16.53	
per Reach	1575.*	Q 20 yr	51,60 62,50	19.25	21.25	21.58	0.007355	2.55	25,94	22.08	
er Reach er Reach	1575.*	G 100 yr	71,60	19.25	21.37	21.74	0,007505	2.70	28.85	24.51	
			90.41 . T :	31-12			<u> </u>				
er Reach	1565.1	Q 2 yr	24,10	19.07	20,41	20.58 20.89	0.007285	1.60	13,42 17.25	13.74 14.40	
er Reach	1565.*	Q 5.yr	34,50 43,30	19.07	20.66	21.11	0.007076	2.18	20.02	16.76	HAN HE HA
er Reach er Reach	1565,*	Q 10 yr Q 20 yr	51.60	19,07	21.01	21.29	0.007110	2.34	22.68	19.61	The said
er Reach	1565.*	Q 50 yr.	62.50	19,07	21.18	21:50	0.007270	2.54	26.25	23.22	
er Reach	1565.*	Q 100 yr	71.60	19.07	21,30	21.67	0.007461	2.70	29,28	25,80	2040an 64 3450an 6
	1		27.2	40.00	20,34	20.50	0.007699	1.78	13.53	13.60	
r Reach or Reach	1555.*	Q 2 yr	24.10 34.50	18.68 18.68	20,341	20,82	0.005869	1,93	17,38	14,32	(var.)
r Reach	1555:	Q 10 yr	43.30	16.88	20.79	21.03	0.008978	2.17	20.13	17,32	34 NM . "
r Reach	1555;*	Q 20 yr	51,60	18.89	20.94	21,22	0,007055	2,33	22.89	20,59	
r Reach	1555.*	Q 50 yr	62.50	18.88	21,10	21,43	0.007269	2.54 2.70	26.62	24.64	
r Reach	1555.7	Q 100 yr	71.60	18.89	21,22	21.59	0.007213	2.7V	68.75	67,43	Jan 1
r Roach	1545.*	Q 2 yr	24,10	18.69	20.27	20.43	0.007000	1.77	13.61	13.45	
r Reach	1545."	Q 5 yr	34,50	18.69	20.55	20.75	5.008852	1.98	17.45	14.25	
r Reach	1545,*	Q 10 yr	43.30	18.69	20.72	20,96	0.006965	2.17	20.24	18,11	14,12192
n Reach	1545.*	O 20 yr	51,60	18.69	20.87	21.15 21.36	0.007088	2.33 2.54	23,11	22.01 26.51	Zarani.
r Reach	1545.* 1545.*	Q 50 yr Q 100 yr	62.50 71.60	18.69	21.03	21.51	0.007648	2.71	30.31	30.08	11367
(Reach	1343,	G (00 y)	71.001	14.0.2	- 50.75						
r Reach	1535,*	Q 2 yr	24,10	18.50	20.20	20.36	8,007002	1,77	13.64	13.29	
(Reach	1535,*	Q 5 yr	34.50	18.50	20,48	20.68	0.006960	1.98	17,45	14.21	
r Reach	1535,*	Q 10 yr	43.30	18.50 18.50	20.65	20.89	0.007067	2.17	20,31	23,86	11 1.1.5
r Reach r Reach	1535.*	Q 20 yr	\$1.60 \$2.50	18.50	20.95	21,28	0.007586	2,56	27.52	29.26	
r Reach	1535.*	Q 100 yr	71.60	16.50	21.07	21,44	0.007844	272	31,19	34,44	
			25								
r.Reach	1525.*	Q 2 yr	24,10	18.32	20.13	20,29	0,007123	1,77	13,65	13:10	
r Reach r Reach	1525.*	Q 5 yr	34,50 43,30	18.32	20.58	20,82	0.007307	2,19	20.36	20.76	1.1.2
(Reach	1525.*	Q 20 yr	51.50	18.32	20.72	21.00	0.007510	2.35	23,64	26.62	1 2
r.Reach	1525.*	Q.50 yr	52.50	18,32	20.87	21.20	0,007842	2,57	28.32	33.92	12547
r Reach	1525.*	Q 100 yr	71.60	18.32	20.99	21.38	0,006053	2.73	32.57	38.76	10 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
_	lana.	0.5	24.10	18,13	20.05	20.22	0.007400	1,79	13.44	12.80	J. (1.44)
r Réach r Réach	1515 1515	Q2yr Q5yr	34.50	18,13	20,33	20.53	0.007532	2.01	17,21	15,70	Terrory
r Reach	1515	Q 10 yr	43,30	18.13	20.49	20,74	0.007772	2.22	20,35	23.26	
r Reach	1515	G 20 yr	51.60	18.13	20.53	20.92	0.007979	2,39	24.06	30.98	
r Fleach	1515	O 50 yr	62.50	18,13	20.79	21,12 21,27	0.008261	2.60 2.75	29.40 34.05	27.80 42.78	INCOME S
r Reach	1515	Q 100 yr	71,60	18,13	20.50	= 1,023	4 ,000,7,1				7,211.00
r Reach	1505.*	0.2 yr	24.10	18.08	19.98	20,14	5,007377	1.79	13,46	12,93	
r Reach	1505.*	Q 5 yr	34,50	18.08	20.25	20,46	0.007528	2.01	17.26	15.76	3.00
r Reach	1505."	Q 10 yr	43,30	18.58	20,42	20.57	0.007765	2.21	20.25	23.09	
r Reach	1505,1	Q 20 yr Q 50 yr	51,60 62,50	18.08	20,55	29.64 21.03	0.008008	2,38	29.37	36.83	100
r Reach r Reach	1505.* 1505.*	Q 100 yr	71.60	18.08	20.83	21,16	0.008063	2.68	34,01	41,21	Tyles
					ş4 d	1,77		1 95 15577		. G. (111)	
r Reach	1495.*	O 2 yr	24.10	18.02	19.91	20.07	0.007028 0.007195	1.79	13,49 17,31	13,97 15,84	
r.Reach	1495.*	O S yr	34,50 43,30	18.02	20.18	20.38 20.59	0.007195	2.20	20,35	23,60	× 1
r Reach r Reach	1495.*	Q 18 yr	51.60	18.02	20.48	20,76	0.007588	2.37	23.96	30.48	
r Reach	1495.*	Q 50 yr	62.50	18,02	20.63	20.96	0.007695	2,55	29,19	36,17	1 30/11
rReach	1495.*	Q 100 yr	71,60	18.02	20.75	21,30	0.007770	2,69	33,66	40.20	التخسية
			24,10	17,97	19.64	20.00	0.007007	1.78	13.52	13,21	
r Reach r Reach	1485.*	Q 2 yr Q 5 yr	24,10 34,50	17,97	20.11	20.31	0.007197	1.99	17.38	15,95	
r Reach	1485,	Q 10 yr	43.39	17.97	20,27	20.51	0.007435	2,20	20.39	23,02	
r Reach	1485,*	Q 20 yr	51,60	17.97	20,40	20.58	0.007600	2.37	28.93	30.37	· idere
rReach	1485.*	O 50 yr	82.50	17.97	20.56	20.88	0.007716	2.55 2.68	29,10 33,48	35.69 39.62	
r.Reach	1485,*	Q 100 yr	71,50	17.97	20.67	120,12	J. W. J. (34)	E.UQ	30,40	V=.4E	
r.Reach	1475.	Q 2 yr	24,10	17.92	19.77	19,93	0.006668	1.78	13.56	13.56	
r Reach	1475.*	O 5 yr.	34.50	17.92	20.04	20.24	0.006872	1,98	17.42	16,10	
r Reach	1475.1	וע פון בו	43.30	17.92	20.20	20.44	0.007102	2.19	20,43	23.16	
r Reach	1475,	Q 20 yr	.51,60	17.92	20,33	20.60	0.007259	2.35 2.54	23,94	39,40 35,83	بنيي
r Reach	1475.*	Q 50 yr	62.50 71.60	17,92	20.60	20.95	0.007482	2.68	33.37	39.23	Their
r Reach	1415.	4 100 pt	7 3,50	11,32				387.7			
r Reach	1465.*	Огуг	24.10	17.87	19.71	19.87	0.005642	1.77	13.50	13.52	
r Reach	1485.*	la syr	34,50	17.87	19.97	20.17	0.006669	1,98	17.49	15.27	* 1 (3)
it Reach	1455."	Q 10 yr	43,30	17.87	20.13	20.37 20.54	0.007104	2,18 2,35	20,49	23,34 30,49	in the
r Fleach Ir Fleach	1465,"	Q 20 yr	51.60 62.50	17.87	20,26	20.54	0.007414	2.54	29,04	25.93	
	43+8⊒-	he we le	ac.an!	15,07	444.113	20,87	0.007499	2.67	33.32	39.27	

RAS Plant Salvin-Final-09 River: Reach River Sta	Salvin Ck Reach: Upp Profile	er Reach (Contin	ued) Min Ch El	W.S. Elev	CIE W.S. E.G. Elev	E.G. Slopa	Vel Chril	Flow Area	Top Width	Froude # Chi
		(m3/s)	(m)	(m)	(m) (m)	(m/m)	(m/s)	(m2)	(m)	
Reach 1455.*	Q 2 yr	24.10	17.62	19.64	19.8	0.005639	1,77	13.63	13.67	6.57
Reach 1455.* rReach 1455.*	Q 5 yr	34,50	17.82	19.90	20.1		1.97	17.53	16,43	0,59 0.81
rReach 1455.	Q 10 yr	43,30	17.62	20,05	20,3		2.18 2.35	20.52 23.98	23,56 30.63	0.63
r Reach [1455.* r Reach [1455.*	Q 20 yr	51.50 62.50	17.62	20.19	20.6		2.53	29.02	36.12	0.65
r Reach 1455.* r Reach 1455.*	Q 100 yr	71.50	17.62	20,45	20.8		2.67	33.28	39.34	0.66
					440	3 0.005337	1,77	13,65	13.83	0.57
r Reach 1445.	Q 2 yr Q 5 yr	24,10 34,50	17.76 17.76	19,58	19.7 20.0		1,97	17.57	(6.60	0.59
r Reach 1445.* r Reach 1445.*	Q 10 yr	43,30	17.76	19.99	20.2		2.17	20.55	23.83	0.61
/ Reach 1445."	O 20 yr	51,60	17.76	20.11	20.3		2.34	23.99	30.85	0.63 0.65
r Reach 1445."	O 50 yr	62.50	17.76	29,26	20.5		2.53 2.67	29,00 33,25	36.40 39.53	0.65
(Reach 1445.*	Q 100 yr	71.60	17.76	20.31		2 0.0072-0			w. 2175.19	
r Reach 1435.*	Q 2 yr	24.10	17.71	19.51	19.6		1.76	13.58	13.59	0.57
r Reach 1435.*	QSyr	34,50	17.71	19,77	19.5		1.96 2.17	17.61 20.59	16.81 24.17	0.59 0.62
r Reach 1435.*	Q 10 yr Q 20 yr	43,30 51,60	17,71 17.71	19.92	20.3		2.34	24.03	31:07	0.64
r Reach 1435.* r Reach 1435.*	Q 50 yr	62.50	17.71	20.19	20.1		2.53	29.00	38.78	0,68
r Reach 1435.*	Q 100 yr	71,60	17,71	20.30	20.6	5 0.007286	2.55	33.27	39.84	0.66
		*****	17.66	19,45	19.0	1 0.006058	1.76	13.71	14,17	0.57
r Reach 1425.* r Reach 1425.*	Q 2 yr Q 5 yr	24,10 34,50	17.66	19,71	19.5		1.96	17.65	17,06	0,50
Reach 1425.*	Q 10 W	43,30	17.66	19.85	20,0		2.16	20.65	24.59	0.62
(Reach 1425.*	D 20 yr	51,60	17.66	19,98	20.8		2.33 2.52	24.08 29.03	31,35 37,20	0.64 0,66
r Reach 1425.*	Q 50 yr	62.50 71.60	17.66 17.66	20,12	20,4 20.5		2.56	33,32	40.24	0.67
r Reach 1425.7	Q 100 yr	7 1,00	, 7, 08							Maria Pela
r Reach 1415.*	D 2 yr	24.10	17.61	19,39	19.4		1.75	13.75	14.35 17.35	0,57 0.60
r Reach 1415."	Q 5 yr	34.50 43.30	17.61 17.61	19,64 19,79	191		1.95 2.16	17.69 20.73	25.12	0.60
r Reach 1415.* r Reach 1415.*	0 15 yr 0 20 yr	51,60	17.61	19.91	20.		2.33	24,17	31.72	0.64
(Reach 1415.*	Q 50 yr	62.50	17.51	20.05	20.		2.52	29.12	37,53	0.66
r Reach 1415.*	Q 100 yr	71.60	17.61	20,16	203	1 0.007019	2.65	33,44	40,76	0.67
- Barret (405 t	O 2 yr	24.10	17.56	19.33	19.4	9 0.005784	1,75	13.79	14,56	0.57
r Reach 1405.1	0.5 yr	34.50	17.56	19.58	19.7	8 0.006132	1,95	17.74	17.67	0.60
r Reach 1405.*	Q 10 yr	43,30	17.56	19.73	19.1		2.15 2.32	20.81	25,70 32,13	0.62 0.64
r Reach 1405."	D 20 yr	51.50	17.56 17.56	19.84 19.99	20.		2.32	29.22	37.92	0.66
r Reach (405.* r Reach (405.*	Q 50 yr	71.60	17.56	20,09	20.2		2.85	33.58	41.35	0.67
(Nudul 1902							5 2 2 2 2			
r Reach 1395.*	Q 2 yr	24.10	17.50	19.28	15.4		1.74	13.63	14,77	0,57
Reach 1395.*	Q 5 yr	34.50 43.30	17.50 17.50	19.52 19.56	19.1 19.1		2.15	20,92	26.39	0,53
r Reach 1395.* r Reach 1395.*	Q 10 yr Q 20 yr	51.60	17,50	19,78	20.1		2.31	24,40	32.53	0.65
r Reach (395.*	D 50 yr	62.50	17.50	19.52	20.1		2.51	29.37	38,41 42.04	0.66 0.67
r Reach 1395.*	Q 100 yr	71,60	17.50	20,03	20,0	7 0.006740	2.54	32.78	42.04	0,07
/ Reach 1365."	Q 2 yr	24.10	17.45	19.22	19.3	7 0.005854	1,74	13.85	14.98	0.58
Reach 1385.*	Q.5 yr	34:50	17,45	19.46	19.6			17,81	18,75	0.61
r Reach 1385.*	Q 10 yr	43.30	17.45	19.60	19.1		2.14 2.31	20.99 24.50	27,06 33,12	0.63 0.65
(Reach 1385.*	0.50 At	51.80	17.45 17.45	19.71 19.65	19.5 20.		2.50	29.49	38.93	0.67
r Reach 1885.* r Reach 1985.*	Q 50 yr	62,50 71,60	17.45	19.96	20.		2.63	33.97	42.80	0.68
TOTAL TOTAL		130.00					1,34,140		45.50	0.58
r Reach 1375.*	Q2yr	24,10	17,40	19.16	19.		1,74	13.85	15.20 19.41	0.61
r Reach 1375.*	Q 5 yr Q 10 yr	34,50 49,30	17,46 17,40	19.54	19.			21.97	27.76	0.63
Reach 1375*	Q 20 yr	51,60	17.40	19.65	19.			24.50	33.65	0.65
rReach 1375.	Q 50 yr	62,50	17.40	19.79	20,		2.50 2.63	29.60 34.16	39.51 43.99	0.61
r Reach 1375.5	Q 100 yr	71.60	17.40	19.90	20.	4 0.006501	2.53	34.15		70. 7.
r Reach 1365.*	G29r	24.10	17.35	19,10				13.87	15,43	0,56
r Reach 1385.*	Q 5 yr	34.50	17.35	19,34	19.			17.87	20.17 28.60	0,61 0,64
r Reach 1365.*	Q 10 yr	43.30	17.25	19,47 19,59	19.			21.17 24,73	28.60 34.29	0.64 0.66
Reach 1365.*	Q 20 yr Q 50 yr	51,60 62,50	17.35 17.35	19.72	20.1		<u> </u>	29.79	40.22	0.67
r Reach 1365.*	Q 100 yr	71,60	17.35	19.83	20.			34,46	45,81	0.68
						0.005485	1.74	13.88	15,67	0.54
Reach 1355.*	0.2 yr	24.10 34.50	17.30 17.30	19.05 19.28	19. 19.			17:51	21,00	0.62
er Reach 1355.*	Q 5 yr Q 10 yr	43.50	17.30	19.41	19.1			21:29	29.53	0.64
Reach 1355.*	Q 20 yr	51.60	17,30	19,53	19.			24,89	35,02	0.66
er Reach 1355,*	Q 50 yr	62.50	17.30	19.66	19.1 20.			30.01 34.87	41.05 47,82	0.68
r Reach 1355,*	O 199 yr	71.60	17.30	19.77	20.	0.000242	1411			
r Reach 1345.7	Q 2 yr	24.10	17.24	18.99	19.			13.86	15.91	0.59
r Reach 1345.*	Q 5 yr	34.50	17.24	19.22	19.			17.95	21,86 30.53	0.62 0.64
er Reach 1345.*	a to yr	43,30	17.24 17.24	19,35 19,46	19.			21,41 25.04	39.53	0.66
n/Reach 1345,* er Reach 1345,*	G 20 yr O 50 yr	51.60 62.50	17.24	19,60	19.	0.006322	2,49	30.25	42.19	0.58
er Reach 1345.*	Q 100 yr	71.50	17,24	19,71	25.		2.60	35.41	49,57	0.69
					1	o corre	1,75	13.80	16.12	0.60
ar Reach 1335,*	Q 2 yr	24,10 34,50	17.19 17.19	18.93 19.16	19,1 19,1			17,94	22.62	0.63
ar Reach 1335.* ar Reach 1335.*	Q-5 yr Q-10 yr	43,30	17.19	13.10	19.		2,14	21.48	31.48	0.63
er Reach 1335.*	G 20 yr	51,60	17.19	19,40	19.	7 0.005330		25,14	36.54	0.67
er Reach 1335,*	Q 50 yr	€2.50	17.19	19.53	19. 19:		2,49	30,47 36:04	44,11 51.58	0.69 0.59
er Reach 1335.*	Q 190 yr	71.60	17.19	19.65	19.	n.noczec	2,03	20.23	1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1	. <u> </u>
or Reach 1325.*	Q 2 yr	24,10	17.14	18.88	19,		1.76		16.33	0.61
	The state of the s	34.50	17.14		19.	0,005836	1.94	17.92	23.43	0,64

C-RAS Plan Reach	: Salvin-Final-09 River: Sa River Sta	Min Ck Reach: Up: Profile	oer Reach (Conti: O Total	Min Ch El	W.S.Ekv	Crit W.S.	E.G. Elev	E.G. Slope	. Vel Chril	Flow Area	Top Width	Froude # Ch
		4	(m3/s)	(m)	(m)	(m):	(m) 19.46	(m/m) 0,005960	(m/s) 2.14	(in2) 21.55	(m) 32.25	G.
oper Reach gor Reach	1325.*	0 10 yr	43.30 51.60	17.14 17.14	19,23 19,34		19,61	0.005360	2.31	25.25	37.58	0.
per Reach	1325.*	Q 50 yr	62.50	17,14	19.47		19,78	0.006177	2.49		46.28	0.
per Reach	1325.7	G 100 yr	71,60	17.14	19.59		19.92	0.005881	2.57	35.84	53.77	0.
por Reach	1315.*	Q2yr	24,10	17.09	18.61		15,97	0.505941	1.78	13.56	16.50	0.
per Heach	1315.*	QSyr	34,50	17,09	19.04		19.24	0,006028	1.95	17.86	24,19	0. 0.
per Reach	1315.*	Q 10 yr	43.30 51.60	17,09	19.17 19.27		19.40 19.54	0,00£110 0.00£277	2.14 2.31	21,60 25,34	33.10 38.57	0.
per Reach per Reach	1315.*	Q 20 yr Q 50 yr	62.50	17.09	19.41		19.72	0.006242	2.48	31.22	48.19	9.
per Reach	1315.1	Q 100 yr	71.60	17.09	19.54		19.85	0,005611	2.55	37,91	56.80	0.
5	report.	Q 2 yr	24,10	17.03	18.75		18.92	0.005976	1,81	13,35	16,62	0,
per Reach	1305.*	Q 5 yr	34.50	17,03	18.98		19.18	0.005936	1,97	17,76	24.91	C.
per Reach	1305.*	Q 10 yr	43.30	17.93	19.11	134	19.34	0.005949	2.15	21.54 25.43	34,07 40,25	0. 0.
per Reach	1305.*	Q 20 yr	51.60 62.50	17.03	19.21 19,35		19,48 19,68	0.006114	2.32 2.46	31.79	50,56	
per Reach per Reach	1305.* 1305.*	C) 50 yr	71.50	17.03	19,49		19.80	0.005401	2.52	39.32	58.93	0
-			V 1-4-1			3.3			0.24	40.04	15.61	0
per Reach	1295.*	O 2 yr	24.10 34.50	16.98 16.98	18.68 18.91	31 925 mass d	16.65 19.11	0.006495	1.85 1.99	13.01 17.55	25.37	0
per Reach	1295.*	Q 10 yr	43,30	16.98	19:05		19.28	0.008179	2.17	21,61	35.15	9.
per Reach	1295.*	Q 20 yr	51.60	18.58	19.15		19,42	0.005341	2.34	25.49	42,42	0
per Reach	1295."	Q 50 yr	62.50	16.98 16.98	19.29 19.44	<u> </u>	19,59	0.005961	2.46 2.48	32.58 41.12	53,61 61,84	0
per Reach	1295.*	Q 100 yr	71,60	F0.56	19.44		12,47		Territorial de la			
per Reach	1265.	Q 2 yr	24,10	16.93	18.59		18,78	0.007088	1,95	12.36	16.27	0
per Reach	1285.1	Q 5 yr	34.50	16.93 16.93	18.63	18.76	19.05 19.22	0,006779 0,006459	2.06	16.88 20.97	24.33 35.30	0
per Reach per Reach	1285,* 1285.*	O 10 yr	43,30 51,60	16.93	19,07	18.85	19.35	0.008559	2.39	24.90	43.46	O
per Reach	1285.*	Q 50 yr	62.50	16.93	19.24		19,53	0.005664	2,45	33.50	56.65	0
per Reach	1285,1	Q 100 yr	71.60	15.93	19,40		19.68	0,004775	2.43	43.26	64.85	0
per Résch	1275	Q 2 yr	24.10	16,88	18,40		18.68	0.011308	2.38	10.13	13.99	0
per Reach	1275	Osyr	34.50	16.88	18,60	18.56	18.94	0.012517		13.36	17,69	0
per Reach	1275	G 10 yr	43,30	16.88	18.74	18.71 18.83	19,11 19,26	0.012748 0.011414	2.72 2.82	16.01 19.26	22,37 32,91	0
per Reach per Reach	1275	0.20 yr 0.50 yr	51,60 62,50	16.85 16.88	18,65 19,19	16.63	19,48	0.005618	2.43	35.00	59,42	
per Reach	1275	Q 100 yr	71.50	16.88	19.35		19,63	0,004505	2.37	46,12	68,00	
					40.00	18,22	18.57	0,013097	2,46	9,80	14,45	0.
per Reach per Reach	1265.* 1265.*	0.2 yr	24.10 34,50	16,80 16,80	18.26 18.48	18,45	18.81	0.013612	2.63	13:12	16.33	0.
per Reach	1265.*	Q 10 yr	43.30	16.80	18,59	18,58	18.98	0,013372	2,79	15,53	19.36	0
per Reach	1265.1	O 20 yr	51.50	16.80	18.78	18,68	19.14	0.009519	2.67 2.22	20.35 39.13	32,12 60,35	0. 0.
per Reach	1285,*	Q 50 yr	62.50 71.60	16.60 16.80	19,17	`	19.58	0.003426	2.18	50.86	69.03	0.
per Reach	1269,	LI 100 y	11.50		10,00				e territa		1,000,000	in Dawii Ing
per Reach	1255.*	CI 2 yr	24.10	16.70	18.17		18.43	0.011429	2.26	10,68	16,17 18,74	0. 0.
per Reach	1255.	Q 10 yr	34.50 43.30	16,70 16,70	18,34 18.53	18.30 18.42	18.85 18.85	0.012307	2.52 2.51	13,70 17,25	19.91	0
iper Reach iper Reach	1255.*	0 20 91	51.60	16.70	18,75	18.53	19,04	0.005298	2,37	23,20	35,59	0
per Reach	1255	C) 50 yr	62.50	16.70	19.19	E	19,38	0.002586	1,89	45.24	63,28	0
per Roach	1255.1	Q 100 yr	71,50	16.70	19.36	.71.	19,53	0,002101	1,94	57.65	70.42	0
per Reach	1245.	Q27r	24.10	16,60	18.05	18.00	18,31	0.012549	2.26	18,58	17.07	O.
per Reach	1245.1	Q 5 yr	34.50	16.60	16.22	18,17	18.54	0.012069	2,50	13,77	16.65	0
per Fleach	1245.*	Q 10 yr	43.38 51.50	15,60 15,60	18.47		18.75 18:97	0.007498	2.34 2.18	18.55 26.30	20.83 40.41	0
per Reach per Reach	1245.1	Q 50 yr	62.50	16.60	19.17		19.33	0.002326	1.84	49.42	61.78	0.
per Reach	1245.1	O 100 yr	71,60	16.60	19,35		19.51	0.002054	1.85	60.82	67.84	. 0
	2007.8		24,10	16.50	17,99	9	18,19	0,008770	2.01	12.91	17,92	0
per Reach per Reach	1235."	Q 2 yr Q 5 yr	24,10 34,50	16.50	18.17		18,43	0.008466	2.26	15.27	18.43	Đ
per Reach	1235.*	O 10 yr	43.30	16.50	16,45		18.67	0.005452	2.11	20,62	22.30	9
per Reach	1235 *	Q 20 yr	51,60	16.50	18.72 19,15	<u>. N.</u>	18,92 19,31	0,003591	1,99 1,72	26.99 52.33	39,72 61,58	0
oer Reach oer Reach	1235.* 1235.*	Q 50 yr	62.50 71.60	16.50 16.50	19.34		19,48	0.001652	1.74	63.73	68.05	<u> </u>
							72.63			2	1720	
oer Reach	1725.	Q 2 yr	24,10 34,50	16.50 16.50	17.60	17,76	18.07 18.34	0.007650	2.34 2.20	10,31	17.29 18.32	0
er Reach er Reach	1225.*	Q 5 yr	34.50 43.30	16.50	18,10		18,61	0.004766	2.01	21,93	25.87	Q
perRoach	1225.1	Q 25 yr	51.50	16.50	18,70	(4 st	18,87	0.003089	1.88	31,85	43.32	
er Reach	1225.	Q 50 yr	£2.50	16.50 16.50	19,16 19,34		19.28 19.46	0.001571	1.62	56.85 58.54	68.74	
per Reach	1225.*	Q 100 yr	71,60	16.50	18.04		127.401	4,20,1442				
per Reach	1215.*	Q 2 yr	24,10	16.40	17,89	17,63	17,94	0.911475	2,21	10.89	17.21	
er Reach	1215.*	O 5 yr	34.50	16,40	18.07		18.28 18.55	0:005313 0:003495	1,96	17.58 24.77	18,30 39,22	2
oer Reach oer Reach	1215.*	Q 10 yr	43.30 51,60	16.40 16.40	18.69		18,64	0.003455	1,73	36.23	47.11	C
er Reach	1215,1	Q 50 yr	62.50	16,40	19,18		19,26	0,091265	1.51	51.76	88.18	
er Reach	1215,	Q 100 yr	71.60	15.40	19,33		19,44	0,001189	1.55	73,20	67.93	
or Reach	1205.*	Q 2 yr	24.10	16.30	17.63		17.83	0.008435	1.98	32,17	17.15	
oer Reach	1205.*	Q.5 yr	34.50	16.30	18.05		18.20	0.004360	1,76	19,62	18.43	
	1205,"	© 10 yr	43.30	16.30	18.38		18,52	0.003026	1.67	27.22 38.93	39.75 46.45	
per Reach	1205.*	O 20 yr	51.60 62.50	16:30 16:30	18,68 19,15		18.81	0.002137		54,60	52,39	- 0
per Reach per Reach	1205.*	Q 100 yr	71.60	16.30	19.33		19,43	0.001151	1.46	76.25	58.20	0
per Reach per Reach per Reach	1205.*											
per Reach per Reach per Reach per Reach	1205.*											
per Reach per Reach per Reach per Reach	1195.1	QZyr	24.10	16.20	17.58 18.03		17,75	0.005705	1,63	13,42 21,19	16.90 18,18	0
per Reach per Reach per Reach per Reach		Q 2 yr Q 5 yr Q 10 yr	24.10 34.50 43.50	16.20 16.20 16.20	17.58 18.03 18.37		17,75 18,16 18,49	0.005705 0.002689 0.002167 0.001563	1.63 1.63 1.57 1.51	13,42 21,19 29,46 42,16	18,18 18,18 33,51 47,51	

	Salvin-Final-09 River: Salvin C River Sta	Profile	O Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chal	Flow Area	Top Width	Fraude # Chi
Reach	LIVE DUI	Fibre	(m3/s)	(m)	(m)	(m)	(m)	(m/m)	(m/s)	(m2)	(m)	
		Q 100 yr	71.60	16.28	19.33		19,42	0.000892	1.41	79.56	66.27	0.0
por Reach	1195."	Ci ton At	11.50	10.20	10.00					1		
	1185.*	Q 2 yr	24.10	16,10	17.56		17,69	0.004448	1.56	15,45	17,13	0.4
per Reach			34.50	16,10	18.02		18,13	0.002675	1.47	23.54	19.30	Đ.
oper Reach	1185,*	Q 5 yr	43,30	16.10	18.35		18.45	0.002165	1,43	33.24	38.64	0.5
pper Reach	1185.1	Q 20 yr	51.60	16,10	18.67		18.77	8.001609	1.39	46,30	46.54	0.5
pper Reach	(185.)		62.50	16.10	19,15		19.22	0,000988	1,26	72.12	61,90	0.3
pper Reach	1185,:	Q 50 yr	71,60	16,10	19.33		19,43	0.000964	1,31	83.52	66.18	. 0.3
pper Reach	1185."	C 100 yr	7,.00	120110	130123						1111	1
	1175."	C 2 yr	24,10	15.00	17,55		17.65	0.002583	1.45	17.23	17,12	0.
pper Reach			34.50	16.00	18,00		18,10	0.001846	1.35	25.67	23.51	0.
pper Reach	1175.	Q 5 yr	43,30	16.00	16,35		18,44	0,001335	1.34	35.59	38,17	9,3
	1175;'	Q 10 yr	51,60	16.00	16.67		18.75	0.001025	1.31	49.97	47.19	0.3
	1175,1	O 20 yr	62.50	18:00	19.14		19.21	0.000563	1.22	75:77	60,65	0.2
pper Reach	1175.*	Q 50 yr	71,60	18.00	19.32		19.39	0.000561	1.27	85.69	64.98	0.
per Reach	1175.	Q 100 yr	71,00	13.00	10.002							196 5.5
			24,10	15.90	17.53	·····	17.65	0.002852	1.28	18.79	17.24	0.
oper Reach	(165.)	O 2 yr	34.50	15.90	17.99		18.07	0.002349	1.27	27.69	24.86	.0.
oper Reach	1185.*	O.5 yr		15,90	18,34		18.42	0.001766	1.27	38.65	38.57	0.3
oper Reach	1165,*	O 10 yr	43.30	15,90	18.56		18,74	0.001356	1,24	52,42	47,92	8,
per Reach	1165,*	O 20 yr	51,60	15.90	19.14		19.20	0.000884	1.14	78.46	59.80	0,
per Reach	1165,*	O 50 yr	62.50 71.65	15.90 15.90	19,14		19.38	0,000881	1.19	89.51	64,49	8.
oper Reach	1185.*	O 100 yr	71,60	(0.90)	13,34		,5,00				*******	
				15.90	17.51		17.58	0.002478	1,19	20,23	17,01	0.
oper Reach	1155.1	Q 2 yr	24.10		17.97		18.05	0.002129	1,21	29.05	25.20	Đ.
oper Reach	1155.*	Q 5 yr	34.50	15,90 15,90	18.33		18.41	0.001627	1,21	49,47	37.86	O.
per Reach	1155.*	Q 10 yr	43.30		18.65		16.72	0.001286	1.20	53.87	46.10	G.
pper Reach	1155.*	Q 20 yr	51,60	15.90			19,19	0,000854	5,11	79.57	59.65	ű.
pper Reach	1155.*	Q 50 yr	62,50	15.90	19,14		19.37	0,000856	1,16	90.65	65.92	0,
oper Reach	1155.*	CI 100 yr	71,60	15.90	19.31		(2.31)	0,00000				
					17,49	15,56	17.54	0,004493	0,98	24,49	17.28	0.
oper Reach	1145	O 2 yr	24,10	15,78			18.01	0,004184	1,05	34.07	27.40	0.
per Reach	1,145	Q 5 yr	34,50	15.78	17.96	16.74	18.38	0.003428	1.07	45.93	37.81	0.
per Reach	1145	Q 10 yr	43.30	15.78	18,32	16.88	18.30	0.002865	1.07	59.50	46.58	0.
pper Reach	1145	O 20 yr	51,60	15.78	18.64	17.00	19,18	0.002883	1.91	85.47	51.78	0.
pper Reach	1145	Q 50 yr	62.50	15.78	19,13	17.14			1,05	97,30	70,61	0.
pper Reach	1145	O 100 yr	71.60	15.78	19,31	17,26	19.36	0.001989	1,03	\$7,00	(31,46)	
									1.3		, , , , , , , , , , , , , , , , , , , 	
oper Reach	1144 Pine Mountain Rd		Culven									
								0.009499	1,57	15.56	13.63	Ď.
pper Reach	1115	Q 2 yr	24.10	14,35	16,24	15.46	16.37			29,17	14,29	D.
oper Reach	1115	Q 5 yr	34.50	14,36	16.55	15.71	16.72	0.007565	1.87	23,43	14.78	0
per Reach	1115	Q 10 yr	43.30	14.35	16.77	15,89	18.98	0.008406	86,5	33,08	25.94	
per Reach	1115	Q 20 yr	51,60	14,36	17.00	15,05		0.007641	2,12		27,80	0
per Reach	7115	Q 50 yr	62.50	14.35	17,21	15,31	17.45	0.008090	2.29	38.75	30.64	0
per Reach	1115	D 100 yr	71,60	14,36	17.38	16,48	17,64	0.006213	2,42	43,73	40.04	
										45.00	13.51	0.
oer Reach	1109.*	O 2 yr	24,10	14,36	16.19	15.46		0.007204	1,62	15.26	13.51	0
per Reach	1109.*	05 yr	34,50	14,36		15.71		0,008575	1.95	19.25	14,14 14.61	0
oper Reach	1109,*	Q 10 yr	43.30	14.36	16,69	15.89		0.009469	2.17	22.31 31.20	25.32	0
oper Reach	1109.1	Q 20 yr	51.60			16.08		0.008632	2,20			0
per Reach	1109.7	Q 50 yr	62.50			16.31	17.39	0,009008	2.38	36.65	27.09	
per Reach	1109.7	Q 100 yr	71.60	14.36	17.30	16.48	17.58	0.009196	2.51	41,36	29.37	<u> </u>
								<u> </u>	ļ			C
per Reach	1103	Q 2 yr	24.10	1,4,36		15.48		0.008108		14,49	13.39	
per Reach	1103	Ci 5 yr	34.50	14.36		15.71	16,61	0.009812	2.03	18.19	13.98	
per Reach	1103	O 10 yr	43,30	14.35		15.89		0.010923	2.28	21.03	14.42	
per Reach	1103	O 20 yr	51.60	14.36		16.00			2.46	23,66	14.81	
par Reach	1103	C) 50 yr	62.50	14.36	17.04	15.31	17,33		2,50	34,21	25.31	
per Reach	1103	G 100 yr	71,60	14.35	17.21	15,48	17,52	6,010493	2,62	38,77	27,91	3
		1	2 4 4 2					<u> </u>				<u> </u>
per Reach	1095	Q 2 yr	24.10	14.36	16.13		16.24	0.001983	1,46	16,66	17.83	1
per Reach	1095	Q 5 yr	34.50	14.36		1	16.56		1,65	22.39	21,05	
per Reach	1095	G 10 yr					16.80		1,78	27.18	22.91	
	1095	Q 20 yr					17.01	0,002303	1,87	31.85	24,59	
	1095	Q 50 yr	62.50				17.27	0.002343	1.98	37,68	26.58	
per Reach		Q 100 yr.	71.60			1	17.46	0.002406	2,08	42.54	28.45	
oer Reach per Reach		- 100 yrs	1	,	1		1	T				
per Reach per Reach	1095				<u> </u>	1	16.10	0.002504	1.48	21,40	29,78	
per Reach per Reach per Reach		D 2 1#	24-17	12.07	15.89							
per Reach per Reach per Reach per Reach	1035	O 2 yr	24.10		15.99 16.29	<u> </u>		0,002535	1,63	21,26	35,53	
per Reach per Reach per Reach per Reach per Reach	1025 1035	Q 5 yr	34,50	14.07	16.29		15,41	0,002535 0,002333		21,26 39,65	35,53 38,00	
per Reach oper Reach oper Reach oper Reach oper Reach oper Reach	1035 1035 1035	Q 5 yr Q 10 yr	34,50 43,30	14.07 14.07	16.29 16.52		15.41 16.65	5.002333	1.71			
per Reach per Reach per Reach oper Reach oper Reach	1025 1035	Q 5 yr	34,50	14.07 14.07 14.07	16.29 16.52 16,73		15,41	0.002333 0.002117	1.71	39.65	38,00	

Reach RiverSta	Salvin Ck Reach: Lower Profile	O Total	Min Ch El		Cit W.S.	E.G. Eliv	E.G. Slope	Vei Clini		Top Width	Froude # Ch
		(m3/s)	(m)	(m)	(m)	(m)	(m/m)	(m/s) 3.11	(m2) 15.30	(m) 18.28	3.
r Reach 913	Q 2 yr	47,35	13,22	14,65	14.65	15,14 15,55	0.016239	3,45	20.93	20,15	5
r Reach 913	0.5 yr	69,10	13.22	14.96	14,96	15.84	0.013306	3.69	25,13	22.02	0
r Reach 913	O 10 yr	86.30	13.22	15.16	15.37	15,11	0.012203	3.67	30,61	29.98	. 0.
r Reach 913	Q 20 yr	104.60	13.22	15.60	15.60	18,41	0.011574	4.09	37.94	33,43	0.
Reach 913	Q 50 yr Q 100 yr	147.10	13.22	15.83	15,83	16.65	0.010268	4,15	46.54	42.60	. 0,
Reach 913	0.10031	144.00									<u> </u>
Reach 865	QZYI	47,30	11.65	14.02	13.61	14,13	0.002818	1,54	31.61	31:91	. 0.
r Reach 865 r Reach 685	Q.5 yr.	59,10	11,66	14.40	13.80	14.53	0.002088	1.63	44.30	32.85	. 0.
r Reach 865	Q10 yr	65.30	11.66	14.59	13.93	14.83	0.051755	1,69	54.28	36.82	0.
Reach 865	Q 20 yr	104.60	11.66	14.95	14.06	15.10	0.001621	1.78	63,94	35.05	0.
Reach 885	Q 50 yr	127.60	11,65	15.38	14.21	15.53	0.001218	1,76	81,57	48.00	0.
Peach 865	0 100 уг	147.10	11.66	15.83	14,33	15,98	0,000695	1.69	104.15	52.38	D
rReach 805	Q2W	47,30	11.60	13,24	13,15	13,72	0.015197	3,05	15.53	13.15	0
(Reach 805	Q 5 yr	69.10	11.50	13,70	13.50	14.21	0.013108	3.15	21.98	16.96 34.22	
Reach 805	Q-10 yr	86,30	11.60	34,10	13,75	14,57	0.009299	3.04	31.73 41.17	37.86	0.
r Reach 805	O 29.yr	104.60	11.50	14.36	14.00	14.65	0.000373	3.16 2.63	74.03	54,23	Ø.
Peach 805	O 50 yr	127.60	11.60	15.06	14.31	15.37	0.003953	231	105,43	55:61	0.
Reach 505	Q 100 yr	1,47,10	11.60	15,63	14,49	15.86	0.002373	£.0(;		30.07	
					40.00	12.45	0,003478	2,11	22.37	14.87	.0.
(Reach 757	Q2yr	47.30	11,19	13,22	12.63	13.45	0.003478	2.33	29,62	16,69	0.
Reach 767	Q 5 yr	69.10	11.19	13.66		14.36	0.002970	2.35	35.68	18.30	0.
r Reach 767	Q 19 yr	66.30	11.19	14,08	13,23	14,65	0.003105	2.53	41,32	20.34	0
r Reach 767	G 20 yr	104.60	11,19	15.05	13.72	15,27	0.001661	2,12	80.46	106.72	. 0
Reach 767	O 50 yr	127.60	11,19	15,68	13.93	15.78	0.000716	1,58	202.41	174.48	. 0
Reach 767	Q 100 yr	147.10	11.19	(2,00)	10,00	100,00					
m (ma		Bridge									
Reach 736 Creek Road I	JIKEJ .	SINGU									
	573	47,30	11.12	12.92	12,23	13.08	0.003949	1.75	26.99	15,54	0
Reach 735	02y 05y	69.10	11.12	13.29	12.50	13,51	0.004450	2.06	33.19	16,55	٥
Reach 735	D 10 yr	86.30	11.12	13.74	12.70	13.97	0.003762	2.13	40,59	16,73	0
	Q 20 yr	104.60	11.12	13.88	12.89	14.58	0,004655	2.43	42,96	15.75	0
	Q 50 yr	127.60	11.12	14.06	13.11	14.45	0,005615	2.77	45.08	15.77	
Reach 1735 Reach 1735	G 100 yr	147,10	11,12	14:17	13,30	14,65	0.005628	3,07	47.95	16,78	.0
Pagell 135	9.44.)	*****			ì						
Reach 870	0.2 yr	47.30	11.00	12.80	12.05	12.88	0.001608	1,23	38.88	30.75	
Reach 670	QSyr	69,10	11,00	13,20	12.28	(3.30)	0.001442	1.39	52.25	38.30	
Reach 1670	O 10 yr	85.30	11.00	13.71	12.41	13.79	0.000884	1.28	74.57	54,47	0
Reach 579	10 20 yr	104.50	11.00	13.86	12.56	13,95	0.001007	1.42	62.30	56.44	0
Reach 570	Q 50 yr	127.60	11.00	14,07	12,73	14,18	8,001081	1.55	93.06	68.18	
Reach 570	Q 100 yr	147.10	11,00	14.20	12.67	14.33	0.001185	1,68	99.88	72,71	0
				l'a							
Reach 498	Q.2.yr.	55,40	9.50	11.91	11.35	12.13	0.011623	2.17	35,47	40.01	
Reach 488	Q 5 yr	92.00	9.50	12,86	11.90	12.93	0.002579	1,14	89.51	52.24	0
Reach 488	Q 10 yr	111.20	9,50	13.54	12.09	13.59	0.001126	0.86	114,44	56.84	
Reach (485	Q 20 yr	129.50	9.50	13.67	12.24	13.74	0.001249	0.93	121,22	58.48	
Reach 498	Q 50 yr	153,20	9,50	13,87	12.34	13.95	0.001324	1.00	131.32	60.32	
Reach 486	Q 160 yr	171.70	9,50	13.99	12.41	14.07	0.001428	1.06	137.25	60.55	
									47.17	22.70	
Reach 430	Q2yr	65,40	8.98	11.72	10.33	11,82	0.002637	1.39	88.25	72.34	
Reach 430	Q5yr	92.00	0.90	12.77	10.64	12.64	0.001198	1.22	122.73	79.83	7
Reach 430	Q 10 yr	111.20	8.98	13.49	10.84	13.54	0.000728	1.09	128.77	80.56	
Reach 430	O 20 yr	129.50	8.98	13.51	11.02	13.68	0.000863	1.34	337,99	81.85	
Reach 430	Q 50 yr	153,20	8.98	13.61	11.23	13.88	0.000992		194,80	£3.21	
Reach 430	Q 100 yr	171.70	6:38	13.97	11.39	14,02	0.000550	1.02	107,00	4941	
						11.61	0.000845	1.35	48:19	22,65	
Reach 420	Q2yr	65,40	8,90	11,71	10.24	12.83	0.000458	1,30	70.78	72.09	
Reach 420	Q571	92.00	8.90	12.74	10.56	13.53	0.000352	1,29	86.38	79.50	4 11
Reach 420	O 10 yr	111.20	8.90	13,45	10.75	13,53	0.000352	0.94	168,17	80,65	2.1
Reach 420	10 20 yr	129,50	8.90 8.90	13.83	11.15	13.87	0,000417	1.01	184,10	82.02	
Reach 420	Q 50 yr	153.20 171.70	8.90	13.97	11.32	14.01	0,000438	1.95	195.72	83.16	51
Reach 420	(O 100 yr	17670	0.09	13.27	(),,,,,,			* 1			
		Calcadi							T I		
Reach 419.5 Dennington	OBUS	Culvert						ĺ	I		
n lear	02yr	65,40	8.80	11.19	10.05	11.35	0.002002	1.74	37.50	26,95	
Reach 385 Reach 385	05yr	92.00	a.so	11.59	10.35	11.62	0,002341	2.10	43.91	37.29	
	Q 10 yr	111.20	8.80	11.85	10.58	12.12	0.002542	2.32	48.00	37.66	
Reach 385	0.20 yr	129.50	8.80	12.06	10.74	12.39	0.002730	2.52	51,48	37,98	
Reach 365	0.50 yr	153.20	8.80	1232	19.96	12.71	0.002947	2.75	55.65	38,37	
Reach 365	0.100 yr	171.70	6.80	12,50	11,13	12.94	0.003122	2.98	58.67	38.84	
47-144		1								الرب المنتقدة	
Reach 348	0.2 yr	65.40	8.01	11.02	1	11.20	0,010721	1.92	39,78	25,92	
Reach 348	Q 5 yr	92.00	6.01	11.43		11,55	0,011503	2.18	50,77	26.34	
React 346	0.10 yr	111.20	8.01	11.69		11.93	0.011517	2,30	59.57	37.42	
Reach 348	0 20 yr	129.50	8.01	11.92		12,15	0.010955	2.35	58,30	37.77	
Reach 348	Q 50 yr	153.20	8.01	12.20		12.44	0.010109	2.37	79.14	38,19	
Reach 348	Q 100 yr	171,70	B.01	12.40		12.65	0,009662	2,40	86,82	38.49	
LINEOU D'O	<u> </u>				, 1						
Reach 257	Qʻzyr	E5.40	2.83	10,14		10.43	0.096642	2,44	33,63	27.77	
Reach 257	05yr	92.00	7,83	10.48		19,85	0.096737	2.78	43.33	29.32	
r Reach 257	0.10 yr	111.20	7.83	10.70		11.12	0.006809	2.99	49.76	30.81	
r Reach 257	Q 20 yr	129.50	7.83	10.88		11,95	0.006969	3.19	55,34	31.29	
r Reach 257	Q 50 yr	153,20	7.83	11.05		11.62	0.007685	3.51	\$0.76	33.86	
	The second secon	171.70	7.83	11.16		11.80	0,008221	3.74	64,71	35,68	

Piwor Sta	Salvin Ck Reach; Low Profile	O Total	Min Ch El			E.G. Eby	E.G. Slope	Vei Chai		Top Width	Froude # C
		(m3/s)	(m)	(m)	(m).	(m)	(m/m)	(m/s)	(m2)	(m)	I
ti 175	02W	65.40	7,21	9.80		9.89	0,005182	1.39	54.24		
h 175	Q.5 yr	92.00	7.21	10.18		10.29	0.005155	1,56	68.72	39.26	
n 175	O 10 yr	111,20	7.21			10,55	0.005150	1.67	78.86 91.24	47.56 66.60	
h 175	0.20 yr	129.50	7.21	10.64		10.78	0.004899	1,73	108.15	68.03	
h 175	O 50 yr	153.20	7.21 7.21			11.20	0,003957	1.72	129,34	58,44	
h 175	G 100 yr	38 787.78		i							
h (100	Q 2 yr	85.40	7.25		8,55	9.59	833200.6	1.06	77.61	51.52	
n 100	Q 5 yr	92.00	7.25		8.75	9,99	0.002849 0.002817	1.19	97.95 111.35	53.36 54,54	
h 100	10 10 yr	111.20	7.25		8.97 8.97	10,25	0.002855	1.36	124.20	61.03	
h 190	0 20 yr 0 50 yr	129.50 153.20	7,25 7,25	10.57	9.10	10.75	0.002744	1,42	149,15	76.77	
n 100 n 100	Q 100 yr	171.70	7.25			10.94	0.002655	1,45	163,68	77.75	1
										20.67	-
n 0	Q 2 yr	- 65,40	6,42	9.17	8,01	9,24 9,60	0.005449	1,12	58.15 69.35	32.67 33.99	
h 0	Q5yr	92.00	6.42 6.42	9.51	8.23 8.37	9,64	0.000086	1,44	77.05	34.85	
h 10 h 10	Q 18 yr Q 20 yr	111.20	6.42	9.93		10,05	0.006586	1,54	£4.20	35,56	
h ID h ID	Q 50 yr	153.20	5.42	10.18	8.65	10.32	0,006877	1,64	93.32	37.29	
th 0	Q 109 yr	171,70	8.42	10,37	8.77	10.52	0.006895	1,72	100,55	41.75	<u> </u>
						9.10	0,009914	1.64	35,54	29,46	
ah -1	Q 2 yi	65.40 92.00	6.25 6,25		 	9,44	0,010071	206	44.58	31,43	
л ј.1 uh -1	Q.5yr Q.10 yr	92.00 111.20	6.25		 	9.67	0.009711	2.17	51.29	32,69	
<u>h -1</u> h -1	G 20 yr	129.50	6.25			9.89	0.009163	2.24	57.89	33,70	
sh i-1	Q 50 yr	153.20	6.25	9.89		10.15	0.008401	2.30	66.74		
di 11	Q 100 yr	171.70	5.25	10.08		10.36	0.597643	2.33	73,78	26,60	-
		65,40	5.40	8,52	8.02	8.73	0.006155	1,47	47.69	52.68	
ah -2 ⊔h -2	Q2y Q5yr	92.00	6.40			9.10	0.004727	1,54	68.02	56.67	
h -2 :h -2	O 10 yr	111.20	5,40			9.36	0,004048	1,57	62.76		
n 2	O 20 yr	129.50	6.40			9,60	0.003562	1,60	97,20		
я́ -2	LO 50 yr	153.20	6.40			9.89	0.003081	1,62 1.64	116.52 131.75	67.61 70.93	
di -2	Q 100 yr	171,70	6.40	9,99	8.75	10.12	6,062799	2.04	131.15	70,00	
	0.35#	65.40	5.82	8.51		8.57	0.002135	1,07	61,00	37,38	
л 3 л -3	(0 2 yr Q 5 yr	92.00	5.82			8.96	0.002226	1.23	75.48	39.72	
h 1-3	Q10 yr	111.20	5,82			9.23	0.002220	1.32	85,90	41.26	
n la	Q 20 yr	129.50	5,82			9,48	0,002165	1,38	95,91 109,08	43.05 45.80	
rh 1-3	Q 50 yr	153,20	.5.82			9,78 10,01	0.002120	1,45 1.50	121.11	59.48	
a 3	0.100 yr	171.70	5.82	9.90		10,01	9,002040	*			
zh -3.5	Q 2 yı	65.40	6.22	8.19	<u> </u>	8,40	0.010975	2.01	32.56	25,74	
h -3.5 h -3.5	Q 5 yr	92.00	6.22	+		8.79	0.010270	2.21	41,71	27.15	
n - 1-3.5	□ 10 yr	111.20	6.22			9.05	0.009388	2.28	48.80	28.19	
h -3.5	Q 20 yr	129.50	6.22			9.31	0,009589	2.32 2.36	55.74 64.88	29,18	
л I-3.5	Q 50 yr	153.20	6.22 5.22			9.83 9.86	0,007693 0,007113	2.38	72.07	31.37	
d) -3.5	Q 100 yr	171.70	9.66	1	<u> </u>						L
a) 4	Qžyr	65.40	5.96	8.24	7,01	8,33	0.002485	1,33	49.09	25.93	
4 4	0.5 yr	92.00	5.98			8,72	0.002980	1,81	57,05	27,33	
ah 4	Q 10 yr	111.20	5.98				0.003157	1,77	68,89 68,24	28.34	
4	Q 20 yr	129.50	5.95 5.99				0.0032311	2.04	75.06		
ah -4	D 50 yr	153.20 171.70					0.003332	2.14	80.23	31,40	
da 14	Q 100 yr	171.75		1	İ		:				
ch -5 Donnington Str	ne .	Culvert								L	<u> </u>
						ļ <u>.</u>	0.001979		51,45	25.03	-
dt -6	QZyr	65,40	5.34			8,16 8,44	0.003979	1,87	56,31		
dh -6	0.5yr	92,09 111,20	5.34			8.64	0,003472	1.86	59.77		
ch -6 ch -6	Q 20 yr	129.50			7.22	8,83	0.003970	2.05	62,91	25.69	
on -9	Q 50 yr	153.20	5.34	8.79	7,43	9,05	0.004573	2.30	65,69	27.77	
d) -5	O 100 yr	171,70		8,91	7,59	9.22	0.005041	2,48	69.38	28.36	-
		<u> </u>			<u> </u>	8,14	0.003026	1.36	47.50	24.47	-
dn -6,5	O 2 yr	65.40				8.41	0.004418	1.74	52.83		
dh 1-65	10.5 yr 10.10 yr	92.00				6.61	0,005227	1,95	55.69		
ch -6.5 ch -5.5	020 yr	129.50				8,79	0.005901	2.13	60.71		
ch 1-6.5	Q 50 yr	153.20				9.02	0,006583	2.34	65.56		
ch -6.5	Q 100 yr	171,70	5.34	8.87	 	9.18	0.007236	2.48	69.20	28,19	
				7,89	<u> </u>	8.00	0.004289	1,46	44.76	29.36	
dh -7	0.5 yr	65.40 92.00				8.20	0.006723	1.91	48.60		
ch -7 ch -7	10.5 yr	111.28				8.35	0,008199	2.18	52.05	35,77	
cn -7 cn -7	O 20 yr		5.58	8.21		8,50	0.009444	2,40	55,47		
ch -7	Q 50 yr	153.20	5.58	£,32		8.68	0.010870	2,57	59.97		
di 7	O 100 yr	171.70	5.53	8.41	ļ	B.82	0.011817	2.85	63.45	41.37	+
		1	4,52	7,80	6.44	7.65	0,001858	1,04	72.14	77,60	1
ch -8	027	65.40 92.00		4			0.902502	1.30	91,45		
ch (-8 ch (-8	0.5yr 0.10 yr						0.003186	1.59	95.80	78.51	
ch -8 ch -8	Q 20 yr	129.50				8.14	0.003767	1.67	102,25		
ch -6	Q 59 yr	153.20	4.52	8,11			0.004422		109.54		
di 48	Q 100 yr	171.70	4,92	8.18	7,37	8,36	0.004859	1.99	115.34	79.60	4

		iver Sta	Reach: Lowe	Q Total	Min Ch El	W.S. Elev	Cra W.S.	E.G. Elev	E.G. Slope	Vel Chal	Flow Area	Top Width	Froude # Chi
Reach	D.	Ner Sia	, rem	(m3/s)	(m)	(m)	(m)	(m)	(m/m)	(m/s)	(m2)	(m)	
	-9		a 2 yt	65,40	5.06	7.76	5,50	7.78	0.000678	08,0	128.71	97.64	
ovor Reach	- AS - AS		Q 5 yr	92.80	5.06	7,81	5,81	7,85	0.001555	1.08	133.87		
ewer Reach		- 3000	Q 10 yr	111.20	5.06	7.86	7.02	7.91	0.002071	1.26	138.37		0.27
ower Reach	-9		0.20 yr	129.50	5.06	7.91	7.13	7.98	0,002549	1,42	143.18	98,79	0,30
.cwer Reach	1.9		Q 50 Yr	153,20	5.05	7.97	7.25	80.8	0.003131	1.50	149.90	99,23	0.34
ewer Reach	-9	**************************************		171.70	5.06	8.03	7,35	8.13	0.903542	1,73	155.50	59.59	. 0.38
awer Reach	-9	<u> </u>	O 100 yr	111,10	2.407								
				85.40	4.50	7.73	6,20	7,75	0,000456	0.58	160.55	109,91	0.13
Lower Reach	-10	March Control	O 2 yr	92.00	4,60	7.78	6,40			0.80	163.95	110:31	0.17
Lower Reach	-10	3.4.2	105yr	111.20	4.50	7,79	6.52			0.95	167.01	110.67	0.21
ower Reach	-10		10 10 yr		4.80	7.82	5.51			1.08	170.44	111,08	0.23
Lower Reach	-10		Q 20 yr	129.50	4.80	7,87	6,77	*****		1,25	175.40	111,66	0.27
own Reach	1-10		Q 50 yr	153.20	4.80	7.91	6,84			1,37	179.78	115.87	0.23
Lower Reach	-10		D 100 yr	-171,75	4.001	- A 1	0.07	1700	1				
						7,72	6.01	7.73	0.000234	0,45	239.00	137,48	0.0
Lower Reach	1-11		Q 2 yr	65,40	4,39		6.32			0,63			0.1
Lower Reach	-11		Q 5 yr	92,00	4.39	7.75	6.45		4				0.1
Lower Reach	1-11		G 10 yr	111.20	4,39		6,54	7.82			248,61		0.10
Lower Reach	-11		Q 20 yr	129,50		7,79		7.86	-		253,56		0.20
Levier Reach	[-11		Q 50 yr	153.20	4.39	7,83	6,69	7.86			257.95		0,23
Lower Reach	-11		Q 100 yr	171.70	4.39	7.85	6,77	7.90	0.001275	,,,,,	Curius		
	1			1					0,000452	0.69	142,46	139,11	0.13
Lower Reach	-12		10.5 Åt	65,40		7,78	.5,95	7.71			142.46	139.11	
Lower Reach	-12		Q 5 yr	92.00		7.70	6.17	-7.73				139.11	
Lower Reach	-12		Q 10 yr	111.20		7.70	6,30	7,74		1,16		139.11	0.2
Lower Reach	-12		O 20 yr	129.50	4:33	7.70	6.45					<u></u>	
Lower Reach	-12		Q 50 yr	153,20	4.33	7,70	6.56					1	
			O 200 in	171.70	4.33	7.70	5.53	7.80	0.003115	1,54	142,46	1 172.11	1 027

	Salvin-Final-09	River; Salvin	O Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chal	Flow Area	Top Width	Fraude # Chl
Reach	River Sta	rione	(m3/s)	(m)	(m)	(m)	(m)	(m/m)	(m/s)	(m2)	(m)	
	910		12.80	22,20	23.93	23.41	24.04	0.007618	1,42	8,99	8,59	0.44
Glengariff Trib	19.0	O 2 yr		22.20	24.11	23,64	24,27	0.011160	1.81	10.54	9.11	0.54
Glenganii Trib	910	Q 5 yr	19.10		24.20	23.81	24,44	0.014676	2.14	11,42	9.39	0,62
Glengariff Trib	910	Q 10 yr	24.50	22.20 22.20	24.28	23,94	24.58	0.017568	2.41	12,18	9.62	0.58
Glengariff Trib	910	Q 20 yr	29.30		24.40	24.12	24.77	0,020811	2,71	13.32	9,96	
Glenganti Trib	910	O 50 yr	36,10	22.20		24.25	24,94	0.020011	2.85	14.60	·	<u> </u>
Glengaritt Trib	910	Q 100 yr	41,60	22,20	24.52	24.23	24,34	5,02 (460)	2.00			<u> </u>
						77.11	22.36	0.011232	1.47	16.20	40,45	0.51
Glengariff Trib	730	Q 2 yr	12.80	20.66	22.23	22.11	22,59	0.007713	1,44	26.25	41,82	0.44
Glengariff Trib	730	O 5 yr	19.10	20.66	22,52		22.78	0.007713	1.42	34.70	42.94	0.40
Glengariii Trib	730	C 10 yr	24.50	20.66	22,72	22.33		0.005183	1.43	41,35	43.80	0.38
Glengariff Trib	730	Q 20 yr	29.30	20,66	22.87	22.39	22,93	0.003143	1.47	49.27	44.81	0,37
Glengariff Trib	730	Q 50 yr	36.10	20.66	23,05	22.48	23,11		1.56	53.63	45.35	0.38
Glengariff Trib	730	@ 100 yr.	41.60	20.66	23,15	22.54	23.22	0.004914	1,30	33,03	70.00	
									4 57	10.92	12,28	0.53
Glengariff Trib	510	Q2yr	17.10	17.99	20.05		20.17	0,009097	1.57	15.86	31.03	0.59
Glengariff Trib	510	Q 5 yr	25.50	17,99	20,28		20,44	0.011808				0.68
Glengaritf Trib	510	Q 10 yr	32.60	17,99	20,34	20,05	20.56	0.016687	2.13	17.77	35,81 39,21	0.68
Glengarilt Trib	510	Q 20 yr	38.80	17.99	20.38	20.25	20.67	0,021014	2,40	19,45		0.79
Glengaritt Trib	510	Q 50 yr	48.10	17,99	20.48	20.44	20,82	0.024906	2.65	23.59	46.56 67,36	0.79
Glengarilf Trib	510	Q 100 yr	55.60	17,99	20,60	20.60	20.91	0.023597	2.63	30,25	67,35	0.73
				i						d'a-		·
Glengarill Trib	410	Q 2 yr	17.10	17.21	18.92	18.61	19.18	0.010595	2,25	7.76	10.00	0.67
Glengariff Trib	410	Q5yr	25.50	17.21	19.23		19.45	0.008291	2.26	20.03	63.02	0.61
Glengariff Trib	410	Q10.yr	32.60	17.21	19,43		19.59	0,008215	2.09	33.33	71,87	0.53
Glengarilf Trib	410	Q 20 yr	39.80	17.21	19.57		19,70	0,005162	1.99	43.84	77.56	0.49
Glenganit Trib	410	Q 50 yr	48,10	17.21	19.71		19.83	0.004746	1.99	55.44	80,15	
Glengarilf Trib	410	Q 100 yr	55.50	17.21	19.81		19.92	0.004630	2:02	63,25	81.85	0.47
Glengariff Trib	330.*	O 2 yr	17.10	16,33	18.07		18,32	0,010952	2.21	7.73	7,61	0.69
Glengariff Trib	330.*	Q5yr	25,50	16,33	18.36		58,88	0.011116	2.54	10.62	12.58	0.71
Glengariff Trib	330.*	O 10 yr	32.60	16.33	18,56	48,35	18.92	0.011078	2,74	13,89	23.40	0.72
Glengaritf Trib	330.*	Q 20 yr	38.60	16.33	18.71	18.55	19.09	0.010759	2.84	18.55	38.98	0.72
Glengariff Trib	330.*	Q 50 yr	48,10	16.33	18.90		19.28	0.009830	2,90	27.20	47.94	0.70
Glengariif Trib	330."	Q 100 yr	55,50	16.33	19,06		19,40	0,008658	2,88	35,11	53.53	0.67
Cloring Co. C.												
Glengariff Trib	250.*	Q2yr	17.10	15,45	17.28		17,49	0.009497	2.05	8.34	8.10	
Glengarilf Trib	250.*	Q5yr	25.50	15.45	17,60		17:87	606800,0	2.29	11,58	12.14	0.65
Glengarilf Trib	250.*	Q10 yr	32.60	15,45	17.53	17.44	18.13	0.008553	2,45	14.72	16.10	0.65
Glengariff Trib	250.*	Q 20 yr	38.80	15.45	17,98	17.63	18.31	0.008487	2.60	17,59	22.08	9.65
Glengaril Trb	250.*	O 50 yr	48,10	15.45	18,18	17.83	18.55	0.008274	2.78	22,24	23,13	0.66
Glengarif Trib	250.*	Q 100 yr	55.50	15,45	18,33	18.01	18.73	0.008086	2.90	26,12	31.07	0.66
Gibigani IID	ESU:	ig tuby.	33.00	10.70								
C(170.*	Q2yr	17.10	14.57	16:32		18,58	0.013747	2.28	7,48	8.21	0.76
Glangariff Trib	170.	Q5yr	25.50	14,57	16.53	16,40	16.91	0.016762	2.73	9.35	9,12	0.86
Glengariff Trib		Q 10 yr	32,60	14,57	16.69	16,60	17.15	0.018031	3.01	10,88	10.55	0.91
Glengariff Trib	170.*	Q 20 yr	38.80	14.57	16.82	16.76	17.84	0.017947	3.20	12.36	1231	0.92
Glongariff Trib			48,10	14.57	16.99	16.95	17,60	0.017704	3.47	14.70	15.07	0.93
Glengariff Trib	170.*	Q 50 yr	55,50	14.57	17.11	17,10	17.78	0.017551	3.65	16.70	17.15	0.94
Glengariff Trib	170.	G IDU yi	35,50	74.07								
200000000000000000000000000000000000000		0.00	17.70	13,69	15,93	<u> </u>	16,02	0,003624	1,36	16,48	32.88	0.41
Glengariti Trib	90	O 2 yr		13.69	16.27		16,37	0.002829	1,44	28.78	38.75	American services and a service and a servic
Glengariff Trb	90	Q 5 yr	25,50	13.69	16.52	<u> </u>	16.61	0.002503	1,49	38.63	42.88	4
Glengariff Trib	90	Q 10 yr	32.60	13.69	16.72		16:82	0.002222	1.52	47.97	46.93	
Glengariff Trib	90	O 20 yr	38.80	~~~ ~~~~~~~~~~	16.98		17.08	0.002030	1,58	60,73	50.98	<u> </u>
Glengaritt Trib	90	O 50 yr	48.10	13.69	17.16		17,26	0.001944	1,63	69.98	52,86	0.34
Glengariff Trib	90	Q 100 yr	55.50	13.69	17,16		17,25	0,00,044	7,00	54.54		
						40.40	15,82	8,004270	1,61	10.60	9.98	0.50
Glengariff Trib	40	Q 2 yr	. 17:10	13,65	15.69	15.17		0.004270	1.80	14,17	11,52	0.52
Glengariti Trib	40	Q5 yr	25,50	13.65	16.02	15.44	16.19		1.92	17,53	18.80	
Glengariff Trib	40	Q 10 yr	32,60	13.65	16,26	15.64	16,44	0.004180	1.92	22.04	21,22	0.32
Glongariff Trib	40.	Q 20 yr	38.60	13,65	15.48	15,79	16.67	0,003674		~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~		
Glengariff Trib	40	Q 50 yr	48,10	13.65	16.75	15.98	16.94	0.003301	2.00	29.10		
Glengariff Trib	40	Q 100 yr	55.50	13.65	16,93	16.14	17,13	0,003040	2.05	36.19	45.62	1 0.5

city design



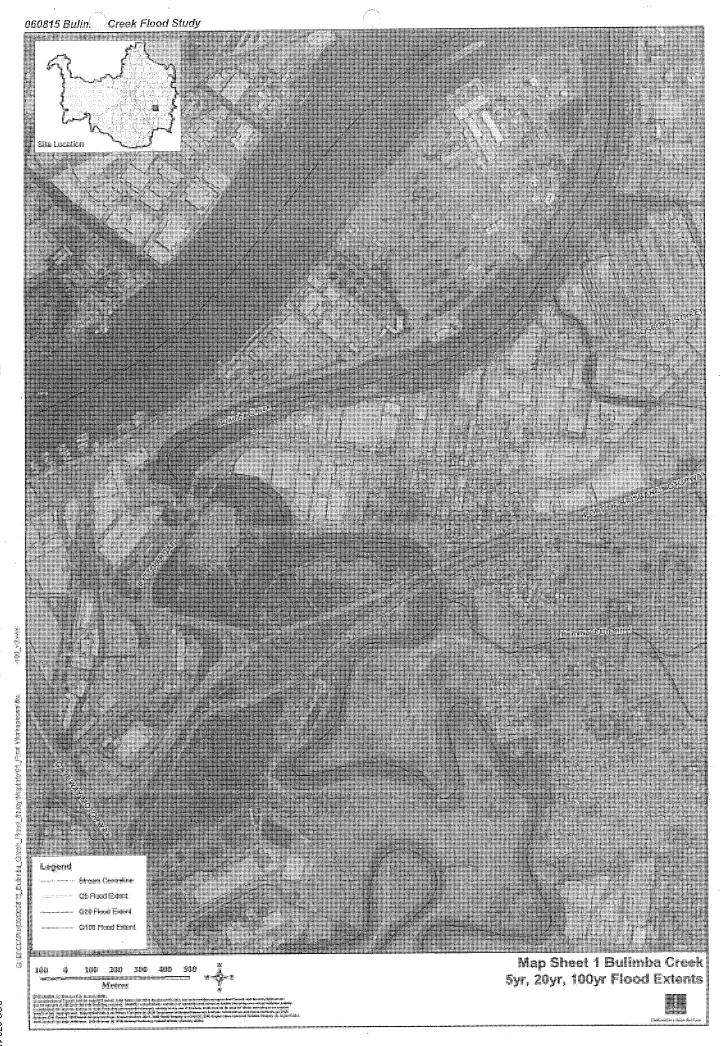
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Appendix J Flood Inundation Plots





Sullmba Crec Tood Study



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BCC.079.1254

BCC.079.1255

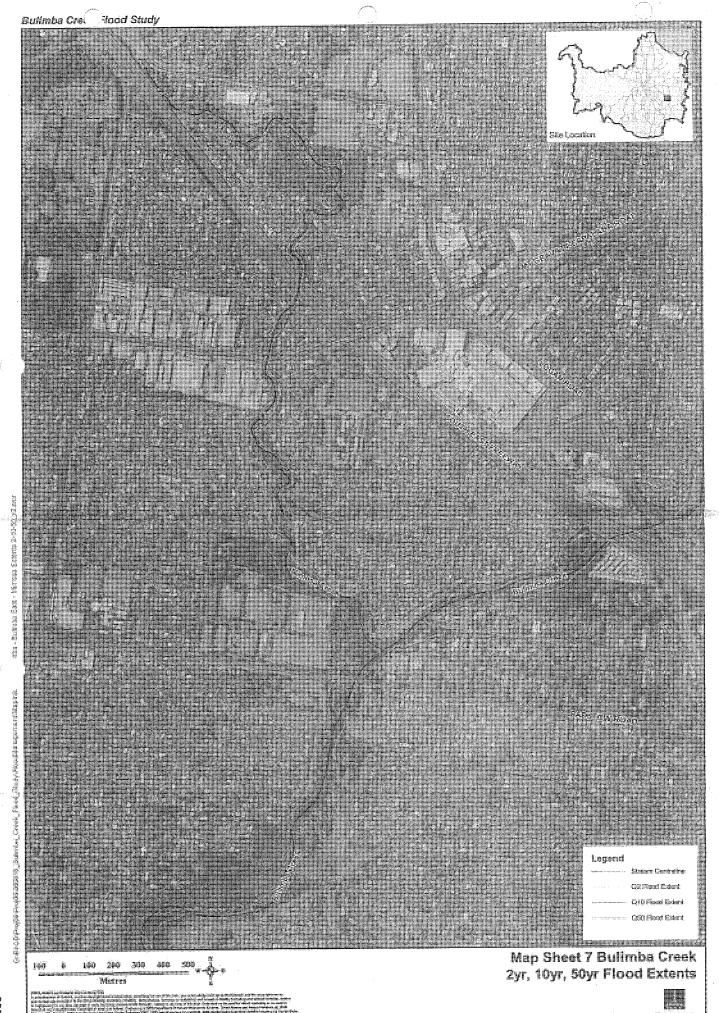
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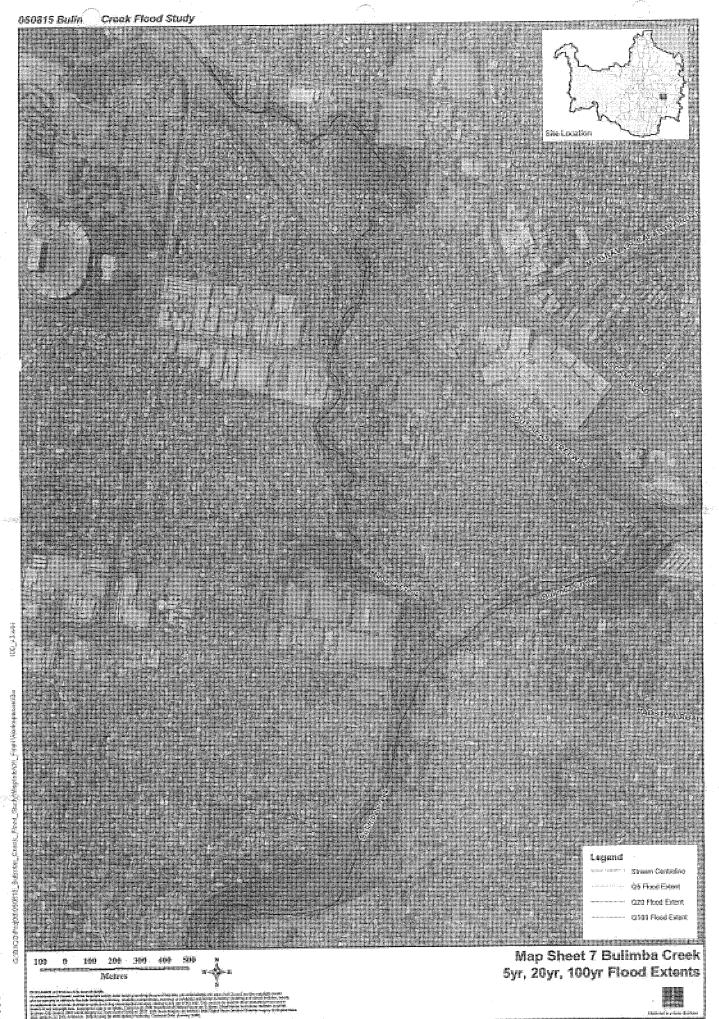
Bullmha Cree. Hood Study



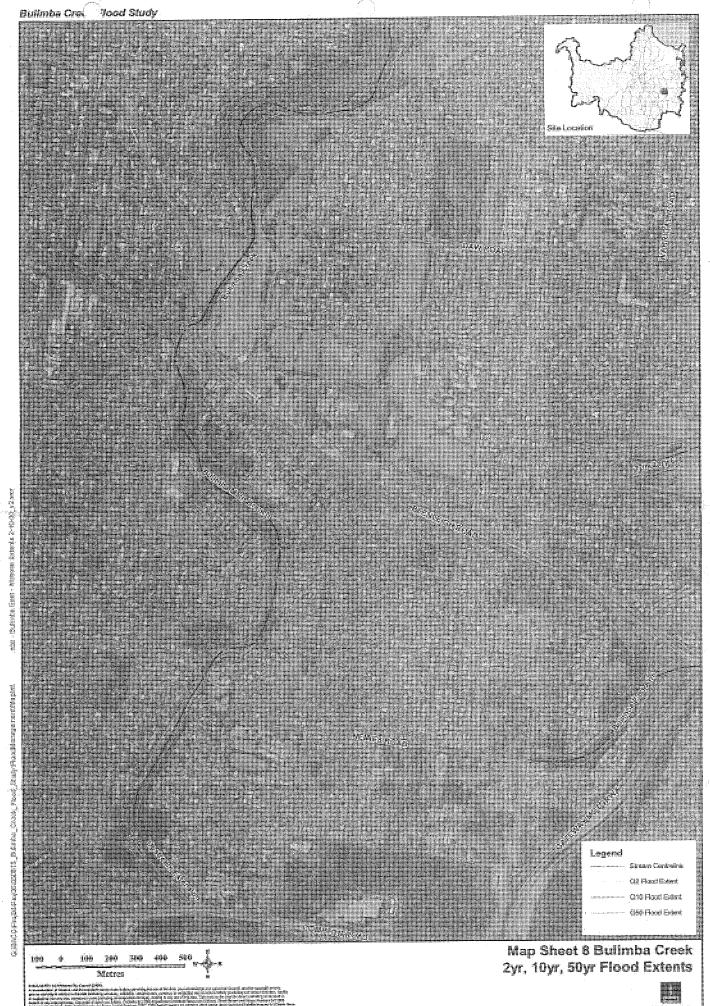


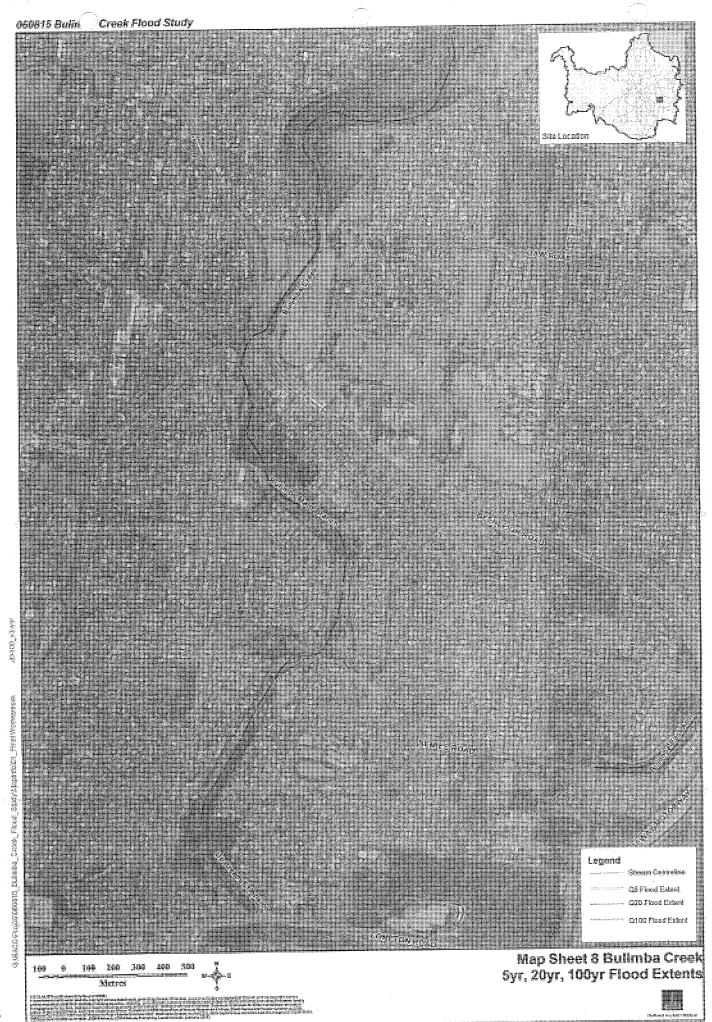


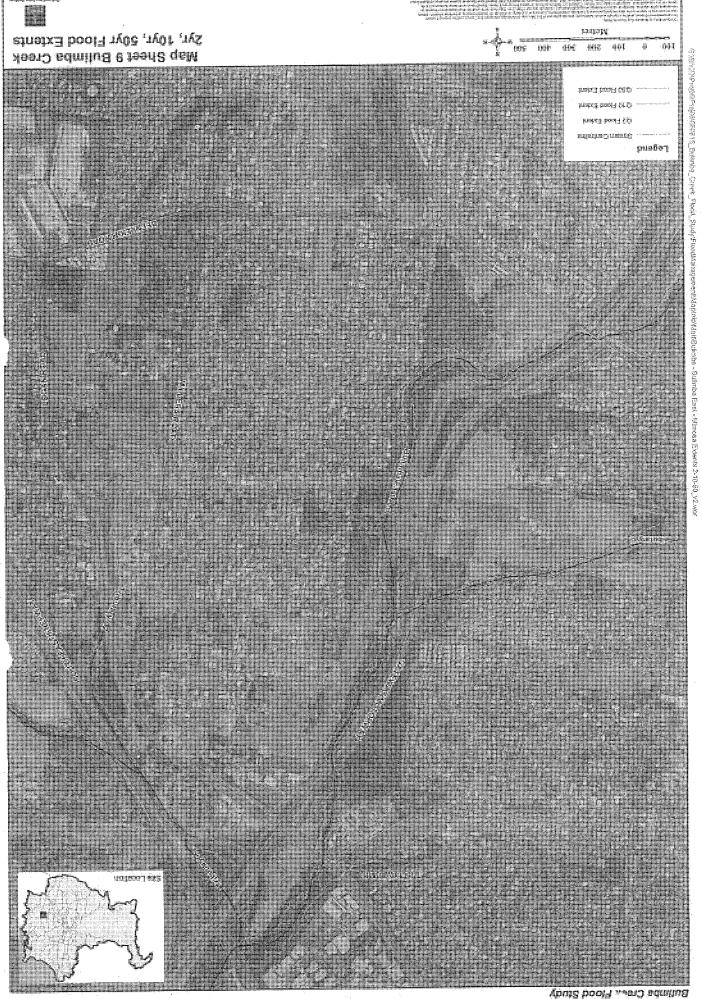
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BCC.079.1267





2-yr, 10-yr & 50-yr Flood Inundation Extents



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city design



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Appendix K Hydraulic Structure Reference Sheets



CREEK	BULIMBA CREEK
LOCATION	NEMIES ROAD, RUNCORN

DATE OF SURVEY: Nov 1989	UBD REF: 220 P11
AERIAL PHOTO No:	STRUCTURE ID:
BCC XS No: BM214	CHAINAGE (m): 17
DCC XX IV. DALL I	

STRUCTURE DESCRIPTION:

ROAD CULVERT

STRUCTURE SIZE

8 / 1500 x 1500 box culverts

For Culverts: Number of cells/pipes & sizes

For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL: 53.57

UPSTREAM OBVERT LÉVEL: \$5.07

DOWNSTREAM INVERT LEVEL: 53.46

DOWNSTREAM OBVERT LEVEL: 54.96

For culverts give floor level.

For bridges give bed level

For Culverts

LENGTH OF CULVERT BARREL AT INVERT (m): 21

LENGTH OF CULVERT BARREL AT OBVERT (m): 21

TYPE OF LINING: Sloping concrete channel (e.g. concrete, stones, brick, corrugated iron)

IS THERE A SURVEYED WEIR PROFILE?

Survey book 6340 / 28

If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard mils whichever is higher.

WEIR WIDTH (m): 21

LOWEST POINT OF WEIR (m AHD): 56.5

(In direction of flow, ie. distance from u/s face to d/s face)

HEIGHT OF GUARDRAILS: 0.5m, Handrail: 1m

DESCRIPTION OF ALL HAND AND GUARD RAILS AND

HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Flex beam guardrail, tubular galvanised monowills handrail, Height: 57.5

The following should also be provided.

Wing wall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE: N/A

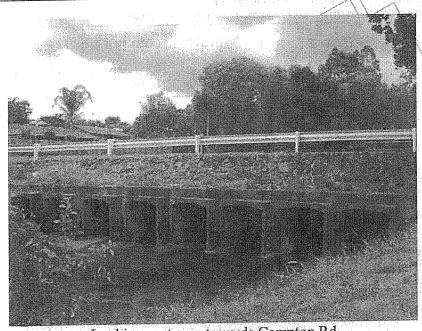
PLAN NUMBER: W5684S2

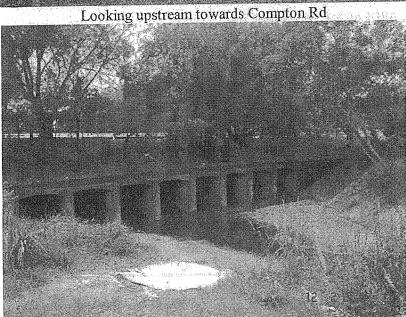
HAS THE STRUCTURE BEEN UPGRADED?

If yes, explain type and date of upgrade. Include plan number and location if applicable.

CREEK	BULIMBA CREEK
LOCATION	NEMIES ROAD, RUNCORN

				province in the contract of th					
ARI (years)		DISCHARO (m³/s)	GE .	U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (mm)	ARI (m²		VELOC (m/s)	
	Weir	Structure	Total	#4 . <u>.</u>		Structure	Weir	Structure	Weir
100	56.3	75.5	131.8	57.7	1050	18	23.5	4.2	2.4
50	38.2	73.5	111.7	57.45	1010	18	17.6	4.1	2.2
20	23.9	71.0	94.8	57.25	955	18	12.7	3.9	1.9
10	13.7	68.3	82.0	57.03	895	18	8.9	_/3.8	1.6
5	4.4	64.4	68.8	56.77	800	18	4.6	3.6	1.0
2	0.0	50.9	50.9	56.15	460	18	~0.0	. < 2.8	0.0





Looking downstream towards Beenleigh Rd HYDRAULIC STRUCTURE REFERENCE SHEET

BULIMBA CREEK CREEK BRANDON ROAD, RUNCORN LOCATION

UBD REF: 220 Q10 DATE OF SURVEY: Nov 1989 STRUCTURE ID: AERIAL PHOTO No: CHAINAGE (m): 370 BCC XS No: BM211

STRUCTURE DESCRIPTION:

ROAD CULVERT

STRUCTURE SIZE

4 / 2700 x 900 box culverts

For Culverts: Number of cells/pipes & sizes

For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL: 51.6

UPSTREAM OBVERT LEVEL: 52.5

DOWNSTREAM INVERT LEVEL: 51.5

DOWNSTREAM OBVERT LEVEL: 52.4

For culverts give floor level.

For bridges give bed level

For Culverts LENGTH OF CULVERT BARREL AT INVERT (m): 20

LENGTH OF CULVERT BARREL AT OBVERT (m); 20

TYPE OF LINING: Stone pitched wing walls (e.g. concrete, stones, brick, corrugated iron)

IS THERE A SURVEYED WEIR PROFILE?

Survey book 6340 / 28

If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher:

WEIR WIDTH (m): 20

LOWEST POINT OF WEIR (m AHD): 53

(In direction of flow, ie. distance from u/s face to d/s face)

HEIGHT OF GUARDRAILS: 0.5m, Handrails: 1m

DESCRIPTION OF ALL HAND AND GUARD RAILS AND

HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Flexi-beam guardrail (refer to WS 18-2.3),

tubular galvanised monowills handrail, Height: 54.0

The following should also be provided.

Wing wall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE: Sep-1997

W10258 PLAN NUMBER:

HAS THE STRUCTURE BEEN UPGRADED? N

If yes, explain type and date of upgrade. Include plan number and location if applicable.

ADDITIONAL COMMENTS:

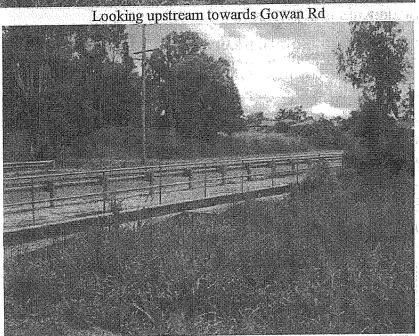
CREEK

BULIMBA CREEK

LOCATION	BRANDON ROAD, RUNCORN	

ARI (years)		DISCHARO (m³/s)	jE.	U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (mm)	ARE (m²		VELOCI (m/s)	ТҮ
	Weir	Structure	Total			Structure	Weir	Structure	Weir
100	113.6	24.8	138.4	54.17	140	9.7	48.2	2.5	2.4
50	95.2	24.7	119.9	54.1	149	9.7	42.4	2.5	2.3
20	77.0	24.8	101.8	54	157	9.7	36.1	2.5	2.2
10	58.6	24.8	83.4	53.93	163	9.7	29.1	2.5	2.1
5	45.6	24.7	70.3	53,84	188	9.7	23.9	<i>,</i> ∕2,5	2.0
2	24.3	24.6	48.9	53.64	240	9.7	14.6	2.4	1.8





Looking downstream towards Beenleigh Rd

CREEK	BULIMBA CREEK
LOCATION	BEENLEIGH ROAD, RUNCORN

DATE OF SURVEY: Nov 1989	UBD REF: 220 P5
AERIAL PHOTO No:	STRUCTURE ID:
BCC XS No: BM197	CHAINAGE(m): 1845

STRUCTURE DESCRIPTION:

ROAD CULVERT

STRUCTURE SIZE

4/3600 x 1200 box culverts

For Culverts: Number of cells/pipes & sizes For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL: 44.5

UPSTREAM OBVERT LEVEL: 45.7

DOWNSTREAM INVERT LEVEL: 44.4

DOWNSTREAM OBVERT LEVEL: 45.6

For bridges give bed level

For culverts give floor level,

For Culverts LENGTH OF CULVERT BARREL AT INVERT (m): 20

LENGTH OF CULVERT BARREL AT OBVERT (m): 20

TYPE OF LINING: Shotcrete (e.g. concrete, stones, brick, corrugated iron)

IS THERE A SURVEYED WEIR PROFILE?

Survey book 6340 / 28

If yes give details ie. Plan number and/or survey book number, Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.

WEIR WIDTH (m): 20

LOWEST POINT OF WEIR (m AHD): 46.63

(In direction of flow, ie. Distance from u/s face to d/s face)

HEIGHT OF GUARDRAILS: 1m

DESCRIPTION OF ALL HAND AND GUARD RAILS AND

HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Tubular galvanised monowills handrail (refer STD. W.M.S.30) Height upstream: 46.16, downstream: 45.8

The following should also be provided.

Wing wall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE: N/A

PLAN NUMBER:

W6203

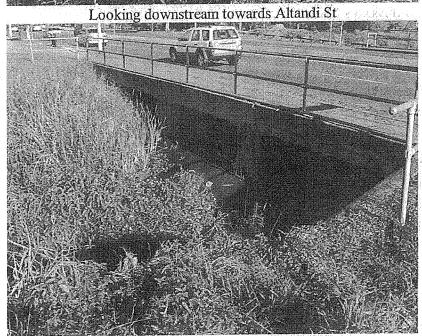
HAS THE STRUCTURE BEEN UPGRADED? N

If yes, explain type and date of upgrade. Include plan number and location if applicable.

CREEK	BULIMBA CREEK	
LOCATION	BEENLEIGH ROAD, RUNCORN	

ARI (years)		DISCHARO (m³/s)	E .	U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (mm)	ARI (m²	2 12 1	VELOC (m/s)	**
	Weir	Structure	Total	——————————————————————————————————————		Structure	Weir	Structure	Weir
100	64.1	63.7	123.6	47.72	915	17.3	27.9	3.7	2.3
50	42.3	62.3	104.6	47.57	877	17.3	22.7	3.6	2.1
20	32.2	60.3	92.5	47.38	827	17.3	17.2	3.5	1.9
10	20.0	57.9	77.9	47.21	770	17.3	12.4	3.4	1.6
5	7.0	54.8	61.8	46.97	674	17.3	7.0	3.2	1.2
2	0.0	45.2	45,2	46,57	447	17.3	0.0	2.4	0.0





Looking upstream towards Nemies Rd

CREEK BULIMBA CREEK BEENLEIGH ROAD (RAIL), RUNCORN LOCATION

UBD REF: 220 P5 DATE OF SURVEY: STRUCTURE ID: AERIAL PHOTO No: CHAINAGE (m): 1950 BCC XS No: BM194 BRIDGE STRUCTURE DESCRIPTION:

2 Spans, 55m OAL STRUCTURE SIZE

For Culverts: Number of cells/pipes & sizes For Bridges: Number of Spans and their lengths

UPSTREAM OBVERT LEVEL: 47.4 UPSTREAM INVERT LEVEL: 43.6

DOWNSTREAM OBVERT LÉVEL: 47.35 DOWNSTREAM INVERT LEVEL: 43.55 For bridges give bed level

For culverts give floor level.

For Culverts

LENGTH OF CULVERT BARREL AT INVERT (m): 8

LENGTH OF CULVERT BARRED AT OBVERT (m): 8

TYPE OF LINING: Compacted selected fill (e.g. concrete, stones, brick, corrugated iron)

IS THERE A SURVEYED WEIR PROFILE?

If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.

LOWEST POINT OF WEIR (m AHD): 49.85 WEIR WIDTH (m): 8

(In direction of flow, ie. Distance from u/s face to d/s face) PIER WIDTH: 1.2m

HEIGHT OF GUARDRAILS: No handrails/guardrails on bridge

DESCRIPTION OF ALL HAND AND GUARD RAILS AND HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: No handrails/guardrails on bridge

The following should also be provided.

Wingwall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE: N/A

PLAN NUMBER: N/A

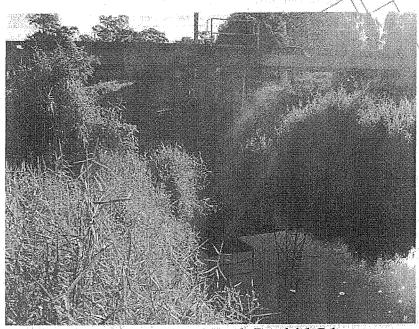
HAS THE STRUCTURE BEEN UPGRADED?

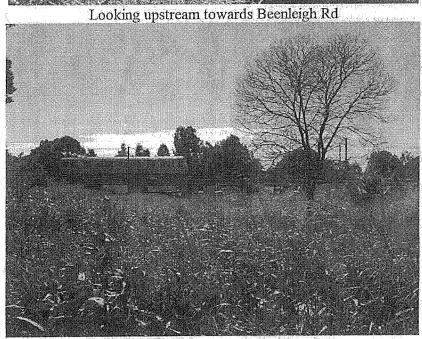
If yes, explain type and date of upgrade. Include plan number and location if applicable.

ADDITIONAL COMMENTS: BRIDGE UNDERGOING WORK AT TIME OF REPORT

CREEK	BULIMBA CREEK
LOCATION	BEENLEIGH ROAD (RAIL), RUNCORN

				\$	***************************************	· · · · · · · · · · · · · · · · · · ·			
ARI (years)	DISCHARGE (m³/s)		Œ	U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (mm)	ARI (m²		VELOC (m/s)	
	Weir	Structure	Total			Structure	Weir	Structure	Weir
100	0.0	129.0	129.0	46.49	608	44.9	0.0	3.0	0.0
50	0.0	111.5	111.5	46.34	537	41.0	0.0	2.9	0.0
20	0.0	92.2	92.2	46.18	442	39.2	0.0	2.4	0.0
10	0.0	77.9	77.9	46.05	364	36.4	0.0	>2.1	0.0
5	0.0	62.9	62.9	45.91	289	32.9	ستر 0.0 أ	1.9	0.0
2	0.0	45.2	45.2	45.74	203	17.3	J 0.0	2.6	0.0





Looking downstream towards Altandi St

CREEK BULIMBA CREEK LOCATION ST LAWRENCE'S FOOT BRIDGE, SUNNYBANK

DATE OF SURVEY: Nov 1989	UBD REF: 220 P4
AERIAL PHOTO No:	STRUCTURE ID:
BCC XS No: BM191	CHAINAGE (m): 2117
STRUCTURE DESCRIPTION: FO	OOT BRIDGE
STRUCTURE SIZE Single span, 12m Total For Culverts: Number of cells/pipes & sizes For Bridges: Num	- 170 April 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
UPSTREAM INVERT LEVEL: 42.3 DOWNSTREAM INVERT LEVEL: 42.25	UPSTREAM OBVERT LEVEL: 44.6 DOWNSTREAM OBVERT LEVEL: 44.55
For culverts give floor level.	For bridges give bed level
For Culverts	

LENGTH OF CULVERT BARREL AT INVERT (m):

LENGTH OF CULVERT BARREL AT OBVERT (m):

TYPE OF LINING: Compacted selected fill (e.g. concrete, stones, brick, corrugated fron)

IS THERE A SURVEYED WEIR PROFILE? If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the road Eg crown, kerb, hand rails guard rails whichever is higher.

Survey book 6340 / 28

WEIR WIDTH (m): 3

LOWEST POINT OF WEIR (m AHD): 44.2

TIDD DEEL SOUTH

(In direction of flow, ie. Distance from w/s face to d/s face)

PIER WIDTH: N/A (Single span)

HEIGHT OF GUARDRAILS: 1m

DESCRIPTION OF ALL HAND AND GUARD RAILS AND HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Tubular galvanised monowills handrail (refer STD. W.M.S.30)

The following should also be provided.

Wing wall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE: N/A

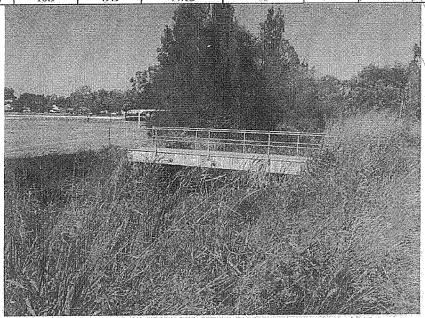
PLAN NUMBER: N/A

HAS THE STRUCTURE BEEN UPGRADED? N

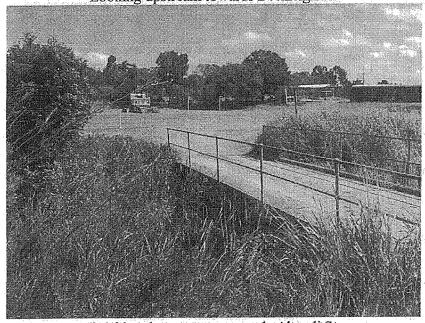
If yes, explain type and date of upgrade. Include plan number and location if applicable.

CREEK	BULIMBA CREEK
LOCATION	ST LAWRENCE'S FOOTBRIDGE, SUNNYBANK

ARI (years)		DISCHARO (m³/s)	JE .	U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (mm)	AR (11	<u>.</u>	VELOC (m/s	
	Weir	Structure	Total			Structure	Weir	Structure	Weir
100	113.3	17.0	130.3	45.6	6	17.5	311.1	1.1	1.7
50	95.6	16.4	112.0	45.47	7	17.6	267.8	1.1	1.6
20	78.9	18.1	97.0	45.24	6	17.6	205.1	1.1	1.7
10	65.3	18.4	83.7	45.07	7	17.6	159.2	<u> </u>	1.7
5	52.3	18.3	70.6	44.89	8	17.6	107,7	1,1	1.1
2	30.2	18.9	49.1	44.62	13	17.4	/ 19.0	(1.1	1.1



Looking upstream towards Beenleigh Rd



Looking downstream towards Altandi St

CREEK	BULIMBA CREEK	
LOCATION	ALTANDI STREET, RUNCORN	

AERIAL PHOTO No:	STRUCTURE ID: B0070
BCC XS No: BM188-6	CHAINAGE (m): 2375

STRUCTURE DESCRIPTION:

FOOT BRIDGE

STRUCTURE SIZE

For culverts give floor level.

3 / 12m spans

For Culverts: Number of cells/pipes & sizes

For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL: 41.82

UPSTREAM OBVERT LEVEL: 43.82

DOWNSTREAM INVERT LEVEL: 41.82

DOWNSTREAM OBVERT LEVEL: 43.82

For bridges give bed level

For Culverts

LENGTH OF CULVERT BARREL AT INVERT (m):

LENGTH OF CULVERT BARRED AT OBVERT (m):

TYPE OF LINING: Compacted selected fill (e.g. concrete, stones, brick, corrugated iron)

IS THERE A SURVEYED WELR PROFILE?

If yes give details ie. Plan number and/or survey book number.

Survey book 6340 / 28

Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.

WEIR WIDTH (m): 4

LOWEST POINT OF WEIR (m AHD): 44.2

(In direction of flow, ie. Distance from ws face to d's face)

PIER WIDTH: 600mm

HEIGHT OF GUARDRAILS: 1m

DESCRIPTION OF ALL HAND AND GUARD RAILS AND

HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Standard R.H.S. footbridge (refer W.M.S. 105/3)

Height: 45.1

The following should also be provided.

Wing wall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE: 01-07-1984

PLAN NUMBER: N/A

HAS THE STRUCTURE BEEN UPGRADED? N

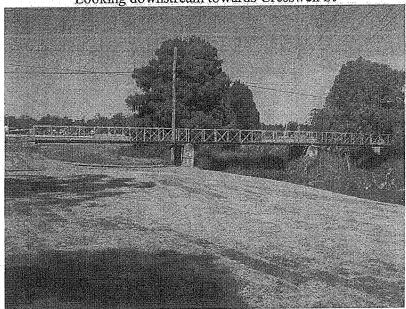
If yes, explain type and date of upgrade. Include plan number and location if applicable.

CREEK	BULIMBA CREEK
LOCATION	ALTANDI STREET, RUNCORN

								and the second second	
ARI (years)	,	DISCHARO (m³/s)	E	U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (mm)	ARE (m²		VELOC (m/s	
	Weir	Structure	Total			Structure	Weir	Structure	Weir
100	57.4	58.5	115.9	45.52	541	27.2	25.3	2.2	2.3
50	37.4	58.2	95.6	45.38	578	27.2	16.4	2.1	2.3
20	22.3	55.6	77.9	45.14	528	27.2	10.8	<i>></i> √2.0	2.1
10	14.4	52.9	67.3	44.96	474	27.2	7,6	2.0	1.9
5	7.6	47.8	55.3	44.76	414	27.2	4.7	< 1.6	1.1
2	30.6	40.1	70.7	44.36	240	27:2	0.9	1.5	0.8



Looking downstream towards Cresswell St



Looking upstream towards Beenleigh Road

CREEK	BULIMBA CREEK
LOCATION	MALBON STREET, SUNNYBANK

AERIAL PHOTO No:	STRUCTURE ID: B1330
BCC XS No: BM179 CI	CHAINAGE (m): 3965

STRUCTURE DESCRIPTION:

FOOTBRIDGE

STRUCTURE SIZE

Single span, 16.2m

For Culverts: Number of cells/pipes & sizes

For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL: 32.92

UPSTREAM OBVERT LEVEL:\35.63

DOWNSTREAM INVERT LEVEL: 32.92

DOWNSTREAM OBVERT LEVEL: 35.63

For culverts give floor level.

For bridges give bed level

For Culverts

LENGTH OF CULVERT BARREL AT INVERT (m):

LENGTH OF CULVERT BARREL AT OBVERT (m):

TYPE OF LINING: Grouted stone pitching (e.g. concrete, stones, brick, corrugated fron)

IS THERE A SURVEYED WEIR PROFILE?

Survey book 6340 / 28

If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.

WEIR WIDTH (m): 4

LOWEST POINT OF WEIR (m AHD): 35.51

(In direction of flow, ie. Distance from w/s face to d/s face)

PIER WIDTH: N/A (Single span)

HEIGHT OF GUARDRAILS: 1m

DESCRIPTION OF ALL HAND AND GUARD RAILS AND

HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Standard welded (refer W.M.S. 105/2) Height: 36.9

The following should also be provided.

Wing wall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutinent details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE: 01-07-1983

PLAN NUMBER: N/A

HAS THE STRUCTURE BEEN UPGRADED? N

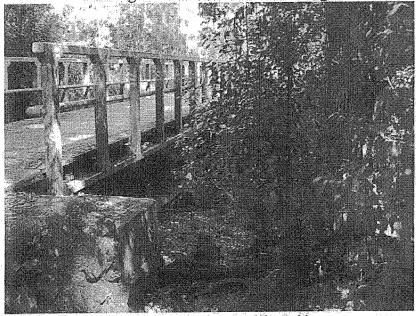
If yes, explain type and date of upgrade. Include plan number and location if applicable.

CREEK	BULIMBA CREEK
LOCATION	MALBON STREET, SUNNYBANK

ARI (years)		DISCHARO (m³/s)	GE .	U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (mm)	AR (n	2	VELOC (m/s	
	Weir	Structure	Total	***************************************		Structure	Weir	Structure	Weir
100	122.6	36.5	154.4	36.72	44	24.8	49.7	1.5	2.5
50	97.8	36.8	134.6	36.6	56	24.8	42.1	1.5	2.3
20	76.5	37.9	114.3	36.46	52	24.8	35.1	1.5	2.2
10	56.6	37.8	94.4	36.31	82	24.8	28.6	1.5	2.0
5	37.3	36.3	73.5	36.14	103	24.8	21.5	1,5	1.8
2	15.3	36.2	51.4	35.9	131	24.8	//11.9	<u>~ 1.5</u>	1.3



Looking from downstream of the Bridge



Looking from upstream of the Bridge

CREEK BULIMBA CREEK

LOCATION PADSTOW ROAD, SUNNYBANK

DATE OF SURVEY: Nov 1989	UBD REF: 201 B17
AERIAL PHOTO No:	STRUCTURE ID:
BCC XS No: BM176	CHAINAGE (m): 4390

STRUCTURE DESCRIPTION:

ROAD CULVERT 'B'

STRUCTURE SIZE

For culverts give floor level.

7/3350 x 2200 box culverts

For Culverts: Number of cells/pipes & sizes For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL: 31.6

UPSTREAM OBVERT LEVEL: 33.8

DOWNSTREAM INVERT LEVEL: 31.5

DOWNSTREAM OBVERT LEVEL: 33.7

For bridges give bed level

For Culverts

LENGTH OF CULVERT BARREL AT INVERT (m): 24

LENGTH OF CULVERT BARREL AT OBVERT (m): 24.

TYPE OF LINING: Precast concrete wing walls (e.g. concrete, stones, brick, corrugated fron)

IS THERE A SURVEYED WEIR PROFILE?

Survey book 6340 / 28

If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.

WEIR WIDTH (m): 24

LOWEST POINT OF WEIR (m AHD): 35.2

(In direction of flow, ie. Distance from u/s face to d/s face)

HEIGHT OF GUARDRAILS: 0.8m, handrails 1m

DESCRIPTION OF ALL HAND AND GUARD RAILS AND

HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Post-and-rail guardrail, galvanised balustrade handrail. Height upstream: 37.3, downstream: 37.2

The following should also be provided.

Wing wall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE: N/A

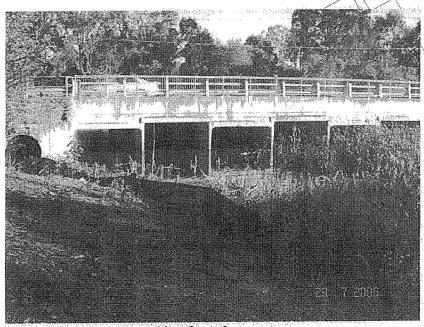
PLAN NUMBER: W10394

HAS THE STRUCTURE BEEN UPGRADED? N

If yes, explain type and date of upgrade. Include plan number and location if applicable.

CREEK	BULIMBA CREEK
LOCATION	PADSTOW ROAD, SUNNYBANK

ARI (years)	DISCHARGE (m³/s)		U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (mm)	AR (n	3	VELOC (m/s		
	Weir	Structure	Total			Structure	Weir	Structure	Weir
100	0.0	87.1	87.1	34.83	114	51.6	0.0	1.7.	0.0
50	0.0	70.8	70,8	34.55	65	51.6	0.0	1.4	0.0
20	0.0	48.4	48.4	34.2	24	51.6	0.0	1.0	0.0
10	0.0	38.1	38.1	33.97	- 12	51.6	0.0	√0.7	0.0
5	0.0	29.6	29.6	33.75	10.28	50.5	0.0	0.7	0.0
2	0.0	21.4	21.4	33.29	10	40.4	0.0 سرر	0.7	0.0



Looking from downstream

Looking from upstream

BULIMBA CREEK - PADSTOW BRANCH **CREEK** PADSTOW ROAD (2), SUNNYBANK LOCATION

STRUCTURE ID:
CHAINAGE(m): 177

STRUCTURE DESCRIPTION:

ROAD CULVERT 'C'

STRUCTURE SIZE

3 / 3000 x 2100 box culverts

For Culverts: Number of cells/pipes & sizes

For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL: 31.3

UPSTREAM OBVERT LEVEL: 33.4

DOWNSTREAM INVERT LEVEL: 31.2

DOWNSTREAM OBVERT LEVEL: 33.3

For bridges give bed level

For culverts give floor level.

For Culverts LENGTH OF CULVERT BARREL AT INVERT (m): 24

LENGTH OF CULVERT BARREL AT OBVERT (m): 24

TYPE OF LINING: Precast concrete wing walls

(e.g. concrete, stones, brick, corrugated iron)

IS THERE A SURVEYED WEIR PROFILE?

Survey book 6340 / 28

If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.

WEIR WIDTH (m): 24

LOWEST POINT OF WEIR (m AHD): 35

(In direction of flow, ie. Distance from u/s face to d/s face)

HEIGHT OF GUARDRAILS: 0.5m, Handrails: 1m

DESCRIPTION OF ALL HAND AND GUARD RAILS AND

HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Flex beam guardrail, tubular galvanised balustrade handrail. Height: 37.0

The following should also be provided.

Wing wall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE: N/A

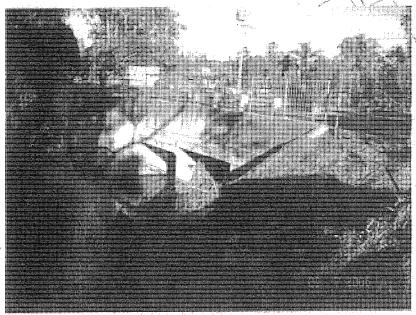
PLAN NUMBER: W10394

HAS THE STRUCTURE BEEN UPGRADED? N

If yes, explain type and date of upgrade. Include plan number and location if applicable.

CREEK	BULIMBA CREEK
LOCATION	PADSTOW ROAD (2), SUNNYBANK

ARI (years)	DISCHARGE (m³/s)		U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (mm)	AR (n		VELOC (m/s		
	Weir	Structure	Total	1		Structure	Weir	Structure	Weir
100	7.9	55.4	63.6	35.23	547	18.9	7.2	2.9	1.1
50	0.9	55.7	57.0	35.04	587	18.9	1.2	2.9	0.8
20	0.0	53.7	53.7	34.74	542	18.9	0.0	2.8	0.0
10	0.0	48.9	48.9	34.43	424	18.9	0.0	2.6	0.0
5	0.0	41.2	41.2	34.1	281	18.9	0.0	2,2	0.0
2	0.0	28.8	28.8	33.52	103	18.9	0.0	<1.5 <u></u>	0.0



Looking from downstream

CREEK **BULIMBA CREEK** LOCATION BLEASBY ROAD, MACGREGOR

DATE OF SURVEY: Nov 1989	UBD REF: 201 D16
AERIAL PHOTO No:	STRUCTURE ID: B0215
BCC XS No: BM173	CHAINAGE (m): 4785

STRUCTURE DESCRIPTION:

FOOTBRIDGE

STRUCTURE SIZE

Single span, 8.7m OAL

For Culverts: Number of cells/pipes & sizes

For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL: 29.45

UPSTREAM OBVERT LEVEL: 31.2

DOWNSTREAM INVERT LEVEL: 29.4

DOWNSTREAM OBVERT LEVEL: 31.15

For bridges give bed level

For culverts give floor level.

For Culverts

LENGTH OF CULVERT BARREL AT INVERT (m):

LENGTH OF CULVERT BARREL AT OBVERT (m):

TYPE OF LINING: Stone pitched wing walls

(e.g. concrete, stones, brick, conjugated iron)

IS THERE A SURVEYED WEIR PROFILE?

If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.

Survey book 6340 / 28

WEIR WIDTH (m): 4.2

LOWEST POINT OF WEIR (m AHD): 30.4

(In direction of flow, ie. Distance from u/s face to d/s face)

PIER WIDTH: N/A (Single span)

HEIGHT OF GUARDRAILS: 1m

DESCRIPTION OF ALL HAND AND GUARD RAILS AND

HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Tubular galvanised monowills handrail, Height: 32.53

The following should also be provided.

Wing wall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

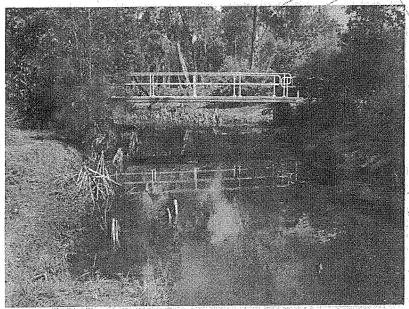
CONSTRUCTION DATE OF CURRENT STRUCTURE: 01-07-1993 PLAN NUMBER: W9181

HAS THE STRUCTURE BEEN UPGRADED? N

If yes, explain type and date of upgrade. Include plan number and location if applicable.

	CREEK	BULIMBA CREEK
-	LOCATION	BLEASBY ROAD, MACGREGOR

					Section 1997	414-214-2			
ARI (years)	DISCHARGE (m³/s)			U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (mm)		EA ¹²)	VELOC (m/s	
	Weir	Structure	Total		*	Structure	Weir	Structure	Weir
100	258.6	12.2	260.8	33.96	32	14.2	196.8	0.8	3.2
50	223.6	12.5	236.1	33.73	19	14.2	196.8	0.9	3.2
20	183.7	12.5	196.2	33.45	11	14.2	191.7	0.9	3.1
10	153:7	12.3	166.0	33.24	: :: []	14.2	162.2	0.9	3.2
5	123.2	12.5	135.7	33.04	. ind 13	14.2	//130.5	€ 0.9	3.2
2	80.2	12,2	92.3	32.61	21	14.2	\ 80:1\	\ 0.9	1.2



Looking towards upstream



Looking towards downstream

CREEK BULIMBA CREEK

LOCATION SOUTH-EAST FREEWAY, MACGREGOR

UBD REF: 201 G15 DATE OF SURVEY: STRUCTURE ID: AERIAL PHOTO No: CHAINAGE (m): 5625 BCC XS No: BM167

STRUCTURE DESCRIPTION:

CULVERT

STRUCTURE SIZE

5/3100 x 3100 box culverts

For Culverts: Number of cells/pipes & sizes For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL: 26.88

UPSTREAM OBVERT LEVEL: 30.0

DOWNSTREAM INVERT LEVEL: 26.5

DOWNSTREAM OBVERT LEVEL: 29.6

For culverts give floor level.

For bridges give bed level

LENGTH OF CULVERT BARREL AT INVERT (m): 54

LENGTH OF CULVERT BARREL AT OBVERT (m): 54

TYPE OF LINING: Precast concrete wing walls

(e.g. concrete, stones, brick, corrugated iron)

IS THERE A SURVEYED WEIR PROFILE?

If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.

WEIR WIDTH (m): 54

LOWEST POINT OF WEIR (m AHD): N/A

(In direction of flow, ie. Distance from u/s face to d/s face)

HEIGHT OF GUARDRAILS: Upstream: 4m, downstream: 1m

DESCRIPTION OF ALL HAND AND GUARD RAILS AND

HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Upstream: Steel-posted, wooden acoustic barrier fence, height 4m, downstream: concrete wall, height 1m

N

The following should also be provided.

Wing wall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE: N/A

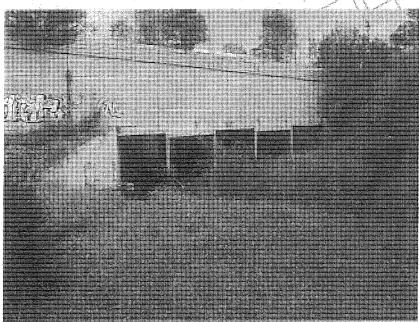
PLAN NUMBER: MRD182428

HAS THE STRUCTURE BEEN UPGRADED? N

If yes, explain type and date of upgrade. Include plan number and location if applicable.

	CREEK	BULIMBA CREEK
-	LOCATION	SOUTH-EAST FREEWAY, MACGREGOR

ARI (years)	DISCHARGE (m³/s)		U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (mm)	ARI (m²		VELOC (m/s)		
	Weir	Structure	Total	2		Structure	Weir	Structure	Weir
100	0.0	199.1	199.1	32.13	1146	48.1	0.0	4.1	0.0
50	0.0	171.7	171.7	31.54	820	48.1	0.0	3.9	0.0
20	0.0	140.3	140.3	30.74	499	48.1	0.0	3.9	0.0
10	0.0	121.2	121.2	30.14	358	46.0	0.0	3.6	0.0
5	0.0	99.6	99.6	29.7	305	40.3	0.0	3.6	0.0
2	0.0	69.9	69.9	28.98	244	29.7	~0.0	₹3.5	0.0



Looking upstream towards Padstow Rd

Looking downstream towards Logan Rd

CREEK GARDEN CITY BRANCH

LOCATION SOUTH-EAST FREEWAY (2), MACGREGOR

	·
DATE OF SURVEY:	UBD REF: 201 G15
AERIAL PHOTO No:	STRUCTURE ID:
BCC XS No: BM167	CHAINAGE (m): 5620
STRUCTURE DESCRIPTION: CULVERT	
STRUCTURE SIZE 2 / 3100 x 3100 box culverts For Culverts: Number of cells/pipes & sizes For Bridges: Number of Spans and the	ir lengths
UPSTREAM INVERT LEVEL: 27.25 UPSTREAM	1 OBVERT LEVEL: 30.35
DOWNSTREAM INVERT LEVEL: 26.85 DOWNSTR For bridges give	EAM OBVERT LEVEL: 29.95 bed level
For Culverts LENGTH OF CULVERT BARREL AT INVERT (m): 52	
LENGTH OF CULVERT BARREL AT OBVERT (m): 52	
TYPE OF LINING: Precast concrete wing walls (e.g. concrete, stones, brick, corrugated iron)	
IS THERE A SURVEYED WEIR PROFILE? If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the toad eg crown, kerb, hand rails guard rails whichever is higher.	
WEIR WIDTH (m): 52 LOWEST PG	OINT OF WEIR (m AHD): N/A
(In direction of flow, ie. Distance from u/s face to d/s face)	\$ · · · · · · · · · · · · · · · · · · ·
HEIGHT OF GUARDRAILS: 0.5m	
DESCRIPTION OF ALL HAND AND GUARD RAILS AND HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Up guardrail	stream: none, downstream: flexi-beam
The following should also be provided. Wing wall/Headwall details, entrance details eg. pipe flush with embankment or project. For bridges, details of piers and section under bridge including abutment details.	ring, socket or square end, entrance rounding, levels. rify Survey Book No.
CONSTRUCTION DATE OF CURRENT STRUCTURE: N/A	PLAN NUMBER: MRD182428
HAS THE STRUCTURE BEEN UPGRADED? N If yes, explain type and date of upgrade. Include plan number and location if applicable	

CREEK	GARDEN CITY BRANCH
LOCATION	SOUTH-EAST FREEWAY (2), MACGREGOR

A TO T.	1	DISCHARG	TE.	U/S WATER	AFFLUX AT	ARI	2 A	VELOC	ITV
ARI	DISCHARGE		1	1	1		i		
(years)		(m^3/s)		LEVEL	MAX FLOW	(m²)	(m/s	
				(m AHD)	(mm)			. 1 %.	
•	Weir	Structure	Total			Structure	Weir	Structure	Weir
100	0.0	74.0	74.0	32.16	1003	19,2	0.0	4.1	0.0
50	0.0	63.3	63.3	31.57	722	19.2	0.0	3.9	0.0
20	0.0	52.1	52.1	30.8	473	19.0	0.0	3.9	0.0
10	0.0	43.0	43.0	30.3	394	16.4	0.0	3,9	0.0
5	0.0	35.2	35.2	29.8	377	13.6	6.0	₹3.8	0.0
2	0.0	22.3	22.3	28.98	245	10.2	` 0.0 ∕	3.3	0.0







Looking downstream towards Logan Rd

CREEK **BULIMBA CREEK**

LOGAN ROAD, MACGREGOR LOCATION

UBD REF: 201 H15 DATE OF SURVEY: Nov 1989

AERIAL PHOTO No: STRUCTURE ID:

BCC XS No: BM165 CHAINAGE (m): 5790

CULVERT STRUCTURE DESCRIPTION:

STRUCTURE SIZE 5/3000 x 3000 box culverts

For Bridges: Number of Spans and their lengths For Culverts: Number of cells/pipes & sizes

UPSTREAM OBVERT LEVEL: 28.26 **UPSTREAM INVERT LEVEL: 25.26**

DOWNSTREAM OBVERT LÉVEL: 28.15 DOWNSTREAM INVERT LEVEL: 25.15 For bridges give bed level For culverts give floor level.

For Culverts

LENGTH OF CULVERT BARREL AT INVERT (m): 47.6

LENGTH OF CULVERT BARREL AT OBVERT (m): 47.6

TYPE OF LINING: Precast concrete wing walls

(e.g. concrete, stones, brick, corrugated iron)

IS THERE A SURVEYED WEIR PROFILE?

If yes give details ie. Plan number and/or survey book number.

Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.

WEIR WIDTH (m): 47.6

LOWEST POINT OF WEIR (m AHD): 30.9

Survey book 6340 / 28

(In direction of flow, ie. Distance from u/s face to d/s face)

HEIGHT OF GUARDRAILS: 0.5m, Handrail: 1m

DESCRIPTION OF ALL HAND AND GUARD RAILS AND

HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Tubular galvanised monowills handrail, flexi beam guardrail

The following should also be provided.

Wing wall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE: N./A

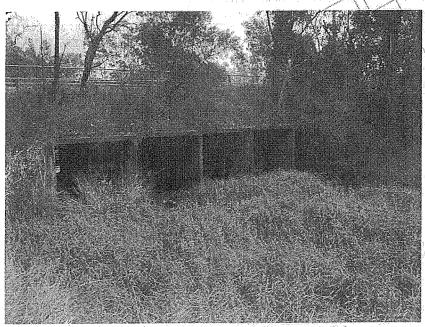
PLAN NUMBER: MRD182429

HAS THE STRUCTURE BEEN UPGRADED? N

If yes, explain type and date of upgrade. Include plan number and location if applicable.

	CREEK	BULIMBA CREEK
-	LOCATION	LOGAN ROAD, MACGREGOR

ARI (years)	DISCHARGE (m³/s)			U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (mm)	ARI (m		VELOCI (m/s)	
	Weir	Structure	Total			Structure	Weir	Structure	Weir
100	1.2	150.0	151.2	30.94	823	45.0	2.2	3.3	0,6
50	0.0	147.6	147.6	30.67	<i>7</i> 91	45.0	0.0	3.3	0.0
20	0.0	135.9	135.9	30.18	617	45.0	0.0	3.0	0.0
10	0.0	119.0	119.0	29.7	396	45.0	0.0	,,-2.6	0.0
5	0.0	97.2	97.2	29.26	246	45.0	0.0	2.2	0.0
2	0.0	69.7	69.7	28.58	117	45.0	- 0.0	(1.6	0.0



Looking downstream towards Kavanagh Rd

CREEK GARDEN CITY BRANCH

LOCATION LOGAN ROAD (2), MACGREGOR

DATE OF SURVEY: Nov 1989	UBD REF: 201 H15
AERIAL PHOTO No:	STRUCTURE ID:
BCC XS No: BM165	CHAINAGE (m): 5790

STRUCTURE DESCRIPTION:

CULVERT

STRUCTURE SIZE

For culverts give floor level.

2/3000 x 3000 box culverts

For Culverts: Number of cells/pipes & sizes

For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL: 24.98

UPSTREAM OBVERT LEVEL: 27.98

DOWNSTREAM INVERT LEVEL: 24.8

DOWNSTREAM OBVERT LEVEL: 27.8

For bridges give bed level

For Culverts

LENGTH OF CULVERT BARREL AT INVERT (m): 30

LENGTH OF CULVERT BARREL AT OBVERT (m): 30

TYPE OF LINING: Precast concrete wing walls

(e.g. concrete, stones, brick, corrugated iron)

IS THERE A SURVEYED WEIR PROFILE?

If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails goard rails whichever is higher. Survey book 6340 / 28

WEIR WIDTH (m): 30

LOWEST POINT OF WEIR (m AHD): 30.5

(In direction of flow, ie. Distance from u/s face to d/s face)

HEIGHT OF GUARDRAILS: Im

DESCRIPTION OF ALL HAND AND GUARD RAILS AND

HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Steel-posted, wooden acoustic barrier fence, Height 4m

The following should also be provided.

Wing wall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE: N/A

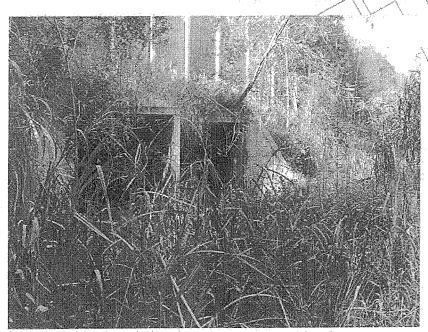
PLAN NUMBER: MRD182429

HAS THE STRUCTURE BEEN UPGRADED? N

If yes, explain type and date of upgrade. Include plan number and location if applicable.

CREEK	GARDEN CITY
LOCATION	LOGAN ROAD (2), MACGREGOR

ARI (years)	DISCHARGE (m³/s)		U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (mm)	ARI (m		VELOC (m/s)		
	Weir	Structure	Total			Structure	Weir	Structure	Weir
100	21.8	56.7	78.5	30.92	713	18.0	15.6	3.2	1.4
50	3.7	56.5	60.2	30.67	769	18.0	4.3	3.1	0.9
20	0,0	51.8	51.8	30.16	625	18.0	0.0	2.9	0.0
10	0.0	44.5	44.5	29.66	390	18.0	0.0	2.5	0.0
. 5	0.0	37.2	37.2	29.18	200	18.0	0.0	2.1	0.0
2	0.0	22.3	22.3	28.51	90	18.0	× 0.0	(1,2	0.0



Logan Road culvert in Garden City branch: looking from upstream

CREEK

BULIMBA CREEK

CRAIG STREET FOOTBRIDGE, WISHART LOCATION

DATE OF SURVEY: Nov 1989	UBD REF: 201 L13
AERIAL PHOTO No:	STRUCTURE ID: B9851
BCC XS No: BM148	CHAINAGE (m): 6935

STRUCTURE DESCRIPTION:

FOOT BRIDGE

STRUCTURE SIZE

2 Span, 38.6m Total

For Culverts: Number of cells/pipes & sizes

For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL: 21.3

UPSTREAM OBVERT LEVEL: 26

DOWNSTREAM INVERT LEVEL: 21.2

DOWNSTREAM OBVERT LEVEL: 25.9

For culverts give floor level.

For bridges give bed level

LENGTH OF CULVERT BARREL AT INVERT (m):

LENGTH OF CULVERT BARREL AT OBVERT (m):

TYPE OF LINING: Grouted stone pitching (e.g. concrete, stones, brick, corrugated iron)

IS THERE A SURVEYED WEIR PROFILE?

Survey book 6340 / 28

If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.

WEIR WIDTH (m): 3

LOWEST POINT OF WEIR (m AHD): 25.3

(In direction of flow, ie. Distance from u/s face to d/s face)

PIER WIDTH: 600mm

HEIGHT OF GUARDRAILS: 1m

DESCRIPTION OF ALL HAND AND GUARD RAILS AND

HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Rectangular galvanised frame, galvanised balustrade handrail, height: Height avg. 26.49 (cambered bridge)

The following should also be provided.

Wing wall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

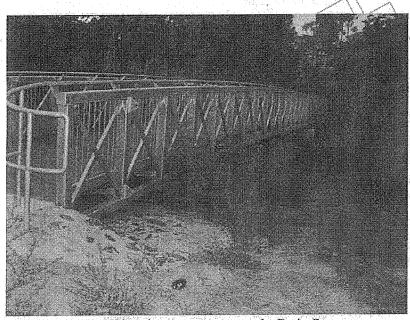
CONSTRUCTION DATE OF CURRENT STRUCTURE: 06-10-2006 PLAN NUMBER: W12453

HAS THE STRUCTURE BEEN UPGRADED? N

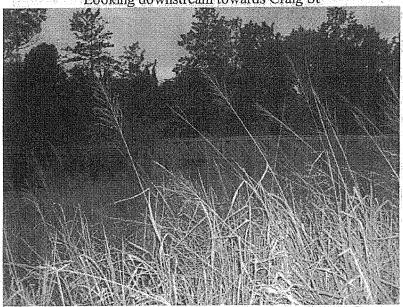
If yes, explain type and date of upgrade. Include plan number and location if applicable.

CREEK	BULIMBA CREEK
LOCATION	CRAIG ST FOOTBRIDGE, WISHART

ARI (years)	DISCHARGE (m³/s)			U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (mm)	ARI (m²		VELOC (m/s)	
	Weir	Structure	Total			Structure	Weir	Structure	Weir
100	205.0	192.4	397.4	27.06	48	130.5	121.6	2.4	2.1
50	122.0	174.8	296.9	26.79	47	130.5	81.9	2.4	2.1
20	108.7	144.2	252.9	26,47	42	130.5	55.0	2.4	2.2
10	62.7	126.1	188.8	26.24	42	130.5	28.8	~2.4	2.1
5	28.3	259.6	287.9	25.96	39	122.7	20.7	2,4	3.1
2	1.6	97.5	99.1	25.48	38	86.2	/1.6	₹2.4	1.8



Looking downstream towards Craig St



Looking upstream towards Kavanagh Road

CREEK BULIMBA CREEK

LOCATION MT. GRAVATT – CAPALABA ROAD, ROCHEDALE

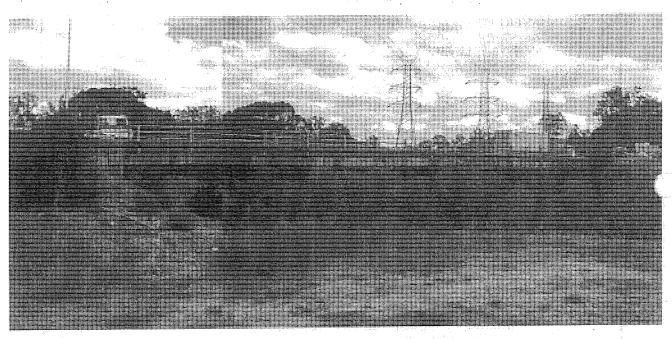
UBD REF: 202 A5 DATE OF SURVEY: Dec 1987 AERIAL PHOTO No: STRUCTURE ID: BCC XS No: BM110 CHAINAGE (m): 10702 BRIDGE STRUCTURE DESCRIPTION: 4/14m spans: 56m Total STRUCTURE SIZE For Bridges: Number of Spans and their lengths For Culverts: Number of cells/pipes & sizes UPSTREAM OBVERT LEVEL: 19.1 varies **UPSTREAM INVERT LEVEL: 11.52** DOWNSTREAM OBVERT LEVEL: 19.a varies DOWNSTREAM INVERT LEVEL: 11.52 For bridges give bed level For culverts give floor level. For Culverts LENGTH OF CULVERT BARREL AT INVERT (m): 20 LENGTH OF CULVERT BARREL AT OBVERT (m): 20 TYPE OF LINING: Grouted stone pitching (e.g. concrete, stones, brick, corrugated iron) IS THERE A SURVEYED WEIR PROFILE? Survey book 6340 / 15A If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher. LOWEST POINT OF WEIR (m AHD): 19.5 WEIR WIDTH (m): 20 (In direction of flow, ie. Distance from w/s face to d/s face) PIER WIDTH: Im HEIGHT OF GUARDRAILS: 0.8m DESCRIPTION OF ALL HAND AND GUARD RAILS AND HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Post-and-rail guardrail, Height 18.5 The following should also be provided. Wing wall/Headwall details, entrance details eg, pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No. CONSTRUCTION DATE OF CURRENT STRUCTURE: N/A PLAN NUMBER: W5952

HAS THE STRUCTURE BEEN UPGRADED? N

If yes, explain type and date of upgrade. Include plan number and location if applicable.

CREEK	BULIMBA CREEK
LOCATION	MT GRAVATT-CAPALABA ROAD, ROCHEDALE

		1		To street about				<u> </u>	
ARI (years)	DISCHARGE (m³/s)		U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (num)	ARI (m²		VELOCI (m/s)		
	Weir	Structure	Total	*		Structure	Weir	Structure	Weir
100	0.0	534.2	534.2	18.17	356	187.5	0.0	2.9	0.0
50	0.0	464.4	464.4	17.85	309	174.6	0,0	2.7	0.0
20	0.0	387.2	387.2	17.45	260	158.5	0.0	//2.5	0.0
10	0.0	332.0	332.0	17.14	223	146.2	0.0	2.3	0.0
5	0.0	273.9	273.9	16.78	186	131.9	~~ 0.0	(1.6	0.0
2	0.0	189.8	189.8	16.22	138	108.2	0.0	1.8	0.0



Looking upstream towards Stackpole Street



Looking downstream towards Ham Road

CREEK	BULIMBA CREEK	
LOCATION	WECKER ROAD, MANSFIELD	

DATE OF SURVEY: Dec 1987	UBD REF: 181 R20
AERIAL PHOTO No:	STRUCTURE ID: B2810
BCC XS No: BM97	CHAINAGE (m): 12139

STRUCTURE DESCRIPTION: ROAD BRIDGE

STRUCTURE SIZE

(3/17m+2/15m) spans, 81m Total

For Culverts: Number of cells/pipes & sizes For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL: 8.9

UPSTREAM OBVERT LEVEL: 15.4 varies

DOWNSTREAM INVERT LEVEL: 8.9

DOWNSTREAM OBVERT LEVEL: 15.4 varies For bridges give bed level

For culverts give floor level.

For Culverts LENGTH OF CULVERT BARREL AT INVERT (m): 14

LENGTH OF CULVERT BARREL AT OBVERT (m): 14

TYPE OF LINING: Grouted stone pitching

(e.g. concrete, stones, brick, corrugated iron)

IS THERE A SURVEYED WEIR PROFILE?

Survey book 6340 / 15A

If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.

WEIR WIDTH (m): 14

LOWEST POINT OF WEIR (in AHD): 14.2

(In direction of flow, ie. Distance from u/s face to d/s face)

PIER WIDTH: ≈ 450mm

HEIGHT OF GUARDRAILS: 0.8m, Handrail: 1m

DESCRIPTION OF ALL HAND AND GUARD RAILS AND

HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Monowills painted balustrade handrail, painted post-and-rail guardrail (refer to details W9520 DRG. No. 31 & 32 A - handrail & DRG. No. 33 - guardrail)

The following should also be provided.

Wing wall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE: 01-07-1995

PLAN NUMBER: W9520

HAS THE STRUCTURE BEEN UPGRADED? N

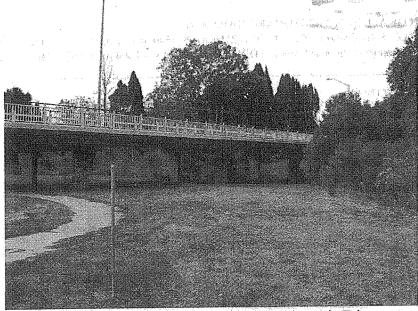
If yes, explain type and date of upgrade. Include plan number and location if applicable.

CREEK	BULIMBA CREEK	
LOCATION	WECKER ROAD, MANSFIELD	

ARI (years)	DISCHARGE (m³/s)			U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (mm)	AREA (m²)		VELOCITY (m/s)	
	Weir	Structure	Total	1		Structure	Weir	Structure	Weir
100	117.6	437.3	554.9	15.51	70	310.4	50.1	1.5	2.4
50	63.7	414.7	478.5	15.2	71	293.4	29.9	1.5	. 2.1
20	24.6	372.3	396.9	14.83	73	266.0	14.4	1.4	1.7
10	7.1	331.7	338.8	14.54	72	242.3	5 <i>.5</i>	<u>1.4</u>	1,3
5	0.1	278.4	278.4	14.19	. 67% 🚟 👀	214.9	0.1	1.3	1.0
2:	0.0	191.3	191.3	13.65	55	169.9	<u>/0.0</u>	1.3	0.0



Looking upstream towards Mt Gravatt-Capalaba Rd



Looking downstream towards Pine Mountain Rd

BULIMBA CREEK CREEK PINE MOUNTAIN ROAD, MANSFIELD LOCATION

DATE OF SURVEY:	UBD REF: 181 N13
AERIAL PHOTO No:	STRUCTURE ID: B0905
BCC XS No: BM66	CHAINAGE (m): 15555

STRUCTURE DESCRIPTION:

BRIDGE

STRUCTURE SIZE

(3 / 20m + 4 / 17.8m) spans, 131.2m Total

For Culverts: Number of cells/pipes & sizes For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL: 3.45

UPSTREAM OBVERT LEVEL: 10.9

DOWNSTREAM INVERT LEVEL: 3.42

DOWNSTREAM OBVERT LEVEL: 10.9

For culverts give floor level.

For bridges give bed level

For Culverts

LENGTH OF CULVERT BARREL AT INVERT (m): 14

LENGTH OF CULVERT BARRED AT OBVERT (m): 14

TYPE OF LINING: Grouted stone pitching (e.g. concrete, stones, brick, corrugated iron)

IS THERE A SURVEYED WEIR-PROFILE?

N

If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.

WEIR WIDTH (m): 14

LOWEST POINT OF WEIR (m AHD): N/A

(In direction of flow, ie. Distance from u/s face to d/s face)

PIER WIDTH: 500mm

HEIGHT OF GUARDRAILS: 0.8m, Handrails: 1m

DESCRIPTION OF ALL HAND AND GUARD RAILS AND

HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Monowills painted balustrade handrail, painted post-and-rail guardrail - Refer to DRG. 42 & 43 in plan W9587

The following should also be provided.

Wing wall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE: 01-07-1996

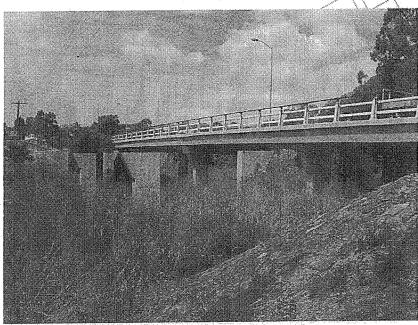
PLAN NUMBER: W9587

HAS THE STRUCTURE BEEN UPGRADED? N

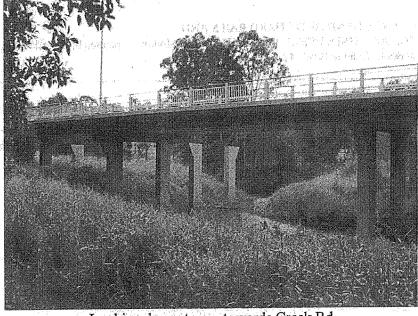
If yes, explain type and date of upgrade. Include plan number and location if applicable.

CREEK	BULIMBA CREEK
LOCATION	PINE MOUNTAIN ROAD, MANSFIELD

ARI (years)		DISCHARO (m³/s)	FE	U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (mm)	ARE (m²	. !	VELOC (m/s)	
	Weir	Structure	Total			Structure	Weir	Structure	Weir
100	0.0	560.4	560.4	10.22	84	390.1	0.0	1.4	0.0
50	0.0	486.9	486.9	9.9	83	352.1	0.0	1.4	0.0
20	0.0	402.7	402.7	9.5	87	300.6	0.0	1.4	0.0
10	0.0	341.4	341.4	9.2	84	261.7	0.0	1.3	0.0
5	0.0	279.3	279.3	8.6	81	220.1	0.0	1.3	0.0
2	0.0	190.9	190.9	8.32	78	158.3	0.0	<u>(1.2</u>	0.0



Looking upstream towards Gateway Motorway



Looking downstream towards Creek Rd

CREEK	BULIMBA CREEK
LOCATION	MEADOWBANK STREET FOOTBRIDGE, CARINDALE

DATE OF SURVEY: Dec 1987	UBD REF: 181 Q10
AERIAL PHOTO No:	STRUCTURE ID: B3090
BCC XS No. BM59	CHAINAGE (m): 16445

STRUCTURE DESCRIPTION:

FOOT BRIDGE

STRUCTURE SIZE

2 spans, 24m Total

For Culverts: Number of cells/pipes & sizes

For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL: 1.55

UPSTREAM OBVERT LEVEL: 5.8

DOWNSTREAM INVERT LEVEL: 1.53

DOWNSTREAM OBVERT LÉVEL: 5.78

For bridges give bed level

For culverts give floor level.

For Culverts
LENGTH OF CULVERT BARREL AT INVERT (m):

LENGTH OF CULVERT BARREL AT OBVERT (m):

TYPE OF LINING: Precast concrete (e.g. concrete, stones, brick, corrugated iron)

IS THERE A SURVEYED WEIR PROFILE?

Survey book 6340 / 15A

If yes give details ie. Plan number and/or survey book number.

Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.

WEIR WIDTH (m): 5

LOWEST POINT OF WEIR (m AHD): 5.9

(In direction of flow, ie. Distance from u/s face to d/s face)

HEIGHT OF GUARDRAILS: 1m

DESCRIPTION OF ALL HAND AND GUARD RAILS AND

HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Rectangular galvanised frame, galvanised balustrade handrail - Refer standard DRG. WMS 105/3

The following should also be provided.

Wing wall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE: 01-07-1990

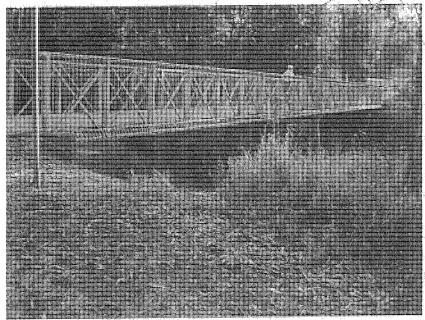
PLAN NUMBER: W8403

HAS THE STRUCTURE BEEN UPGRADED? N

If yes, explain type and date of upgrade. Include plan number and location if applicable.

CREEK	BULIMBA CREEK
LOCATION	MEADOWBANK ST FOOTBRIDGE, CARINDALE

ARI (years)	DISCHARGE (m³/s)		GE	U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (mm)	ARI (m²		VELOCI (m/s)	
	Weir	Structure	Total			Structure	Weir	Structure	Weir
100	522.8	70.4	593.2	9.64	14	52.0	404.4	1.4	1.6
50	447.0	69.8	516.8	9.29	14	52,0	360.3	1.3	1.7
20	361.9	69.8	431.6	8.85	14	52.0	304.5	1.3	1.6
10	297.9	69.8	367.8	8.47	. 15	52.0	260.4	/ 4.3	1.6
5.	235.4	68.8	304.2	8.06	15	52.0	211.1	1.3	1.6
2	144.2	69.8	214.0	7.38	19	52.0	2131.8	(1.3	1.6



Looking downstream towards Eromanga St

LOCATION	WINSTANLEY STREET, CARINDALE
CREEK	BULIMBA CREEK

DATE OF SURVEY: Nov 1983	UBD REF: 181 P7
AERIAL PHOTO No:	STRUCTURE ID: B2170
BCC XS No: CD10	CHAINAGE (m): 17338

STRUCTURE DESCRIPTION:

BRIDGE

STRUCTURE SIZE

3 / 17m spans: 51m Total

For Culverts: Number of cells/pipes & sizes

For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL: 1.83

UPSTREAM OBVERT LEVEL: 6.6

DOWNSTREAM INVERT LEVEL: 1.83

DOWNSTREAM OBVERT LEVEL: 6.6

For culverts give floor level,

For bridges give bed level

For Culverts

LENGTH OF CULVERT BARREL AT INVERT (m): 15

LENGTH OF CULVERT BARREL AT OBVERT (m): 15

TYPE OF LINING: Shotcrete (e.g. concrete, stones, brick, corrugated iron)

IS THERE A SURVEYED WEIR PROFILE?

Survey book 6340 / 13

If yes give details ie. Plan number and/or survey book number.
Note: This section should be at the highest part of the road
eg crown, kerb, hand rails guard rails whichever is higher.

WEIR WIDTH (m): 15

LOWEST POINT OF WEIR (m AHD): 6.4

(In direction of flow, ie. Distance from w/s face to d/s face)

PIER WIDTH: 1100mm

HEIGHT OF GUARDRAILS: 0.8m, Handrails: 1m

DESCRIPTION OF ALL HAND AND GUARD RAILS AND

HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Monowills painted balustrade handrail, painted post-and-rail guardrail (refer DWG. 9512 – 138 &139)

The following should also be provided.

Wing wall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE: 01-07-1982

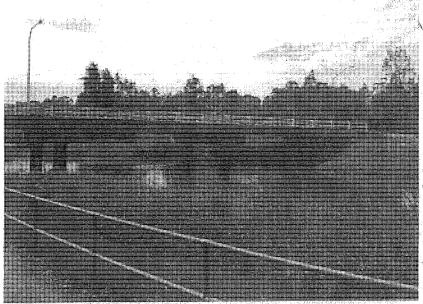
PLAN NUMBER: W9512

HAS THE STRUCTURE BEEN UPGRADED? N

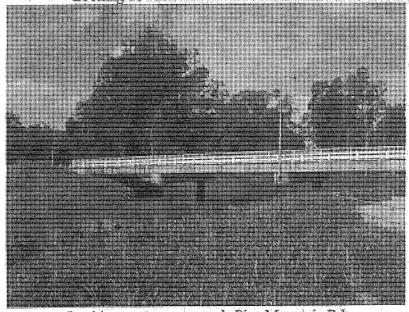
If yes, explain type and date of upgrade. Include plan number and location if applicable.

CREEK	BULIMBA CREEK
LOCATION	WINSTANLEY STREET, CARINDALE

ARI (years)	DISCHARGE (m³/s)		U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (mm)	ARE (m²		VELOC (m/s)		
	Weir	Structure	Total			Structure	Weir	Structure	Weir
100	311.3	319.5	630.8	8.2	72	151.7	106.8	2.1	2.9
50	223.3	307.4	-513.3	7.88	86	151.7	82.9	2.1	2.6
20	126.3	305.2	431.5	7.46	97	151.7	56.2	2.0	2.2
10	65.1	296.3	361.4	7.12	88	151.7	36.9	<i>,</i> ∼2.0	1.7
5	18.7	275.8	294.4	6.72	64	151.7	17.9	1.8	1,0
2	0.0	205.6	205.6	6.09	17	139.8	√ 0.0	<u>{1.4</u>	0.0



Looking downstream towards Cleveland Rd



Looking upstream towards Pine Mountain Rd

CREEK	BULIMBA
LOCATION	OLD CLEVELAND ROAD, CARINDALE

DATE OF SURVEY: Nov 1983	UBD REF: 181 P4
AERIAL PHOTO No:	STRUCTURE ID: B9204 & B9104
BCC XS No: CD06 – MODEL, BM48 - ACTUAL	CHAINAGE (m): 17935

STRUCTURE DESCRIPTION:

BRIDGE

STRUCTURE SIZE

7 Span, 84m Total

For Culverts: Number of cells/pipes & sizes

For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL: 1.8

UPSTREAM OBVERT LEVEL: 9.4

DOWNSTREAM INVERT LEVEL: 1.8

DOWNSTREAM OBVERT LEVEL: 9.4

For culverts give floor level.

For bridges give bed level

For Culverts

LENGTH OF CULVERT BARREL AT INVERT (m): 15

LENGTH OF CULVERT BARREL AT OBVERT (m):15

TYPE OF LINING: Grouted stone pitching (e.g. concrete, stones, brick, corrugated iron)

IS THERE A SURVEYED WEIR PROFILE?

Survey book 6340 / 13

If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the road Eg crown, kerb, hand rails guard rails whichever is higher.

WEIR WIDTH (m): 15

LOWEST POINT OF WEIR (m AHD): 10.5

(In direction of flow, ie. Distance from u/s face to d/s face)

PIER WIDTH: UNKNOWN

HEIGHT OF GUARDRAILS: 0.8m, Handrails: 1m

DESCRIPTION OF ALL HAND AND GUARD RAILS AND

HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Monowills painted balustrade handrail, painted post-and-rail guardrail (Ref. B9204/9104)

The following should also be provided.

Wing wall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

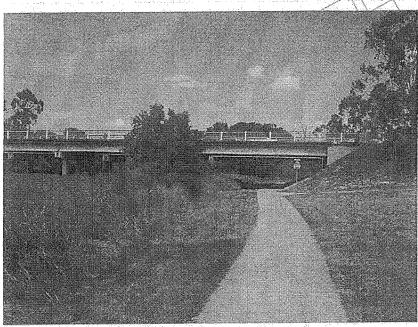
CONSTRUCTION DATE OF CURRENT STRUCTURE: 01-07-1979/76 PLAN NUMBER: N/A

HAS THE STRUCTURE BEEN UPGRADED? N

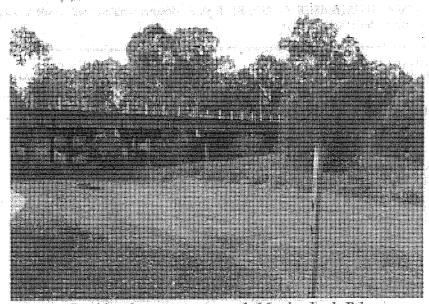
If yes, explain type and date of upgrade. Include plan number and location if applicable.

CREEK	BULIMBA CREEK
LOCATION	OLD CLEVELAND ROAD, CARINDALE

ARI (years)			Œ.	U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (mm)	ARI (m²	2.00	VELOC (m/s)	
: - 4	Weir	Structure	Total			Structure	Weir	Structure	Weir
100	0.0	823.0	823.0	6.95	25	281.7	0.0	3.7	0.0
50	0.0	796.0	796.0	6.65	26	263.1	0.0	3.5	0.0
20	0.0	704.6	704.6	6.26	4	222.8	0.0	3.3	0.0
10	0.0	587.2	587.2	5.93	4	178.8	0.0	<i></i> 3.3	0.0
5	0.0	444.0	444.0	5.56		177.1	0.0	2.9	0.0
2	0.0	300.5	300.5	5.04	7	136.8	/ 0.0	2.8	0.0



Looking upstream towards Winstanley St



Looking downstream towards Meadowlands Rd

CREEK	BULIMBA CREEK
LOCATION	SCRUB ROAD FOOTBRIDGE, CARINDALE

DATE OF SURVEY: Aug 1987	UBD REF: 182 B4
AERIAL PHOTO No:	STRUCTURE ID: B2360
BCC XS No: BM41	CHAINAGE (m): 19205
STRUCTURE DESCRIPTION:	BRIDGE
STRUCTURE SIZE 3 Span, 45.6m Total For Culverts: Number of cells/pipes & sizes For Bridges: Num	nber of Spans and their lengths
UPSTREAM INVERT LEVEL: -1.24	UPSTREAM OBVERT LEVEL: 4.4
DOWNSTREAM INVERT LEVEL: -1.24 For culverts give floor fevel.	DOWNSTREAM OBVERT LEVEL: 4.4 For bridges give bed level
For Culverts LENGTH OF CULVERT BARREL AT INVERT	(m).

LENGTH OF CULVERT BARREL AT OBVERT (m)/

TYPE OF LINING: Shotcrete (e.g. concrete, stones, brick, corrugated iron)

IS THERE A SURVEYED WEIR PROFILE?

If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the road

eg crown, kerb, hand rails guard rails whichever is higher.

WEIR WIDTH (m): 4

LOWEST POINT OF WEIR (m AHD): 2.05

(In direction of flow, ie. Distance from u/s face to d/s face)

PIER WIDTH: 400mm

Survey book 6340 / 15

HEIGHT OF GUARDRAILS: 1m

DESCRIPTION OF ALL HAND AND GUARD RAILS AND

HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Rectangular galvanised frame, galvanised balustrade handrail - Refer DWG, WMS 105/38

The following should also be provided.

Wing wall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

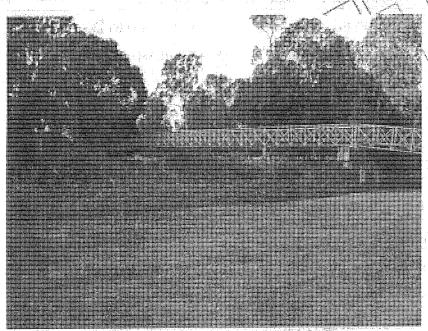
CONSTRUCTION DATE OF CURRENT STRUCTURE: 01-07-1989 PLAN NUMBER: W8258/4

HAS THE STRUCTURE BEEN UPGRADED? N

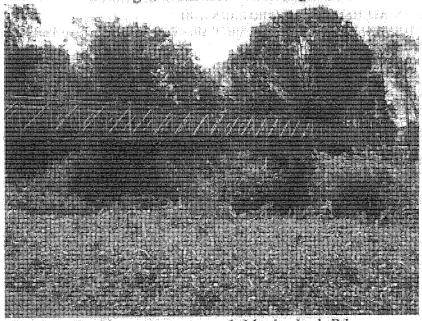
If yes, explain type and date of upgrade. Include plan number and location if applicable.

CREEK	BULIMBA CREEK
LOCATION	SCRUB ROAD FOOTBRIDGE, CARINDALE

£	F			V - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 -		1		1777.00	Tr. T
ARI	DISCHARGE (m³/s)		Discretification		AFFLUX AT	AREA (m²)		VELOCITY (m/s)	
(years)			(m^3/s) LEVEL 1	MAX FLOW (mm)					
					(m AHD)				
21 T	Weir	Structure	Total			Structure	Weir	Structure	Weir
100	514.4	116.2	630.5	6.14	8	127.3	549.6	0.9	1.1
50	426.1	109.3	535.4	5.83	9	172.2	486.5	0.8	1.1
20	339.5	100.2	435.9	5.45	8	127.2	412.4	0.8	1.1
10	275:0	94.9	369.8	5.14	8	127.2	353.9	<i>></i> -0.8	1.1
5	212.5	88.1	300.7	4.79	8	127.2	294.7~	0.7	1.1
2	128.4	78.5	206.9	4.22	8	125.5	<i>,</i> 205.6	(0.7	1.5



Looking downstream towards Wright St



Looking upstream towards Meadowlands Rd

CREEK	BULIMBA CREEK
LOCATION	MEADOWLANDS ROAD, CARINDALE

DATE OF SURVEY: Dec 1987	UBD REF: 182 D2
AERIAL PHOTO No:	STRUCTURE ID: B2300
BCC XS No: BM8GHD	CHAINAGE (m): 20270

STRUCTURE DESCRIPTION:

BRIDGE

STRUCTURE SIZE

4/17 m spans; 68m Total

For Culverts: Number of cells/pipes & sizes.

For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL: -2.35

UPSTREAM OBVERT LEVEL: 5.5

DOWNSTREAM INVERT LEVEL: -2.35

DOWNSTREAM OBVERT LEVEL: 5.5

For bridges give bed level

For culverts give floor level.

For Culverts LENGTH OF CULVERT BARREL AT INVERT (m): 15

LENGTH OF CULVERT BARREL AT OBVERT (m)/15

TYPE OF LINING: Grouted stone pitching (e.g. concrete, stones, brick, corrugated iron)

IS THERE A SURVEYED WEIR PROFILE?

If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher

WEIR WIDTH (m): 15

LOWEST POINT OF WEIR (m AHD): 5.35

(In direction of flow, ie. Distance from u/s face to d/s face)

PIER WIDTH: 750mm

Survey book 6340 / 15A

HEIGHT OF GUARDRAILS: 0.8m, Handrail: 1m

DESCRIPTION OF ALL HAND AND GUARD RAILS AND

HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Painted balustrade handrail, painted post-and-rail guardrail (refer DRG, 1897/8-10)

The following should also be provided.

Wing wall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

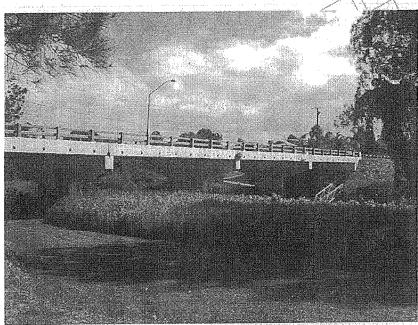
CONSTRUCTION DATE OF CURRENT STRUCTURE: 01-07-1984 PLAN NUMBER: W4281

HAS THE STRUCTURE BEEN UPGRADED? N

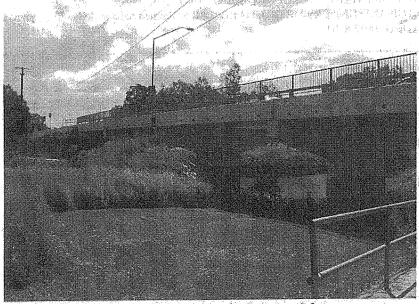
If yes, explain type and date of upgrade. Include plan number and location if applicable.

CREEK	BULIMBA CREEK
LOCATION	MEADOWLANDS ROAD, CARINDALE

ARI (years)	DISCHARGE (m³/s)		U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (mm)	ARF (m²		VELOCI (m/s)		
	Weir	Structure	Total	(III AAD)	(111111)	Structure	Weir	Structure	Weir
100	0.0	611.8	611.8	5.3	152	253.4	0.0	2.4	0.0
50	0.0	529.4	529.4	5.03	98	247.9	0.0	2.2	0.0
20	0.0	433.7	433.7	4.72	54	237.9	0.0	1.8	0.0
10	0.0	363.8	363.8	4.47	31	227.3	0.0	<i>></i> √1.6	0.0
5	0.0	294.9	294.9	4.19	16	213.0	سر 0.0	1.4	0.0
2	0.0	199.9	199.9	3.72	9	185.3	<u> </u>	<u> </u>	0.0



Looking upstream towards Cleveland Rd



Looking downstream towards Gateway Motorway

CREEK	BULIMBA CREEK
LOCATION	PRESTON ROAD FOOTBRIDGE,
	CARINA

DATE OF SURVEY:	UBD REF: 162 B19
ĄERIAL PHOTO No:	STRUCTURE ID: B1611
BCC XS No: BM19GHD	CHAINAGE (m): 21885

STRUCTURE DESCRIPTION:

FOOT BRIDGE

STRUCTURE SIZE

Single span, 16.7m Total

For Culverts: Number of cells/pipes & sizes

For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL: -1.59

UPSTREAM OBVERT LEVEL: 2.1

DOWNSTREAM INVERT LEVEL: -1.59

DOWNSTREAM OBVERT LEVEL: 2.1

For culverts give floor level.

For bridges give bed level

For Culverts

LENGTH OF CULVERT BARREL AT INVERT (m):

LENGTH OF CULVERT BARREL AT OBVERT (m):

TYPE OF LINING: Compacted selected fill (e.g. concrete, stones, brick, corrugated iron)

IS THERE A SURVEYED WE'R PROFILE?

If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.

WEIR WIDTH (m): 5

LOWEST POINT OF WEIR (m AHD): 1.55

(In direction of flow, ie. Distance from u/s face to d/s face)

PIER WIDTH: N/A (Single span)

HEIGHT OF GUARDRAILS: 1m

DESCRIPTION OF ALL HAND AND GUARD RAILS AND

HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Rectangular painted handrail + tubular painted monowills handrail (Refer plan W9348)

The following should also be provided.

Wing wall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE: 01-07-1993

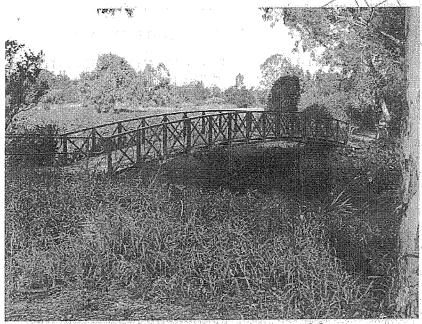
PLAN NUMBER: W9348

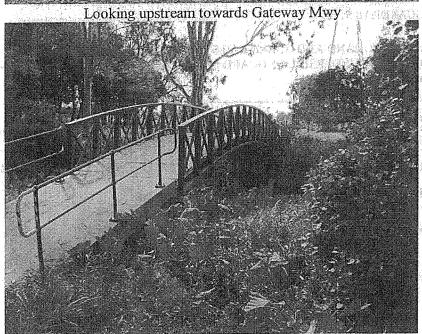
HAS THE STRUCTURE BEEN UPGRADED? N

If yes, explain type and date of upgrade. Include plan number and location if applicable.

CREEK	BULIMBA CREEK
LOCATION	PRESTON ROAD FOOTBRIDGE, CARINA

								4,2,3,4	
ARI (years)	DISCHARGE (m³/s)			U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (mm)	AREA (m²)		VELOCITY (m/s)	
	Weir	Structure	Total		, , , , , , , , , , , , , , , , , , , ,	Structure	Weir	Structure	Weir
100	554.3	46.6	601.0	4.69	8	56.9	981.3	0.8	1.4
50	475.1	46.9	496.0	4.46	8	56.9	838.8	0.8	1.4
20	387.0	47.6	434.6	4.17	8	56.9	667.6	0.8	1.4
10	312.5	48.2	360.7	3.93	8	56.9	534.2	J.0.8	1.4
5	243.7	47.8	291.5	3.67	8	56.9	398.4	0.8	1.4
2	147.8	46.5	194.3	3.22	9	56.9	203.3	(0.8	1.5





Looking downstream towards Wynnum Rd

CREEK	BULIMBA CREEK
LOCATION	WYNNUM ROAD, MURRARIE

DATE OF SURVEY: Nov 1983	UBD REF: 161 P12
AERIAL PHOTO No:	STRUCTURE ID: B2240/30
BCC XS No: BM26	CHAINAGE (m): 25885

STRUCTURE DESCRIPTION:

BRIDGE

STRUCTURE SIZE

3 spans-total length 45.7m Total

For Culverts: Number of cells/pipes & sizes

For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL: -2.66

UPSTREAM OBVERT LEVEL: 5

DOWNSTREAM INVERT LEVEL: -2.66

DOWNSTREAM OBVERT LEVEL: 5

For bridges give bed level

For culverts give floor level.

LENGTH OF CULVERT BARREL AT INVERT (m), 25

LENGTH OF CULVERT BARREL AT OBVERT (m)/25

TYPE OF LINING: Shotcrete (e.g. concrete, stones, brick, corrugated iron)

IS THERE A SURVEYED WEIR PROFILE?

Survey book 6340 / 13

If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.

WEIR WIDTH (m): 25

LOWEST POINT OF WEIR (m AHD): 3.5

(In direction of flow, ie. Distance from u/s face to d/s face)

PIER WIDTH: 600mm

HEIGHT OF GUARDRAILS: 0.8m, Handrail: 1m

DESCRIPTION OF ALL HAND AND GUARD RAILS AND

HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Painted post-and-rail guardrail, painted balustrade handrail, height 6.176 (refer W5407 - 15A)

The following should also be provided.

Wing wall/Headwall details, entrance details eg. pipe flush with embankment of projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE: 1975/55

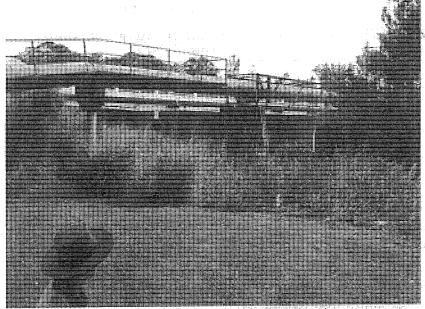
PLAN NUMBER: W5407

HAS THE STRUCTURE BEEN UPGRADED? N

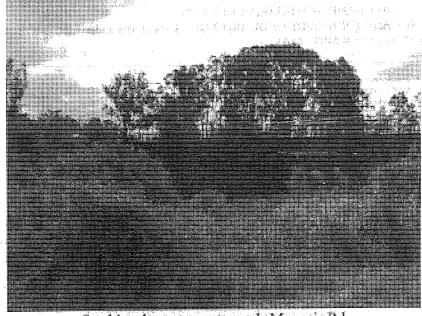
If yes, explain type and date of upgrade. Include plan number and location if applicable.

CREEK	BULIMBA CREEK	
LOCATION	WYNNUM ROAD, MURRARIE	3 1 1 1 1 2 2

ARI (years)	DISCHARGE (m³/s)		U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (mm)	ARE (m²		VELOC (m/s		
	Weir	Structure	Total	9 9 1 4		Structure	Weir	Structure	Weir
100	13.7	434.8	448.5	3.81	242	200.7	11.1	2.2	1,2
50	1.5	379.2	380.6	3.58	211	189.7	1.7	2.0	0.9
20	0.0	318.8	318.8	3.28	164	177.3	0.0	1.8	0.0
10	0.0	272.7	272.7	3.2	132	167.2	0.0	/1.6	0.0
5	0.0	227.7	227.7	2.7	101	156.5	0.0	1.5	0.0
2	0.0	163.4	163.4	2.43	59	139.9	<u>/0.0</u>	(1.2	0.0



Looking upstream towards Creek Rd



Looking downstream towards Murarrie Rd

CREEK	BULIMBA CREEK
LOCATION	MURRARIE ROAD, MURRARIE

DATE OF SURVEY: Nov 1983	UBD REF: 161 R9
AERIAL PHOTO No:	STRUCTURE ID: B1490
BCC XS No: BM22DS	CHAINAGE (m): 26730

STRUCTURE DESCRIPTION:

BRIDGE

STRUCTURE SIZE

3 / 15m spans, 45m OAL

For Culverts: Number of cells/pipes & sizes

For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL: -3.9

UPSTREAM OBVERT LEVEL: 2.6

DOWNSTREAM INVERT LEVEL: -3.9

DOWNSTREAM OBVERT LEVEL: 2.6

For bridges give bed level

For culverts give floor level.

For Culverts LENGTH OF CULVERT BARREL AT INVERT (m): 15

LENGTH OF CULVERT BARREL AT OBVERT (m)/15

TYPE OF LINING: Compacted selected fill

(e.g. concrete, stones, brick, corrugated iron)

Survey book 6340 / 13 IS THERE A SURVEYED WEIR PROFILE?

If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.

WEIR WIDTH (m): 15

LOWEST POINT OF WEIR (m AHD): 2.36

(In direction of flow, ie. Distance from u/s face to d/s face)

PIER WIDTH: 760mm

HEIGHT OF GUARDRAILS: 1m

DESCRIPTION OF ALL HAND AND GUARD RAILS AND

HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Galvanised post-and-rail guardrail, height 4.52 (refer DRG, W.M.S. 100/2A)

The following should also be provided.

Wing wall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE: 01-07-1985

PLAN NUMBER: W6759

HAS THE STRUCTURE BEEN UPGRADED? N

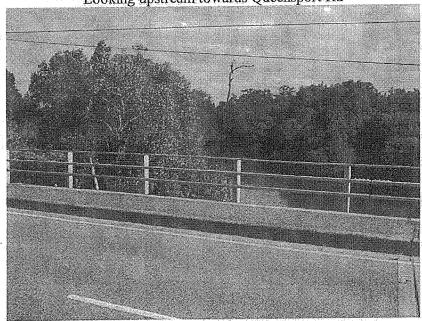
If yes, explain type and date of upgrade. Include plan number and location if applicable.

CREEK	BULIMBA CREEK
LOCATION	MURRARIE ROAD, MURRARIE

ARI (years)	DISCHARGE (m³/s)		U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (mm)	AREA (m²)		VELOCITY (m/s)		
	Weir	Structure	Total			Structure	Weir	Structure	Weir
100	144.1	246.2	390.3	3.23	98	180,5	73.4	1.4	2.0
50	84.9	238.5	550.6	3.05	106	180.5	49.3	1.3	1.8
20	32.4	224.2	256.6	2.81	102	180.5	23.7	1.2	1.4
10	11.0	207.0	218.0	2.7	88	179.9	10.8	1:2	1.0
5	1.2	182.0	183.1	2.4	71	174.1	2.9	1)1	0.4
2	0.0	135.6	135.6	2.2	48	161.7	~ O.O	0.8	0.0



Looking upstream towards Queensport Rd



Looking upstream towards Wynnum Road from bridge

CONTENT OF THE PROPERTY OF THE	*****
CREEK	BULIMBA
LOCATION	GATEWAY VIADUCT, MURARRIE

DATE OF SURVEY:	UBD REF: 162 A9
AERIAL PHOTO No:	STRUCTURE ID:
BCC XS No: 39GHD	CHAINAGE (m): 26950

STRUCTURE DESCRIPTION:

BRIDGE (viaduct)

STRUCTURE SIZE

Multiple spans / 450m Total length

For Culverts: Number of cells/pipes & sizes

For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL: -3.7

UPSTREAM OBVĘRT LĘVEL: 3.9

DOWNSTREAM INVERT LEVEL: -3.75

DOWNSTREAM OBVERT LÉVEL: 3.85

For culverts give floor level.

For bridges give bed level

For Culverts

LENGTH OF CULVERT BARREL AT INVERT (m): 40

LENGTH OF CULVERT BARREL AT OBVERT (m): 40

TYPE OF LINING: Compacted selected fill (e.g. concrete, stones, brick, corrugated iron)

IS THERE A SURVEYED WEIR PROFILE?

If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.

WEIR WIDTH (m): 40

LOWEST POINT OF WEIR (m AHD): N/A

(In direction of flow, ie. Distance from u/s face to d/s face)

PIER WIDTH: 1200mm

HEIGHT OF GUARDRAILS: 1m

DESCRIPTION OF ALL HAND AND GUARD RAILS AND

HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Concrete freeway wall guardrail

The following should also be provided.

Wing wall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abuttnent details. Specify Survey Book No.

N

CONSTRUCTION DATE OF CURRENT STRUCTURE: N/A

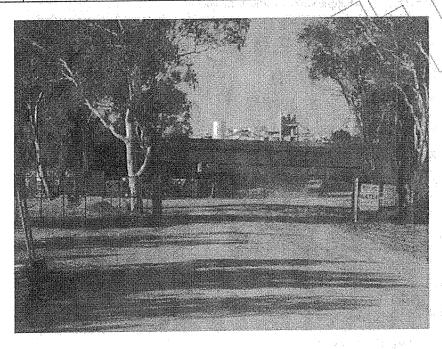
PLAN NUMBER: A04A -8002

HAS THE STRUCTURE BEEN UPGRADED? N

If yes, explain type and date of upgrade. Include plan number and location if applicable.

	BULIMBA CREEK
CREEK	
LOCATION	GATEWAY BRIDGE, MURARRIE

					1	1 177	٠. ١	TOTAC	ITV
ARI	DISCHARGE (m³/s)				AFFLUX AT	the state of the s		VELOCITY (m/s)	
(years)				LEVEL	MAX FLOW				
				(m AHD)	(mm)				
	Weir	Structure	Total			Structure	Weir	Structure	Weir
100	0.0	370.2	370.2	3.07	9	468.9	0.0	0.8	0.0
50	0.0	315.3	315.3	2.89	27	412.1	0.0	0.8	0.0
20	0.0	254.0	254.0	2.67	26	346.1	0.0	0.8	0.0
10	0.0	216.9	216.9	2.51	28	299.5	0.0	0.7	0.0
5	0.0	182.8	182.8	2.34	31	256.2	0.0	0.7	0.0
2	0.0	135,4	135,4	2.09	25	207.4	<u> </u>	© 0.7	0.0



CREEK	BULIMBA CREEK
LOCATION	CLEVELAND - RAIL, CARINDALE

DATE OF SURVEY:	UBD REF: 162 D2
AERIAL PHOTO No:	STRUCTURE ID:
BCC XS No: BM52	CHAINAGE (m): 34500

STRUCTURE DESCRIPTION:

BRIDGE

STRUCTURE SIZE

7 Spans, 105m Total

For Culverts: Number of cells/pipes & sizes

For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL: -2.5

UPSTREAM OBVERT LEVEL: 2.91

DOWNSTREAM INVERT LEVEL: -2.5

DOWNSTREAM OBVERT LEVEL: 2.91

For bridges give bed level

For culverts give floor level.

LENGTH OF CULVERT BARREL AT INVERT (m): 15

LENGTH OF CULVERT BARREL AT OBVERT (m), 15

TYPE OF LINING: Shotcrete (e.g. concrete, stones, brick, corrugated iron)

IS THERE A SURVEYED WEIR PROFILE?

If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.

WEIR WIDTH (m): 15

LOWEST POINT OF WEIR (m AHD): 4

(In direction of flow, ie. Distance from u/s face to d/s face)

PIER WIDTH: 1000mm

HEIGHT OF GUARDRAILS: No handrails/guardrails on bridge

DESCRIPTION OF ALL HAND AND GUARD RAILS AND

HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: No handrails/guardrails on bridge

The following should also be provided.

Wing wall/Headwall details, entrance details eg, pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE: N/A

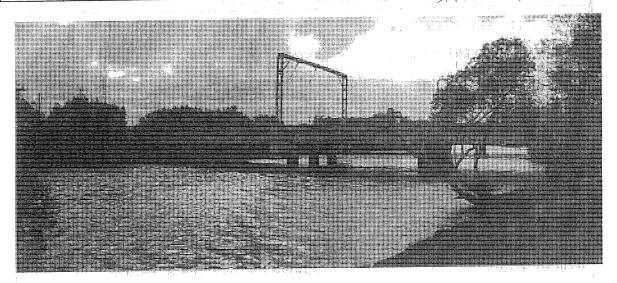
PLAN NUMBER: \$20262

HAS THE STRUCTURE BEEN UPGRADED? N

If yes, explain type and date of upgrade. Include plan number and location if applicable.

-	CREEK	BULIMBA CREEK
	LOCATION	CLEVELAND-RAIL, CARINDALE

ARI (years)	DISCHARGE (m³/s)		U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (mm)	AREA (m²)		VELOCITY (m/s)		
	Weir	Structure	Total			Structure	Weir	Structure	Weir
100	0.0	484.9	482.2	2.6	175	272.5	0.0	1.8	0.0
50	0.0	422.8	422.8	2.37	152	254.7	0.0	1.7	0.0
20	0.0	353.6	353.6	2.11	126	233.9	0.0	1.5	0.0
10	0.0	302.2	302.2	1.91	106	217.5	0.0	1.4	0.0
5	0.0	250.3	250.3	1.7	85	201.9	0.0	1.2	0.0
2	0.0	172.9	172.9	1.39	53	178.6	0.0	(1.0	0.0



Looking downstream towards Lytton Rd

CREEK	BULIMBA CREEK	
LOCATION	LYTTON ROAD, HEMMANT	

DATE OF SURVEY: Nov 1983	UBD REF: 142 A20				
AERIAL PHOTO No:	STRUCTURE ID:				
BCC XS No: BM6	CHAINAGE (m): 35680				

STRUCTURE DESCRIPTION:

BRIDGE

STRUCTURE SIZE

3 / 25m spans; 75m Total

For Culverts: Number of cells/pipes & sizes

For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL: -3.39

UPSTREAM OBVERT LEVEL: 2.8

DOWNSTREAM INVERT LEVEL: -3.39

DOWNSTREAM OBVERT LEVEL: 2.8

For bridges give bed level

For culverts give floor level.

For Culverts

LENGTH OF CULVERT BARREL AT INVERT (m): 11

LENGTH OF CULVERT BARREL AT OBVERT (m)/11

TYPE OF LINING: Grouted stone pitching (e.g. concrete, stones, brick corrugated iron)

IS THERE A SURVEYED WEIR PROFILE?

If yes give details ie. Plan number and/or survey book number.

Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.

Survey book 6340 / 13

WEIR WIDTH (m): 11

LOWEST POINT OF WEIR (m AHD): N/A

(In direction of flow, ie. Distance from u/s face to d/s face)

PIER WIDTH: 600mm

HEIGHT OF GUARDRAILS: 0.8m, Handrail: 1m

DESCRIPTION OF ALL HAND AND GUARD RAILS AND

HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Galvanised balustrade handrail, galvanised postand-rail guardrail (Ref. W5947), Height 6.643

The following should also be provided.

Wing wall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE: N/A

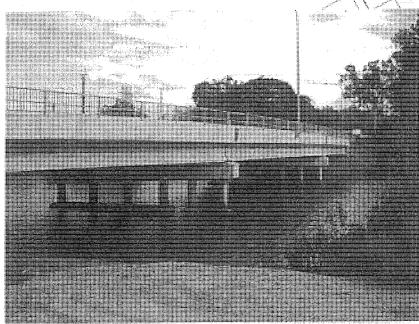
PLAN NUMBER: W5947

HAS THE STRUCTURE BEEN UPGRADED? N

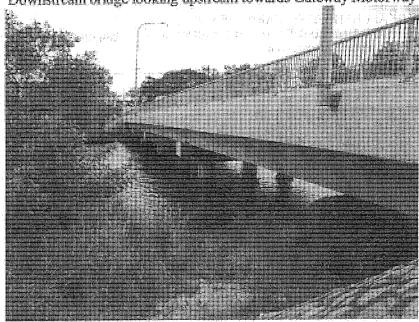
If yes, explain type and date of upgrade. Include plan number and location if applicable.

CREEK	BULIMBA CREEK	7
LOCATION	LYTTON ROAD, HEMMANT	

					<u> </u>				
ARI	1		U/S WATER AFFLUX AT		AREA		VELOCITY		
(years)			LEVEL	MAX FLOW (mm)	(m²)		(m/s)		
			(m AHD)						
	Weir	Structure	Total			Structure	Weir	Structure	Weir
100	0.0	501.0	501.0	2.12	122	281.2	0.0	1.8	0.0
50	0.0	434.3	434.3	1.94	107	268.4	0.0	1.6	0.0
20	0.0	360.8	360.8	1.72	89	253.7	0.0	1.4	0.0
10	0.0	306.4	306.4	1.57	74	243.8	0.0	1.3	0.0
5	0.0	252.3	252,3	1.42	58	233,9	0.0	1.1	0.0
2	0.0	173.8	173.8	1.22	35	221.0	. 0.0	(0.8	0.0



Downstream bridge looking upstream towards Gateway Motorway



Looking upstream towards Gateway Motorway

CREEK	MINNIPPI BRANCH
LOCATION	WYNNUM ROAD MINNIPPI, TINGALPA

DATE OF SURVEY: Nov 1983	UBD REF: 162 C14
AERIAL PHOTO No:	STRUCTURE ID: B2220/1
BCC XS No: BM31GHD	CHAINAGE (m): 1125

STRUCTURE DESCRIPTION:

BRIDGE

STRUCTURE SIZE

Single span, 14m Total

For Culverts: Number of cells/pipes & sizes

For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL: 0.05

UPSTREAM OBVERT LEVEL: 3.3

DOWNSTREAM INVERT LEVEL: 0.04

DOWNSTREAM OBVERT LEVEL: 3.29

For bridges give bed level

For culverts give floor level.

For Culverts

LENGTH OF CULVERT BARREL AT INVERT (m): 21

LENGTH OF CULVERT BARREL AT OBVERT (m)/21

TYPE OF LINING: Compacted selected fill (e.g. concrete, stones, brick corrugated iron)

IS THERE A SURVEYED WEIR PROFILE?

Survey book 6340 / 13

If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.

WEIR WIDTH (m): 21

LOWEST POINT OF WEIR (m AHD): 3.3

(In direction of flow, ie. Distance from w/s face to d/s face)

PIER WIDTH: N/A (Single span)

HEIGHT OF GUARDRAILS: 0.5m concrete guardrail + 0.5m balustrade

DESCRIPTION OF ALL HAND AND GUARD RAILS AND

HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Galvanised balustrade handrail bolted to concrete guardrail - Refer DWG, W4282/16

The following should also be provided.

Wing wall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE: 1962/70 PLAN NUMBER: W4282/16

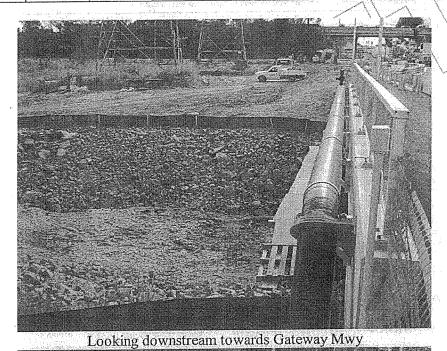
HAS THE STRUCTURE BEEN UPGRADED? N

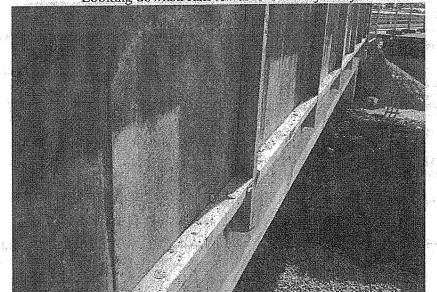
If yes, explain type and date of upgrade. Include plan number and location if applicable.

ADDITIONAL COMMENTS: BRIDGE UNDERGOING WORK AT TIME OF REPORT

Γ	CREEK	MINNIPPI CREEK
r	LOCATION	WYNNUM ROAD MINNIPPI, TINGALPA

ARI (years)	DISCHARGE (m³/s)			U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (mm)	ARE (m²		VELOCI (m/s)	
	Weir	Structure	Total			Structure	Weir	Structure	Weir
100	4.4	63.1	67.5	3.47	512	22.1	5.9	3.0	0.8
50	0.0	56.1	56.I	3.25	470	20.6	0.0	2.8	0.0
20	0.0	43.2	43.2	2.89	310	19.0	0.0	2.3	0.0
10	0.0	31.6	31.5	2.6	190	17.8	0.0	<i>,</i> √1.8	0.0
5	0.0	20.2	20.2	2.31	90	16.4	سر 0.0	1.2	0.0
2	0.0	5.2	5,2	1.85	2	13.3	/0.0	(0.4	0.0





Looking upstream towards Gateway Mwy

CREEK	BULIMBA CREEK EAST
LOCATION	BEENLEIGH ROAD – SOUTH,
	RUNCORN

DATE OF SURVEY:	UBD REF: 221 G10
AERIAL PHOTO No:	STRUCTURE ID:
BCC XS No: BE282	CHAINAGE (m): 820

STRUCTURE DESCRIPTION:

CULVERT

STRUCTURE SIZE

4/1650 x 600 box culverts

For Culverts: Number of cells/pipes & sizes

For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL: 48.66

UPSTREAM OBVERT LÉVEL: 49.26

DOWNSTREAM INVERT LEVEL: 48.63

DOWNSTREAM OBVERT LEVEL: 49.23

For culverts give floor level.

For bridges give bed level

For Culverts

LENGTH OF CULVERT BARREL AT INVERT (m): 12

LENGTH OF CULVERT BARREL AT OBVERT (m): 12

TYPE OF LINING: Compacted selected fill (e.g. concrete, stones, brick, corrugated iron)

IS THERE A SURVEYED WEIR PROFILE?

If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.

WEIR WIDTH (m): 12

LOWEST POINT OF WEIR (m AHD): 49.7

(In direction of flow, ie. Distance from u/s face to d/s face)

HEIGHT OF GUARDRAILS: 0.75m, Handrail: 1m.

DESCRIPTION OF ALL HAND AND GUARD RAILS AND

HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Double flexi-beam guardrail, tubular galvanised monowills handrail (Ref. G-10-39/14)

N

The following should also be provided,

Wing wall/Headwall details, entrance details eg. pipe flush with embankment of projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE: N/A

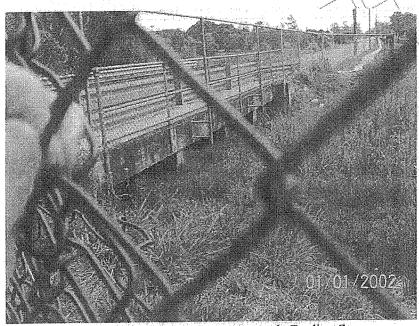
PLAN NUMBER: G-10-39/14

HAS THE STRUCTURE BEEN UPGRADED? N

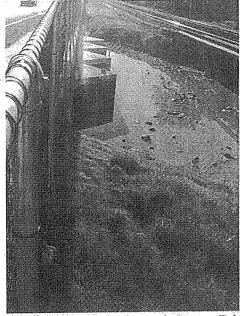
If yes, explain type and date of upgrade. Include plan number and location if applicable.

CREEK	BULIMBA CREEK EAST
LOCATION	BEENLEIGH ROAD - SOUTH, RUNCORN

ARI (years)	DISCHARGE (m³/s)		U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (mm)			VELOCITY (m/s)		
	Weir	Structure	Total			Structure	Weir	Structure	Weir
100	47.2	11.6	58.8	50.31	38	4.0	47.9	2.8	1.5
50	41.1	11.9	53.0	50.25	39	4.0	41.2	2.7	1.5
20	33.1	10.5	43.6	50.19	119	4.0	21.7	2.7	1.5
10	24.8	11.2	36.0	50.14	192	4.0	17.5	~2.7	1.4
5	18.4	11.2	29.6	50.07	267	4.0	13.9	2.7	1.3
2	8.2	11.2	19.5	49.9	420	4.0	7.6	₹2.9	1.2



Looking from downstream towards Besline St



Looking upstream towards Persse Rd

CREEK	BULIMBA CREEK EAST
LOCATION	BEENLEIGH ROAD - RAIL,
	RUNCORN

DATE OF SURVEY:	UBD REF: 221 G10
AERIAL PHOTO No:	STRUCTURE ID:
BCC XS No: BE279	CHAINAGE (m): 845

STRUCTURE DESCRIPTION:

CULVERT

STRUCTURE SIZE

10 / 1500 x 1150 box culverts

For Culverts: Number of cells/pipes & sizes

For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL: 48.63

UPSTREAM OBVERT LEVEL: 49.78

DOWNSTREAM INVERT LEVEL: 48.57

DOWNSTREAM OBVERT LEVEL: 49.72

For bridges give bed level

.

For culverts give floor level.

For Culverts
LENGTH OF CULVERT BARREL AT INVERT (m): 6

LENGTH OF CULVERT BARREL AT OBVERT (m): 6

TYPE OF LINING: Brick

(e.g. concrete, stones, brick, corrugated iron)

IS THERE A SURVEYED WEIR PROFILE?

If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.

WEIR WIDTH (m): 6

LOWEST POINT OF WEIR (m AHD): 49.85

(In direction of flow, ie. Distance from u/s face to d/s face)

PIER WIDTH: UNKNOWN

HEIGHT OF GUARDRAILS: No handrails/guardrails on bridge

DESCRIPTION OF ALL HAND AND GUARD RAILS AND

HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: No handrails/guardrails on bridge

The following should also be provided:

Wing wall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

N

CONSTRUCTION DATE OF CURRENT STRUCTURE: N/A

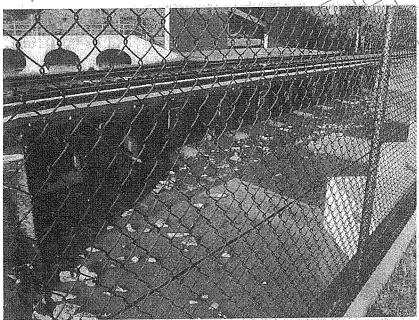
PLAN NUMBER: N/A

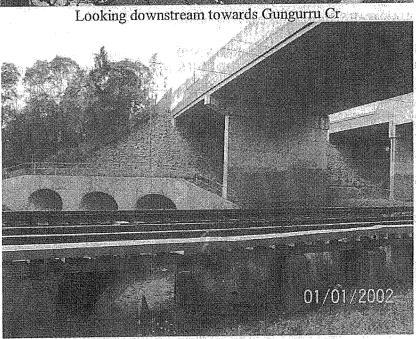
HAS THE STRUCTURE BEEN UPGRADED? N

If yes, explain type and date of upgrade. Include plan number and location if applicable.

CREEK	BULIMBA CREEK EAST
LOCATION	BEENLEIGH ROAD - RAIL, RUNCORN

ARI	DISCHARGE			U/S WATER	AFFLUX AT	AREA		VELOCITY	
(years)	(m³/s)				MAX FLOW	(m²)		(m/s)	
()			(m AHD)	(mm)					
	Weir	Structure	Total			Structure	Weir	Structure	Weir
100	31.2	26.4	57.6	50.27	74	17.3	22,5	2.4	1.4
50	23.4	24.1	42.1	50.22	96	18,2	15.7	2.4	1.3
20	8.1	28.4	36.5	50.07	195	17.3	8.2	2.4	1.0
10	2.2	28.7	30.9	49.95	297	17.1	3.0	~2.6	0.7
5	0.0	26.6	26.6	49.8	361	10.3	0.0	2.6	0.0
2	0.0	19.3	19.3	49.52	376	8.3	<u>/0.0</u>	2.3	0.0





Looking downstream towards Gungurru Cr

CREEK	BULIMBA CREEK EAST
LOCATION	BEENLEIGH ROAD - GATEWAY,
	RUNCORN

DATE OF SURVEY:	UBD REF: 221 G10
AERIAL PHOTO No:	STRUCTURE ID:
BCC XS No: BE277	CHAINAGE (m): 876
	CHELUDA

STRUCTURE DESCRIPTION:

CULVERT

STRUCTURE SIZE

3 / 2400 diameter pipe culverts

For Culverts: Number of cells/pipes & sizes

For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL: 47.41

UPSTREAM OBVERT LEVEL: 49.81

DOWNSTREAM INVERT LEVEL: 46.66

DOWNSTREAM OBVERT LEVEL: 49.09

For culverts give floor level.

For bridges give bed level

For Culverts

LENGTH OF CULVERT BARREL AT INVERT (m): 55

LENGTH OF CULVERT BARREL AT OBVERT (m): 55

TYPE OF LINING: Precast concrete wing walls (e.g. concrete, stones, brick, corrugated iron)

IS THERE A SURVEYED WEIR PROFILE?

N

If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.

WEIR WIDTH (m): 55

LOWEST POINT OF WEIR (m AHD): 49.8

(In direction of flow, ie. Distance from u/s face to d/s face)

HEIGHT OF GUARDRAILS: 1m

DESCRIPTION OF ALL HAND AND GUARD RAILS AND

HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Tubular galvanised monowills handrail

The following should also be provided.

Wing wall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE: N/A.

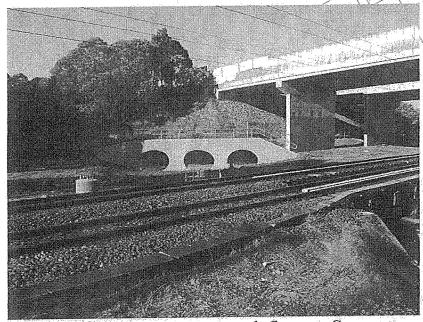
PLAN NUMBER: N/A

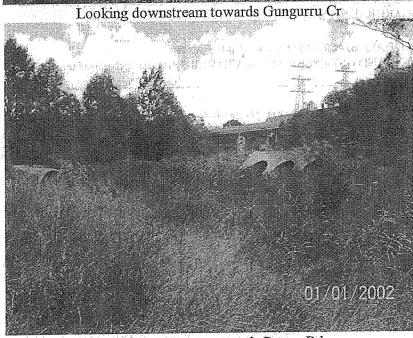
HAS THE STRUCTURE BEEN UPGRADED? N

If yes, explain type and date of upgrade. Include plan number and location if applicable.

 CREEK	BULIMBA CREEK EAST
 LOCATION	BEENLEIGH ROAD - GATEWAY, RUNCORN

ARI (years)	DISCHARGE (m³/s)			1 0,0 11.2	AFFLUX AT MAX FLOW (mm)	AREA (m²)		VELOCITY (m/s)	
	Weir	Structure	Total			Structure	Weir	Structure	Weir
100	8.3	39.0	47.4	50.2	1548	10.1	6.5	3.9	1.3
50	5.1	37.4	42.5	50.11	1540	9.8	4.4	3.8	1.1
20	0.2	28.4	28.6	49.87	1392	9.1	0.3	3.6	0.6
10	0.0	30.3	30.3	49.64	1245	8.7	0.0	3.5 پر	0.0
5	0.0	25.4	25.4	49.42	1132	7.8	0.0	3.3	0.0
2	0.0	18.2	18.2	49.11	1022	6.2	~0.0	2.9	0.0





Looking upstream towards Persse Rd

CREEK	BULIMBA CREEK EAST
LOCATION	UNDERWOOD ROAD, EIGHT MILE
	PLAINS

DATE OF SURVEY: Sep 1987	UBD REF: 221 K5
AERIAL PHOTO No:	STRUCTURE ID:
BCC XS No: BE262	CHAINAGE (m): 2767

STRUCTURE DESCRIPTION:

CULVERT

STRUCTURE SIZE

4/3700 x 1800 box culverts

For Culverts: Number of cells/pipes & sizes

For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL: 35.33

UPSTREAM OBVERT LEVEL: 37.13

DOWNSTREAM INVERT LEVEL: 35.21

DOWNSTRÈAM OBVERT LEVEL: 37.01

For culverts give floor level.

For bridges give bed level

For Culverts

LENGTH OF CULVERT BARREL AT INVERT (m): 17

LENGTH OF CULVERT BARREL AT OBVERT (m): 17

TYPE OF LINING: Compacted selected fill (e.g. concrete, stones, brick, corrugated iron)

IS THERE A SURVEYED WEIR PROFILE?

Survey book 6340 / 18

If yes give details ie, Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.

WEIR WIDTH (m): 17

LOWEST POINT OF WEIR (m AHD): 38.3

(In direction of flow, ie. Distance from u/s face to d/s face)

HEIGHT OF GUARDRAILS: 0.5m

DESCRIPTION OF ALL HAND AND GUARD RAILS AND HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Flex beam guardrails (Ref. W8055)

The following should also be provided.

Wing wall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE: N/A

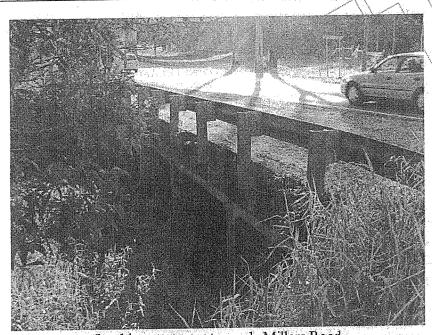
PLAN NUMBER: W8055

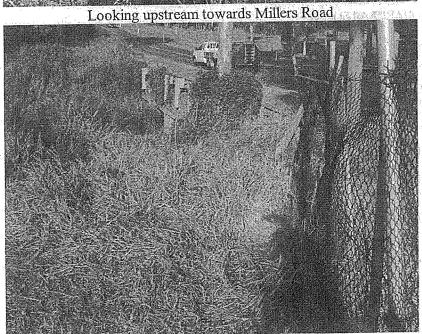
HAS THE STRUCTURE BEEN UPGRADED? N

If yes, explain type and date of upgrade. Include plan number and location if applicable.

CREEK	BULIMBA CREEK EAST
LOCATION	UNDERWOOD ROAD, EIGHT MILE PLAINS

ARI (years)	DISCHARGE (m³/s)		U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (mm)	AREA (m²)		VELOCITY (m/s)		
	Weir	Structure	Total			Structure	Weir	Structure	Weir
100	28.4	62.1	90.6	38.73	167	26.6	17.4	2.3	1.7
50	14.3	62.1	76.4	38.59	160	26.4	11.2	2.3	1.3
20	0.0	57.6	57.6	38.15	164	26.6	0.0	2.2	0.0
10	0.0	51.2	51.2	37.89	107	26.6	0.0	1.9	0.0
5	0.0	42.5	42.5	37.63	65	26.6	0.0	1.6	0.0
2	0.0	29.7	29.7	37.24	26	26.6	~ 0.0	(1.2	0.0





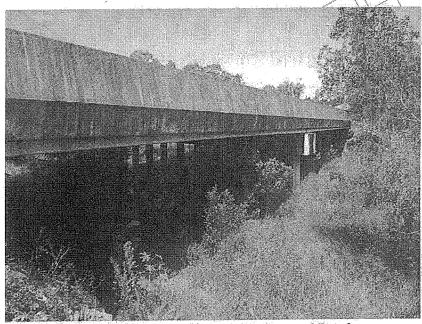
Looking downstream towards Gaskell Street

CREEK	BULIMBA CREEK EAST
LOCATION	GATEWAY MOTORWAY, EIGHT MILE
	PLAINS

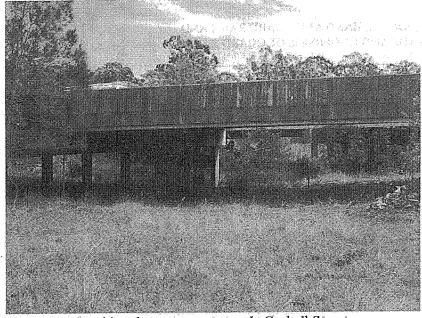
DATE OF SURVEY: Sep 1987	UBD REF: 221 L3
AERIAL PHOTO No:	STRUCTURE ID:
BCC XS No: BE257	CHAINAGE (m): 3330
STRUCTURE DESCRIPTION:	BRIDGE
STRUCTURE SIZE 2 Spans, 40m Total For Culverts: Number of cells/pipes & sizes For Bridges: No	umber of Spans and their lengths
UPSTREAM INVERT LEVEL: 32.17	UPSTREAM OBVERT LEVEL: 37.3
DOWNSTREAM INVERT LEVEL: 32.15 For culverts give floor level.	DOWNSTREAM OBVERT LEVEL: 37.28 For bridges give bed level
For Culverts LENGTH OF CULVERT BARREL AT INVER	T (m): 40
LENGTH OF CULVERT BARREL AT OBVER	XT (m): 40
TYPE OF LINING: Compacted rock aggregate (e.g. concrete, stones, brick, corrugated iron)	
IS THERE A SURVEYED WER PROFILE? If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.	Survey book 6340 / 18
WEIR WIDTH (m): 40	LOWEST POINT OF WEIR (m AHD): 38
(In direction of flow, ie. Distance from u/s face to d/s face)	PIER WIDTH: 700mm
HEIGHT OF GUARDRAILS: 1m	
DESCRIPTION OF ALL HAND AND GUARD HEIGHTS TO TOP AND UNDERSIDE OF GU	RAILS AND JARD RAILS: Concrete freeway wall guardrail
The following should also be provided. Wing wall/Headwall details, entrance details eg. pipe flush with For bridges, details of piers and section under bridge including	n embankment or projecting, socket or square end, entrance rounding, levels, abutment details. Specify Survey Book No.
CONSTRUCTION DATE OF CURRENT STR	UCTURE: N/A PLAN NUMBER: 249804
HAS THE STRUCTURE BEEN UPGRADED? If yes, explain type and date of upgrade. Include plan number a	N nd location if applicable.
ADDITIONAL COMMENTS:	

CREEK	BULIMBA CREEK EAST
LOCATION	GATEWAY MOTORWAY, EIGHT MILE PLAINS

					5/11/14 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1				<u> </u>
ARI	DISCHARGE (m³/s)		U/S WATER	AFFLUX AT	ARI		VELOC		
(years)			LEVEL	MAX FLOW (m)	(m/s)	(m/s)	
	The second secon			(m AHD)	(mm)				
	Weir	Structure	Total			Structure	Weir	Structure	Weir
100	0.0	87.9	87.9	35.5	13	73.9	0.0	1.3	0.0
50	0.0	75.6	75.6	35.36	13	68.4	0.0	1.1	0.0
20	0.0	63.9	63.9	35.24	14	61.6	0.0	0.1	0.0
10	0.0	55.1	55.1	35.1	16	55.9	0.0	4.0	0.0
5	0.0	45,6	45.6	34.93	17	49.3	0.0	0.9	0.0
2	0.0	32.0	32.0	34.59	16	38.8	0.0	0.8	0.0



Looking upstream towards Underwood Road



Looking downstream towards Gaskell Street

CREEK	BULIMBA CREEK EAST
LOCATION	LOGAN ROAD (BOX CULVERT), EIGHT MILE
:	PLAINS

DATE OF SURVEY: Sep 1987	UBD REF: 221 L2		
AERIAL PHOTO No:	STRUCTURE ID:		
BCC XS No: BE254	CHAINAGE(m): 3748		

STRUCTURE DESCRIPTION:

CULVERT

STRUCTURE SIZE

2/2400 x 2400 box culverts

For Culverts: Number of cells/pipes & sizes

For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL: 30.57

UPSTREAM OBVERT LEVEL: 32.97

DOWNSTREAM INVERT LEVEL: 30.37

DOWNSTRÈAM OBVERT LEVEL: 32.77

For culverts give floor level.

For bridges give bed level

For Culverts

LENGTH OF CULVERT BARREL AT INVERT (m): 32

LENGTH OF CULVERT BARREL AT OBVERT (m): 32

TYPE OF LINING: Concrete channel (e.g. concrete, stones, brick, corrugated iron)

IS THERE A SURVEYED WEIR PROFILE?

Survey book 6340 / 18

If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.

WEIR WIDTH (m): 32

LOWEST POINT OF WEIR (m AHD): 33.7

(In direction of flow, ie. Distance from u/s face to d/s face)

HEIGHT OF GUARDRAILS: 0.5m, Handrail: 1m

DESCRIPTION OF ALL HAND AND GUARD RAILS AND

HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Tubular galvanised monowills handrail, flex beam guardrail (Ref. W6088)

The following should also be provided.

Wing wall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE: N/A

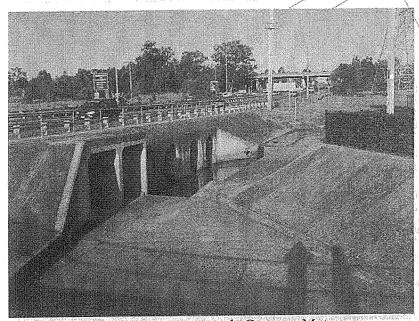
PLAN NUMBER: W6088

HAS THE STRUCTURE BEEN UPGRADED? N

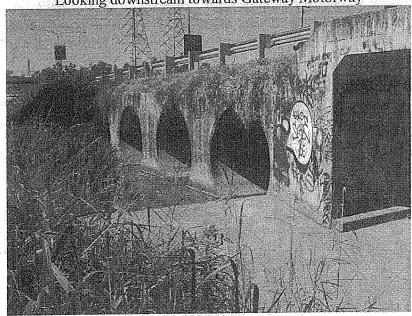
If yes, explain type and date of upgrade. Include plan number and location if applicable.

CREEK	BULIMBA CREEK EAST	
LOCATION	LOGAN ROAD (BOX CULVERT), EIGHT MILE PLAINS	

ARI (years)	DISCHARGE (m³/s)			U/S WATER LEVEL	AFFLUX AT MAX FLOW	AREA (m²)		VELOCITY (m/s)	
Q -111-7				(m AHD)	(mm)			Structure	Weir
	Weir	Structure	Total (2-boxes)			Structure	Weir		and the second
100	0.0	28.8	28.8	33.26	1037	7.5	0.0	4.0	0.0
50	0.0	24.4	24.4	32.98	943	6.7	0.0	3.8	0.0
20	0.0	19.9	19.9	32.67	860	5.8	0.0	3.5	0.0
10	0.0	16.0	16.0	32.36	742	5.0	سرر0.0	3.2	3.1
5	0.0	12.6	12.6	32.08	648	4.3	0.0	3.0	0.0
2	0.0	7.8	7.8	31.68	533	3.1	// 0.0	2.5	0.0



Looking downstream towards Gateway Motorway



Looking upstream towards Gateway Motorway

CREEK	BULIMBA CREEK EAST
LOCATION	LOGAN ROAD (PIPE CULVERT), EIGHT MILE
	PLAINS

DATE OF SURVEY: Sep 1987	UBD REF: 221 L2
AERIAL PHOTO No:	STRUCTURE ID:
BCC XS No: BE254	CHAINAGE (m): 3748

STRUCTURE DESCRIPTION:

CULVERT

STRUCTURE SIZE

4 / 2400 diameter pipe culverts

For Culverts: Number of cells/pipes & sizes

For Bridges; Number of Spans and their lengths

UPSTREAM INVERT LEVEL: 29.89

UPSTREAM OBVERT LEVEL: 32.29

DOWNSTREAM INVERT LEVEL: 29.77

DOWNSTREAM OBVERT LEVEL: 32.17

For bridges give bed level

For culverts give floor level.

For Culverts LENGTH OF CULVERT BARREL AT INVERT (m): 32

LENGTH OF CULVERT BARREL AT OBVERT (m): 32

TYPE OF LINING: Concrete channel (e.g. concrete, stones, brick, corrugated iron)

IS THERE A SURVEYED WEIR PROFILE?

Survey book 6340 / 18

If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.

WEIR WIDTH (m): 32

LOWEST POINT OF WEIR (m AHD): 33.7

(In direction of flow, ie. Distance from u/s face to d/s face)

HEIGHT OF GUARDRAILS: 0.5m, Handrail: Im

DESCRIPTION OF ALL HAND AND GUARD RAILS AND

HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Tubular galvanised monowills handrail, flex beam guardrail (Ref. W6088)

The following should also be provided.

Wing wall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE: N/A

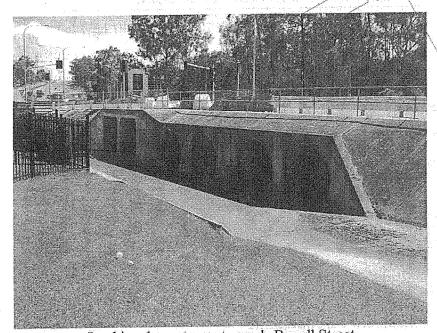
PLAN NUMBER: W6088

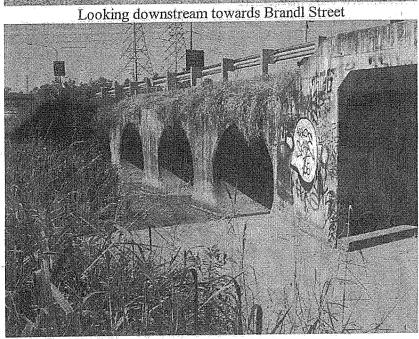
HAS THE STRUCTURE BEEN UPGRADED? N

If yes, explain type and date of upgrade. Include plan number and location if applicable.

CREEK	BULIMBA CREEK EAST	
LOCATION	LOGAN ROAD (PIPE CULVERT), EIGHT MILE PLAINS	

ARI (years)	DISCHARGE (m³/s)		U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (mm)	ARI (m²		VELOCI (m/s)		
	Weir	Structure	Total (3 pipes)			Structure	Weir	Structure	Weir
100	0.0	67.8	67.8	33.26	1037	17.7	0.0	4.5	0.0
50	0.0	60.2	60.2	32.98	943	14.6	0.0	4.2	0.0
20	0.0	51.8	51.8	32.67	860	13.4	0.0	3.9	0.0
. 10	0.0	43.8	43.8	32.36	742	12.2	0.0	3.6	0.0
5	0.0	36.3	36.3	32.08	648	10.8	0.0	3.4	0.0
2	0.0	25.6	25.6	31.68	<i>5</i> 33	8.6	0.0	3.0	0.0





Looking upstream towards Gateway Motorway

HYDRAULIC STRUCTURE REFERENCE SHEET

CREEK	BULIMBA CREEK EAST
LOCATION	PACIFIC MOTORWAY, EIGHT MILE
	PLAINS

DATE OF SURVEY: Sep 1987	UBD REF: 201 M20
AERIAL PHOTO No:	STRUCTURE ID:
BCC XS No: BE247	CHAINAGE (m): 4305
STRUCTURE DESCRIPTION:	CULVERT
STRUCTURE SIZE 5 / 3050 x 2700 box culve For Culverts: Number of cells/pipes & sizes For Bridges: Number of	erts of Spans and their lengths
UPSTREAM INVERT LEVEL: 27.34	UPSTREAM OBVERT LEVEL: 30.04
	DOWNSTREAM OBVERT LEVEL: 29.95 For bridges give bed level
For Culverts LENGTH OF CULVERT BARREL AT INVERT (m)	
LENGTH OF CULVERT BARREL AT OBVERT (no TYPE OF LINING: Shotcrete (e.g. concrete, stones, brick, corrugated iron)	1): 52
IS THERE A SURVEYED WEIR PROFILE? If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.	urvey book 6340 / 17
WEIR WIDTH (m): 52	LOWEST POINT OF WEIR (m AHD): 30.95
(In direction of flow, ie. Distance from u/s face to d/s face)	
HEIGHT OF GUARDRAILS: 1.2m	
DESCRIPTION OF ALL HAND AND GUARD RAI HEIGHTS TO TOP AND UNDERSIDE OF GUARD	ILS AND D RAILS: Flex beam guardrail
The following should also be provided. Wing wall/Headwall details, entrance details eg. pipe flush with embar For bridges, details of piers and section under bridge including abutme	inkment or projecting, socket or square end, entrance rounding, levels, ent details. Specify Survey Book No.
CONSTRUCTION DATE OF CURRENT STRUCT	URE: N/A PLAN NUMBER: N/A
HAS THE STRUCTURE BEEN UPGRADED? N	ration if applicable.

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ADDITIONAL COMMENTS:

If yes, explain type and date of upgrade. Include plan number and location if applicable.

CREEK	BULIMBA CREEK EAST
LOCATION	PACIFIC MOTORWAY, EIGHT MILE PLAINS

ARI (years)	DISCHARGE (m³/s)		PE.	U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (mm)	ARE (m²		VELOCI (nı/s)	
	Weir	Structure	Total			Structure	Weir	Structure	Weir
100	62.0	148.9	210.9	31.8	938	41,2	33.3	3.6	1.9
50	31.7	145.0	176.7	31.6	953	41.2	19.3	3.5	1.6
20	7.3	140.3	147.6	31.28	890	41.2	6.1	3.4	1.2
10	0.1	128.0	128.1	31.1	745	41.2	0.3	3,1	0.5
5	0.0	109.5	109.5	30.4	526	41.1	// 0.0	< 2.7	0.0
2	0.0	80.4	80.4	30	309	36.4	0.0	2.2	0.0

(No picture available)

CREEK	BULIMBA CREEK EAST
LOCATION	EIGHT MILE PLAINS – PARK 'N' RIDE

DATE OF SURVEY: Sep 1987	UBD REF: 201 N19
AERIAL PHOTO No:	STRUCIURE ID:
BCC XS No: BE245	CHAINAGE (m): 4608
STRUCTURE DESCRIPTION: BRIDGE	E
STRUCTURE SIZE 2 / 25m spans; 50m Total For Culverts: Number of cells/pipes & sizes For Bridges: Number of Spans and	their lengths
UPSTREAM INVERT LEVEL: 26.6 UPSTREAM	AM OBVERT LEVEL: 30.7
	TREAM OBVERT LEVEL: 30.69 give bed level
For Culverts LENGTH OF CULVERT BARREL AT INVERT (m): 10	
LENGTH OF CULVERT BARRED AT OBVERT (m): 10	
TYPE OF LINING: Shotcrete (e.g. concrete, stones, brick, corrugated iron)	
IS THERE A SURVEYED WEIR PROFILE? If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.	k 6340 / 17
WEIR WIDTH (m): 10 LOWEST	POINT OF WEIR (m AHD): 31.3
(In direction of flow, ie: Distance from u/s face to d/s face) PIER WII	DTH: UNKNOWN
HEIGHT OF GUARDRAILS: 1m	
DESCRIPTION OF ALL HAND AND GUARD RAILS AND HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS:	Flexi beam guardrail
The following should also be provided. Wing wall/Headwall details, entrance details eg. pipe flush with embankment or profesor bridges, details of piers and section under bridge including abutment details.	ojecting, socket or square end, entrance rounding, levels. Specify Survey Book No.
CONSTRUCTION DATE OF CURRENT STRUCTURE: N/A	PLAN NUMBER: N/A
HAS THE STRUCTURE BEEN UPGRADED? N If yes, explain type and date of upgrade. Include plan number and location if applie	cable.

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***************************************	CREEK	BULIMBA CREEK EAST
	LOCATION	EIGHT MILE PLAINS

ARI (years)	DISCHARGE (m³/s)		U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (mm)	ARI (m²		VELOC (m/s)		
	Weir	Structure	Total	1		Structure	Weir	Structure	Weir
100	0.0	200.6	200.6	29.92	229	80.3	0.0	3.3	0.0
50	0.0	174.3	174.3	29.62	232	68.7	0.0	3,2	0.0
20	0.0	146.7	146.7	29.28	227	56.4	0.0	/3.4	0.0
10	0.0	127.2	127.2	29.04	232	47.9	0.0	3.4	0.0
5	0.0	108.8	108.8	28.86	286	33.2	√ó.o	₹3.3	0.0
2	0.0	79.4	79.4	28.51	357	27.8	0.0	2.9	0.0

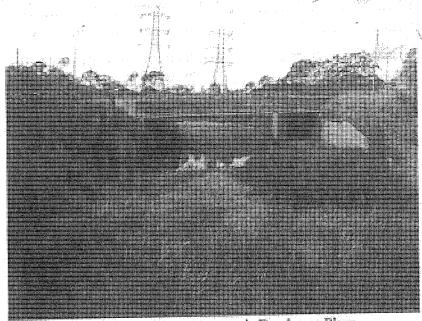
(No picture is available)

Creamin	BULIMBA CREEK EAST
LOCATION	MILES PLATTING ROAD, EIGHT MILE PLAINS

DATE OF SURVEY: Sep 1987	UBD REF: 201 N19
AERIAL PHOTO No:	STRUCTURE ID: B9967
BCC XS No: BE244	CHAINAGE (m): 4660
STRUCTURE DESCRIPTION: BRIDGE	
STRUCTURE SIZE Single span, 24m Total For Culverts: Number of cells/pipes & sizes For Bridges: Number of Spans and t	heir lengths
UPSTREAM INVERT LEVEL: 25.3 UPSTREAM	AM OBVERT DEVEL: 31.5
DOWNSTREAM INVERT LEVEL: 25.28 DOWNST For culverts give floor level.	REAM OBVERT LEVEL: 31.48 ye bed level
For Culverts LENGTH OF CULVERT BARREL AT INVERT (m): 24	
LENGTH OF CULVERT BARRED AT OBVERT (m): 24	
TYPE OF LINING: Concrete block wing walls (e.g. concrete, stones, brick, corrugated iron)	
IS THERE A SURVEYED WEIR PROFILE? If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.	ok 6340 / 17
WEIR WIDTH (m): 24 LOWEST	POINT OF WEIR (m AHD): 30.5
(In direction of flow, ie. Distance from u/s face to d/s face). PIER WIL	OTH: N/A (Single span)
HEIGHT OF GUARDRAILS: 1m	
DESCRIPTION OF ALL HAND AND GUARD RAILS AND HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: 0	Concrete wall guardrail
The following should also be provided. Wing wall/Headwall details, entrance details eg. pipe flush with embankment or pro For bridges, details of piers and section under bridge including abutment details.	jecting, socket or square end, entrance rounding, levels. Specify Survey Book No.
CONSTRUCTION DATE OF CURRENT STRUCTURE: N/A	PLAN NUMBER: N/A
HAS THE STRUCTURE BEEN UPGRADED? N If yes, explain type and date of upgrade. Include plan number and location if applic	able.
ADDITIONAL COMMENTS:	

CREEK	BULIMBA CREEK EAST
	MILES PLATTING ROAD, EIGHT MILE PLAINS
LOCATION	MILES PLATTING ROAD, EIGHT MILE PRIMITS

ARI (years)	DISCHARGE (m³/s)		U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (mm)	ARE (m²	1	VELOC (m/s)		
	Weir	Structure	Total		,	Structure	Weir	Structure	Weir
100	0.0	200.8	200,8	29.63	197	86.0	0,0	2.3	0.0
50	0.0	174.4	174.4	29.33	158	80.0	0.0	2.2	0.0
20	0.0	146.8	146.8	29	120	73.1	0.0	2.0	0.0
10	0.0	127.2	127.2	28.75	95	67.7	0.0	1.9	0.0
5	0.0	108.7	108.7	28.5	80	62.4	0.0	1,8	0.0
2	0.0	79.5	. 79.5	28.1	50	53.0	0.0	<u> </u>	0.0



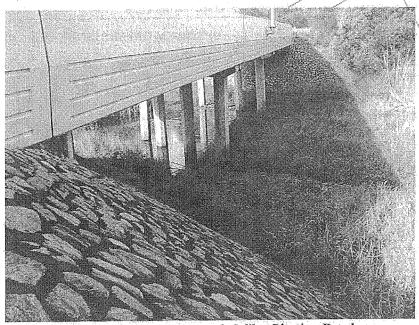
Looking downstream towards Daydream Place

CREEK	BULIMBA CREEK EAST
LOCATION	GATEWAY ON-OFF RAMP, EIGHT MILE
	PLAINS

DATE OF SURVEY: Sep 1987	UBD REF: 201 N18
AERIAL PHOTO No:	STRUCTURE ID:
BCC XS No: BE240	CHAINAGE (m): 5010
STRUCTURE DESCRIPTION: BRIDGE	
STRUCTURE SIZE: 2 / 15m spans; 30m Total For Culverts: Number of cells/pipes & sizes For Bridges: Number of Spans and the	eir lengths
UPSTREAM INVERT LEVEL: 24.35 UPSTREAM	M OBVERT LEVEL: 29.2
DOWNSTREAM INVERT LEVEL: 24.33 DOWNSTF For culveris give floor level.	REAM OBVERT LEVEL: 29.18 bed level
For Culverts LENGTH OF CULVERT BARREL AT INVERT (m) 230	
LENGTH OF CULVERT BARREL AT OBVERT (m): 30 TYPE OF LINING: Grouted stone pitching (e.g. concrete, stones, brick, conjugated iron)	
IS THERE A SURVEYED WEIR PROFILE? Survey book (If yes give details ie, Plan number and/or survey book number.	5340 / 17
Note: This section should be at the highest part of the road	
Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.	POINT OF WEIR (m AHD): 29.7
Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher. WEIR WIDTH (m): 30 LOWEST I	POINT OF WEIR (m AHD): 29.7 TH: 600mm
Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher. WEIR WIDTH (m): 30 LOWEST I	
Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher. WEIR WIDTH (m): 30 LOWEST I (In direction of flow, ie. Distance from u/s face to d/s face) PIER WID	TH: 600mm
Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher. WEIR WIDTH (m): 30 LOWEST I (In direction of flow, ie. Distance from u/s face to d/s face) PIER WIDTH HEIGHT OF GUARDRAILS: 1m DESCRIPTION OF ALL HAND AND GUARD RAILS AND	oncrete freeway wall guardrail
Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher. WEIR WIDTH (m): 30 LOWEST F. (In direction of flow, ie. Distance from u/s face to d/s face) PIER WIDTHEIGHT OF GUARDRAILS: 1m DESCRIPTION OF ALL HAND AND GUARD RAILS AND HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Co. The following should also be provided.	oncrete freeway wall guardrail

CREEK	BULIMBA CREEK EAST
LOCATION	GATEWAY ON-OFF RAMP, EIGHT MILE PLAINS

				Charatan Alicin (SA)	SHARE SALES				
ARI (years)	DISCHARGE (m³/s)		U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (mm)	ARI (m²		VELOC (m/s)		
	Weir	Structure	Total			Structure	Weir	Structure	Weir
100	0.0	206.0	206.0	28.76	516	63.0	0.0	3.3	0.0
50	0.0	178.6	178.6	28.48	449	58.4	0.0	3.1	0.0
20	0.0	149.9	149,9	28.17	382	53.0	0.0	<u>2.8</u>	0.0
10	0.0	130.4	130.4	27.95	342	48.5	0.0	2.7	0,0
5	0.0	111.7	111.7	27.72	301	44.3	∕ 0.0	< 2.5	0.0
2	0.0	81.4	81.4	27.32	234	36.6	\nearrow 0,0 \land	2.2	0.0



Looking upstream towards Miles Platting Road

CREEK	MIMOSA CREEK
LOCATION	NAGLE STREET, MOUNT GRAVATT

UBD REF: 201 B10
STRUCTURE ID: B1520
CHAINAGE (m): 1739
neir lengths
M OBVERT LEVEL: 44.1 REAM OBVERT LEVEL: 44.05 ve hed level

WEIR WIDTH (m): 12

LOWEST POINT OF WEIR (m AHD): 44.49

(In direction of flow, ie. Distance from ws face to d's face)

PIER WIDTH: N/A (Single span)

HEIGHT OF GUARDRAILS: 1m

DESCRIPTION OF ALL HAND AND GUARD RAILS AND HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Rectangular galvanised balustrade handrail (Ref. W1800), Height 46.9

The following should also be provided.

Wing wall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE: 01-07-1971 PLAN NUMBER: W1800

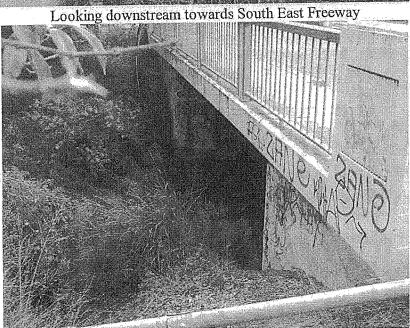
HAS THE STRUCTURE BEEN UPGRADED? N

If yes, explain type and date of upgrade. Include plan number and location if applicable.

	and the second s	
	CREEK	MIMOSA CREEK
-	LOCATION	NAGLE STREET, UPPER MOUNT GRAVATT
- 1	LOCALLOCA	

ARI (years)	DISCHARGE (m³/s)		U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (mm)	ARE (m²		VELOCI (m/s)		
	Weir	Structure	Total			Structure	Weir	Structure	Weir
100	43.0	60.5	103.5	45.27	165	29.3	22.1	2.3	2.0
50	26.0	60.6	86.8	45.11	190	29.3	15.4	2.3	1.8
20	6.3	64.2	70.5	44.82	205	29.3	5.4	2.3	1.2
10	0.8	60.0	60.8	44.62	140	29.3	1.1	2.3	0.7
5	0.0	50.9	50.9	44.35	126	27.3	0.0	2.3	0.0
2	0.0	36.4	36.4	43.95	100	20.0	0.0	2.3	0.0





Looking upstream towards Klumpp Road

CREEK	MIMOSA CREEK
LOCATION	PACIFIC MOTORWAY, UPPER MOUNT
	GRAVATT

DATE OF SURVEY:	UBD REF: 201 A11
AERIAL PHOTO No:	STRUCTURE ID:
BCC XS No: MI194	CHAINAGE (m): 1895

STRUCTURE DESCRIPTION: CULVERT

STRUCTURE SIZE

3 / 3000 x 2700+2 x 3000 x 1000 box culverts

For Culverts: Number of cells/pipes & sizes

For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL: 41.1

UPSTREAM OBVERT LEVEL: 43.8

DOWNSTREAM INVERT LEVEL: 40.9

DOWNSTREAM OBVERT LEVEL: 43.6

For bridges give bed level

For culverts give floor level.

For Culverts LENGTH OF CULVERT BARREL AT INVERT (m): 50

LENGTH OF CULVERT BARREL AT OBVERT (m):/50

TYPE OF LINING: Compacted selected fill + gabions

(e.g. concrete, stones, brick corrugated fron)

IS THERE A SURVEYED WEIR PROFILE?

If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.

WEIR WIDTH (m): 50

LOWEST POINT OF WEIR (m AHD): N/A

(In direction of flow, ie. Distance from u/s face to d/s face)

HEIGHT OF GUARDRAILS: 0.5m concrete guardrail + 2.5m acoustic barrier

DESCRIPTION OF ALL HAND AND GUARD RAILS AND

HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Steel posted acoustic barrier fence + concrete guardrail

The following should also be provided.

Wing wall/Headwall details, entrance details eg. Pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE: N/A

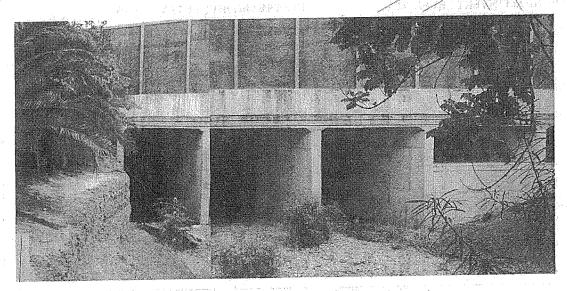
PLAN NUMBER: MRD178308

HAS THE STRUCTURE BEEN UPGRADED? N

If yes, explain type and date of upgrade. Include plan number and location if applicable.

The second secon	
CREEK	MIMOSA CREEK
LOCATION	PACIFIC MOTORWAY, UPPER MOUNT GRAVATT

ARI (years)	DISCHARGE (m³/s)			U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (mm)	AREA (m²)		VELOCITY (m/s)	
	Weir	Structure	Total	V		Structure	Weir	Structure	Weir
100	0.0	98.2	98.2	44.45	604	30.3	0.0	4.4	0.0
50	0.0	84.6	84.6	44.2	554	26.5	0.0	4.2	0.0
20	0.0	71.4	71.4	43.89	468	23.7	0.0	4.0	0.0
0	0.0	61.0	61.0	43.71	450	21.5	0.0	3.9	0.0
5	0.0	50.8	50.8	43.46	410	18.0	0.0	3.7	0.0
2	0.0	36.1	36.1	43.07	400	10.4	0.0	3.4	0.0



Looking downstream towards Kessels Road

CREEK	MIMOSA CREEK	
LOCATION	KESSELS ROAD	

DATE OF SURVEY:	UBD REF: 201 A12
AERIAL PHOTO No:	STRUCTURE ID:
BCC XS No: None	CHAINAGE (m): 2255

STRUCTURE DESCRIPTION:

BRIDGE

STRUCTURE SIZE:

2 / 12m spans; 24m Total

For Culverts: Number of cells/pipes & sizes For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL: 38

UPSTREAM OBVERT LEVEL: 41.2

DOWNSTREAM INVERT LEVEL: 37.9

DOWNSTREAM OBVERT LEVEL: 41.1

For bridges give bed level

For culverts give floor level.

For Culverts LENGTH OF CULVERT BARREL AT INVERT (m): 25

LENGTH OF CULVERT BARREL AT OBVERT (m) 25

TYPE OF LINING: Grouted stone pitching (e.g. concrete, stones, brick, corrugated iron)

IS THERE A SURVEYED WEIR PROFILE?

If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.

WEIR WIDTH (m): 25

LOWEST POINT OF WEIR (m AHD): 41.71

(In direction of flow, ie. Distance from u/s face to d/s face)

PIER WIDTH: 600mm

HEIGHT OF GUARDRAILS: 0.85m

DESCRIPTION OF ALL HAND AND GUARD RAILS AND

HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Rectangular painted balustrade handrail

The following should also be provided.

Wing wall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE: N/A

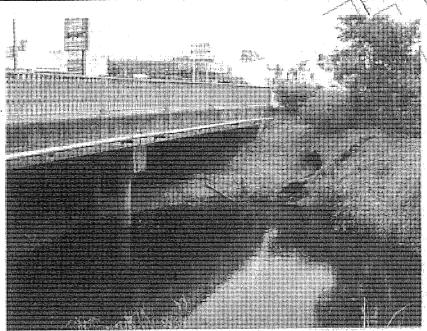
PLAN NUMBER: W4324

HAS THE STRUCTURE BEEN UPGRADED? N

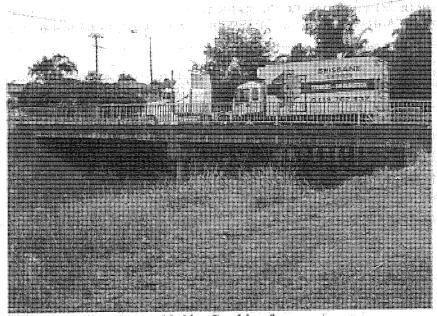
If yes, explain type and date of upgrade. Include plan number and location if applicable.

-	CREEK	MIMOSA CREEK	
	LOCATION	KESSELS ROAD, MACGREGOR	

ARI (years)	DISCHARGE (m³/s)			U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (mm)	ARE (m²		VELOC (m/s)	
	Weir	Structure	Total	1		Structure	Weir	Structure	Weir
100	13.7	98.4	112.1	42.19	262	50.6	10.5	1.9	1.3
50	2.6	91.5	94.1	41.99	243	50.6	2.7	1.8	0.9
20	0.0	79.3	79.3	41.7	169	50.4	0.0	1.6	0,0
10	0.0	68.2	68.2	41.41	83	46.8	0,0	1.5	0.0
5	0.0	56.2	56.2	41.2	63	42.0	0.0	1.4	0.0
2	0.0	40.5	40.5	40.81	44	35.0	<u>/0.0</u>	(1.2	0.0



Kessels Road Bridge looking from downstream



Kessels Road bridge Looking from upstream

CREEK	MIMOSA CREEK
LOCATION	PARKWAY STREET,
	MACGREGOR

DATE OF SURVEY:	UBD REF: 201 A13
AERIAL PHOTO No:	STRUCTURE ID; B1580
BCC XS No: MI11	CHAINAGE (m): 2648

STRUCTURE DESCRIPTION:

BRIDGE

2 spans, 27.5m Total

For Culverts: Number of cells/pipes & sizes For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL: 36.4

UPSTREAM OBVERT LEVEL: 39.9

DOWNSTREAM INVERT LEVEL: 36.3

DOWNSTRÈAM OBVERT LEVEL: 39.8

For culverts give floor level.

For bridges give bed level

For Culverts

LENGTH OF CULVERT BARREL AT INVERT (m): 12

LENGTH OF CULVERT BARREL AT OBVERT (m): 12

TYPE OF LINING: Grouted stone pitching (e.g. concrete, stones, brick, corrugated iron)

IS THERE A SURVEYED WE'R PROFILE?

If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.

WEIR WIDTH (m): 12

LOWEST POINT OF WEIR (m AHD): 40

(In direction of flow, ie. Distance from u/s face to d/s face)

PIER WIDTH: 400mm

HEIGHT OF GUARDRAILS: 1m

DESCRIPTION OF ALL HAND AND GUARD RAILS AND

HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Tubular galvanised balustrade handrail (Refer DWG. in plan W3533)

The following should also be provided.

Wing wall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE: 01-07-1966

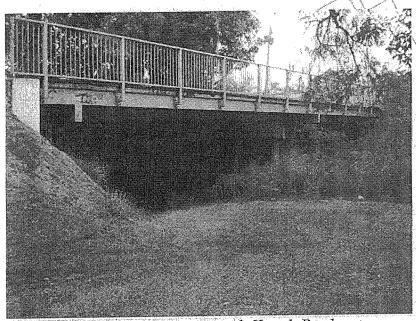
PLAN NUMBER: W3533

HAS THE STRUCTURE BEEN UPGRADED? N

If yes, explain type and date of upgrade. Include plan number and location if applicable.

CR	EEK	MIMOSA CREEK
LOCA	TION	PARKWAY STREET, MACGREGOR

ARI (years)	. 2		U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (mm)	. ARI (m²		VELOC (m/s)		
	Weir	Structure	Total			Structure	Weir	Structure	Weir
100	0.2	110.3	110.5	40.07	230	46.6	0.3	2.4	0.8
50	0.0	95.3	95.3	39.87	200	43.2	0.0	2.2	0.0
20	0.0	78.8	78.8	39.62	170	40.7	0.0	2.0	0.0
10	0.0	67.4	67.4	39.43	140	36.0	0.0	1.9	0.0
5	0.0	56.1	56.1	39.22	120	32.5	0.0	1.7	0.0
2	0.0	39.5	39.5	38.87	80	26.7	//0,0	1.5	0.0



Looking upstream towards Kessels Road



Looking downstream towards Padstow Road

CREEK	TRIBUTARY A
LOCATION	SCHOOL ROAD TO FREEWAY, EIGHT MILE
	PLAINS

DATE OF SURVEY:	UBD REF: 221 P3
AERIAL PHOTO No:	STRUCTURE ID:
BCC XS No: BE1020	CHAINAGE (m): 2072

STRUCTURE DESCRIPTION:

CULVERT

STRUCTURE SIZE

3 / 3100 x 2100 box culverts

For Culverts: Number of cells/pipes & sizes For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL: 32.96

UPSTREAM OBVERT LEVEL: 35.06

DOWNSTREAM INVERT LEVEL: 32.76

DOWNSTREAM OBVERT LEVEL: 34.86

For culverts give floor level.

For bridges give bed level

For Culverts

LENGTH OF CULVERT BARREL AT INVERT (m): 52

LENGTH OF CULVERT BARREL AT OBVERT (m): 52

TYPE OF LINING: Concrete channel (e.g. concrete, stones, brick, corrugated iron)

IS THERE A SURVEYED WEIR PROFILE?

If yes give details ie, Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.

WEIR WIDTH (m): 52

LOWEST POINT OF WEIR (m AHD): 37.35

(In direction of flow, ie. Distance from u/s face to d/s face)

HEIGHT OF GUARDRAILS: 0.5m, Handrail: 1m

DESCRIPTION OF ALL HAND AND GUARD RAILS AND

HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Tubular galvanised monowills handrail, flex beam guardrail

The following should also be provided.

Wing wall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE: N/A

PLAN NUMBER: MRDGATEWAY

HAS THE STRUCTURE BEEN UPGRADED? N

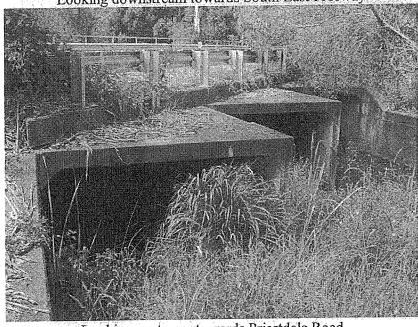
If yes, explain type and date of upgrade. Include plan number and location if applicable.

CREEK	TRIBUTARY A
LOCATION	SCHOOL ROAD TO FREEWAY, EIGHT MILE PLAINS

ARI (years)	DISCHARGE (m³/s)		U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (mm)	ARF (m²	A	VELOC (m/s		
	Weir	Structure	Total			Structure	Weir	Structure	Weir
100	0.0	67.6	67.6	36.54	868	19.5	0.0	3.5	0.0
50	0.0	59.2	59.2	36.09	573	19.5	0.0	. 3.0	0.0
20	0.0	50.0	50.0	35.75	413	19.5	0.0	2.6	0.0
10	0.0	42.8	42.8	35.45	270	19.5	0.0	∠2.2	0.0
5	0.0	35.3	35.3	35.16	160	19.4	0.0	1.8	0.0
2	0.0	25,4	25.4	34.79	80	16.8	0.0	<u>(1.5</u>	0.0



Looking downstream towards South East Freeway



Looking upstream towards Priestdale Road

CREEK	TRIBUTARY A
LOCATION	SOUTH-EAST FREEWAY OFFRAMP, EIGHT MILE
	PLAINS

DATE OF SURVEY:	UBD REF: 221 N2
AERIAL PHOTO No:	STRUCTURE ID:
BCC XS No: BE1005	CHAINAGE (m): 2545

STRUCTURE DESCRIPTION:

CULVERT

STRUCTURE SIZE

9 / 2400 x 1800 box culverts

For Culverts: Number of cells/pipes & sizes

For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL: 30.73

UPSTREAM OBVERT LEVEL: 32.53

DOWNSTREAM INVERT LEVEL: 30.56

DOWNSTREAM OBVERT LEVEL: 32.36

For bridges give bed level

For culverts give floor level.

For Culverts

LENGTH OF CULVERT BARREL AT INVERT (m): 17

LENGTH OF CULVERT BARREL AT OBVERT (m): 17

TYPE OF LINING: Shotcrete (e.g. concrete, stones, brick, corrugated iron)

IS THERE A SURVEYED WEIR PROFILE?

If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.

WEIR WIDTH (m): 17

LOWEST POINT OF WEIR (m AHD): 33.4

(In direction of flow, ie. Distance from u/s face to d/s face)

HEIGHT OF GUARDRAILS: 1m

DESCRIPTION OF ALL HAND AND GUARD RAILS AND

HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Concrete freeway wall guardrail

The following should also be provided.

Wing wall/Headwall details, entrance details eg, pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE: N/A

PLAN NUMBER: N/A

HAS THE STRUCTURE BEEN UPGRADED? N

If yes, explain type and date of upgrade. Include plan number and location if applicable.

CREEK	TRIBUTARY A
LOCATION	SOUTH-EAST FREEWAY OFFRAMP, EIGHT MILE PLAINS

ARI (years)	DISCHARGE (nr³/s)			U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (mm)	ARE (m²	."	VELOCI (m/s)	
	Weir	Structure	Total	7		Structure	Weir	Structure	Weir
100	20.3	95.9	116.2	33.77	316	38.9	15.9	2.5	1.3
50	4.2	95.9	100.1	33.57	327	38.9	5.1	2,5	0.8
20	0.0	84.5	84.5	33.19	235	38.9	0.0	2,2	0,0
10	0.0	72.6	72.6	32.9	158	38.9	0.0	√4.9	0.0
5	0.0	60.3	60.3	32,6	98	38.5	0.0	1.9	0,0
2	0.0	43.4	43.4	32.19	71	31.2	~··0.0	(1,8	0.0

(No photos available)

CREEK	TRIBUTARY A				
LOCATION	GATEWAY MOTORWAY, EIGHT MILE				
	PLAINS				

DATE OF SURVEY:	UBD REF: 221 M1
AERIAL PHOTO No:	STRUCTURE ID:
BCC XS No: BE1005	CHAINAGE (m): 2805

STRUCTURE DESCRIPTION:

PIPE CULVERTS

STRUCTURE SIZE

2/3300 diameter

For Culverts: Number of cells/pipes & sizes For Bridge

For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL: 28.37

UPSTREAM OBVERT LEVEL: 31.67

DOWNSTREAM INVERT LEVEL: 27.88

DOWNSTREAM OBVERT LEVEL: 31.18

For culverts give floor level.

For bridges give bed level

For Culverts

LENGTH OF CULVERT BARREL AT INVERT (m): 128

LENGTH OF CULVERT BARREL AT OBVERT (m):128

TYPE OF LINING: Shotcrete (e.g. concrete, stones, brick, corrugated iron)

IS THERE A SURVEYED WER PROFILE?

If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.

WEIR WIDTH (m): 128

LOWEST POINT OF WEIR (m AHD): 38.4

(In direction of flow, ie. Distance from u/s face to d/s face)

HEIGHT OF GUARDRAILS: 1m

DESCRIPTION OF ALL HAND AND GUARD RAILS AND

HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Concrete freeway wall guardrail

The following should also be provided.

Wing wall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE: N/A

PLAN NUMBER: MRDGATEWAY

HAS THE STRUCTURE BEEN UPGRADED? N

If yes, explain type and date of upgrade. Include plan number and location if applicable.

CREEK	TRIBUTARY A
LOCATION	GATEWAY MOTORWAY, EIGHT MILE PLAINS

ARI (years)		DISCHAI (m³/s)	1 ³ /s) LEVE		U/S WATER AFFLUX AT LEVEL MAX FLOW			VELOCITY (m/s)	
	Weir	Structure	Total (from six culverts)	(m AHD)	(mm)	Structure	Weir	Structure	Weir
100	0.0	40.9	40.9	32.5	312	17.1	0.0	2.4	0.0
50	0.0	35.2	35.2	32.19	215	17.1.	0.0	2.4	0.0
20	0.0	29.8	29.8	31.78	130	17.1	0.0	2.6	0.0
10	0.0	26.1	26.1	31.8	158	16.7	0.0	2,6	0.0
5	0.0	21.8	21.8	30.8	59	15.3	0.0	2.6	0.0
2.	0.0	15.9	15.9	30.4	52	12:5	0.0	\2.6	0.0

(No photos available)

CREEK	TRIBUTARY A
LOCATION	GATEWAY MOTORWAY (2), EIGHT MILE
	PLAINS

DATE OF SURVEY:		UBD REF: 221 M1
AERIAL PHOTO No:		STRUCTURE ID:
BCC XS No: BE1005		AMTD (m): 2805
STRUCTURE DESCRIPTION:	ULVERT	
STRUCTURE SIZE 3 / 3500 diameter pipe cul For Culverts: Number of cells/pipes & sizes For Bridges: Number of		ir lengths
	UPSTREAM	OBVERT LEVEL: 31.88
DOWNSTREAM INVERT LEVEL; 27.88 For culverts give floor level.	DOWNSTR For bridges give	EAM OBVERT LEVEL: 31.38 bed lovel
For Culverts LENGTH OF CULVERT BARREL AT INVERT (m) LENGTH OF CULVERT BARREL AT OBVERT (m)	7 1	
TYPE OF LINING: Compacted rock aggregate (e.g. concrete, stones, brick, corrugated iron)		
IS THERE A SURVEYED WEIR PROFILE? If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.		
WEIR WIDTH (m): 128	LOWEST P	OINT OF WEIR (m AHD): 38.4
(In direction of flow, ie. Distance from u/s face to d/s face)	PIER WIDT	H: UNKNOWN

HEIGHT OF GUARDRAILS: 1m

DESCRIPTION OF ALL HAND AND GUARD RAILS AND HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Concrete freeway wall guardrail

The following should also be provided.

Wing wall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE: N/A

PLAN NUMBER: MRDGATEWAY

HAS THE STRUCTURE BEEN UPGRADED? N

If yes, explain type and date of upgrade. Include plan number and location if applicable.

CREEK	TRIBUTARYA
LOCATION	GATEWAY MOTORWAY (2), EIGHT MILE PLAINS

ARI (years)		DISCHARGE (m³/s)		U/S WATER LEVEL	AFFLUX AT MAX FLOW	AREA (m²)		VELOCITY (m/s)	
	Weir	Structuré	Total (from 3 culverts)	(m AHD)	(m AHD) (mm)	Structure	Weir	Structure	Weir
100	0.0	69.9	69.9	32.5	316	28.9	0.0	2.4	0.0
50	0.0	60.3	60.3	32.19	326	28.9	0.0	2.4	0.0
20	0.0	51.3	51.3	31.78	235	28.7	0.0	2.4	0.0
10	0.0	44.4	44.4	31.38	158	27.1	0.0	2,5	0.0
.5	0.0	36.9	36.9	30.98	98	24.3	0.0	(2.7	0.0
2	0.0	27.0	27.0	30.47	71	19:7	₹ 0:0	2.6	0.0

(No photos available)

CREEK	TRIBUTARY B
LOCATION	DANCE COURT NO. 1, EIGHT MILE PLAINS

UBD REF: 221 K2 DATE OF SURVEY: STRUCTURE ID: AERIAL PHOTO No: CHAINAGE (m): 1062 BCC XS No: BE2030

STRUCTURE DESCRIPTION:

CULVERT

STRUCTURE SIZE

2/3650 x 1500 box culverts

For Culverts: Number of cells/pipes & sizes

For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL: 33.83

UPSTREAM OBVERT LEVEL: 35.33

DOWNSTREAM INVERT LEVEL: 33.7

DOWNSTREAM OBVERT LEVEL: 35.2

For bridges give bed level

For culverts give floor level.

For Culverts

LENGTH OF CULVERT BARREL AT INVERT (m): 20

LENGTH OF CULVERT BARREL AT OBVERT (m)/20

TYPE OF LINING: Concrete channel + grouted stone pitching (e.g. concrete, stones, brick, corrugated iron)

IS THERE A SURVEYED WEIR PROFILE?

If yes give details ie, Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.

WEIR WIDTH (m): 20

LOWEST POINT OF WEIR (m AHD): 35.88

(In direction of flow, ie. Distance from u/s face to d/s face)

HEIGHT OF GUARDRAILS: 1m

DESCRIPTION OF ALL HAND AND GUARD RAILS AND

HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Tubular galvanised monowills handrail (Ref. W8983)

The following should also be provided.

Wing wall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE: Nov-1992

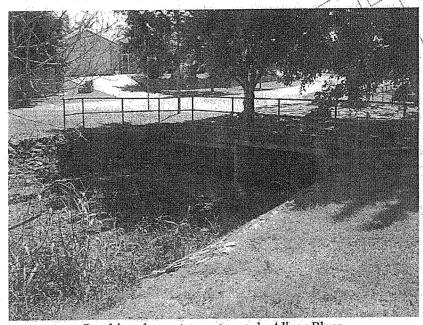
PLAN NUMBER: W8983

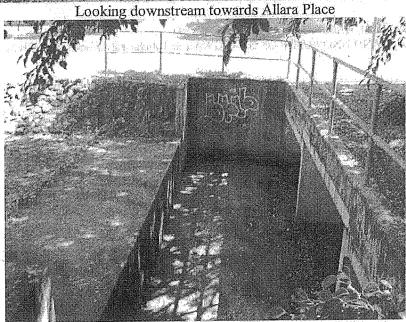
HAS THE STRUCTURE BEEN UPGRADED? N

If yes, explain type and date of upgrade. Include plan number and location if applicable.

CREEK	TRIBUTARY B
LOCATION	DANCE COURT NO.1, EIGHT MILE PLAINS

ARI (years)	1 12	DISCHAF (m³/s)		U/S WATER LEVEL	AFFLUX AT MAX FLOW	AREA (m²)		VELOCITY (m/s)	
4	Weir	Structure	Total (from No.1&No.2)	(m AHD)	(mm)	Structure	Weir	Structure	Weir
100	3.0	33.5	36.5	36.04	798	9.4	3.2	3.6	0.9
50	1.5	32.2	33.6	35.98	778	9.2	1.9	3.5	0.8
20	0.0	26.3	26.3	35.71	645	8.0	0.0	3.3	0.0
10	0.0	24.7	24.7	35.63	640	7.7	0.0	/3.2	0.0
5	0.0	20.8	20.8	35.44	584	6.8	0.0	3.0	0.0
2	0.0	14.4	14.4	35.09	528	5.3	0.0	2.7	0.0





Looking downstream - drop structure

CREEK	TRIBUTARY B
LOCATION	DANCE COURT NO. 2, EIGHT MILE PLAINS

UBD REF: 221 K2 DATE OF SURVEY: STRUCTURE ID: AERIAL PHOTO No: CHAINAGE (m): 1062 BCC XS No: BE2020

STRUCTURE DESCRIPTION:

CULVERT

STRUCTURE SIZE

1/3650 x 1700 box culverts

For Culverts: Number of cells/pipes & sizes

For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL: 33.83

UPSTREAM OBVERT LEVEL: 35.53

DOWNSTREAM INVERT LEVEL: 33.7

DOWNSTREAM OBVERT LEVEL: 35.4

For bridges give bed level

For culverts give floor level.

For Culverts LENGTH OF CULVERT BARREL AT INVERT (m): 20

LENGTH OF CULVERT BARREL AT OBVERT (m)/20

TYPE OF LINING: Concrete channel (e.g. concrete, stones, brick, corrugated iron)

IS THERE A SURVEYED WEIR PROFILE?

If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.

WEIR WIDTH (m): 20

LOWEST POINT OF WEIR (m AHD): 35.88

(In direction of flow, ie. Distance from u/s face to d/s face)

HEIGHT OF GUARDRAILS: 1m

DESCRIPTION OF ALL HAND AND GUARD RAILS AND

HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Tubular galvanised monowills handrail (Ref. W8983)

The following should also be provided.

Wing wall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE: Nov-1992

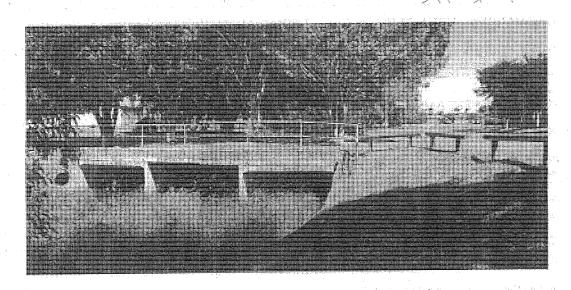
PLAN NUMBER: W8983

HAS THE STRUCTURE BEEN UPGRADED? N

If yes, explain type and date of upgrade. Include plan number and location if applicable.

CREEK	TRIBUTARY B
LOCATION	DANCE COURT NO.2, EIGHT MILE PLAINS

				리고에 가는 사람들이 되었다.	化电路分配 联合的 連升的	and the second second			
ARI (years)		DISCHAI (m³/s)		U/S WATER LEVEL	AFFLUX AT MAX FLOW	AREA (m²)		VELOCITY (m/s)	
Quay	Weir	Structure	Total (from No.3)	(m AHD)	(mm)	Structure	Weir	Structure	Weir
100	3.0	16.5	19.5	36.04	799	4.7	3.2	3.5	0.9
50	1.5	15.8	17.3	35.98	778	4.5	1.9	3,5	0.8
20	0.0	12.9	12.9	35.71	645	4.0	0.0	3,3	0.0
10	0.0	12.1	12.1	35.63	640	3.8	0.0	3.2	0.0
5	0.0	10.2	10,2	35,44	584	3.4	0.0	3.0	0.0
2	0.0	7.1	7.1	35.09	528	2.6	0.0	2.7	0.0



Looking upstream towards Bordeaux Street

CREEK	TRIBUTARY B
LOCATION	LOGAN ROAD, EIGHT MILE PLAINS

DATE OF SURVEY:	UBD REF: 221 LI
AERIAL PHOTO No:	STRUCTURE ID:
BCC XS No: NIL	CHAINAGE (m): 1361

STRUCTURE DESCRIPTION:

CULVERT

STRUCTURE SIZE

 $1/2.6 \times 2.6$

For Culverts: Number of cells/pipes & sizes

For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL: 31.05

UPSTREAM OBVERT LEVEL: 33.65

DOWNSTREAM INVERT LEVEL: 31

DOWNSTREAM OBVERT LEVEL: 33.6

For bridges give bed level

For culverts give floor level.

For Culverts

LENGTH OF CULVERT BARREL AT INVERT (m): 28

LENGTH OF CULVERT BARREL AT OBVERT (m)/28

TYPE OF LINING: Precast concrete wing walls (e.g. concrete, stones, brick, corrugated iron)

IS THERE A SURVEYED WEIR PROFILE?

If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.

WEIR WIDTH (m): 28

LOWEST POINT OF WEIR (m AHD): 33.4

(In direction of flow, ie. Distance from u/s face to d/s face)

HEIGHT OF GUARDRAILS: 0.5m

DESCRIPTION OF ALL HAND AND GUARD RAILS AND

HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Flexi-beam guardrail

The following should also be provided.

Wing wall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE: N/A

PLAN NUMBER: N/A.

HAS THE STRUCTURE BEEN UPGRADED? N

If yes, explain type and date of upgrade. Include plan number and location if applicable.

CREEK	TRIBUTARY B
LOCATION	LOGAN ROAD, EIGHT MILE PLAINS

ARI (years)	DISCHARGE (m³/s)		U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (mm)	ARI (m²		VELOC (m/s))	
	Weir	Structure	Total		:" 	Structure	Weir	Structure	Weir
100	4.8	15.6	20.4	33.84	485	5.9	3.9	2.9	1.2.
50	1.8	15.2	17.0	33.72	480	5.6	1.7	2.8	1.0
20	1.5	14.7	16.1	33.62	469	5.5	1.5	2.8	1.0
10	0.5	13.9	14.4	33.52	436	5.4	0.6	2.7	0.9
5	0.0	12.8	12.8	33.41	382	5.2	0.0	2.6	0.0
2	0.0	11.3	11.3	33.27	344	4.9	0.0	2.3	0.0



Looking downstream towards South-East Freeway

CREEK	TRIBUTARY C
LOCATION	GATEWAY, RUNCORN

DATE OF SURVEY:	UBD REF: 221 J6
AERIAL PHOTO No:	STRUCTURE ID:
BCC XS No: BE3000	CHAINAGE (m): 1008

STRUCTURE DESCRIPTION:

CULVERT

STRUCTURE SIZE

4 / 2700 diameter pipe culverts

For Culverts: Number of cells/pipes & sizes

For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL: 36.9

UPSTREAM OBVERT LEVEL: 39.6

DOWNSTREAM INVERT LEVEL: 36.6

DOWNSTREAM OBVERT LEVEL: 39.3

For bridges give bed level

For culverts give floor level.

For Culverts LENGTH OF CULVERT BARREL AT INVERT (m): 90

LENGTH OF CULVERT BARREL AT OBVERT (m)/90

TYPE OF LINING: Shotcrete (e.g. concrete, stones, brick, corrugated iron)

IS THERE A SURVEYED WEIR PROFILE?

If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.

WEIR WIDTH (m): 90

LOWEST POINT OF WEIR (m AHD): 42

(In direction of flow, ie. Distance from u/s face to d/s face)

HEIGHT OF GUARDRAILS: 1m

DESCRIPTION OF ALL HAND AND GUARD RAILS AND

HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Concrete freeway wall guardrail

The following should also be provided.

Wing wall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE: N/A

PLAN NUMBER: N/A

HAS THE STRUCTURE BEEN UPGRADED? N

If yes, explain type and date of upgrade. Include plan number and location if applicable.

CREEK	TRIBUTARY C
LOCATION	GATEWAY, RUNCORN

ARI (years)	DISCHARGE (m³/s)			U/S WATER AFFLUX AT LEVEL MAX FLOW (m AHD) (mm)	AREA (m²)		VELOCITY (m/s)		
i	Weir	Structure	Total			Structure	Weir	Structure	Weir
100	0.0	28,0	28.0	39.11	69	20.5	0.0	2.6	0.0
50	0.0	24.4	24,4	38.95	42	19.4	0.0	2.5	0.0
20	0.0	20.7	20.7	38.55	71	15.5	0.0	2.4	0.0
10	0.0	17.5	17.5	38.5	516	12.9	0.0	2.4	0.0
5	0.0	14.4	14.4	38.5	580	10.2	0.0	2.4	0.0
2	0.0	10.2	10.2	38.5	928	5.0	/ 0.0	2.2	0.0

(No photo available)

CREEK	TRIBUTARY B1	
LOCATION	GASKELL STREET, EIGHT MILE	
	PLAINS	

DATE OF SURVEY:	UBD REF: 221 K2
AERIAL PHOTO No:	STRUCTURE ID:
BCC XS No: BE2000	CHAINAGE (m): 1030
CTPLICTED DESCRIPTION.	CITYERT

STRUCTURE DESCRIPTION:

CULVERI

STRUCTURE SIZE

3 / 3000 x 1500 box culverts

For Culverts: Number of cells/pipes & sizes

For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL: 31.3

UPSTREAM OBVERT LEVEL: 32.8

DOWNSTREAM INVERT LEVEL: 31.2

DOWNSTREAM OBVERT LEVEL: 32.7

For bridges give bed level

For culvens give floor level.

For Culverts LENGTH OF CULVERT BARREL AT INVERT (m): 22

LENGTH OF CULVERT BARREL AT OBVERT (m): 22

TYPE OF LINING: Precast concrete wing walls (e.g. concrete, stones, brick, corrugated iron)

IS THERE A SURVEYED WEIR PROFILE?

If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.

WEIR WIDTH (m): 22

LOWEST POINT OF WEIR (m AHD): 33.4

(In direction of flow, ie. Distance from u/s face to d/s face)

HEIGHT OF GUARDRAILS: 0.5m, Handrail: 1m

DESCRIPTION OF ALL HAND AND GUARD RAILS AND

HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Flex beam guardrail, galvanised mesh handrail

The following should also be provided.

Wing wall/Headwall details, entrance details eg. pipe flush with embankment of projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE: N/A

PLAN NUMBER: N/A

HAS THE STRUCTURE BEEN UPGRADED? N

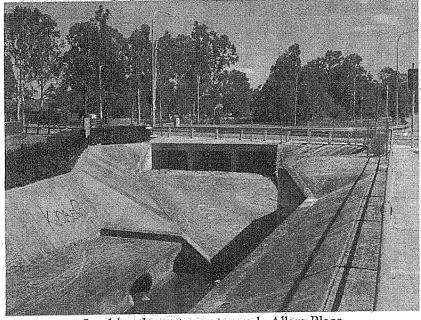
If yes, explain type and date of upgrade. Include plan number and location if applicable.

	CREEK	TRIBUTARY B1
-	LOCATION	GASKELL STREET, EIGHT MILE PLAINS

ARI (years)	DISCHARGE (m³/s)		U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (mm)	ARE (m²		VELOCI (m/s)		
	Weir	Structure	Total			Structure	Weir	Structure	Weir
1.00	0.0	28.2	28.2	33.23	27	13.5	0.0	3.1	0.0
50	0.0	24.8	24.8	32.92	15	13.5	0.0	3.0	0.0
20	0.0	21.0	21.0	32.62	29	12.5	0.0	2.8	0.0
10	0.0	17.9	17.9	32.37	23	10.1	0.0	2.7	0.0
5	0.0	14.1	14.1	32.19	111	7.7	0.0	2.5	0.0
2	0,0	8.7	8.7	31.99	232	4.6	<u>~0.0</u>	₹2.1	0.0



Looking upstream towards Gateway Motorway



Looking downstream towards Allara Place

CREEK	MINNIPPI
LOCATION	GATEWAY MOTORWAY, TINGALPA

DATE OF SURVEY:	UBD REF: 162 B15
AERIAL PHOTO No:	STRUCTURE ID:
BCC XS No: BM30GHD	CHAINAGE (m): 748

STRUCTURE DESCRIPTION: MINIMUM ENERGY CULVERTS

STRUCTURE SIZE

6/3000 x 3000 box culverts

For Culverts: Number of cells/pipes & sizes

For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL: 1.0

UPSTREAM OBVERT LEVEL: 4.00

DOWNSTREAM INVERT LEVEL: 0.85

DOWNSTREAM OBVERT LEVEL: 3.85

For bridges give bed level

For culverts give floor level.

LENGTH OF CULVERT BARREL AT INVERT (m): 60

LENGTH OF CULVERT BARREL AT OBVERT (m)/60

TYPE OF LINING: Precast concrete wing walls (e.g. concrete, stones, brick, corrugated iron)

IS THERE A SURVEYED WEIR PROFILE?

If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.

WEIR WIDTH (m): 60

LOWEST POINT OF WEIR (m AHD): N/A

(In direction of flow, ie. Distance from u/s face to d/s face)

HEIGHT OF GUARDRAILS: 2m concrete guardrail + 2m acoustic barrier

DESCRIPTION OF ALL HAND AND GUARD RAILS AND

HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Flex beam guardrail, concrete guardrail + steel posted acoustic fence

The following should also be provided.

Wing wall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE: N/A

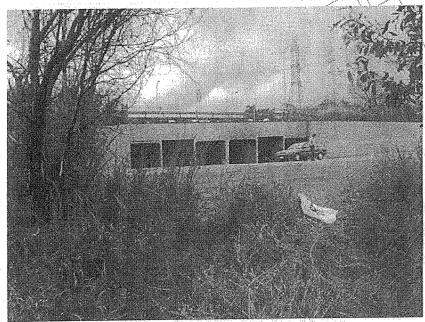
PLAN NUMBER: A04B-3010

HAS THE STRUCTURE BEEN UPGRADED? N

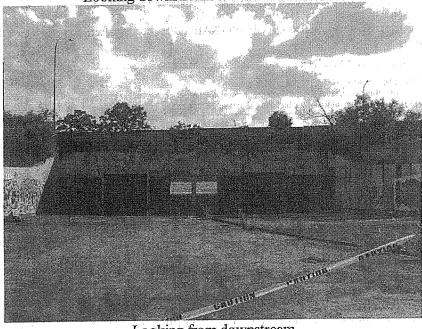
If yes, explain type and date of upgrade. Include plan number and location if applicable.

CREEK	MINNIPPI BRANCH
LOCATION	GATEWAY MOTORWAY, TINGALPA

ARI (years)	DISCHARGE (m³/s)		U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (mm)	ARE (m²		VELOC (m/s)		
	Weir	Structure	Total			Structure	Weir	Structure	Weir
100	0.0	74.0	74.0	3.97	122	54.3	0.0	1.4	0.0
50	0.0	62.3	62.3	3.76	70	50.9	0.0		0.0
20	0.0	48.2	48.2	3.45	43	46.0	0.0	1.1	0.0
10	.0.0	35.2	35.2	3.2	19	42.0	0.0	0.8	0.0
5	0.0	22.3	22.3	2.93	.8	31.2	0.0	0.6	0.0
2	0.0	2.8	2.8	2,24	4	24.5	J 0.0	0.1	0.0



Looking downstream towards Creek Road



Looking from downstream

CREEK	MURARRIE BRANCH
LOCATION	GATEWAY CULVERTS, MURARRIE

DATE OF SURVEY:	UBD REF: 162 C14
AERIAL PHOTO No:	STRUCTURE ID:
BCC XS No: 30GHD	Chainage (m): 475

STRUCTURE DESCRIPTION: MINIMUM ENERGY CULVERTS

STRUCTURE SIZE

For culverts give floor level.

11 / 2000 x 1600 box culverts

For Culverts: Number of cells/pipes & sizes

For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL: 1

UPSTREAM OBVERT LEVEL: 2.6

DOWNSTREAM INVERT LEVEL: 0.9

DOWNSTREAM OBVERT LEVEL: 2.5

For bridges give bed level

For Culverts

LENGTH OF CULVERT BARREL AT INVERT (m).34

LENGTH OF CULVERT BARREL AT OBVERT (m)/34

TYPE OF LINING: Precast concrete wing walls

(e.g. concrete, stones, brick corrugated iron)

IS THERE A SURVEYED WEIR PROFILE?

If yes give details ie, Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.

WEIR WIDTH (m): 34

LOWEST POINT OF WEIR (m AHD): 3

(In direction of flow, ie. Distance from u/s face to d/s face)

HEIGHT OF GUARDRAILS: 1.9m

DESCRIPTION OF ALL HAND AND GUARD RAILS AND

HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Steel-posted chain-link fence

The following should also be provided.

Wing wall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE: N/A

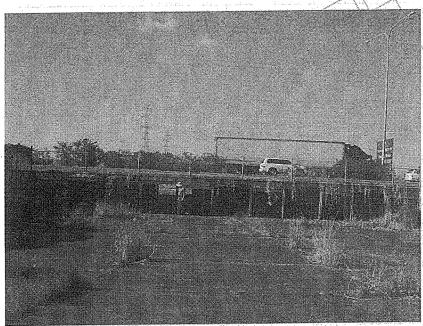
PLAN NUMBER: A04B-301C

HAS THE STRUCTURE BEEN UPGRADED? N

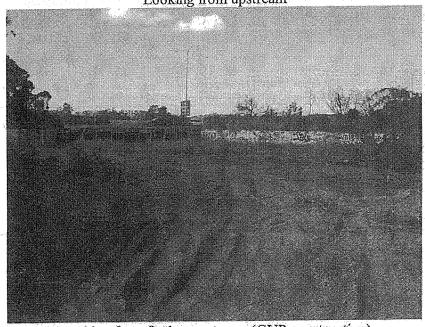
If yes, explain type and date of upgrade. Include plan number and location if applicable.

CREEK	MURARRIE BRANCH
LOCATION	GATEWAY CULVERTS, MURARRIE

ARI (years)	DISCHARGE (m³/s)		U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (mm)	ARI (m²		VELOC (m/s)	ITY	
	Weir	Structure	Total			Structure	Weir	Structure	Weir
100	10.9	66.5	77.4	3.23	250	35.2	11.3	1.9	1.0
50	0.3	65.3	65.4	3.05	238	35.2	0.7	1.9	0.7
20	0.0	61.5	61.5	2.8	209	35.2	0.0	1.8	0.0
10	0.0	53.1	53,1	2.65	174	32.0	0.0	1.7	0.0
5	0.0	43.0	43.0	2.43	136	28.9	0.0	1.5	0.0
2	0.0	26.9	26.9	2.13	77	24.0	/ 0.0	(1.1	0.0



Looking from upstream



Looking from further upstream (GUP construction)

CREEK	TINGALPA BRANCH
LOCATION	DOWNSTREAM OF GATEWAY,
	TINGALPA

UBD REF: 162 B15 DATE OF SURVEY: STRUCTURE ID: AERIAL PHOTO No: CHAINAGE (m): 950 BCC XS No: BM30GHD **CULVERT** STRUCTURE DESCRIPTION: 3 / 1200 diameter pipe culverts STRUCTURE SIZE For Bridges: Number of Spans and their lengths For Culverts: Number of cells/pipes & sizes UPSTREAM OBVERT LEVEL: 1.8 UPSTREAM INVERT LEVEL: 0.6 DOWNSTRÈAM OBVERT LEVEL: 1.62 DOWNSTREAM INVERT LEVEL: 0.42 For bridges give bed level For culverts give floor level. For Culverts LENGTH OF CULVERT BARREL AT INVERT (m): 25 LENGTH OF CULVERT BARREL AT OBVERT (m): 25 TYPE OF LINING: Shotcrete (e.g. concrete, stones, brick, corrugated iron) IS THERE A SURVEYED WEIR PROFILE? If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher. LOWEST POINT OF WEIR (m AHD): 3.85 WEIR WIDTH (m): 25 PIER WIDTH: UNKNOWN (In direction of flow, ie. Distance from u/s face to d/s face) HEIGHT OF GUARDRAILS: 2m DESCRIPTION OF ALL HAND AND GUARD RAILS AND HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS: Concrete freeway wall guardrail The following should also be provided. Wing wall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No. CONSTRUCTION DATE OF CURRENT STRUCTURE: N/A PLAN NUMBER: N/A HAS THE STRUCTURE BEEN UPGRADED? N

K-113

ADDITIONAL COMMENTS:

If yes, explain type and date of upgrade. Include plan number and location if applicable.

CREEK	MINNIPPI CREEK
LOCATION	GATEWAY MOTORWAY, TINGALPA

ARI (years)	1		U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (mm)	AREA (m²)		VELOCITY (m/s)		
	Weir	Structure	Total			Structure	Weir	Structure	Weir
100	0.0	74.0	74.0	3.97	122	54.3	0.0	1,4	0.0
50	0.0	62.3	62.3	3.76	70	50.9	0.0	1.2:	0.0
20	0.0	48.2	48.2	3.45	43	46.0	0.0	1.1	0.0
10	0.0	35.2	35.2	3.2	19	42.0	0.0	0,8	0.0
5	0.0	22.3	22.3	2.93	8	31.2	0.0	0.6	0.0
2	0.0	2.8	2.8	2,24	4	24.5	€ 0.0	0.1	0.0







Taigum Drain Flood Study

Report A - Model Calibration

Report B - Design Events

July 2011



Prepared for Water Resources City Planning and Sustainability



Taigum Drain Flood Study Report A - Model Calibration

July 2011

Prepared by Built and Natural Environment City Project Office

Prepared for Water Resources City Planning and Sustainability



Taigum Drain Flood Study Report A – Model Calibration

City Project Office
Floor 1 Green Square
505 St Pauls Terrace
Fortitude Valley QLD 4006

Issue No.	Date of Issue	(Author/s)		Edited Proofre		Reviewed By Approved for (Project Dire			
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1 Introduction

1.1 Purpose

In 2009, City Design was commissioned to investigate the existing hydrology and hydraulic models and provide a ranked list prioritising the flood models requiring maintenance and enhancement works. Following that in 2010, City Design was commissioned by Water Resource Branch to introduce a level of service for all future flood modelling and provide a rolling schedule for the eight highest priority flood model upgrades to assist with Council's future planning and budgeting. This task is listed as priority 1 in the Lord Mayor's Taskforce on Suburban Flooding (BCC, 2005) and aims to reduce the impact of flooding. Taigum Drain Flood Study was identified for the flood model upgrade with the highest priority.

The purpose of the Taigum Drain Flood Study was to determine flood levels within the Taigum Drain Catchment for the range of standard storm events. These flood levels will be used for setting development guideline levels for the future development within the Taigum Drain Catchment.

The Taigum Drain Flood Study Report describes the development of the hydrological model using the XPRAFTS software, development of the TUFLOW hydraulic model, hydraulic and hydrologic models calibration and verification, presenting the methodology and results of the design event analyses from 2 year Average Recurrence Interval (ARI) to 100 year ARI and providing the flood maps for the Taigum Drain Catchment.

1.2 Previous Studies on Taigum Drain

Preliminary work to define waterway corridors throughout Taigum began in 1997 as part of the Master Drainage Plan for Carseldine and Taigum Catchments (WBM Oceanics Australia). The defined corridors in 1997 Master Drainage Plan were revised by the Taigum Waterway Investigation (BCC 2002). The corridor definition process was finalised and completed two years later as part of Taigum Waterway Investigation (BCC 2004).

 Master Drainage Plan for Carseldine and Taigum Catchments (WBM OCEANICS AUSTRALIA 1997)

A Master Drainage (MDP) of the Carseldine and Taigum catchments was prepared by WBM Oceanics Australia in March 1997. The MDP identified waterway corridors for ultimate development of the catchment downstream of Beams Road (i.e. for the open drain). These corridors were between 15 and 45 metres wide and were designed to convey the 'Q50 overland event' (WBM 1997, p. 51). As well as proposing corridor widths, the MDP also recommended that the corridors be partly vegetated and provide for public access. Natural channel form, which would involve a considerable degree of revegetation, was recommended.

Taigum Waterway Investigation (BCC 2002)

An investigation of Taigum Waterway was undertaken by BCC (2002). It included review of the MDP and the hydraulic model. The investigation raised concern about the following issues:

- The corridors proposed in the MDP are based on the Q50 flood event. The City Plan (BCC 2000) recommends that waterway corridor widths be set to a minimum of 60 metres, 30 metres either side of the centre line of the channel (BCC 2000, Map 2: Waterways Corridors and Wetlands). The corridors proposed by the MDP are less



than 60m and hence do not comply with the City Plan. BCC (2002) redesigned the corridor width of the Taigum Waterway for the reach downstream of Roghan Road. The corridor widths upstream of Roghan Road were not increased as development had already been approved and constructed based on the MDP recommendations (WBM, 1997).

- The BCC (2002) study also rectified an inconsistency found in the MDP regarding the use of Manning's roughness 'n-value'. The average 'n-value' used in the BCC (2002) study was 0.06 downstream of Roghan Road. This value was chosen because it maintained the Q100 flood levels upstream of Roghan Road at or below approved Q100 flood levels.

The modelling methodology and quality controls (e.g. run logs) used in the 2002 model appear to be in good order. However, modelled cross-sections are based on about ten year survey. The hydraulic modelling was undertaken using a very older version of MIKE11 model (Version 3.2), which is not supported by the software vendor Danish Hydraulic Institute.

Taigum Waterway Investigation (BCC 2004)

In March 2004, Water Resources Branch commissioned City Design to undertake a hydraulic investigation of Taigum Drain to assist in the preparation of Local Plan and Infrastructure Charges Plan in the Taigum Area. This investigation included upgrading the 2002 hydraulic model, finalising the waterway corridor and providing 100 year ARI design flood levels in Taigum Waterway. A variable corridor width (a corridor of varying width but with a minimum width of 60 m) was recommended which was used in this flood study.

1.3 Catchment Description

Taigum Drain is a tributary of the Cabbage Tree Creek and has an approximate catchment area of 250Ha. It flows through Brisbane's northern suburbs of Zillmere and Taigum and merges with the Cabbage Tree Creek downstream of the Gateway Motorway at Taigum which eventually discharges into Morton Bay. The location of the Taigum Drain Catchment is shown in *Figure 1A*.

Taigum Drain is moderately flat along its length. Upper portions of the catchment being typically sloped at less than 3% while lower portions of the catchment are quiet flat and low lying. The very lower reach of Taigum Drain is tidal affected.

The upper portion of the waterway, upstream of Beams Road with the exception of a section in Mungo Scott Park, is all comprised of underground trunk drainage. The trunk drainage system passes under and through the mobile home park at the corner of Beams and Handford Roads, before discharging to an open drainage channel. There is a modified section of Taigum Drain (i.e. having been channelised) upstream of Roghan Road as a result of the recent development. The flow travels in a northerly direction and passes under Quarrion Street, Roghan Road and Church Road. The drainage line continues in a north - north easterly direction, in a generally confined condition, before passing under Gateway Motorway and entering Cabbage Tree Creek.

1.4 Study Elements

The Taigum Drain Flood Study consists of two elements;

- 1. Model set up and calibration
- 2. Design event modelling

BCC.079.0277



Report A - Model Calibration

Hydrologic and hydraulic models of Taigum Drain were developed for the primary waterway within the catchment study area. The hydrologic model simulates catchment rainfall-runoff and, in a simplified approach, the movement of flood waters down the waterway. The hydraulic model simulates the movement of flood waters using advanced mathematics, thereby giving a more accurate representation of flood behaviour, particularly where downstream effects and hydraulic structures are influential.

Calibration is a process of model parameter adjustment by which flood levels generated by the model using recorded rainfall are compared with recorded flood level data for the event in question. When sufficient points are in agreement the model is considered to be "calibrated" to that event. By calibrating to a range of historical flood events the model can be used more confidently to represent the action of the catchment and to develop design event flood levels.

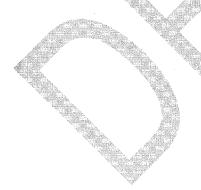
The model was calibrated to the May 2009 and October 2010 events.

This report, Report A – Model Calibration documents the data used in the XP-RAFTS and TUFLOW models and the details of the modelling for the Taigum Drain system.

Report B - Design Event Modelling

Following on from Report A, Report B – Design Event Modelling provides the results of the design event model simulations obtained using the calibrated/verified hydrologic and hydraulic models. The 100, 50, 20, 10, 5 and 2 year ARI events were modelled. Peak flood maps are represented in *Appendix A* of Report B.

Report B also incorporates the impact of future development (Flood Regulation Line) on flood levels.





2 Available Data

2.1 Hydrographic Data

2.1.1 Continuous Rainfall Gauges

C_R560 and LCR566 are the closest continuous rainfall gauges to Taigum Drain Catchment with the recorded historical data from 1994 to present. The C_R560 and LCR566 gauge data was used for the model calibration. The gauges information are summarised in *Table 2.1*. The locations of the gauges are shown in *Figure 2A*. The Z_R850 gauge was discarded as it was recently installed and does not have sufficient data for calibration purposes.

Table 2.1: Pluviograph Information

Station	Location	Operation Period	Rainfall data availability			
ID			20/05/09 Event	07/02/10 Event	11/10/10 Event	13/01/11 Event
C_R560	Cabbage Tree Creek, Deagon	June 1994 to present	1	1	1	1
LCR566	Little Cabbage Tree Ck, Aspley Reservoir	June 1994 to present	1	√ √	√ √	7

2.1.2 Continuous Streamflow Gauges

There is no continuous streamflow gauge available within Taigum Drain Catchment area and as such the calibration of hydrology model was not undertaken.

2.1.3 Maximum Height Gauges (MHG)

There are four maximum height gauges (MHGs) within the Taigum Drain Catchment and one downstream of Gateway Motorway for which records are available from 2009 onwards. All five gauges were used to source data for calibration purposes; one gauge downstream of Roghan Road, one upstream of Church Road, one north of Poplar Place Cal-de-sac, one in front of 334 Muller Road and one downstream of Gateway Motorway which are shown in *Figure 2A*. *Table 2.2* summarises peak flood levels recorded at each MHG for the calibration events.

Table 2.2: Maximum Flood Height Recordings from MHGs

		Peak Flood L	evel (m AHD)				
Gauge ID	Event Date						
	May 09	February 10	October 10	January 11			
C340	5.34	N/A	5.64	5.36			
C330	4.79	4.15	5.15	4.89			
C320	3.23	N/A	3.78	3.00			
C310	2.47	N/A	2.97	N/A			
C300	2.49	2.54	2.84	N/A			

N/A - No data available



2.2 Topographic Data

2.2.1 DEM

The 2009 Airborne Laser Scanning (ALS) survey data was used for the creation of 0.5m Digital Elevation Model (DEM) for the two dimensional (2D) domain of the TUFLOW model.

2.2.2 Creek Cross Sections

Cross section data used to define waterway bathymetry in the TUFLOW hydraulic model obtained from a detailed ground survey of the cross sections undertaken by J.A. Liddle Surveys Pty Ltd in 2011. The surveyed cross sections were used for development of the 1D channel in the TUFLOW model.

2.3 Hydraulic Structures

Details of the hydraulic structures included in TUFLOW model were sourced from the following:

- Detailed survey by J.A. Liddle Surveys Pty Ltd in 2011
- As constructed drawings
- Hydraulic structure reference sheets (HSRS) provided in Master Drainage Plan Report of Carseldine and Taigum Catchment (1997)

Structure information for all structures included in the TUFLOW model is summarised in *Table B.1* of *Appendix B* and also in the Hydraulic Structure Reference Sheets (HSRS) provided in *Appendix C* of Report B Design Modelling.





3 Model Descriptions

3.1 Introduction

Hydrologic models simulate the catchment rainfall-runoff and, in a simplified approach, the movement of flood waters down the waterway. Hydraulic models simulate the movement of flood waters using more advanced mathematics, thereby giving a more accurate representation of flood behaviour, particularly where downstream effects and hydraulic structures are influential.

The hydrologic model was set up based on the XP-RAFTS software version 2009 (XP Software, 2009) and is described in **Section 3.2**.

The 1D/2D hydraulic model was developed based on TUFLOW version 2010-10-AC-w32 (TUFLOW, 2011). Unsteady models simulate the progression of a flood wave down the channel over time and therefore have the ability to simulate:

- the rise and fall of a flood;
- storage effects of floodplains; and
- overland flowpaths

The unsteady hydraulic model is described in Section 3.3.

3.2 Hydrologic Model

Sub-catchments are represented as nodes within the XP-RAFTS to provide points within the model where total and localised flow hydrograph information can be extracted. The hydrologic model included a total of 25 sub-catchments or nodes to describe the 250ha catchment.

Sub-catchment boundaries were determined based on a review of existing catchment delineations and updated in accordance with the local topography using 0.5 metre contours and local drainage networks.

A further eight "dummy" nodes were incorporated into the model to allow flow hydrographs to be derived downstream of junctions. Catchment area, landuse (impervious and pervious factors), slope and roughness (PERN) values were used to define the sub-catchments.

A large portion of the Taigum Drain Catchment is residentially developed with some rural, community, open space and industrial zoning. Waterway corridor exists along the Taigum Drain with a significant amount of open space and park along the channel corridor. The existing landuse plan for Taigum Drain Catchment is presented in *Figure 3A* and the break-up of existing landuse types is shown in *Figure 4A*.



Figure 4A: Existing Landuse within the Taigum Drain Catchment

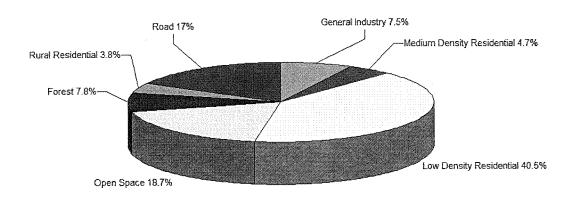


Table 3.1 shows the fraction impervious values adopted and Table B.2 in Appendix B summarises the subcatchment properties.

Table 3.1:Adopted Fraction Impervious Values for Taigum Drain Catchment- Existing Scenario

Development Type	Fraction Impervious
General Industry	0.90
Medium Density Residential	0.70
Low Density Residential	0.50
Open Space	0.05
Forest	0.00
Rural Residential	0.10
Road	0.90

Note: The above table is an amalgam of the Brisbane City Council Department of Works Supplement to QUDM (Brisbane City Council 1994, p.QUDM-BCC-2) and the Queensland Urban Drainage Manual (QUDM) (Neville Jones & Associates and Australian Water Engineering, 1993, Tables 5.04.1 and 5.04.2).



XP-RAFTS allows each sub-catchment to be divided into two sub-areas to reflect impervious and pervious portions. Due to the extent of catchment development, this approach was followed for all sub-catchments in the model.

The fraction impervious of sub-catchments was determined in accordance with the Brisbane City Council Department of Works Supplement to QUDM (Brisbane City Council 1994, p.QUDM-BCC-2) and the Queensland Urban Drainage Manual (QUDM) (Neville Jones & Associates and Australian Water Engineering 1993, Tables 5.04.2 and 5.04.1).

Table 3.2 broadly identifies the landuse classification within the Taigum Drain Catchment for the existing development condition.

Table 3.2 Areas of landuse – Existing development scenario

Land Use Type	Total Area (ha)	% of Total Area
General Industry	19.0	7.5
Medium Density Residential	11.8	4.7
Low Density Residential	101.6	40.5
Open Space	47.1	18.7
Forest	19.5	7.8
Rural Residential	9.4	3.8
Road	42.8	17.0

An average impervious value of 47% was obtained for the catchment.

The impervious fraction in the XP-RAFTS software was set to 2% for pervious areas and 100% for impervious areas. PERN values, which are a multiplication factor applied to the storage delay time coefficient "B" in the storage discharge relationship of the XP-RAFTS hydrologic simulation at each to take into account the roughness of each subcatchment (Aitken, 1975) and were set to 0.040 and 0.015 for pervious and impervious subcatchments respectively.

The drainage paths of the Taigum Drain Catchment were represented in the XP-RAFTS model by a number of links, including channel routing links, lagging links and dummy lagging links (with zero lag time). Channel cross sections are a requirement for and were applied to routing links and were sourced from 2009 ALS survey data. Mannings 'n' values for each cross section were initially derived based on site inspection and 2009 Aerial photo.

Figure 5A, shows the XP-RAFTS catchment plan, nodes and links. Full details regarding each link used in the model (including length, slope, adopted cross section and Mannings 'n' values) are listed *Table B.3* in *Appendix B*.



3.3 Hydraulic Model

A TUFLOW model was developed for the study area combining both 2D and 1D element. The TUFLOW model was developed using TUFLOW version 2010-10-AC-w32 (TUFLOW, 2011).

Taigum Drain 2011 TUFLOW calibration model includes the following features:

- 1 Branch^{*}
- 32 cross sections
- 7 broad crested weirs and 10 culverts to describe the crossings within the model
- 25 inflow sources (over area) within the model
- 2 locations for the downstream boundary condition at the end of model

A 5m grid was used to define area topography in the two dimensional domain. The hydraulic model is a combination of 1D and 2D components with a 1D branch comprising of the links to represent the main channel (low flow channel) and the channel crossing such as culverts and bridges throughout the site area. It is hereafter referred to as the '2D model'.

Model Layout

The hydraulic model extent covers only the main branch of Taigum Drain from downstream of Colonial Mobile Village north of Beams Road in Zillmere to Gateway Motorway in Taigum.

Model Cross Sections

Cross sections were sourced from the 2011 survey undertaken by J.A. Liddle Surveys Pty Ltd. The cross sections were extended in a few instances to the full extent of the 1D channel using 2009 ALS survey data.

All surveyed cross sections were implemented into 1D component of TUFLOW model. The locations of surveyed cross sections are shown in *Figure 6A*.

Model Parameters

Mannings 'n' values were adopted based on site inspection and aerial photography. An initial water level (IWL) equal to the fixed downstream boundary levels were set for all model scenarios to enable them to begin a simulation with no water in the system or to run "dry". A time step of one and two seconds were adopted for the 1D and 2D component of the model respectively.

Hydraulic Structures

In total, 10 crossings, road and footbridge, were modelled including eight culverts and two bridges. Weirs were employed for better representation of the road crests or top of the handrails. All culverts and bridges were modelled as online structure in 1D component of the model and the handrails are presumed to be blocked. Hydraulic Structures Reference Sheets are provided in *Appendix C of Report B*. Structure locations are shown in *Figure 7A*.



Model inflows

A total of 25 inflows for Taigum Drain calibration model were defined to reflect the hydrologic behaviour of the channel and minimise localised increases in flow due to concentrated local inflows. The inflows were defined as flows over the sub-catchment. All inflow catchments in hydraulic model have the identical names to the nodes in hydrologic model. The inflow locations are shown in *Figure 8A*.

Tailwater Conditions

A fixed tailwater level was adopted for this study. The MHG level records for Cabbage Tree Creek were obtained from gauge C300 for calibration events and were used to inform the downstream boundary condition at Cabbage Tree Creek.





4 Calibration

4.1 Calibration Events

Calibration events were selected by considering the relative size of the event and the availability of data for each event. The Taigum Drain MHG Gauges have been installed in recent years (After 2004) and no event prior to 2009 has been recorded. As such, there are only limited historical data available including the following events which were chosen for the purpose of calibration.

Calibration Events

- May 2009
- October 2010

4.1.1 Hydrologic Model Calibration

As there is no stream gauge in Taigum Drain Catchment, the calibration of hydrologic model was not undertaken. However, the model results were verified against the flows calculated using Rational Method. It should be noted that the developed XP-RAFTS model does not represent the real storage of the catchment and as such the results can only be used as the inflow into the hydraulic model. The XP-

RAFTS model parameter BX¹ was varied to achieve the better match of modelled flows to calculated rational method flows and to improve the hydraulic model calibration.

Initial and continuing losses were estimated considering the previous three days of rainfall for each historical event and adjusted to improve the hydraulic model calibration. The adopted losses are summarised in *Table 4.1* and antecedent conditions for each event are discussed in further detail in *Sections 4.2* and *4.3*. A BX¹ value of 0.8 was adopted for the calibration process, where the BX value is a factor applied to the storage delay time coefficient (B) in the XP-RAFTS simulation. The RAFTS default value of -0.285 was used for the storage non-linearity exponent "n".

Table 4.1 Adopted Initial and Continuing Loss Rates for Taigum Drain Catchment

F.2.2	Initial Lo	oss (mm)	Continuing Loss (mm/h)		
Event	Pervious	Impervious	Pervious	Impervious	
May 2009	0	0	2	0	
October 2010	0	0	2 .	0	

4.1.2 Hydraulic Model Calibration

Based on available 2009 aerial photography and the site inspection, no channel, structure and floodplain modifications occurred after selected calibration events and as such all structures and surveyed cross sections were used in hydraulic model for the calibration events.

¹ The XP-RAFTS parameter BX is a multiplication factor for the B parameter, where B = storage delay time coefficient



Manning's n roughness values were varied to improve the correlation of the modelled peak level with recorded data. Adopted manning's n values were not varied across calibration events and values were chosen with the acceptable range to represent the best calibration outcome with all events taken into consideration.

A summary of differences between the recorded and modelled flood levels at each of the MHGs is given in *Table* 4.2. Each event result is analysed in more detail in the following sections.

Table 4.2 Difference between Recorded and Modelled Flood Levels at MHG Locations

	Calibration Events			
MHG	May 09 (m)	Oct 10 (m)		
C340	-0.13	-0.10		
C330	-0.12	-0.20		
C320	0.15	-0.17		
C310	0.08	-0.01		

Blue Modelled result less than recorded level Red Modelled result greater than recorded level

4.2 May 2009 Event

The May 2009 event occurred on the 20th day of the month and was triggered by heavy and prolonged rainfall which occurred across Brisbane and surrounds. The May 2009 flood was described as Brisbane's worst since 1974 at the time of flood. During May 2009 event, the western suburbs received the highest rainfalls.

Four MHG within the Taigum Drain Catchment and one immediately downstream of Gateway Motorway were operational during the May 2009 event. The recorded maximum height gauge readings indicate the May 2009 event was less severe than the October 2010 and January 2011 events.

The rain which fell on the 20th May followed on from significant falls on the 19th May. Due to the Cabbage Tree Creek rise, the area very downstream of Taigum Drain Catchment suffered from creek flooding.

Rainfall gauge stations indicate there was a continues rainfall at all nearby gauges for almost two days prior to the event and the catchment could be therefore considered relatively wet and creek levels likely to be high. The rainfall distribution has CR560 data applied to all the sub-catchments except for the sub-catchment upstream of the railway which adopts the rainfall data from LCR566. Based on the Intensity Frequency Duration (IFD) curves of the recorded rainfall, the frequency of the event was in the order of 2 to 5 years ARI for the time of concentration of 1 hour. The IFD curves are shown in *Figure 9A*.

Table B.4 in Appendix B summarises the rainfall distribution adopted within the catchment for the event.



An initial loss of 0mm and continuous losses of 2mm and 0mm were adopted for previous and impervious areas respectively.

The flood extent for May 2009 event is shown in *Figure 10A*, *Appendix A*. Recorded and modelled peak flood levels for the May 2009 event are presented *Table 4.3*. *Figure 11A* shows a longitudinal profile comparing the May 2009 recorded peak flood levels versus modelled peak flood level at each MHG location for the Taigum Drain.

Sensitivity runs using BX = 2.1 and the above initial loss and continuing loss in the XP-RAFTS model resulted in a particularly good calibration for the 2009 event. However, a BX =0.8 was found to provide a significantly improved calibration for both the 2009 and 2011 events.

Table 4.3 Recorded & Modelled Peak Flood Levels, May 2009

MHG	May 09 Recorded Level	May 09 Modelled Level ¹	Difference (m)
C340	(mAHD) 5.34	(mAHD) 5.21	-0.13
C330	4.79	4.67	-0.12
C320	3.23	3.38	0.15
C310	2.47	2,55	0.08

1bx = 0.8

Blue Modelled result less than recorded level Red Modelled result greater than recorded level

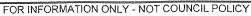
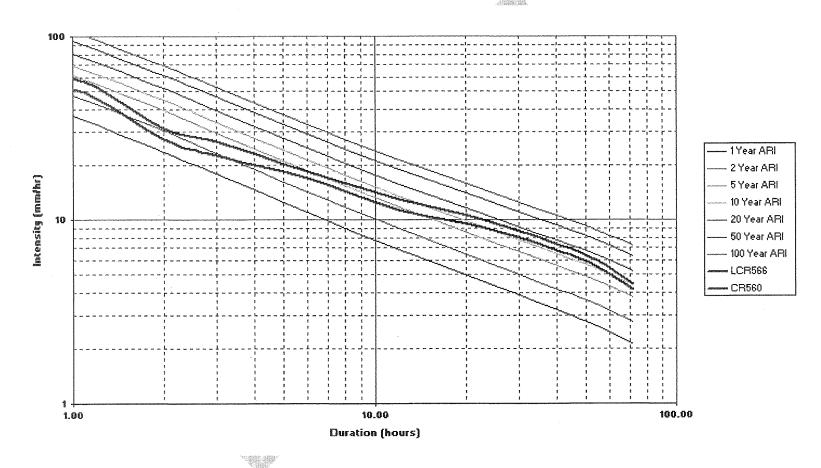


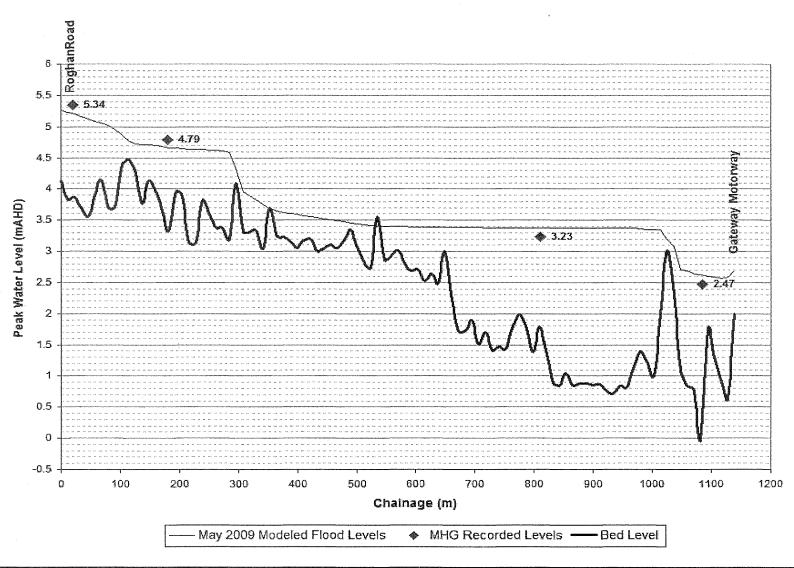


Figure 9A IFD Curve, May 2009



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4.3 October 2010 Event

Occurring on the 11th October, this flood event was triggered by intense and prolonged rainfall across Brisbane and surrounds. The northern suburbs received the highest rainfalls. The rain which fell on the 11th October followed on from moderate falls between the 8th and 10th October.

Moderate flooding was recorded in Cabbage Tree Creek. Due to the Cabbage Tree Creek rise the area very downstream of Taigum Drain Catchment suffered from creek flooding.

Four MHG within the Taigum Drain Catchment and one immediately downstream of Gateway Motorway were operational during the October 2010 event. The records from all MHG's within Taigum Drain Catchment indicate this is the largest event recorded during the period of operation of these gauges and it is the largest event modelled as part of the calibration process.

Rainfall records from two rainfall stations close to the Taigum Drain Catchment are available for this event. Gauges CR560 and LCR566 were selected as the source for rainfall data input for the event. The rainfall distribution has CR560 data applied to all the sub-catchments except for the sub-catchment upstream of the railway which adopts the rainfall data from LCR566. Based on the IFD curves of the recorded rainfall, the frequency of the event was in the order of 5 to 10 years ARI for the time of concentration of 1 hour. The IFD curve are shown in *Figure 12A*.

Rainfall gauge stations indicate there was continues rainfall at all nearby gauges for couple of days prior to the event and the catchment could be therefore considered relatively wet and creek levels likely to be high. An initial loss of 0mm and continuous losses of 2mm and 0mm were adopted for previous and impervious areas respectively. *Table B.4* in *Appendix B* summarises the rainfall distribution adopted within the catchment for the event.

The flood extent for October 2010 event is shown in *Figure 13A*, *Appendix A*. Recorded and modelled peak flood levels for the October 2010 event are presented *Table 4.4*. *Figure 14A* shows a longitudinal profile comparing the October 2010 recorded peak flood levels versus modelled peak flood level at each MHG location for the Taigum Drain.

Sensitivity runs using BX = 2.1 and the above initial loss and continuing loss in the XP-RAFTS model resulted in a reasonable match with recorded levels. However, a BX =0.8 was found to provide a significantly improved calibration for both the 2009 and 2010 events.



Recorded & Modelled Peak Flood Levels, October 2011 Table 4.4

MHG	Oct 10 Recorded Level (mAHD)	Oct 10 Modelled Level ¹ (mAHD)	Difference (m)
C340	5.64	5.54	-0.1
C330	5.15	4.95	-0.2
C320	3.87	3.61	-0.17
C310	2.97	2.96	-0.01

1bx = 0.8

Blue Modelled result less than recorded level Red Modelled result greater than recorded level

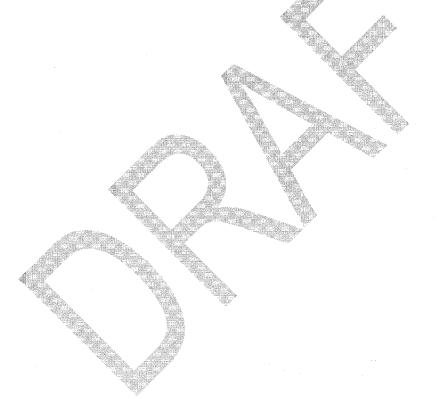




Figure 12A IFD Curve, October 2010

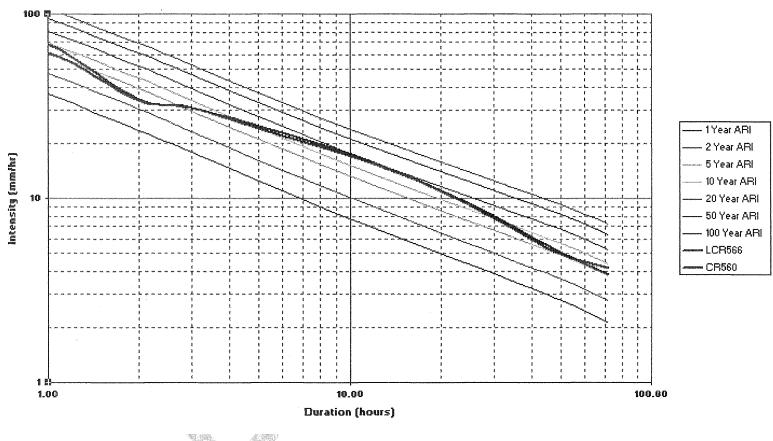
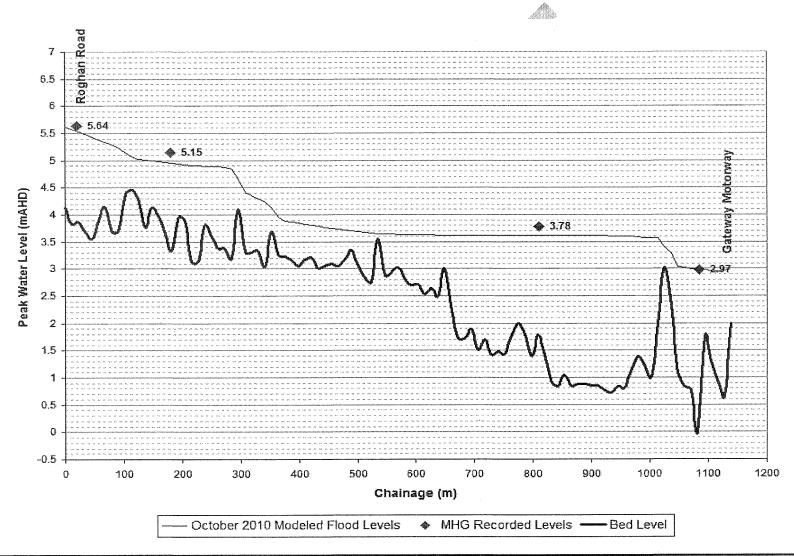






Figure 14A Taigum Drain Calibration, October 2010





4.4 Structure Verification

The Taigum Drain TUFLOW model includes eight sets of culverts and two small bridges. The headlosses at three key structures including Quarrion Street, Roghan Road and Church Road were verified using an independent hydraulic modelling package namely HEC-RAS (version 4.1.0). The headloss predicted by HEC-RAS was then compared against losses calculated by the Taigum Drain TUFLOW 2011 model. Both calibration events were used for the assessment. The results of both hydraulic models are shown in *Table 4.5*.

The results demonstrate the consistency between results from TUFLOW and HEC-RAS model.

2011 structural survey data was used to setup the HEC-RAS models. Inflows and tailwater conditions were taken from the TUFLOW model at corresponding upstream and downstream cross sections. The HEC-RAS models incorporated at least two sections upstream and downstream of the structure to ensure results captured inlet and outlet losses.

Table 4.5 Verification of Structure Head Losses

Structure	Event	Flow (m3/s)	TUFLOW (m)	HEC RAS (m)	Difference (m)
	May 09	9.95	0.04	0.07	-0.03
Quarrion Street	Oct 10	12.86	0.03	0.06	-0.03
	May 09	17.93	0.02	0.07	-0.05
Roghan Road	Oct 10	27.88	0.06	0.20	-0.14
Church Road	May 09	18.21	0.04	0.03	+0.01
Church Road	Oct 10	26.77	0.05	0.04	+0.01



4.5 Sensitivity to model parameters

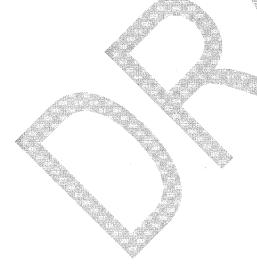
The sensitivity of the Taigum Drain 2011 TUFLOW model to adopted model parameters was tested by varying Storage Coefficient (BX) in XP-RAFTS model.

Sensitivity runs using BX = 2.1 with same initial loss and continuing loss in the XP-RAFTS model resulted in a reasonable match with recorded levels. The peak water level dropped by a maximum of 110mm across MHG recorded levels. However, a BX =0.8 was found to provide a significantly improved calibration for both the 2009 and 2010 events.

4.6 Calibration summary

A good agreement in calibration was achieved for the Taigum Drain 2011 model. The following comments should be noted:

- Model results are often lower than recorded results. This is considered acceptable on the basis that it is within the 300 mm acceptable tolerance.
- Flood levels for gauge C310 is influenced by the flood level in Cabbage Tree Creek for both calibration events.





5 References

BCC 2000, Brisbane City Plan 2000, BCC, Brisbane

BCC in draft, Taigum Waterway Investigation, prepared by Brisbane City Council, June 2004

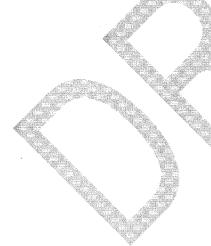
BCC, Stormwater Investigation Report 246, 252 and 258 Church Road Taigum, Prepared by MRG Water Consulting Pty Ltd for BCC, May 2007

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TUFLOW, TUFLOW Manual 2010-10-AA, TUFLOW, 2010, Australia

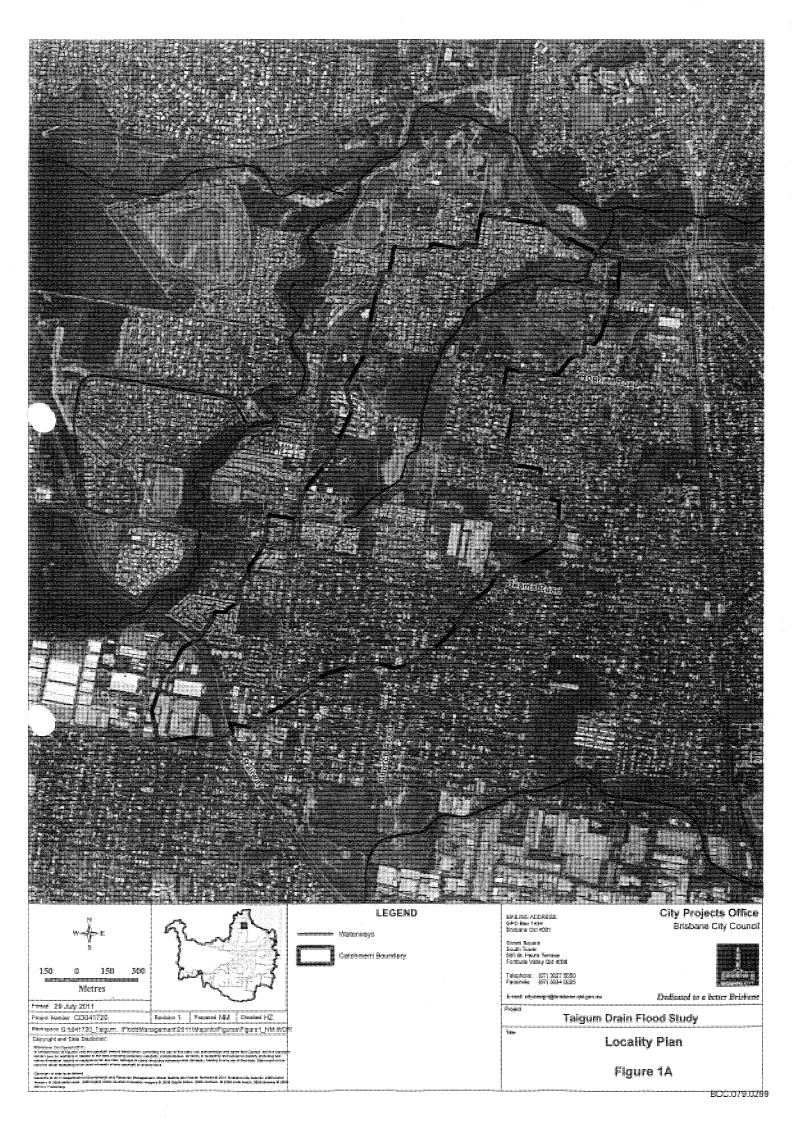
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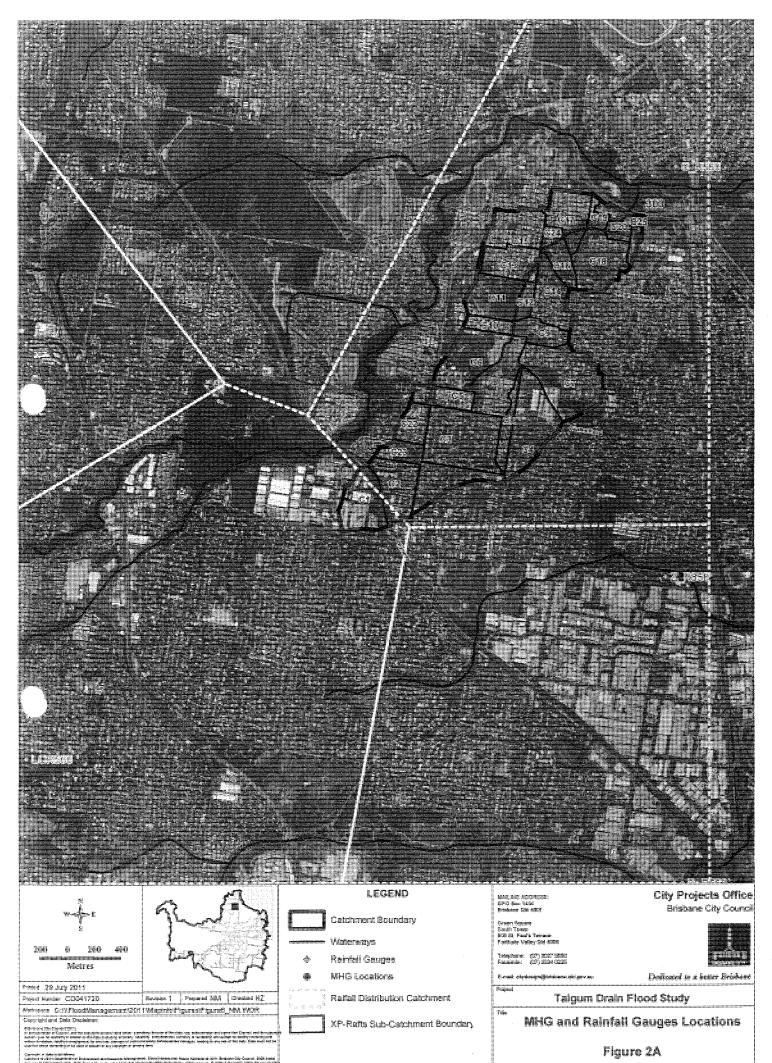


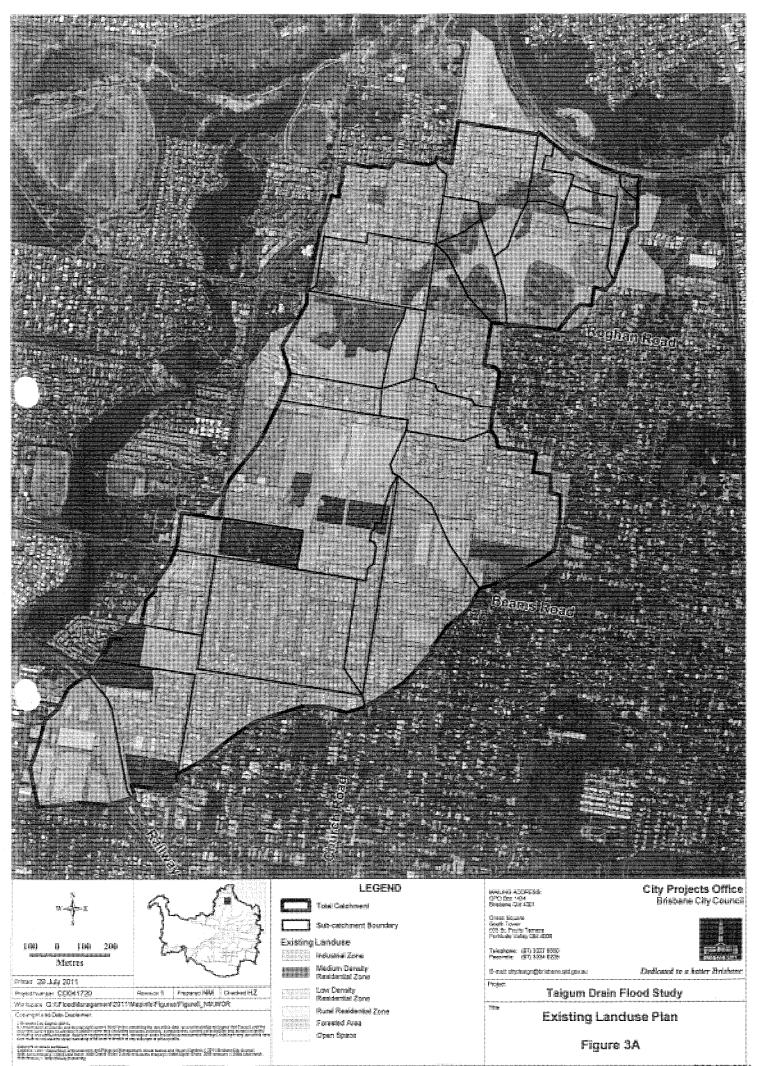


APPENDIX A: Figures

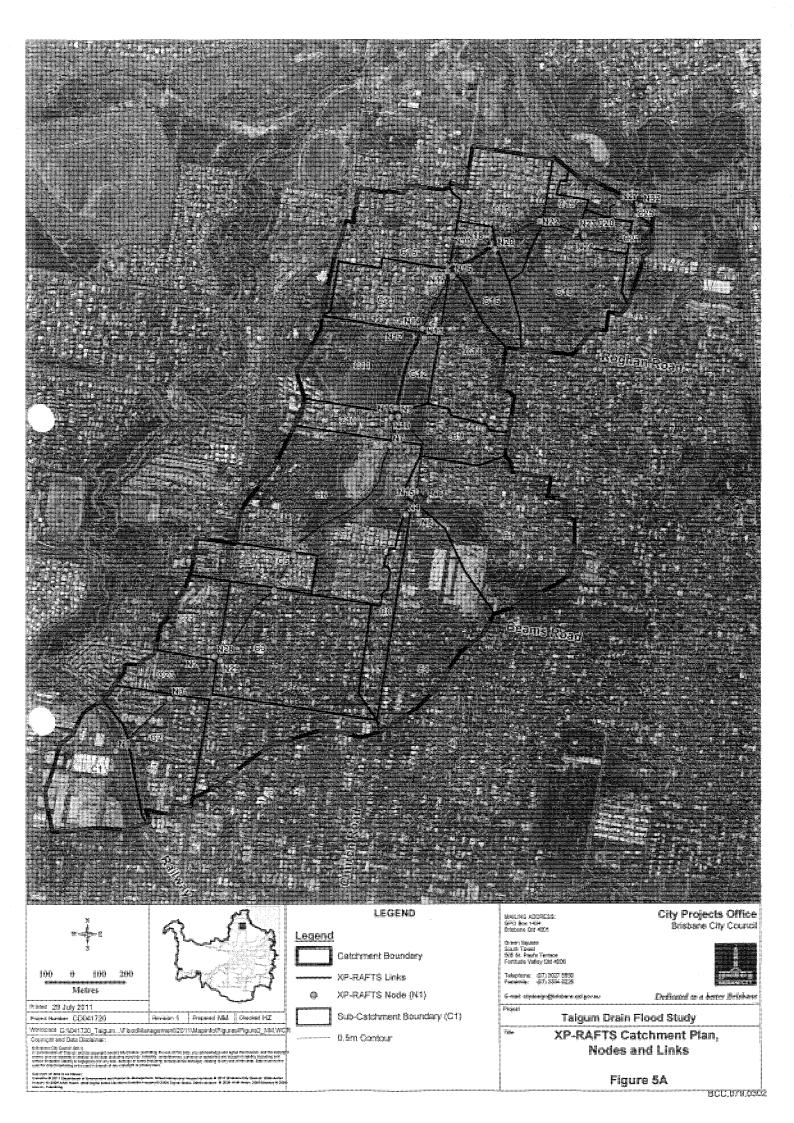


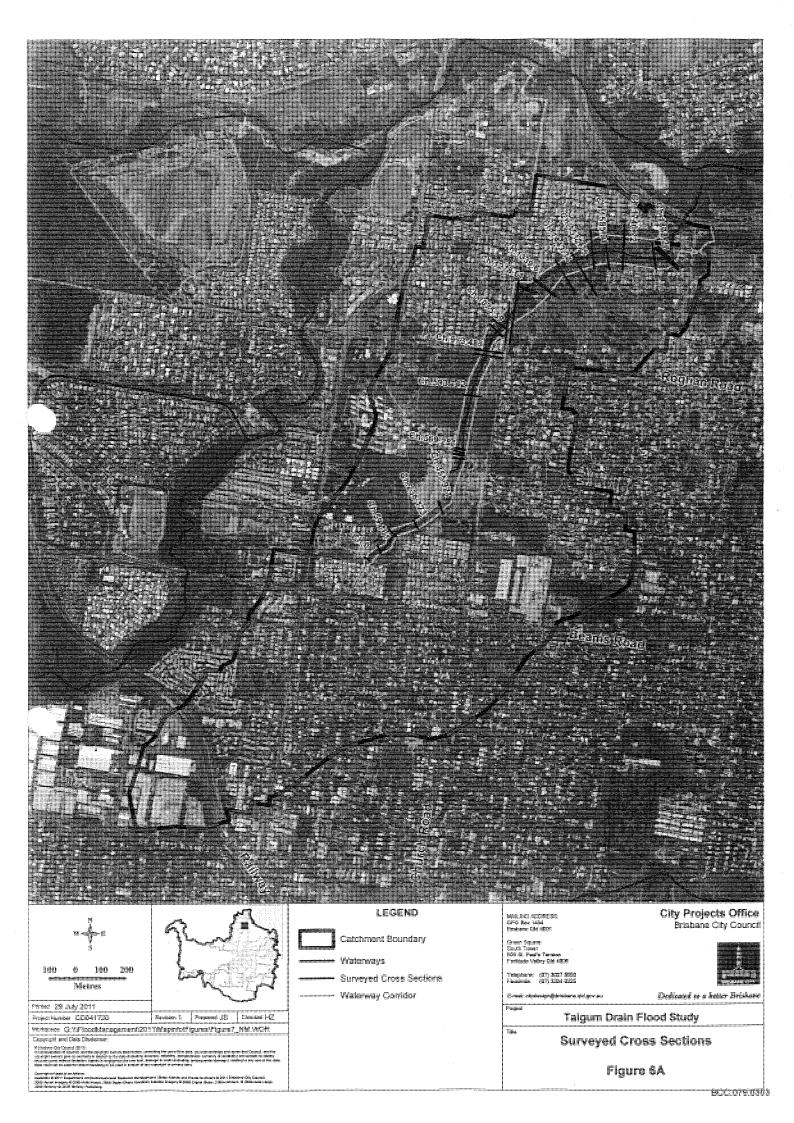




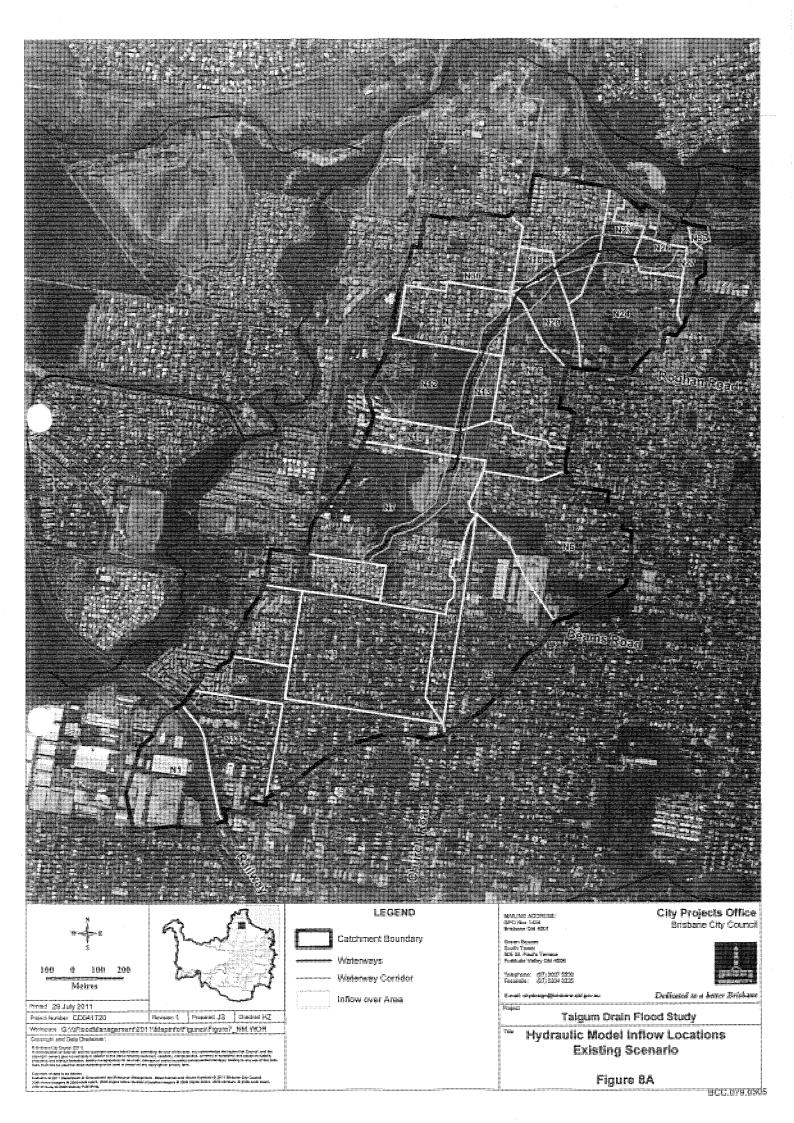


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APPENDIX B: Model Data





Table B.1: Hydraulic Structure- 2011 TUFLOW Model

Location	Approx. Chainage	Structure Description	Modelled As
Quarrion Street	562	4/(3.6Wx1.5H) RCBC	Culverts + Weir
Roghan Road	982	3/(3.6Wx1.5H) RCBC	Culverts + Weir
Church Road	1192	4/(5.7Wx1.35H) RCBC	Culverts + Weir
401A Church Road	1281	2/1.725 RCP	Culverts + Weir
401 Church Road	1342	Timber Bridge 5m span	Bridge
334 Muller Road	1930	Remaining of an old Timber Bridge 8.5m span	Bridge
334 Muller Road	1985	2/1.825 RCP+2/1.425 RCP	Culverts + Weir
350 Muller Road	N/A	1/1.725 RCP+1/1.625 RCP	Culverts
Gateway Motorway 1	N/A	2/(2.4Wx2.1H)+2/(2.4Wx1.9H)+1/(2.4Wx2.5H) RCBC	Culverts
Gateway Motorway 2	N/A	3/(1.5Wx1.5H) RCBC	Culverts

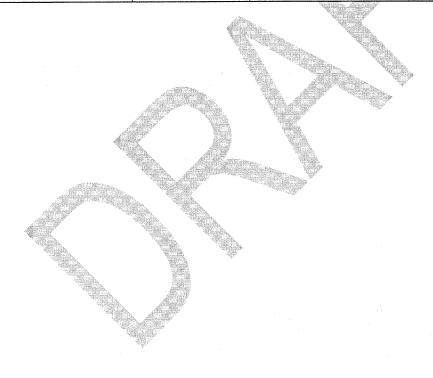




Table B.2: Existing Landuse Break up for XP-RAFTS Sub-Catchments

Ca. Name	Ca. Area (Ha)	Road (%)	Industrial (%)	Residential Low Density (%)	Open Space (%)	Forest (%)	Rural Residential (%)	Medium Density Residential (%)	Impervious Area (%)	Pervious Area (%)
c1	12.56	0.23	0.77	0.00	0.00	0.00	0.00	0.00	0.90	0.10
c2	11.98	0.19	0.00	0.51	0.00	0.00	0.00	0.30	0.63	0.37
cЗ	23.38	0.25	0.00	0.75	0.00	0.00	0.00	0.00	0.60	0.40
c4	18.50	0.19	0.39	0.31	0.07	0.00	0.04	0.00	0.69	0.31
c5	6.54	0.13	0.00	0.24	0.00	0.00	0.00	0.63	0.68	0.32
c6	29.29	0.07	0.00	0.21	0.47	0.00	0.17	0.08	0.26	0.74
с7	23.05	0.17	0.09	0.46	0.15	0.12	0.01	0.00	0.47	0.53
с8	4.89	0.34	0.00	0.58	0.02	0.00	0.00	0.06	0.64	0.36
c9	6.31	0.14	0.00	0.38	0.48	0.00	0.00	0.00	0.34	0.66
c10	3.73	0.07	0.00	0.83	0.10	0.00	0.00	0.00	0.49	0.51
11	11.75	0.04	0.00	0.28	0.68	0.00	0.00	0.00	0.21	0.79
c12	2.81	0.14	0.00	0.00	0.86	0.00	0.00	0.00	0.17	0.83
c13	9.85	0.26	0.00	0.60	0.00	0.14	0.00	0.00	0.54	0.46
c14	11.06	0.19	0.00	0.57	0.04	0,20	0.00	0.00	0.46	0.54
c15	11.81	0.30	0.00	0.63	0.01	0.06	0.00	0.00	0.59	0.41
c16	5.04	0.01	0.00	0.00	0.30	0.65	0.04	0.00	0.03	0.97
c17	10.87	0.17	0.00	0.57	0.15	0.11	0.00	0.00	0.44	0.56
c18	14.74	0.05	0.00	0.11	0.39	0.23	0.21	0.00	0.14	0.86
c19	2.37	0.08	0.00	0.29	0.63	0.00	0.00	0.00	0.25	0.75
c20	2.32	0.04	0.00	0.12	0.84	0.00	0.00	0.00	0.14	0.86
c21	4.51	0.26	0.00	0.19	0.39	0.17	0.00	0.00	0.34	0.66
c22	5.93	0.26	0.00	0.73	0.00	0.01	0.00	0.00	0.60	0.40
c23	15.15	0.22	0.00	0.49	0.00	0.19	0.00	0.09	0.51	0.49
c24	1.90	0.20	0.00	0.53	0.00	0.27	0.00	0.00	0.44	0.56
c25	0.48	0.44	0.00	0.00	0.00	0.56	0.00	0.00	0.39	0.61

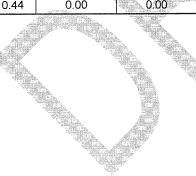




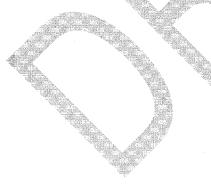
Table B.3: Hydrologic Model Sub-Catchment Properties – Existing Catchment Development

Catchment Name	Inflow Node	Catchment Slope (%)	Existing Catchment Pervious Area (ha)	Existing Catchment Impervious Area (ha)	Pervious PERN	Impervious PERN
C1	N1	2.83	1.26	11.30	0.04	0.015
C2	N31	2.87	4.40	7.58	0.04	0.015
C3	N3	2.07	9.39	13.99	0.04	0.015
C4	N5	2.04	5.79	12.72	0.04	0.015
C5	N8	3.23	2.10	4.44	0.04	0.015
C6	N7	4.04	21.58	7.71	0.04	0.015
C7	N6	3.44	12.19	10.85	0.04	0.015
C8	N4	2.30	1.78		0.04	0.015
C9	N9	3.65	4.17	2.14	0.04	0.015
C10	N10	3.73	1.92	1.81	0.04	0.015
C11	N12	3.81	9.28	2.47	0.04	0.015
C12	N13	0.18	2.34	0.47	0.04	0.015
C13	N17	2.46	4.57	5.27	0.04	0.015
C14	N16	2.46	5.97	5.09	0.04	0.015
C15	N30	1.79	4.90	6.91	0.04	0.015
C16	N20	4.27	4.88	0.16	0.04	0.015
C17	N22	1.79	6. 05	4.82	0.04	0.015
C18	N24	3.05	12.62	2.12	0.04	0.015
C19	N23	0.89	1.78	0.59	0.04	0.015
C20	N26	1.12	1.99	0.32	0.04	0.015
C21	N27	2.10	2.97	1.55	0.04	0.015
C22	N28	2.62	2.36	3.57	0.04	0.015
C23	N2	2.60	7.43	7.72	0.04	0.015
C24	N18	2.31	1.06	0.85	0.04	0.015
C25	N32	5.00	0.29	0.19	0.04	0.015



Table B.4: XP-RAFTS Rainfall Assignment and Rainfall Totals- Calibration Events

Catchment Name	Inflow Node	Rainfall Gauge	Total Rainfall Oct 10 (mm)	Total Rainfall May 09 (mm)
C1	N1	LCR566	229	214
C2	N31	CR560	227	233
C3	N3	CR560	227	233
C4	N5	CR560	227	233
C5	N8	CR560	227	233
C6	N7	CR560	227	233
C7	N6	CR560	227	233
C8	N4	CR560	227	233
C9	N9	CR560	227	233
C10	N10	CR560	227	233
C11	N12	CR560	227	233
C12	N13	CR560	227	233
C13	N17	CR560	227	233
C14	N16	CR560	227	233
C15	N30	CR560	227	233
C16	N20	CR560	227	233
C17	N22	CR560	227	233
C18	N24	CR560	227	233
C19	N23	CR560	227	233
C20	N26	CR560	227	233
C21	N27	CR560	227	233
C22	N28	CR560	227	233 .
C23	N2	CR560	227	233
C24	N18	CR560	227	233
C25	N32	CR560	227	233





Taigum Drain Flood Study Report B - Design Event Modelling

July 2011

Prepared by
Built and Natural Environment
City Project Office

Prepared for Water Resources City Planning and Sustainability



Taigum Drain Flood Study Report B - Design Event Modelling

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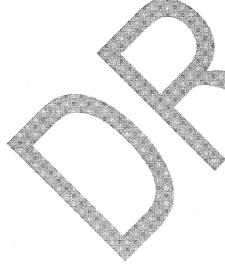


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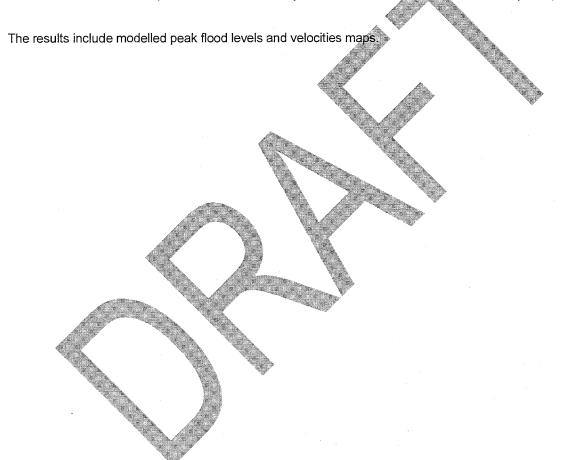


1 Introduction

Following on from Report A – Model Calibration, Report B provides the results of the design event model simulations obtained using the XP-RAFTS hydrologic model and the calibrated TUFLOW hydraulic model. The 100, 50, 20, 10, 5 and 2 year ARI (average recurrence interval) events were modelled.

Using the calibrated TUFLOW model, the following scenarios were investigated as part of the design event modelling:

- Existing Scenario (Existing conditions with ultimate catchment development),
- Ultimate Scenario (model includes waterway corridor and ultimate catchment development).





2 Model Data

2.1 Design Rainfall

Design event modelling was carried out using the Australian Rainfall and Runoff temporal pattern. The 2, 5, 10, 20, 50 and 100 year Average Recurrence Interval (ARI) flood events were modelled. Storm Durations from 30 minutes to 6 hours were initially modelled. However, the peak flood levels and discharges within the study area were produced by storms of 60 minutes duration.

2.2 Tailwater Conditions

During events in Cabbage Tree Creek, the area downstream of Taigum Drain acts as a backwater flood storage area. Consequently, the water level in this section of channel will be essentially equal to the peak flood level in Cabbage Tree Creek at the mouth of Taigum Drain.

Due to the relatively small catchment area of Taigum Drain compared to Cabbage Tree Creek and its location in reference to the entire Cabbage Tree Creek catchment, the following coincident catchment flow conditions and tailwater levels were adopted in Taigum Drain.

A fixed tailwater level from existing Cabbage Tree Creek Flood Study was adopted for this study. The combination of adopted catchment flow conditions and tailwater levels for different ARI's are shown in *Table 2.1*.

Table 2.1 Catchment Flow vs. Tailwater Conditions in Taigum Drain

1788		
	Catchment Flow	Tailwater Condition
	2 Year ARI	2 Year ARI
	5 Year ARI	2 Year ARI
	10 Year ARI	2 Year ARI
	20 Year ARI	5 Year ARI
	50 Year ARI	10 Year ARI
	100 Year ARI	20 Year ARI

2.3 Topographic and Structure Data

As described in the Model Calibration Report, survey of the creeks and hydraulic structures for this study was undertaken by J.A. Liddle Surveys Pty Ltd in 2011. The cross sections were extended in a few instances to the full extent of the 1d channel using 2009 Airborne Laser Scanning (ALS) survey data. The Hydraulic Structure Reference Sheet (HSRS) are presented in *Appendix C*.

2.4 Land Use

The calibrated RAFTS model was altered to reflect the ultimate catchment development situation as detailed in the Brisbane City Plan (2000).



3 Design Event Modelling

Design event modelling was undertaken using the XP-RAFTS and calibrated TUFLOW models.

TUFLOW model uses the inflow hydrographs from XP-RAFTS model for all design events at various locations throughout the catchment.





4 Hydrological Modelling

4.1 Model Setup

Design events for 2, 5, 10, 20, 50, and 100 year ARI were modelled in RAFTS to develop hydrographs for the ultimate catchment scenario for input into the hydraulic model.

As discussed in **Section 2**, to consider future development, the impervious areas associated with certain subcatchments were modified to represent changes in land use under ultimate catchment development. These were the only modifications made to the calibrated hydrologic model.

Land-use properties (impervious and pervious areas) for each sub-catchment were recalculated based on future development and are contained in *Table B.1* in *Appendix B*.

The ultimate landuse plan for Taigum Drain Catchment is shown in *Figure 1B* and the break-up of existing land use types is shown in *Figure 2B*.

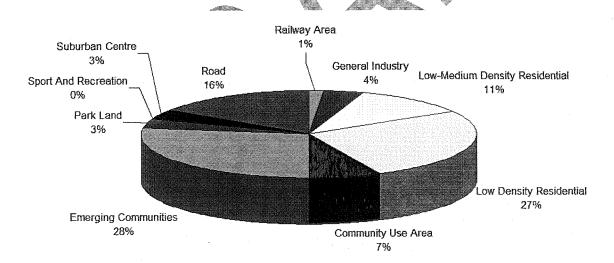


Figure 2B: Ultimate Landuse within the Taigum Drain Catchment



Table 4.1 shows the fraction impervious values adopted.

Table 4.1 Adopted Fraction Impervious Values for Taigum Drain- Ultimate Scenario

Development Type	Fraction Impervious
Community Use Area (Railway)	0.80
Community Use Area (Health, Education, Utility Services, Community Facilities)	0.60
General Industry	0.20
Low-Medium Density Residential	0.65
Low Density Residential	0.50
Emerging Community	0.65
Park Land	0.05
Sport and Recreation	0.40
Multi Purpose Centre	0.90
Road	0.90

Note: The above table is an amalgam of the Brisbane City Council Department of Works Supplement to QUDM (Brisbane City Council 1994, p.QUDM-BCC-2) and the Queensland Urban Drainage Manual (QUDM) (Neville Jones & Associates and Australian Water Engineering, 1993, Tables 5.04.1 and 5.04.2).

The fraction impervious of sub-catchments was determined in accordance with the Brisbane City Council Department of Works Supplement to QUDM (Brisbane City Council 1994, p.QUDM-BCC-2) and the Queensland Urban Drainage Manual (QUDM) (Neville Jones & Associates and Australian Water Engineering 1993, Tables 5.04.2 and 5.04.1).

JULY 2011



Table 4.2 broadly identifies the land use classification within Taigum Drain Catchment for the ultimate developed condition.

Table 4.2 Areas of land use – Existing development scenario

Land Use Type	Total Area (ha)	% of Total Area
Community Use Area (Railway)	3.5	1.4
Community Use Area (Health, Education, Utility Services, Community Facilities)	17.3	6.9
General Industry	9.7	3.9
Low-Medium Density Residential	27.3	10.9
Low Density Residential	67.6	27.0
Emerging Community	68.9	27.5
Park Land	8.4	3.3
Sport and Recreation	0.9	0.3
Multi Purpose Centre	8.3	3.3
Road	38.9	15.5

An average impervious value of 64% was obtained for the ultimate catchment.

The sub-catchment properties for ultimate condition are summarised in Table B.2 in Appendix B.

4.2 Model Verification

The RAFTS model was verified against the calculated Rational Methods flows. Due to the lack of historical stream flow data within the catchment the Rational Method was used to verify the RAFTS model. The Rational Method was used to calculate peak flows at an appropriate location for the 100 year ARI storm event.

The checking points locations are shown in *Figure 3B*. *Errorl Reference source not found..3* below shows the comparison between the estimated design discharge from the RAFTS model and the Rational Method for the 100 year ARI events. Time of concentration was estimated using the standard inlet time and the average catchment velocity extracted from the TUFLOW model.

As shown in *Error! Reference source not found..3*, the estimated design discharge from RAFTS compared to the Rational Method is within a 20% range and is considered acceptable considering the limitations of the Rational Method.

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Table 4.3 Comparison between XP-RAFTS and Rational Method Results

Checking Locations	Estimated Time of Concentration (min)	XP-RAFTS Nodes	XP-RAFTS Flows (m ³ /s)	Rational Method Flows (m³/s)	Difference (%)
1	27	N7	46.12	45.83	0.6
2	31	N14	81.98	71.76	12.5
2	33	N17	81.58	73.58	9.8
4	46	N27	97.16	79.32	18.4





5 Hydraulic Modelling

5.1 Model Setup

The calibrated Taigum Drain 2011 TUFLOW model as described in Report A - Model Calibration was updated to represent the ultimate conditions in the Taigum Drain Catchment.

Based on aerial photos no waterway crossings and creek mitigation works constructed after May 2011 event and as such structural data and catchment topography remains the same. The following changes were made to hydraulic calibration models to represent design model scenarios:

- Including the waterway corridor for Ultimate Scenario only
- Adopting a tailwater boundary relevant to each design events as discussed in Section 2.
- Adopting new inflow hydrographs from XP-RAFTS design events models.

XP-RAFTS design event flows were applied to the TUFLOW model. A total of 25 inflows for Taigum Drain Existing Scenario and 17 inflows for Taigum Drain Ultimate Scenario were defined to reflect the hydrologic behaviour of the channel and minimise localised increases in flow due to concentrated local inflows. All inflow points are identical to those in the calibration model for Existing Scenario however inflow locations have changed in the Ultimate Scenario due to different model set up. All inflow catchments and points in hydraulic model have the identical names to the nodes in hydrologic model. The inflow locations for the Ultimate Scenario are shown in *Figure 4B*.

The design scenarios were considered for the 2, 5, 10, 20, 50, and 100 year ARI design events.

5.2 Modelling Scenarios

5.2.1 Existing Scenario

The Existing Scenario represents the current catchment topography while the catchment is fully developed as outlined in City Plan (2000). As discussed above, the inflow hydrographs and tailwater level were altered in calibration model to represent the existing model scenario. The peak flood levels resulted from this scenario are used to produce the flood maps for the existing condition and can not be used for the planning purposes.

5.2.2 Ultimate Scenario

The ultimate scenario introduces the waterway corridor in the existing TUFLOW model scenario as vertical walls to only allowing for flow within the waterway corridors.

The Waterway Corridors (WC) serve as development control lines. They are determined based on creek hydraulics, creeks ecology and environmental planning issues. The WC's are used as planning line boundaries in which filling and/or development is restricted, with the objective of limiting the impacts associated with flooding. Taigum Waterway Investigation, June 2004 introduced a waterway corridor extent for Taigum Drain which was



adopted for this study. It was also advised in the same study that the vegetation densities in waterway corridor should be maintained at current levels and as such no vegetation growth or riparian corridor was modelled as part of this flood study. The calibration model was altered to include the waterway corridor, new inflow hydrographs and tailwater level. The peak flood levels resulted from this model scenario will determine flood levels across the Taigum Drain Catchment.





6 Final Model Results

6.1 Flood Levels and Discharges

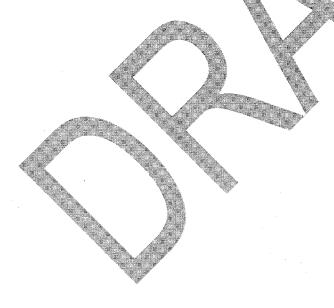
Anticipated flood levels were calculated for the 2, 5, 10, 20, 50 and 100 year ARI events assuming the presence of:

- future development as outlined in City Plan (2000);
- waterway corridors (as described in Section 5.2.2);
- tailwater level as discussed in Section 2.

Appendix C of this report contains structure dimensions and associated flow results for the ultimate TUFLOW model design run scenarios in Hydraulic Structure Reference Sheets. In addition the peak flood levels for the Ultimate Scenario are detailed for all ARI at MHG locations and all structures and are represented in *Table B.3*.

6.2 Flood Mapping

The area of inundation, flood depth and velocity for the full range of ARI from 2 year event through to the 100 year event are shown on *Figure 5B* to *Figure 40B* in *Appendix A*.





7 References

BCC 2000, Brisbane City Plan 2000, BCC, Brisbane

BCC in draft, Taigum Waterway Investigation, prepared by Brisbane City Council, June 2004

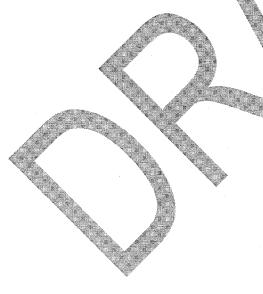
BCC, Stormwater Investigation Report 246, 252 and 258 Church Road Taigum, Prepared by MRG Water Consulting Pty Ltd for BCC, May 2007

BCC, Master Drainage Plan for the Carseldine and Taigum Catchments, Prépared by WBM Oceanics Australia for BCC, June 1997

BCC, Cabbage Tree Creek Flood Study Upgrade Report, prepared by Brisbane City Council, 1996 (updated 2000- refer addendum).

TUFLOW, TUFLOW Manual 2010-10-AA, TUFLOW, 2010, Australia

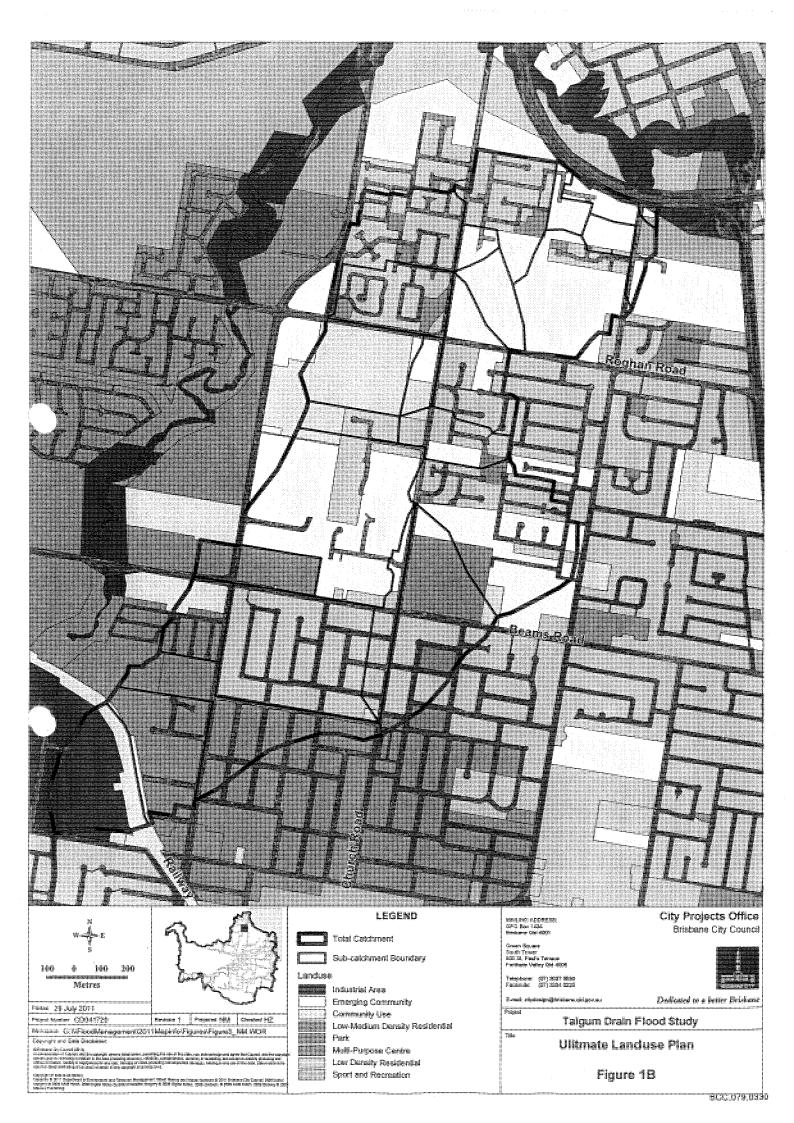
IEAust (Institution of Engineers Australia), Australian Rainfall and Runoff, Volume 1 – A Guide to Flood Estimation, IEAust, 1987, Canberra, ACT



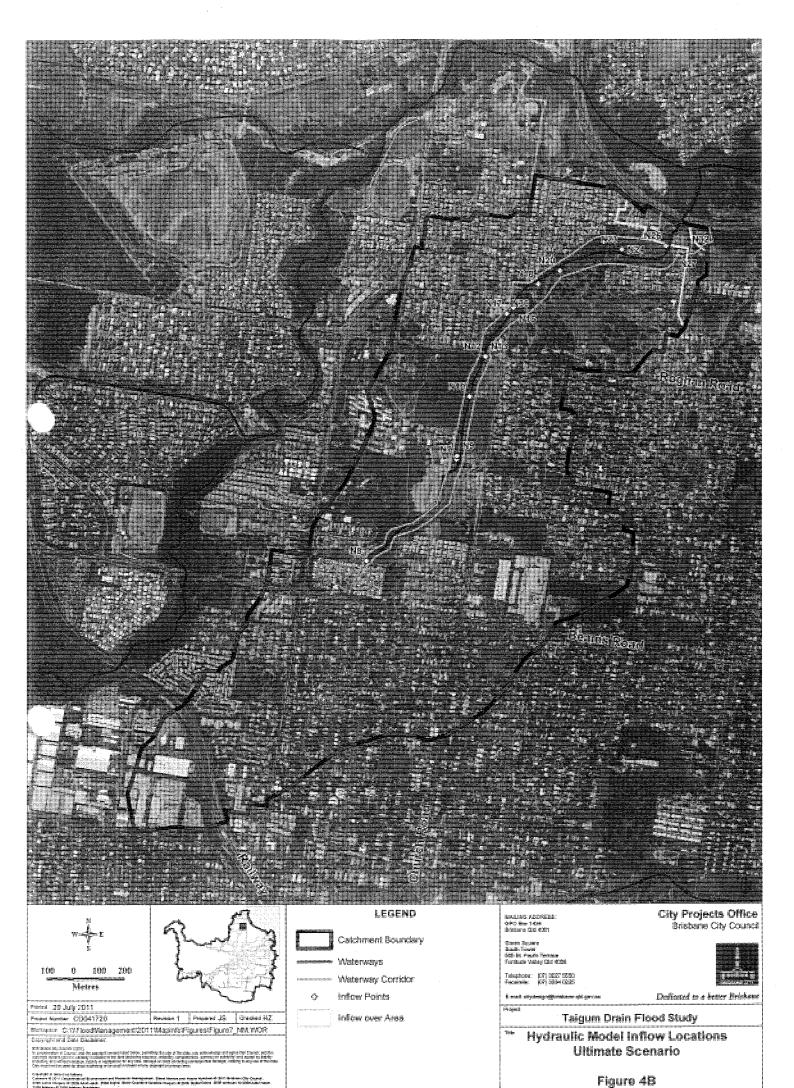


APPENDIX A: Figures

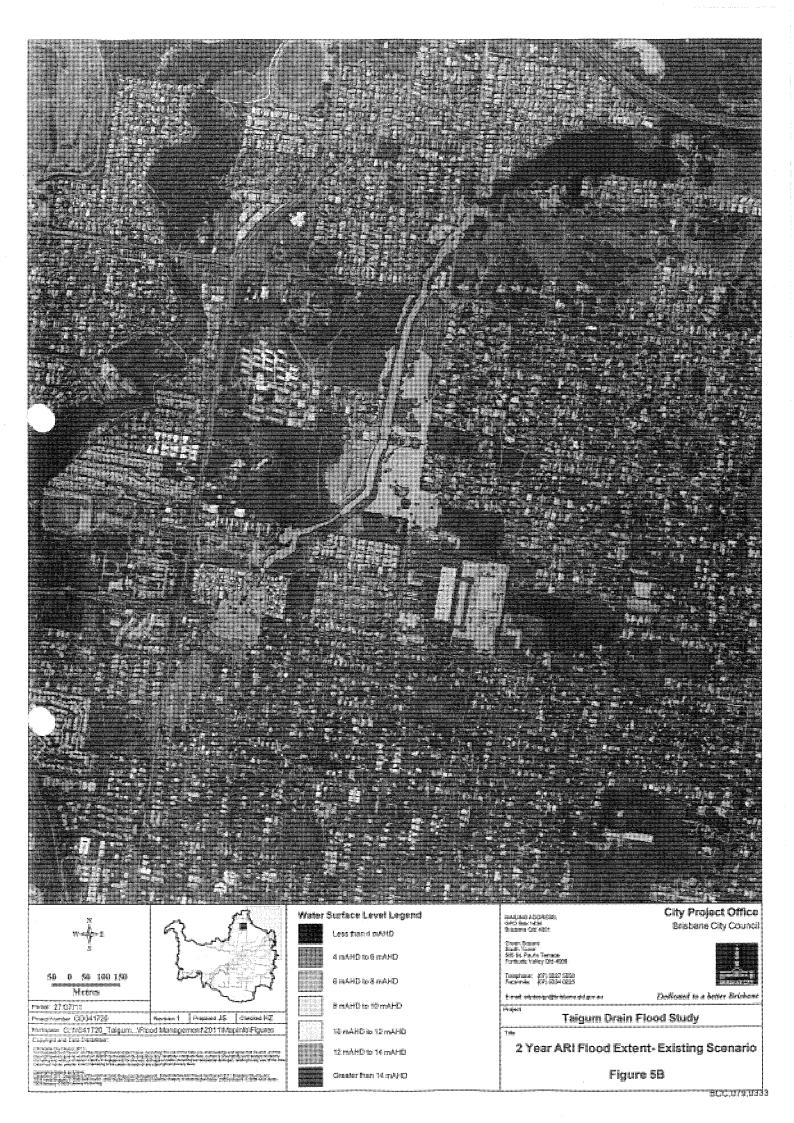




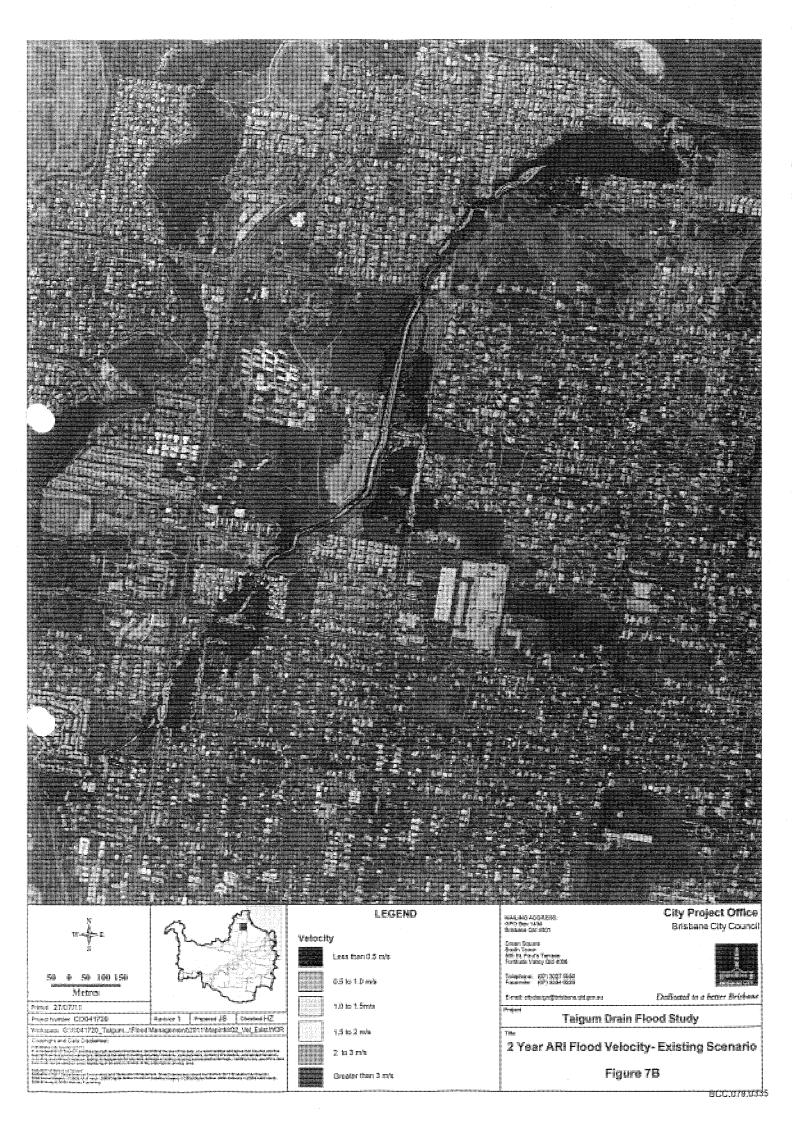




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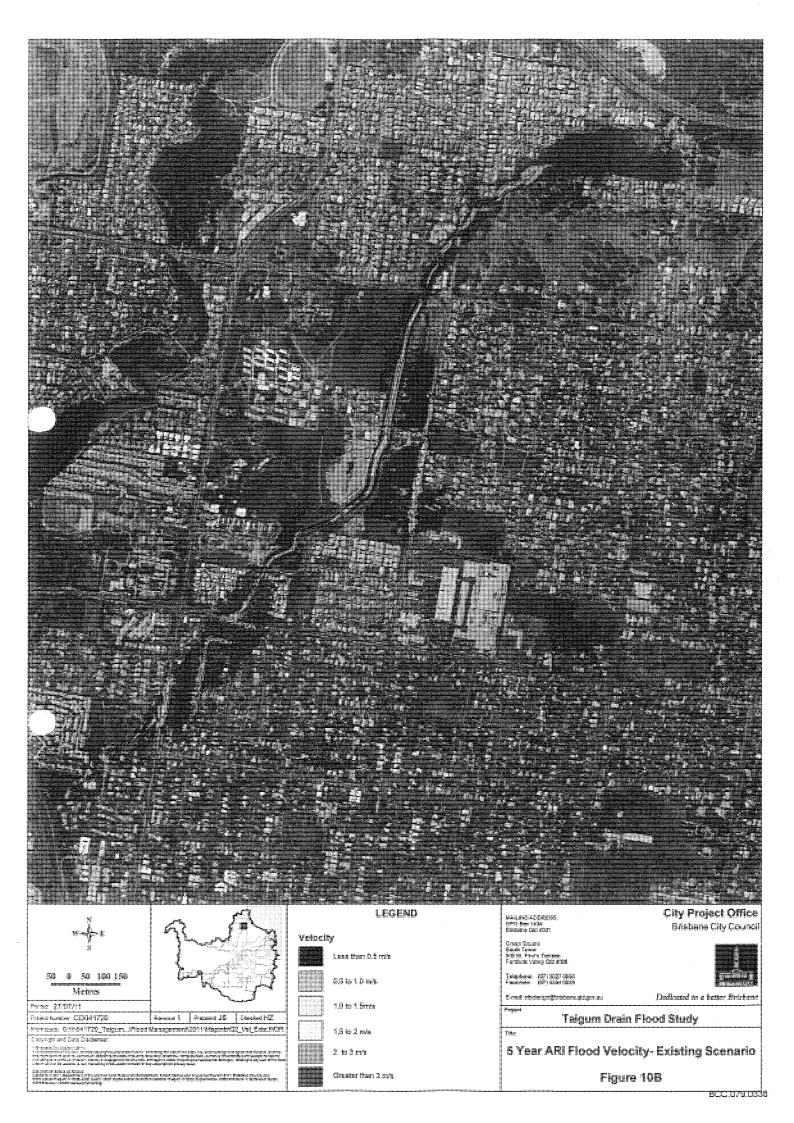






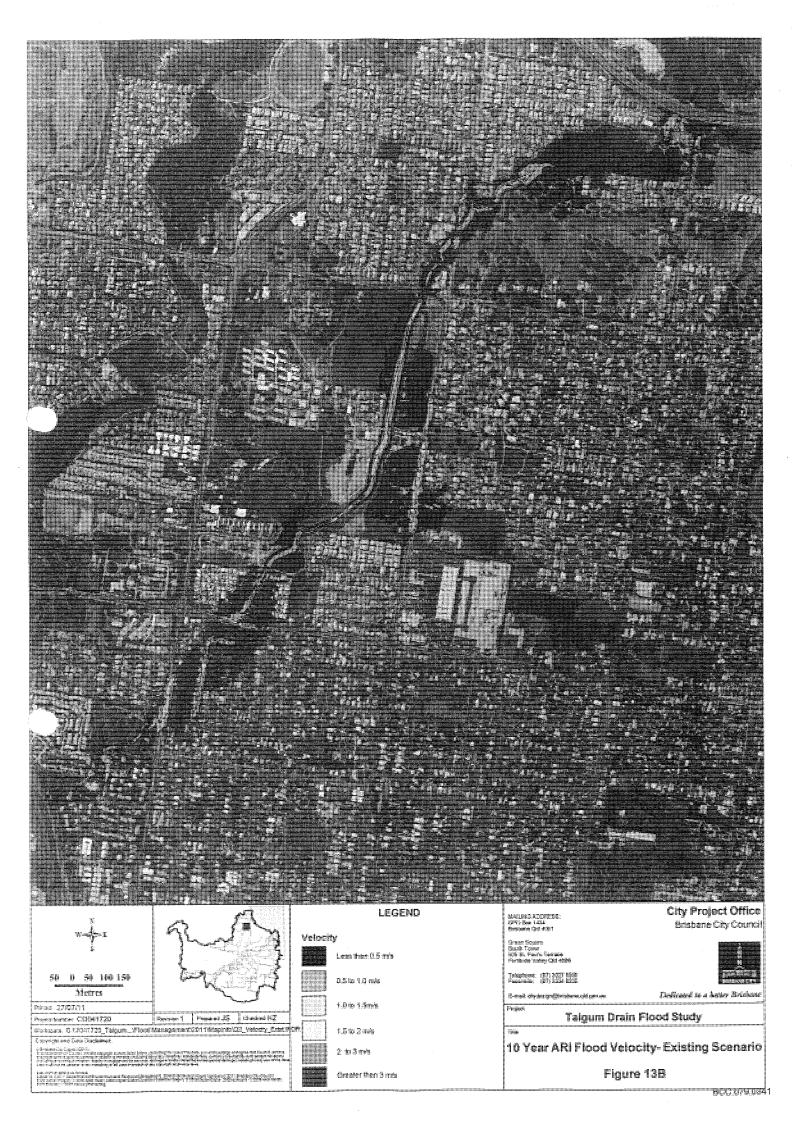






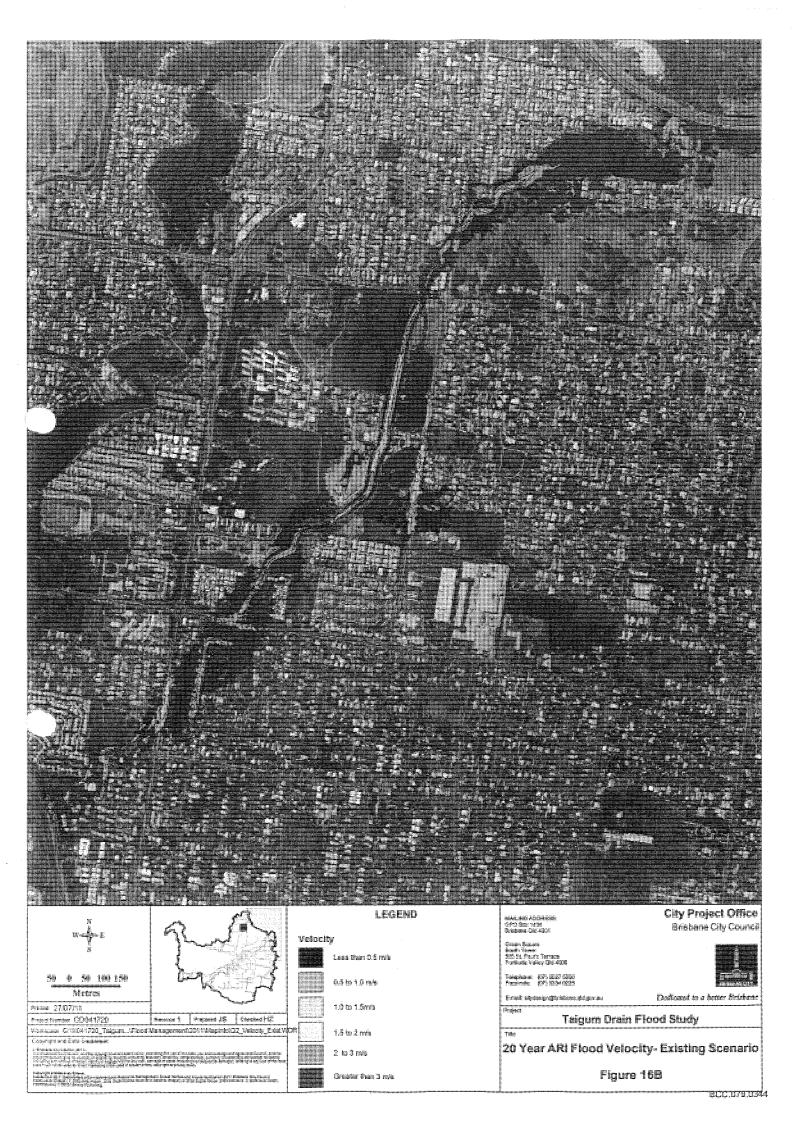


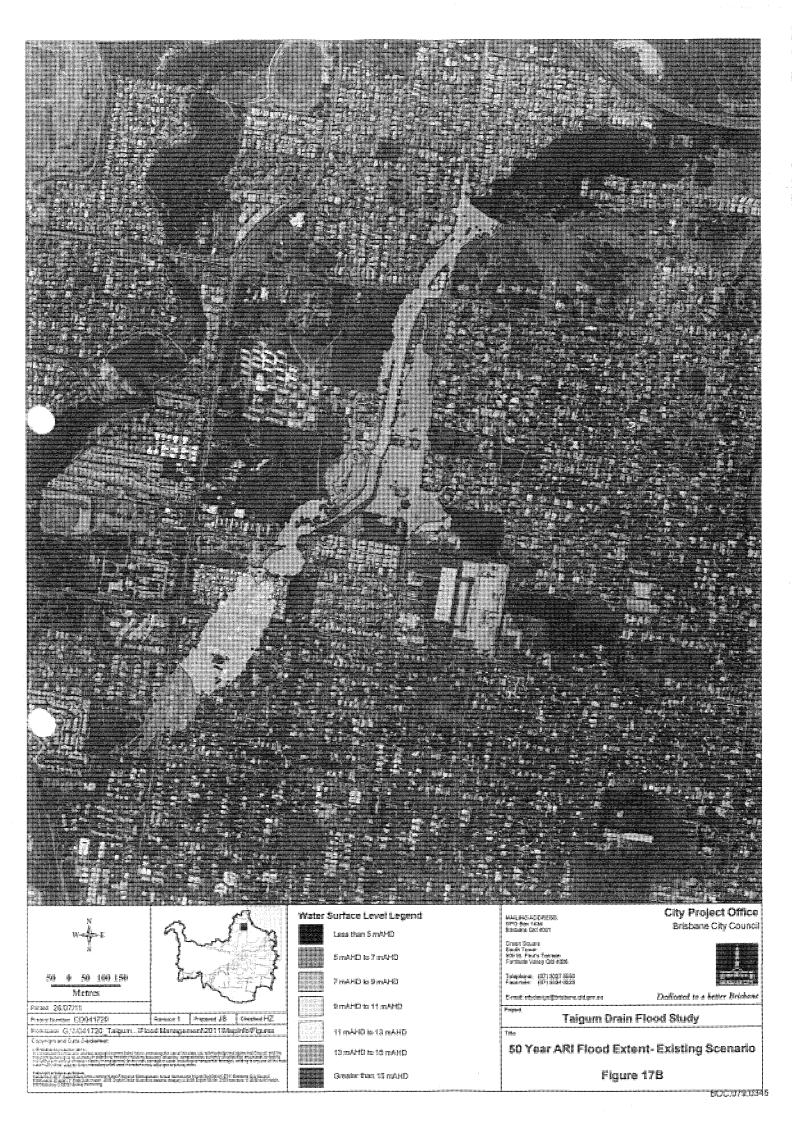


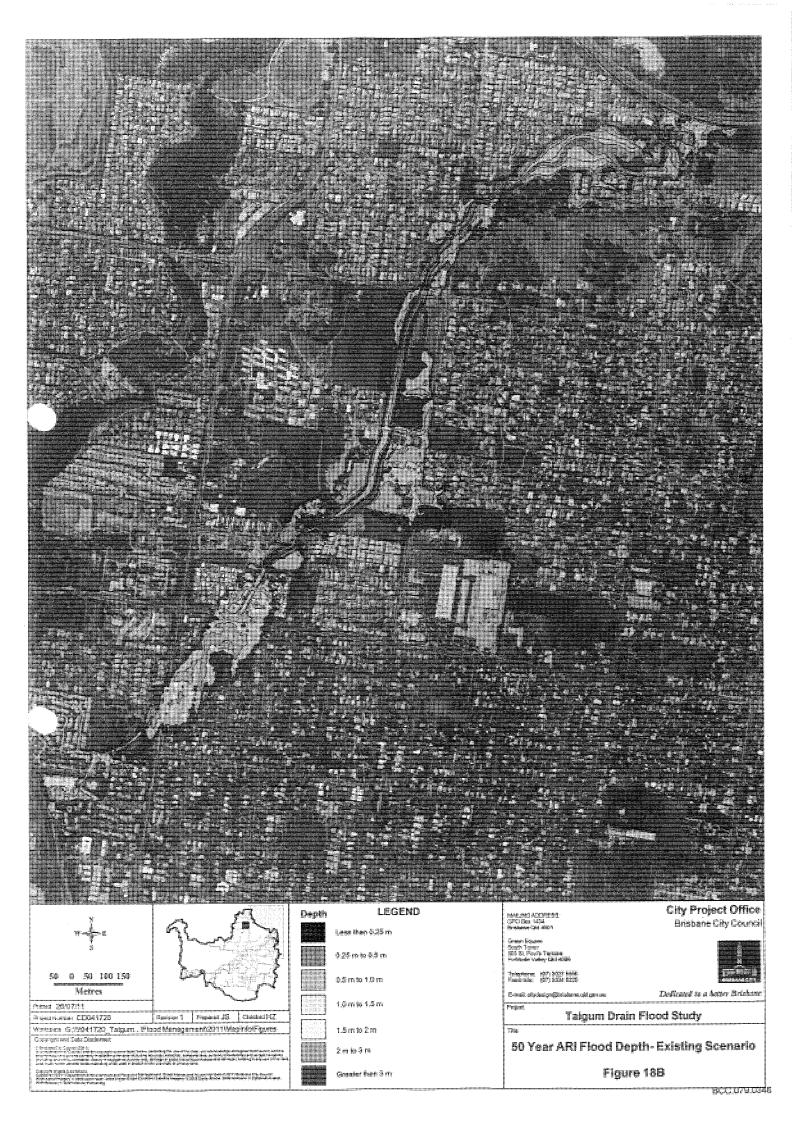


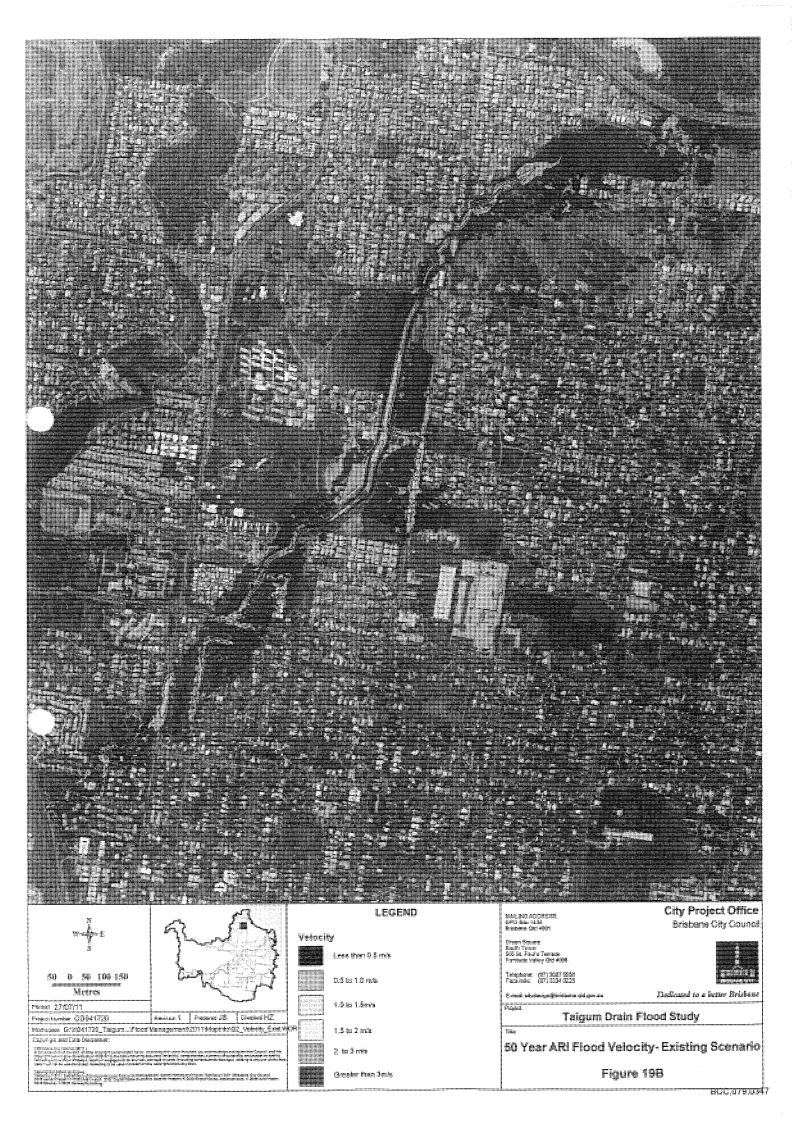






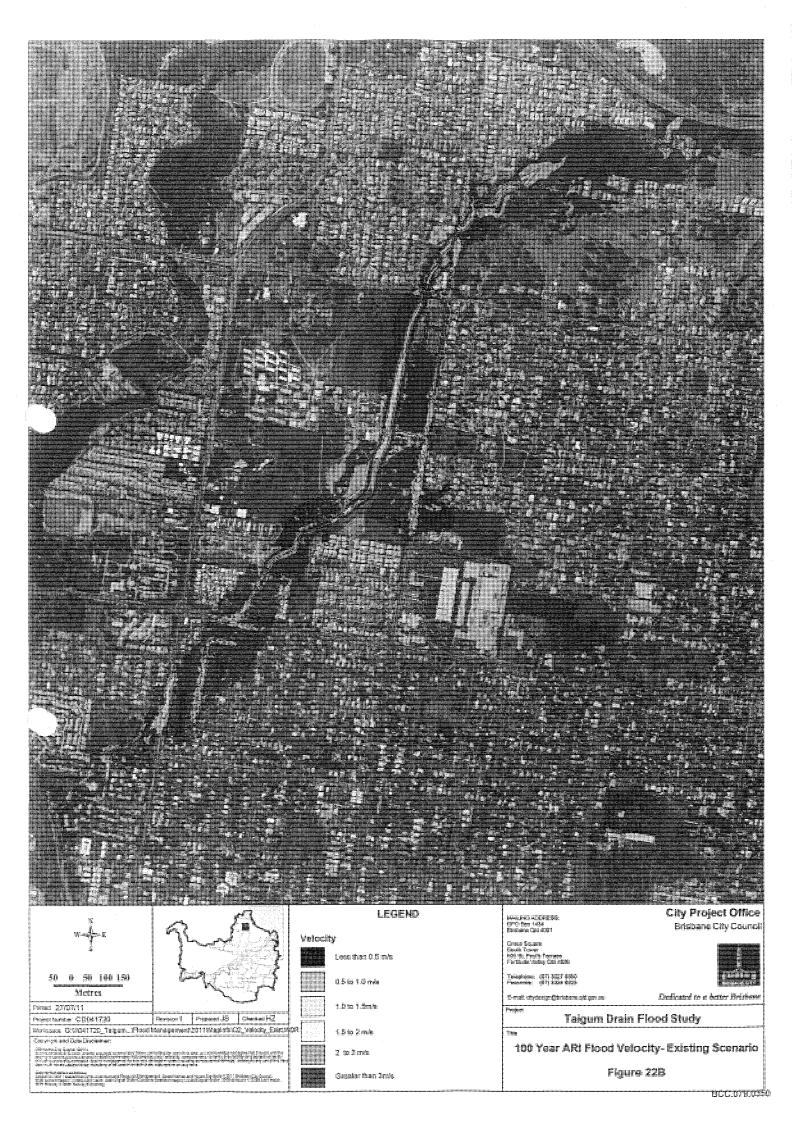
















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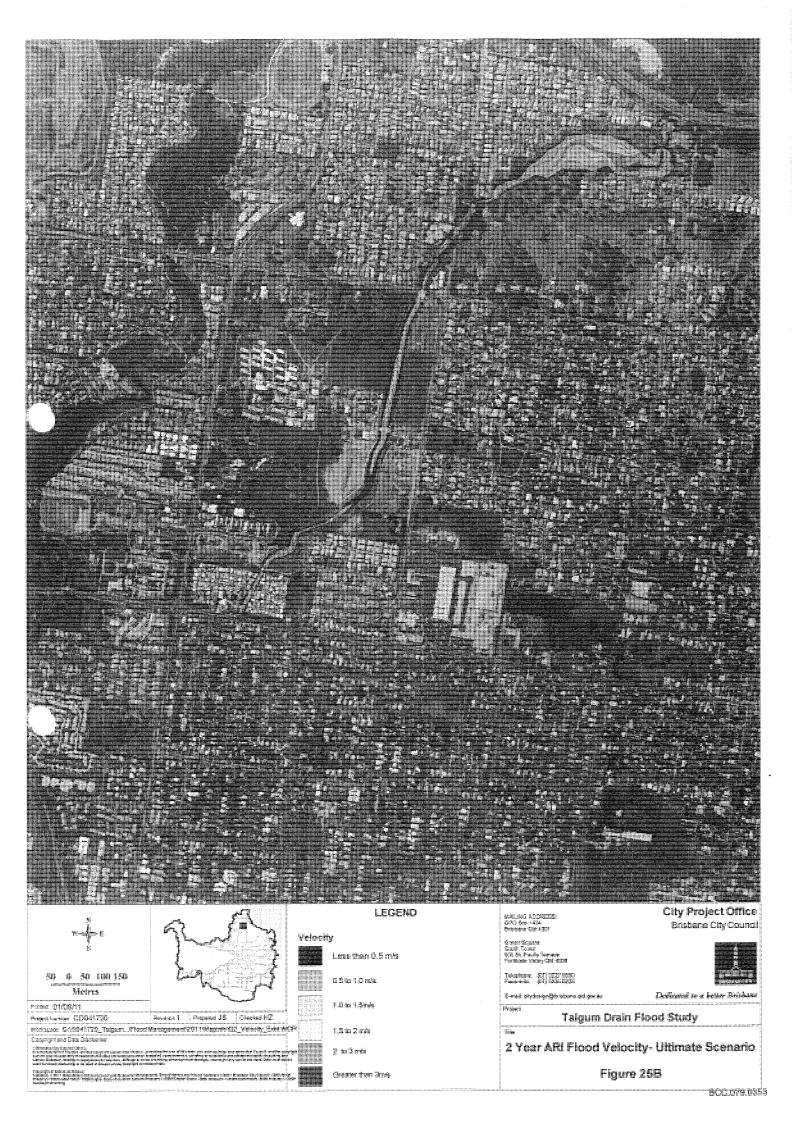
Taigum Drain Flood Study

2 Year ARI Flood Extent- Ultimate Scenario

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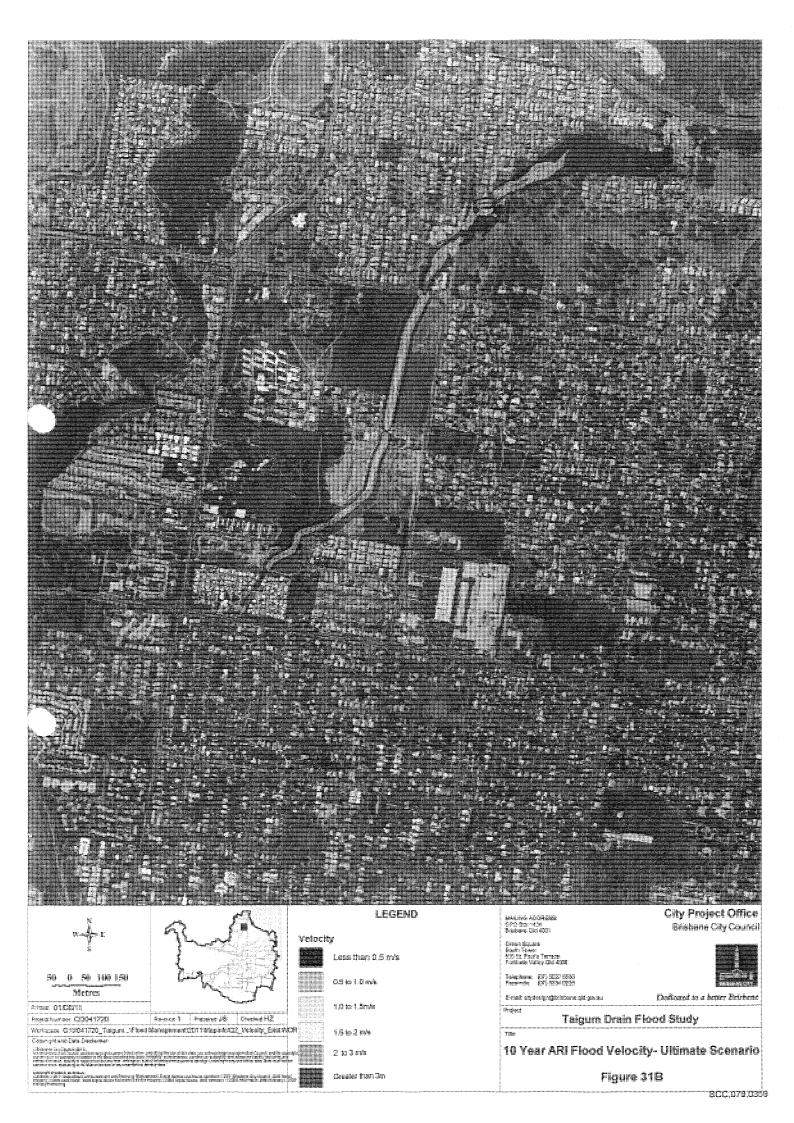
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Taigum Drain Flood Study

10 Year ARI Flood Depth- Ultimate Scenario

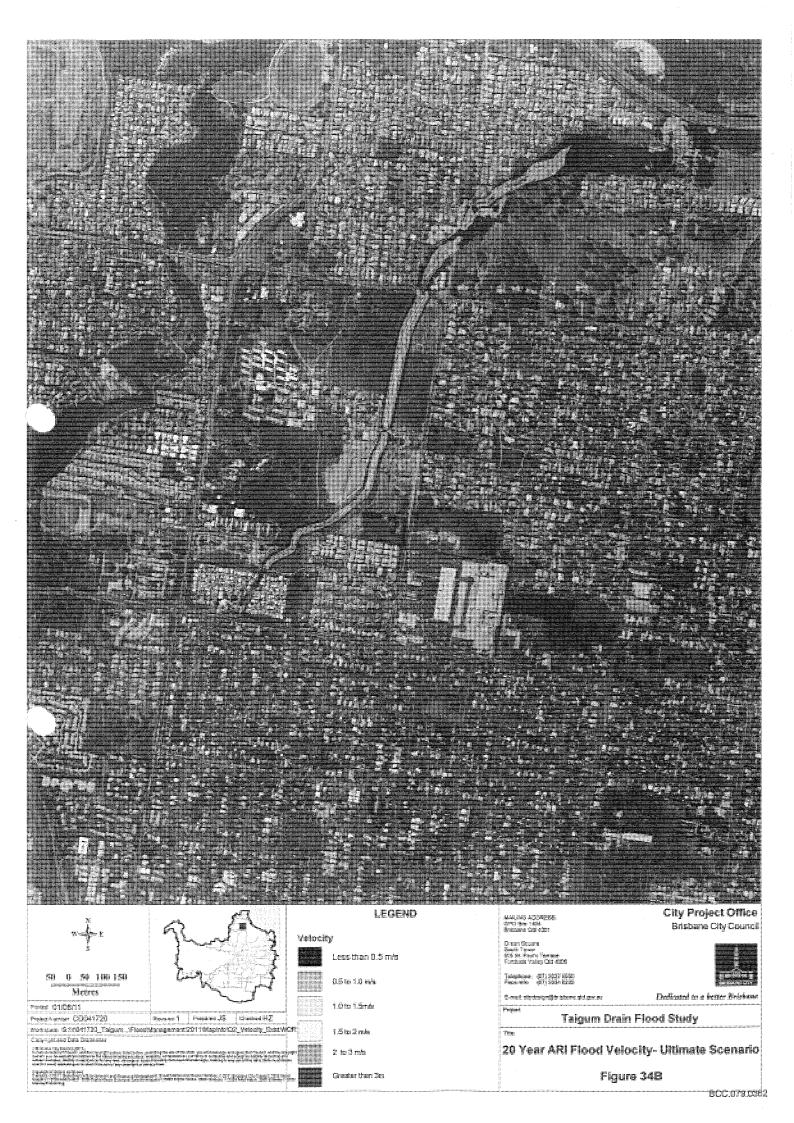
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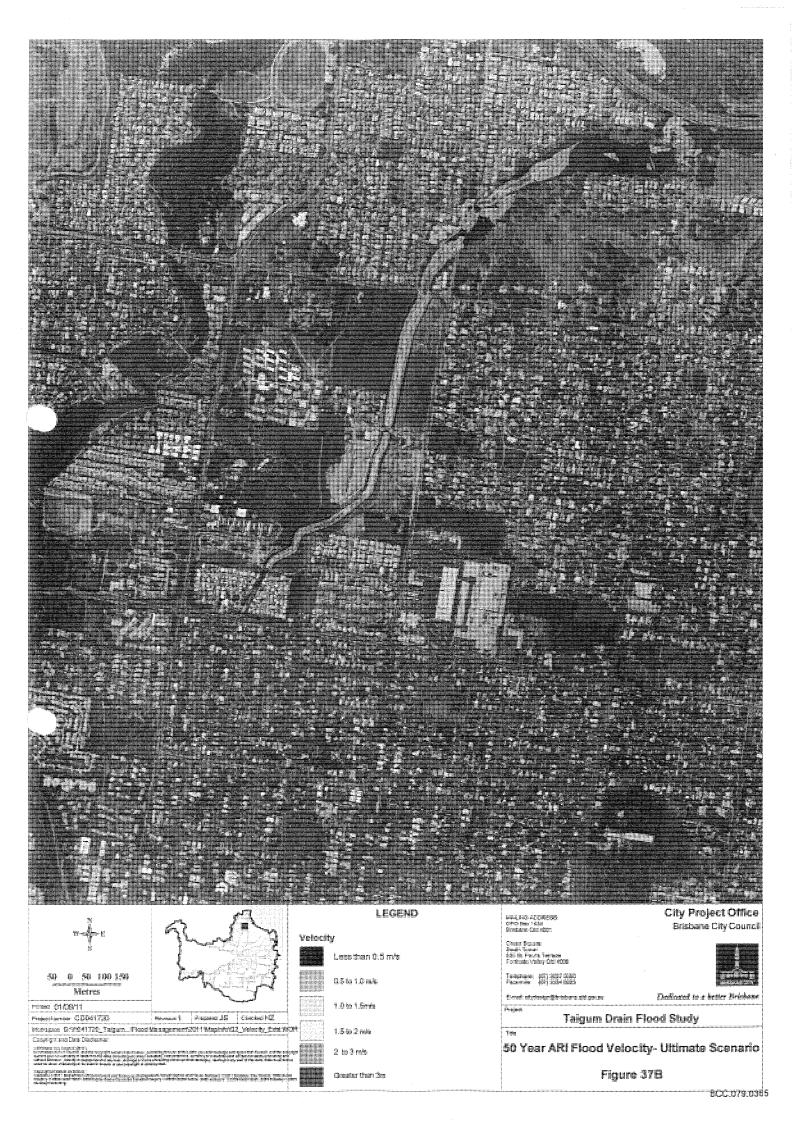






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Taigum Drain Flood Study

100 Year ARI Flood Extent-Ultimate Scenario

Figure 388



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APPENDIX B: Model Data and Results





Table B.1: Existing Landuse Break up for XP-RAFTS Sub-Catchments

Catchment Name	Catchment Area (Ha)	Road (%)	Industrial (%)	Residential Low Density (%)	Open Space (%)	Forest (%)	Rural Residential (%)	Medium Density Residential (%)	Percentage Impervious Area	Percentage Pervious Area	Pervious Area (Ha)	Impervious Area (Ha)
c1	12.56	0.23	0.77	0.00	0.00	0.00	0.00	0.00	0.90	0.10	1.26	11.30
c2	11.98	0.19	0.00	0.51	0.00	0.00	0.00	0.30	0.63	0.37	4.40	7.58
c3	23.38	0.25	0.00	0.75	0.00	0.00	0.00	0.00	0.60	0.40	9.39	13.99
c4	18.50	0.19	0.39	0.31	0.07	0.00	0.04	0.00	0.69	0.31	5.79	12.72
c5	6.54	0.13	0.00	0.24	0.00	0.00	0.00	0.63	0.68	0.32	2.10	4.44
c6	29.29	0.07	0.00	0.21	0.47	0.00	0.17	0.08	0.26	0.74	21.58	7.71
с7	23.05	0.17	0.09	0.46	0.15	0.12	0.01	0.00	0.47	0.53	12.19	10.85
с8	4.89	0.34	0.00	0.58	0.02	0.00	0.00	0.06	0.64	0.36	1.78	3.11
c9	6.31	0.14	0.00	0.38	0.48	0.00	0.00	0.00	0.34	0.66	4.17	2.14
c10	3.73	0.07	0.00	0.83	0.10	0.00	0.00	0.00	0.49	0.51	1.92	1.81
c11	11.75	0.04	0.00	0.28	0.68	∖ 0.00 △	0.00	0.00	0.21	0.79	9.28	2.47
c12	2.81	0.14	0.00	0.00	0.86	0.00	0.00	0.00	0.17	0.83	2.34	0.47
c13	9.85	0.26	0.00	0.60	0.00	0.14	0.00	0.00	0.54	0.46	4.57	5.27
c14	11.06	0.19	0.00	0.57	0.04	0.20	0.00	0.00	0.46	0.54	5.97	5.09
c15	11.81	0.30	0.00	0.63	0.01	0.06	0.00	0.00	0.59	0.41	4.90	6.91
c16	5.04	0.01	0.00	0.00	0.30	0.65	0.04	0.00	0.03	0.97	4.88	0.16
c17	10.87	0.17	0.00	0.57	0.15	0.11	0.00	0.00	0.44	0.56	6.05	4.82
c18	14.74	0.05	0.00	0.11	0.39	0.23	0.21	0.00	0.14	0.86	12.62	2.12
c19	2.37	0.08	0.00	0.29	0.63	0.00	0.00	0.00	0.25	0.75	1.78	0.59
c20	2.32	0.04	0.00	0.12	0.84	0.00	0.00	0.00	0.14	0.86	1.99	0.32
c21	4.51	0.26	0.00	0.19	0.39	0.17	0.00	0.00	0.34	0.66	2.97	1.55
c22	5.93	0.26	0.00	0.73	0.00	0.01	0.00	0.00	0.60	0.40	2.36	3.57
c23	15.15	0.22	0.00	0.49	0.00	0.19	0.00	0.09	0.51	0.49	7.43	7.72
c24	1.90	0.20	0.00	0.53	0.00	0.27	0.00	0.00	0.44	0.56	1.06	0.85
c25	0.48	0.44	0.00	0.00	0.00	0.56	0.00	0.00	0.39	0.61	0.29	0.19



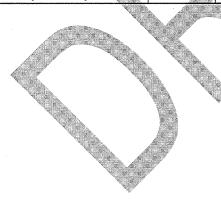
Table B.2: Hydrologic Model Sub-Catchment Properties – Ultimate Catchment Development

Catchment Name	Inflow Node	Catchment Slope (%)	Ultimate Catchment Pervious Area (ha)	Ultimate Catchment Impervious Area (ha)	Pervious PERN	Impervious PERN
C1	N1	2.83	1.54	11.02	0.04	0.015
C2	N31	2.87	3.73	8.25	0.04	0.015
C3	N3	2.07	9.37	14.01	0.04	0.015
C4	N5	2.04	5.31	13.19	0.04	0.015
C5	N8	3.23	2.07	4.46	0.04	0.015
C6	N7	4.04	10.47	< 18.83 × ×	0.04	0.015
C7	N6	3.44	8.10	14.94	0.04	0.015
C8	N4	2.3	1.67	3.22	0.04	0.015
C9	N9	3.65	2.72	3.59	0.04	0.015
C10	N10	3.73	1.60	2.13	0.04	0.015
C11	N12	3.81	4.54	7.21	0.04	0.015
C12	N13	0.18	0.95	1:86	0.04	0.015
C13	N17	2.46	4.50	5.34	0.04	0.015
C14	N16	2.46	4.11	6 .95	0.04	0.015
C15	N30	1.79	4.81	7.00	0.04	0.015
C16	N20	4.27	1.75	3.29	0.04	0.015
C17	N22	1.79	4.81	6.05	0.04	0.015
C18	N24	3.05	5.34	9.39	0.04	0.015
C19	N23	0,89	0.78	1.59	0.04	0.015
C20	N26	1.12	0.83	1.49	0.04	0.015
C21	N27	2.1	1.47	3.04	0.04	0.015
C22	N28	2.62	1.80	4.13	0.04	0.015
C23	N2*	2.6	6.24	8.91	0.04	0.015
C24	N18	2.31	0.57	1.33	0.04	0.015
C25	N32	5	0.15	0.33	0.04	0.015



Table B.3: Peak Flood Levels for the Ultimate Scenario(mAHD)

Location	100 yr ARI	50 yr ARI	20 yr ARI	10 yr ARI	5 yr ARI	2 yr ARI
		2D Result	S		I	
MHG 340	6.20	6.11	5.99	5.88	5.79	5.59
MHG 330	5.49	5.40	5.30	5.19	5.10	4.92
MHG 320	4.09	3.92	3.79	3.68	3.59	3.41
MHG 310	3.67	3.20	2.83	2.46	2.37	2.20
		1D Result	S			•
Quarrion Street u/s	7.05	6.90	6.73	6.56	6.43	6.18
Quarrion Street d/s	7.00	6.86	6.71	6.55	6.43	6.17
Roghan Road u/s	6.69	6.54	6.38	6.21	6.07	5.76
Roghan Road d/s	6.31	6.22	6.10	5.99	5.90	5.68
Church Road u/s	5.50	5.41	5.31	5.19	5.11	4.92
Church Road d/s	5.42	5.33	5.23	5.13	5.05	4.87
401A Church Road Culverts u/s	5.38	5.29	5.20	5.09	5.01	4.83
401A Church Road Culverts d/s	5.16	5.08	4.98	4.85	4.74	4.45
401 Church Rd Bridge u/s	5.04	4.94	4.81	4.68	4.55	4.17
401 Church Rd Bridge d/s	4.51	4.39	4.27	4.16	4.06	3.88
334 Muller Rd Bridge u/s	4.06	3.88	3.75	3.65	3.57	3.40
334 Muller Rd Bridge d/s	3.99	3.82	3.70	3.61	3.53	3.37
334 Muller Rd Culverts u/s	3.97	3.79	3 .67	3.58	3.51	3.35
334 Muller Rd Culverts d/s	3.90	3,64	3.45	3.30	3.18	2.97
350 Muller Rd Culverts u/s	3.66	3.2 3	2.91	2 :65	2.57	2.42
350 Muller Rd Culverts d/s	3.65	3.18	2.80	2.42	2.34	2.20
Gateway Motorway-1 u/s	3.65	3.17	2.77	2.34	2.26	2.26
Gateway Motorway-2 u/s	3.63	3.12	2.64	2.08	2.07	2.07





APPENDIX C: Hydraulic Structure Refrence Sheet (HSRS)





CREEK	Taigum Drain
LOCATION	Quarrion Street

DATE OF SURVEY: 13/05/2011	UBD REF: Map110, F16
AERIAL PHOTO No:	STRUCTURE ID: N/A
BCC XS No:	CHAINAGE (m): Ch562

STRUCTURE DESCRIPTION:

ROAD CULVERT

STRUCTURE SIZE

For culverts give floor level.

4/[3.6Wx1.5H]

For Culverts: Number of cells/pipes & sizes

For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL: 5.00

UPSTREAM OBVERT LEVEL: 6.46

DOWNSTREAM INVERT LEVEL: 4.95

DOWNSTREAM OBVERT LEVEL: 6.41

For bridges give bed level

For Culverts

LENGTH OF CULVERT BARREL AT INVERT (m):

12.03m

LENGTH OF CULVERT BARREL AT OBVERT (m):12.03m

TYPE OF LINING: Concrete (e.g. concrete, stones, brick, corrugated iron)

IS THERE A SURVEYED WEIR PROFILE? Refer to Sec1 of the attached surveyed sections

If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.

WEIR WIDTH (m):20m

LOWEST POINT OF WEIR (m AHD):8.32

(In direction of flow, ie. distance from u/s face to d/s face)

HEIGHT OF GUARDRAILS:

Handrail: 1.13m

DESCRIPTION OF ALL HAND AND GUARD RAILS AND HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS:

The following should also be provided.

Wingwall/Headwall details, entrance details eg pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE:

PLAN NUMBER:

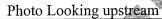
HAS THE STRUCTURE BEEN UPGRADED?

If yes, explain type and date of upgrade. Include plan number and location if applicable.



CREEK	Taigum Drain
LOCATION	Quarrion Street ·

ARI (years)	DISCHARGE (m³/s)			U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (mm)	ARE (m²		VELOC (m/s)	
	Weir	Structure	Total	Y was		Structure	Weir	Structure	Weir
100	0.186	46.71	46.90	7.05	0.05	21.60	0.38	2.163	0.489
50	0	41.53	41.53	6.90	0.03	17.56	0	2.365	0
20	0	35.80	35.80	6.73	0.02	18.12	0	1.976	0
10	0	30.35	30.35	6.56	0.01	14.21	0	2.135	0
5	0	26.34	26.34	6.43	0.01	13.25	0	1.988	0
2	0	19.73	19.73	6.18	0.01	16.55	7 0	1.192	0



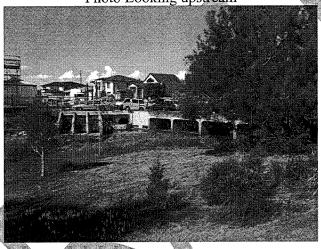
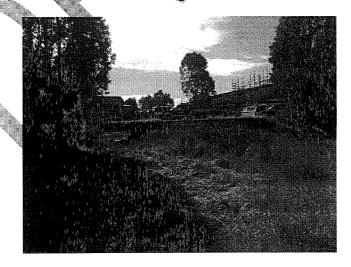


Photo Looking downstream





CREEK	Taigum Drain	
LOCATION	Roghan Road	-

DATE OF SURVEY: 16/05/2011	UBD REF: Map110, G14
AERIAL PHOTO No:	STRUCTURE ID: C0183B
BCC XS No:	CHAINAGE (m): Ch 982

STRUCTURE DESCRIPTION:

ROAD CULVERT

 $\begin{tabular}{ll} STRUCTURE\ SIZE & 3/[3.6Wx1.5H] \\ For\ Culverts:\ Number\ of\ cells/pipes\ \&\ sizes & For\ Bridges:\ Number\ of\ Spans\ and\ their\ lengths \\ \end{tabular}$

UPSTREAM INVERT LEVEL: 3.7

UPSTREAM OBVERT LEVEL: 5.2

DOWNSTREAM INVERT LEVEL: 3.61

DOWNSTREAM OBVERT LEVEL: 5.11

For culverts give floor level.

For bridges give bed level

For Culverts

LENGTH OF CULVERT BARREL AT INVERT (m):

17.73m

LENGTH OF CULVERT BARREL AT OBVERT (m):17.73m

TYPE OF LINING: Concrete (e.g. concrete, stones, brick, corrugated iron)

IS THERE A SURVEYED WEIR PROFILE?

Refer to Sec2 of the attached surveyed sections

If yes give details ie. Plan number and/or survey book number Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.

WEIR WIDTH (m):18m

LOWEST POINT OF WEIR (m AHD):7.03

(In direction of flow, ie. distance from u/s face to d/s face)

HEIGHT OF GUARDRAILS:

Handrail: 1.07m

DESCRIPTION OF ALL HAND AND GUARD RAILS AND HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS:

The following should also be provided.

Wingwall/Headwall details, entrance details eg, pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE:

PLAN NUMBER:

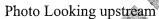
HAS THE STRUCTURE BEEN UPGRADED?

If yes, explain type and date of upgrade. Include plan number and location if applicable.



CREEK	Taigum Drain
LOCATION	Roghan Road

ARI (years)	DISCHARGE (m³/s)			U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (mm)	ARE (m²		VELOC (m/s)	
	Weir	Structure	Total			Structure	Weir	Structure	Weir
100	22.51	51.59	74.10	6.69	0.37	16.22	13.40	3.18	1.68
50	16.26	48.79	65.05	6.54	0.33	16.22	10.42	3.01	1.56
20	9.92	45.40	55.32	6.38	0.27	16.22	7.09	2.80	1.40
10	4.77	41.84	46.61	6.21	0.22	16.22	3.91	2.58	1.22
5	2.14	38.27	40.41	6.07	0.17	16.22	2.04	2.36	1.05
2	0.03	30.31	30.34	5.76	0.08	16.04	0.06	1.89	0.47



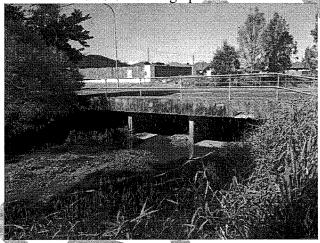
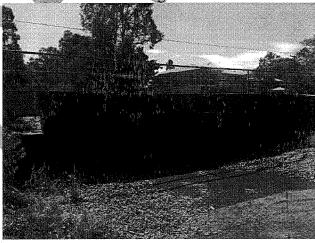


Photo Looking downstream





CREEK	Taigum Drain
LOCATION	Church Road

DATE OF SURVEY: 18/05/2011	UBD REF: Map110, G13
AERIAL PHOTO No:	STRUCTURE ID: N/A
BCC XS No:	CHAINAGE (m): Ch1192

STRUCTURE DESCRIPTION:

ROAD CULVERT

 $\begin{tabular}{ll} STRUCTURE\ SIZE & 4/[5.7Wx1.35H] \\ For Culverts: Number of cells/pipes \& sizes & For Bridges: Number of Spans and their lengths \\ \end{tabular}$

UPSTREAM INVERT LEVEL: 2.66

UPSTREAM OBVERT LEVEL: 4.01

DOWNSTREAM INVERT LEVEL: 2,46

DOWNSTREAM OBVERT LEVEL: 3.81

For bridges give bed level

For culverts give floor level.

For Culverts

LENGTH OF CULVERT BARREL AT INVERT (m):

21.9m

LENGTH OF CULVERT BARREL AT OBVERT (m):21.9m

TYPE OF LINING: Concrete (e.g. concrete, stones, brick, corrugated iron)

IS THERE A SURVEYED WEIR PROFILE? Refer to Sec3 of the attached surveyed sections

If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.

WEIR WIDTH (m):30m

LOWEST POINT OF WEIR (m AHD):5.96

(In direction of flow, ie distance from u/s face to d/s face)

HEIGHT OF GUARDRAILS:

Handrail: 1.18m

DESCRIPTION OF ALL HAND AND GUARD RAILS AND HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS:

The following should also be provided.

Wingwall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE:

PLAN NUMBER:

HAS THE STRUCTURE BEEN UPGRADED?

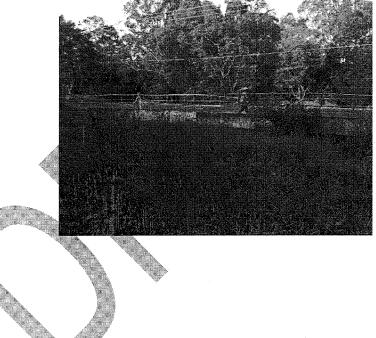
If yes, explain type and date of upgrade. Include plan number and location if applicable.



CREEK	Taigum Drain
LOCATION	Church Road

ARI (years)	DISCHARGE (m³/s)		U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (mm)	1	AREA (m²)		ITY	
- CONTRACTOR OF THE CONTRACTOR	Weir	Structure	Total			Structure	Weir	Structure	Weir
100	27.23	29.13	56.36	5.50	0.08	30.78	32.03	0.95	0.85
50	23.69	28.05	51.74	5.41	0.08	30.78	28.54	0.91	0.83
20	19.89	26.85	46.74	5.31	0.07	30.78	24.86	0.87	0.80
10	16.36	25.40	41.76	5.19	0.07	30.78	21.25	0.82	0.77
5	13.55	24.32	37.87	5.11	0.06	30.78	17.83	0.79	0.76
2	8.57	22.75	31.32	4.92	0.05	30.78	11.28	0.74	0.76

NA Photo Looking downstream





CREEK	Taigum Drain
LOCATION	401A Church Rd

DATE OF SURVEY: 18/05/2011

AERIAL PHOTO No:

BCC XS No:

UBD REF: Map110, G13

STRUCTURE ID:

CHAINAGE (m): Ch1281

STRUCTURE DESCRIPTION:

ROAD CULVERT

STRUCTURE SIZE

2/1.725m RCP

For Culverts: Number of cells/pipes & sizes

For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL: 2.19&2.42

UPSTREAM OBVERT LEVEL: 4.00&4.23

DOWNSTREAM INVERT LEVEL: 2.16&2.26

DOWNSTREAM OBVERT LEVEL: 3,99&4.07

For bridges give bed level

For culverts give floor level.

For Culverts LENGTH OF CULVERT BARREL AT INVERT (m):

3.87

LENGTH OF CULVERT BARREL AT OBVERT (m):3.87

TYPE OF LINING: Concrete (e.g. concrete, stones, brick, corrugated iron)

IS THERE A SURVEYED WEIR PROFILE? Refer to Sec4 of the attached surveyed sections

If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.

WEIR WIDTH (m):10m

LOWEST POINT OF WEIR (m AHD):5.46

(In direction of flow, ie. distance from u/s face to d/s face)

HEIGHT OF GUARDRAILS:

Handrail: 1.25m

DESCRIPTION OF ALL HAND AND GUARD RAILS AND HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS:

The following should also be provided.

Wingwall/Headwall details, entrance details eg pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE:

PLAN NUMBER:

HAS THE STRUCTURE BEEN UPGRADED?

If yes, explain type and date of upgrade. Include plan number and location if applicable.

ADDITIONAL COMMENTS:

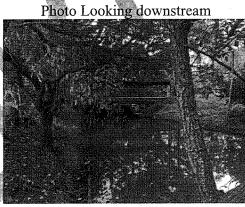
JULY 2011



CREEK	Taigum Drain
LOCATION	401A Church Road

ARI	· · · · · · · · · · · · · · · · · · ·	DISCHARGE				AFFLUX				VELOCITY		
(years)	(m^3/s)				AT MAX	(m^2)			(m/s)			
				LEVEL	FLOW							
	Weir	Structure	Structure	Total	(m AHD)	(mm)	Structure	Structure	Weir	Structure	Structure	Weir
100	31.22	8.74	9.46	49.42	5.38	0.22	2.34	1.67	19.04	3.74	5.66	1.64
50	29.10	8.75	9.48	47.33	5.29	0.22	2.34	2.34	17.74	3.74	4.05	1.64
20	26.53	8.81	9.44	44.78	5.20	0.22	2.34	2.34	16.48	3.77	4.04	1.61
10	23.82	8.75	9.49	42.06	5.09	0.24	2.34	2.34	15.17	3.74	4.06	1.57
5	20.70	8.7	9.44	38.84	5.01	0.27	2.33	2.34	13.62	3.73	4.04	1.52
2	13.87	8.49	9.27	31.63	4.83	0.38	2.34	2.34	10.20	3.63	3.97	1.36







CREEK	Taigum Drain	
LOCATION	401 Church Rd	

DATE OF SURVEY: 18/05/2011 UBD REF: Map110, G13 STRUCTURE ID: N/A **AERIAL PHOTO No:** CHAINAGE (m): Ch1342 BCC XS No:

STRUCTURE DESCRIPTION:

Timber Bridge

STRUCTURE SIZE

For culverts give floor level.

5.0 Span x 3.9L

For Culverts: Number of cells/pipes & sizes For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL: 1.59

UPSTREAM OBVERT LEVEL:

DOWNSTREAM INVERT LEVEL: 1.61

DOWNSTREAM OBVERT LEVEL:

For bridges give bed level

For Culverts

LENGTH OF CULVERT BARREL AT INVERT (m):

LENGTH OF CULVERT BARREL AT OBVERT (m):3.9m

TYPE OF LINING: No Lining (e.g. concrete, stones, brick, corrugated iron)

Refer to Sec 5 of the attached surveyed sections IS THERE A SURVEYED WEIR PROFILE?

If yes give details ie. Plan number and/or survey book number Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.

WEIR WIDTH (m):5.0m

LOWEST POINT OF WEIR (m AHD):5.16

(In direction of flow, ie. distance from u/s face to d/s face)

HEIGHT OF GUARDRAILS:

Handrail: 1.0m

DESCRIPTION OF ALL HAND AND GUARD RAILS AND HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS:

The following should also be provided.

Wingwall/Headwall details, entrance details eg pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE:

PLAN NUMBER:

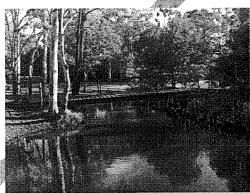
HAS THE STRUCTURE BEEN UPGRADED?

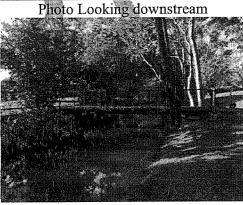
If yes, explain type and date of upgrade. Include plan number and location if applicable.



CREEK	Taigum Drain
LOCATION	401 Church Rd

ARI (years)	DISCHARGE (m³/s)		U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (mm)	ARE (m²		VELOC: (m/s)		
	Weir	Structure	Total			Structure	Weir	Structure	Weir
100	26.13	46.05	72.18	5.04	0.53	11.15	16.97	4.13	1.54
50	20.38	45.73	66.11	4.94	0.55	11.15	14.15	4.10	1.44
20	13.98	44.58	58.56	4.81	0.54	11.15	10.67	4.00	1.31
10	8.10	43.08	51.18	4.68	0.52	11.15	6.98	3.86	1.16
5	3.77	41.53	45.3	4.55	0.49	11.15	3.77	3.72	1.00
2	0	34.66	34.66	4.17	0.29	11.15	0.00	3.11	0







CREEK	Taigum Drain
LOCATION	334 Muller Road

UBD REF: Map110, K13 DATE OF SURVEY: 24/05/2011 STRUCTURE ID: N/A **AERIAL PHOTO No:** BCC XS No: CHAINAGE (m): Ch1930

STRUCTURE DESCRIPTION:

Timber Bridge

STRUCTURE SIZE

8.5 Span x 0.62L

For Culverts: Number of cells/pipes & sizes

For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL: -0.74

UPSTREAM OBVERT LEVEL:

DOWNSTREAM INVERT LEVEL: -0.76

DOWNSTREAM OBVERT LEVEL:

For culverts give floor level.

For bridges give bed level

For Culverts

LENGTH OF CULVERT BARREL AT INVERT (m):

0.62m

LENGTH OF CULVERT BARREL AT OBVERT (m):0.62m

TYPE OF LINING: No Lining (e.g. concrete, stones, brick, corrugated iron)

IS THERE A SURVEYED WEIR PROFILE? Refer to Sec6 of the attached surveyed sections

If yes give details ie. Plan number and/or survey book number, Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.

WEIR WIDTH (m):8.5m

LOWEST POINT OF WEIR (m AHD):1.82

(In direction of flow, ie. distance from u/s face to d/s face)

HEIGHT OF GUARDRAILS: Handrail:

DESCRIPTION OF ALL HAND AND GUARD RAILS AND HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS:

The following should also be provided.

Wingwall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE:

PLAN NUMBER:

HAS THE STRUCTURE BEEN UPGRADED?

If yes, explain type and date of upgrade. Include plan number and location if applicable.

ADDITIONAL COMMENTS:

This is the remaining of a timber bridge crossing.



CREEK	Taigum Drain
LOCATION	334 Muller Road

ARI (years)	DISCHARGE (m³/s)			U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (mm)	ARI (m²		VELOC (m/s)	
	Weir	Structure	Total			Structure	Weir	Structure	Weir
100	52.38	29.34	81.72	4.06	0.02	23.10	130.95	1.27	0.40
50	43.65	28.88	72.53	3.88	0.03	23.10	111.92	1.25	0.39
20	34.55	26.90	61.45	3.75	0.03	22.99	98.71	1.17	0.35
10	26.13	24.12	50.25	3.65	0.03	22.97	90.10	1.05	0.29
5	21.66	20.61	42.27	3.57	0.02	23.16	83,31	0.89	0.26
2	14.41	14.69	29.1	3.40	0.02	22.95	72.05	0.64	0.20



Photo Looking downstream





CREEK	Taigum Drain
LOCATION	334 Muller Road

DATE OF SURVEY: 24/05/2011	UBD REF: Map110, K13
AERIAL PHOTO No:	STRUCTURE ID: N/A
BCC XS No:	CHAINAGE (m): Ch1985

STRUCTURE DESCRIPTION:

ROAD CULVERT

STRUCTURE SIZE

*2/1.825m RCP & **1/1.425m RCP & ***1/1.425m RCP

For Culverts: Number of cells/pipes & sizes For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL:

UPSTREAM OBVERT LEVEL:

*0.9 & **-0.32&***1.72

***3.24

DOWNSTREAM INVERT LEVEL:

DOWNSTREAM OBVERT LEVEL:

***3.15

*1&**-0.41&***1.64 For culverts give floor level.

For bridges give bed level

For Culverts

LENGTH OF CULVERT BARREL AT INVERT (m):

4.7m

LENGTH OF CULVERT BARREL AT OBVERT (m):4.7m

TYPE OF LINING: Concrete (e.g. concrete, stones, brick, corrugated iron)

IS THERE A SURVEYED WEIR PROFILE? Refer to Sec7 of the attached surveyed sections If yes give details ie. Plan number and/or survey book number.

Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.

WEIR WIDTH (m):5.5m

LOWEST POINT OF WEIR (m AHD):3.4

(In direction of flow, ie. distance from u/s face to d/s face)

HEIGHT OF GUARDRAILS:

Handrail:

DESCRIPTION OF ALL HAND AND GUARD RAILS AND HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS:

The following should also be provided.

Wingwall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE:

PLAN NUMBER:

HAS THE STRUCTURE BEEN UPGRADED?

If yes, explain type and date of upgrade. Include plan number and location if applicable.



CREEK	Taigum Drain
LOCATION	334 Muller Road

ARI (years)	DISCHARGE (m³/s)					U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW	_ 1				VELOCITY (m/s)			
	Weir	Structure	Structure	Structure	Total	,	(mm)		i -	Structure	Weir	1	l	Structur	Weir
								ure	ure			e	e	е	
100	54.81	8.99	4.49	2.72	71.01	3.97	0.07	5.23	2.61	1,59	40.60	1.72	1.72	1.71	1.35
50	45.56	10.93	7.16	3.30	66.95	3.79	0.14	5.23	3.43	1.59	33.75	2.09	2.09	2.08	1.35
20	38.62	11.62	5.81	3.47	59.52	3.67	0.22	5.23	2.62	1.56	29.04	2.22	2.22	2.22	1.33
10	27.39	11.97	7.16	3.52	50.04	3.58	0.29	4.60	2.61	1.43	22.09	2.60	2.74	2.46	1.24
5	19.66	11.96	7.16	3.52	42.30	3.51	0.33	4.60	2,61	1.43	16.95	2.60	2.74	2.46	1.16
2	7.32	11.93	7.16	3.46	29.87	3.35	0.38	4,59	2.61	1.41	7.79	2.60	2.74	2.46	0.94







CREEK	Taigum Drain
LOCATION	350 Muller Road

DATE OF SURVEY: 20/05/2011	UBD REF: Map110, K13
AERIAL PHOTO No:	STRUCTURE ID: N/A
BCC XS No:	CHAINAGE (m):

STRUCTURE DESCRIPTION:

ROAD CULVERT

STRUCTURE SIZE

*1/1.725m RCP & **1/1.625m RCP

For Culverts: Number of cells/pipes & sizes For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL:

UPSTREAM OBVERT LEVEL:

*-0.45& **-0.51

*1.32&**1.25

DOWNSTREAM INVERT LEVEL:

DOWNSTREAM OBVERT LEVEL:

*-0.26& **-0.67

*1.49&**1.09 For bridges give bed level

For culverts give floor level.

For Culverts

LENGTH OF CULVERT BARREL AT INVERT (m):

*9.9m&**9.56m

LENGTH OF CULVERT BARREL AT OBVERT (m): *9.9m&**9.56m

TYPE OF LINING: Concrete

(e.g. concrete, stones, brick, corrugated iron)

IS THERE A SURVEYED WEIR PROFILE? Refer to Sec8 of the attached surveyed sections

If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.

WEIR WIDTH (m):

LOWEST POINT OF WEIR (m AHD):

(In direction of flow, ie. distance from u/s face to d/s face)

HEIGHT OF GUARDRAILS:

Handrail: 0.7m

DESCRIPTION OF ALL HAND AND GUARD RAILS AND HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS:

The following should also be provided.

Wingwall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE:

PLAN NUMBER:

HAS THE STRUCTURE BEEN UPGRADED?

If yes, explain type and date of upgrade. Include plan number and location if applicable.



CREEK	Taigum Drain
LOCATION	350 Muller Road

ARI		DISCH	IARGE		U/S	AFFLUX		AREA		VELOCITY			
(years)		(m	³ /s)		WATER	AT MAX		(m^2)		(m/s)			
					LEVEL	FLOW							
	Weir	Structure	Structure	Total	(m AHD)	(mm)	Structure	Structure	Weir	Structure	Structure	Weir	
100	79.57	2.16	1.97	83.70	3.66	0.01	2.35	2.14	169.30	0.92	0.92	0.47	
50	70.70	2.33	2.13	75.16	3.23	0.04	2.35	2.13	124.04	0.99	1.00	0.57	
20	58.59	2.84	2.59	64.02	2.91	0.11	2.35	2.14	66.58	1.21	1.21	0.88	
10	45.62	4.00	3.66	53.28	2.65	0.23	2.33	2.14	59.25	1.72	1.71	0.77	
5	37.53	3.97	3.63	45.13	2.57	0.24	2.34	2.14	50.72	1.70	1.70	0.74	
2	24.43	3.87	3.46	31.76	2.42	0.22	2.39 🦑	2.14	38.17	1.62	1.62	0.64	

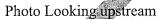
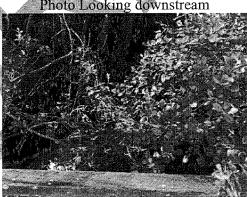




Photo Looking downstream





CREEK	Taigum Drain
LOCATION	Gateway Motorway

DATE OF SURVEY: 20/05/2011	UBD REF: Map110, K13
AERIAL PHOTO No:	STRUCTURE ID: N/A
BCC XS No:	CHAINAGE (m):

STRUCTURE DESCRIPTION:

ROAD CULVERT

STRUCTURE SIZE

*2/[2.4Wx2.1H] & *2/[2.4Wx1.9H] &**1/[2.4Wx2.5H]

For Culverts: Number of cells/pipes & sizes For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL: *-0.5 & **-0.8

UPSTREAM OBVERT LEVEL:

DOWNSTREAM INVERT LEVEL:*\$** -1.12

DOWNSTREAM OBVERT LEVEL:

For culverts give floor level.

For bridges give bed level

For Culverts

LENGTH OF CULVERT BARREL AT INVERT (m):

LENGTH OF CULVERT BARREL AT OBVERT (m):47m

TYPE OF LINING: Concrete (e.g. concrete, stones, brick, corrugated iron)

IS THERE A SURVEYED WEIR PROFILE?

If yes give details ie. Plan number and/or survey book number, Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.

WEIR WIDTH (m):

LOWEST POINT OF WEIR (m AHD):

(In direction of flow, ie. distance from u/s face to d/s face)

HEIGHT OF GUARDRAILS:

Handrail:

DESCRIPTION OF ALL HAND AND GUARD RAILS AND HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS:

The following should also be provided.

Wingwall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE:

PLAN NUMBER:

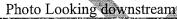
HAS THE STRUCTURE BEEN UPGRADED?

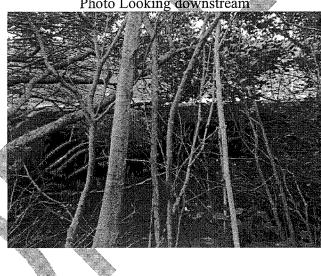
If yes, explain type and date of upgrade. Include plan number and location if applicable.



CREEK	Taigum Drain
LOCATION	Gateway Motorway

ARI		DISCHARGE					AFFLUX		ARE	EA		VELOCITY				
(years)		(m^3/s)					AT MAX		(m ²	·)		(m/s)				
						LEVEL	FLOW									
	Weir	Structur	Structur	Structur	Total	(m AHD)	(mm)	Structur	Structur	Structur	Weir	Structur	Structur	Structur	Weir	
		ę	e	е				е	е	е		е.	е	е		
100	0	23.04	25.69	15.49	64.22	3.65	N/A	9.12	10.08	6.00	0	2.53	2.55	2.58	0	
50	0	21.20	23.64	14.26	59.10	3.17	N/A	9.12	10.08	6.00	0	2.32	2.35	2.38	0	
20	0	18.32	20.42	12.32	51.06	2.77	N/A	9.12	10.08	6.00	0	2.01	2.03	2.05	0	
10	0	16.43	18.31	11.04	45.78	2.34	N/A	9.12	10.08	6.00	, 0	1.80	1.82	1.84	0	
5	0	14.11	15.73	9.48	39.32	2.26	N/A	9.12	10.08	6.00	0	1.55	1.56	1.58	0	
2	0	12.78	14.24	8.59	35.61	2.26	N/A	9.12	10.08	6.00	0	1.40	1.41	1.43	0	







CREEK	Taigum Drain	
LOCATION	Gateway Motorway	

DATE OF SURVEY: N/A UBD REF: AERIAL PHOTO No: STRUCTURE ID: BCC XS No: CHAINAGE (m):

STRUCTURE DESCRIPTION:

ROAD CULVERT

STRUCTURE SIZE

3/[1.5Wx1.5H]

For Culverts: Number of cells/pipes & sizes

For Bridges: Number of Spans and their lengths

UPSTREAM INVERT LEVEL: -0.215

UPSTREAM OBVERT LEVEL:

DOWNSTREAM INVERT LEVEL: -1.115

DOWNSTREAM OBVERT LEVEL:

For bridges give bed level For culverts give floor level.

LENGTH OF CULVERT BARREL AT INVERT (m):

LENGTH OF CULVERT BARREL AT OBVERT (m):40m

TYPE OF LINING: Concrete (e.g. concrete, stones, brick, corrugated iron)

IS THERE A SURVEYED WEIR PROFILE?

If yes give details ie. Plan number and/or survey book number. Note: This section should be at the highest part of the road eg crown, kerb, hand rails guard rails whichever is higher.

WEIR WIDTH (m):

LOWEST POINT OF WEIR (m AHD):

(In direction of flow, ie. distance from u/s face to d/s face)

HEIGHT OF GUARDRAILS:

Handrail:

DESCRIPTION OF ALL HAND AND GUARD RAILS AND HEIGHTS TO TOP AND UNDERSIDE OF GUARD RAILS:

The following should also be provided.

Wingwall/Headwall details, entrance details eg. pipe flush with embankment or projecting, socket or square end, entrance rounding, levels. For bridges, details of piers and section under bridge including abutment details. Specify Survey Book No.

CONSTRUCTION DATE OF CURRENT STRUCTURE:

PLAN NUMBER:

HAS THE STRUCTURE BEEN UPGRADED?

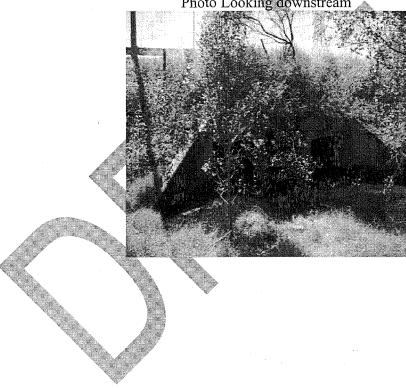
If yes, explain type and date of upgrade. Include plan number and location if applicable.



CREEK	Taigum Drain	
LOCATION	Gateway Motorway	

ARI (years)	DISCHARGE (m³/s)		1		U/S WATER LEVEL (m AHD)	AFFLUX AT MAX FLOW (mm)	ARF (m²		VELOC (m/s)	
	Weir	Structure	Total			Structure	Weir	Structure	Weir	
100	0	16.16	16.16	3.63	N/A	6.75	0	2.39	0	
50	0	14.40	14.40	3.12	N/A	6.75	0	2.13	0	
20	0	10.84	10.84	2.64	N/A	6.75	0	1.61	0	
10	0	4.90	4.90	2.08	N/A	6.75	0	0.73	0	
5	0	3.93	3.93	2.07	N/A	6.75	0	0.58	0	
2	0	4.21	4.21	2.07	N/A	6.75	0	0.62	0	

N/A Photo Looking downstream



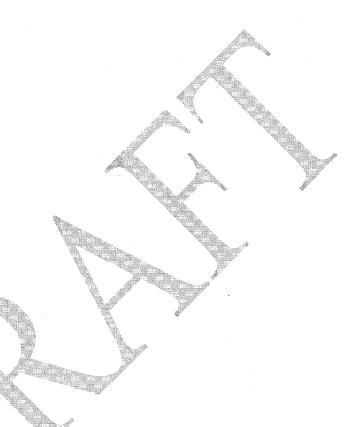


Carseldine Channel Flooding Investigation

July 2011

Prepared for
Water Resources Branch
CITY PLANNING AND SUSTAINABILITY

Prepared by
Water & Environment
City Projects Office
BRISBANE INFRASTRUCTURE



City Projects Office

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1.0 Introduction

1.1 Background

Prior to this investigation, a major flood study for the Carseldine Channel was undertaken for Brisbane City Council in 1997 by consultants WBM. This study was termed the *Master Drainage Plan for the Carseldine and Taigum Catchments*. For the purposes of this report, this previous study will be known as the "original" and any references using the word "original" should be taken as referring to this study.

The 1997 study used an XP-RAFTS model for the catchment hydrology and a MIKE11 model for the waterway hydraulics. As there are no flood level recording stations within the catchment, both models were un-calibrated and could not be verified against actual flooding events. The original study considered both the existing and ultimate catchment conditions and also incorporated mitigation options to alleviate flooding.

Following on from work undertaken by WBM for the original flood study, the Council considered a number of flood management options. The option that gained major acceptance at the time was termed Upgrade M and predominantly involved major channel works to the Carseldine Channel from the upstream end of the Bill Brown Sports Field to the downstream model boundary. The other area of proposed major channel works was within the Gympie Road Channel. Modifications to the Gympie Road Channel have subsequently been completed as part of the Tallowood Grove development. Other portions of the waterway were assumed to be left in their existing condition.

Consultants John Wilson and Partners (JWP), working on behalf of Brisbane City Council, undertook work in relation to defining a waterway corridor between Lacey Road and North Coast Railway. As part of this work they proposed a further variation of Upgrade M, termed Option A. Option A entailed all of the modifications of the former with the addition of the upgrade of the Lacey Road Culvert and major channel works between Lacey Road and the Railway to be undertaken in conjunction with the adjacent development. Modifications to this channel have subsequently been completed as part of the Somerset Estate development.

During the finalisation of this study further recent development downstream of the North Coast Railway line has been identified to impact on some of the results of this study.

1.2 Objectives

The objectives of this flooding investigation are as follows:

- To update the original RAFTS and MIKE11 models using the latest available information at the commencement of this study.
- To ascertain the 2, 5, 10, 20, 50 and 100-yr ARI flood levels for the Ultimate catchment development conditions
- To report on the flood level results and compare them against those previously determined, including the previous flood mitigation options.
- To identify flooding problem areas.
- To determine appropriate waterway corridors for the Carseldine channels.



2.0 Model Update

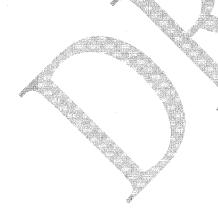
2.1 General

This section details the major updates which have been made to the original RAFTS hydrologic model and the MIKE11 hydraulic model to incorporate the changes in land use (i.e. developments) which have occurred since the original study was completed in 1997, and the commencement of this study in 2005. The more specific changes made to the models to define the Ultimate conditions are discussed in Section 3.

RAFTS 2000 Version 6.5 and MIKE11 Version 2005 SP4 were used for this study.

2.2 RAFTS Model

Figure 2.1 indicates the sub-catchment arrangement used in the updated RAFTS model. The original RAFTS model assumed that a significant proportion of the undeveloped land between the North Coast Railway Line and the Landfill Area contributed to the Landfill Channel (See Figure 2.2 for locations), which runs to the south of the Landfill area. Whilst this would have been correct in 1997, subsequent developments adjacent to the Landfill Channel have changed the existing overland flow pattern, such that all flows are now directed towards the main Carseldine Channel, this change is now reflected in the model. Also, the previous work assumed the catchment boundary for this area extended as far as Roghan Road. For the purposes of this flooding investigation it has been assumed that the contributing catchment area extends significantly further south of Roghan Road as shown. This is to account for the potential redirection of drainage accompanying future development.



2.3 MIKE11 Model

2.3.1 Network Schematic

Figure 2.2 indicates the network schematic and cross-section layout used in the updated MIKE11 model. The general network schematic for the original MIKE11 model was not altered substantially during the upgrade process. The branch schematic lines were adjusted (as required) to incorporate any changes to the horizontal alignment of the channels. This resulted in the model chainages for the majority of cross-sections being different from the original model.

A link channel between the Carseldine Channel and the Telegraph Road Channel was added to the model at Chainage 11799 on the Carseldine Reach. The purpose of this was to enable the flow to distribute on both sides of the Bill Brown Sports Field, which is believed to occur during a flooding event. The Telegraph Road Channel was extended approximately 200 m further upstream, to just upstream of the Bill Brown Sports Field. This enabled the link channel to be connected at this location.

The Telegraph Road Detention Basin Reach was removed from the MIKE11 model and replaced by a point inflow into the Telegraph Road Channel. The hydrologic effects of the Detention Basin were modelled in RAFTS and as such the attenuation and lagging effects are incorporated in the point inflow discharge hydrograph.

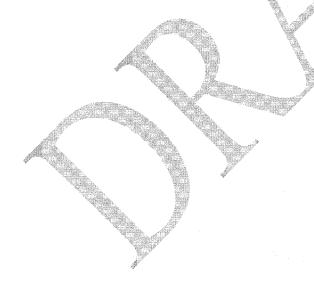
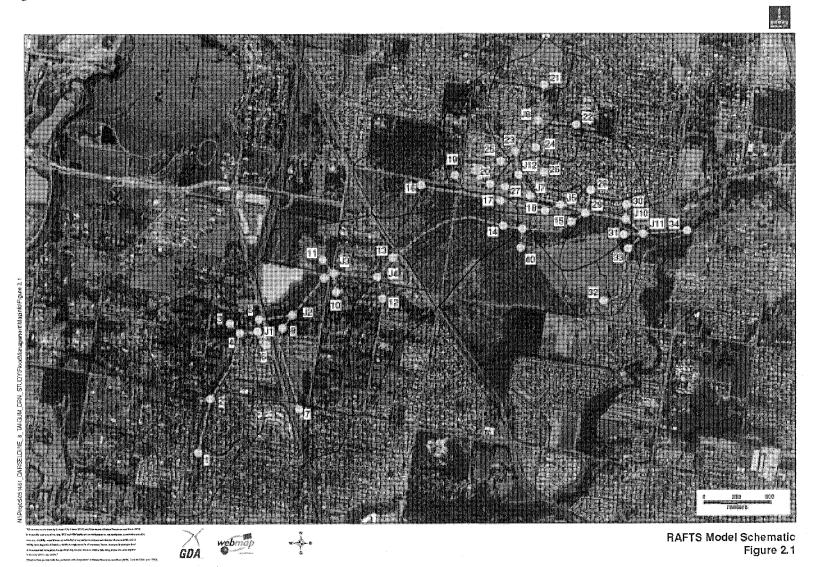


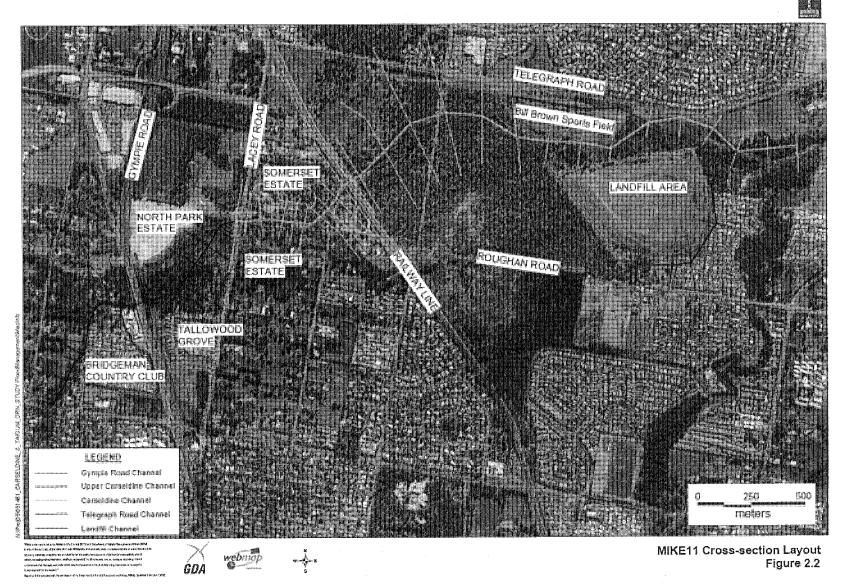
Figure 2.1 RAFTS Model Schematics



Carseldine Channel - Flooding Investigation



Figure 2.2 MIKE11 Model Schematics



Carseldine Channel - Flooding Investigation



2.3.2 Cross-sectional Information

The following items detail the review and subsequent modifications made (if required) to the original MIKE11 cross-sectional information. All cross-sections were "re-processed" in MIKE11 using a fixed number of equidistant points to improve the reliability of the model.

Upper Carseldine Channel (Section upstream of Gympie Road)

The original MIKE11 model was comprised of surveyed cross-sectional information of which the majority was considered outdated due to the construction of residential development projects. The cross-sectional information was updated from as-built drawing information for the Bridgeman Country Club Estate development. This was supplemented with 2002 ALS data at locations where the cross-sections needed to be extended laterally.

Upper Carseldine Channel (Section between Gympie Road and Lacey Road)

The cross-sectional information in the original MIKE11 model appeared to be representative of the catchment conditions in 2005. Some cross-sections needed to be extended laterally for which the topographic information was obtained from 2002 ALS data and development application drawings of the North Park Estate development.

Gympie Road Channel (Parallel to Gympie Road)

The original MIKE11 model was comprised of surveyed cross-sectional information of which the majority was outdated. The cross-sectional information was updated from development application design drawing information for the Tallowood Grove development, which was the best available data.

Carseldine Channel (Between Lacey Road and North Coast Railway)

The original MIKE11 model was comprised of surveyed cross-sectional information which was outdated. The cross-sectional information was updated from as-built drawing information for the Somerset Estate development. The as-built drawing information was supplemented with 2002 ALS data at locations where the cross-sections needed to be extended laterally.

Carseldine Channel (Between North Coast Railway and Landfill Area)

The cross-sectional information in the original MIKE11 model appeared to be representative of the 2005 catchment conditions. Some cross-sections were extended laterally for which the topographic information was obtained from ALS data.

Carseldine Channel (At Landfill Area)

The cross-sectional information in the original MIKE11 model appeared to be representative of the catchment conditions in 2005. Some cross-sections were extended laterally for which the topographic information was obtained from 2002 ALS data.

Carseldine Channel (Downstream of Landfill Area)

The cross-sectional information in the MIKE11 model appeared to be representative of the current conditions; as such the cross-sectional information was not changed.

Telegraph Road Channel (Parallel to Telegraph Road)

The cross-sectional information in the original MIKE11 model appeared to be representative of the 2005 catchment conditions. The Channel was extended further upstream with the addition of an extra cross-section. Also, two new cross-sections were added upstream and downstream of the access road to the Bill Brown Sports Field, to improve the model performance.

Landfill Channel

The original MIKE11 model was comprised of surveyed cross-sectional information which was outdated. This cross-sectional information was not updated as flood level information in this area was not in the scope of this study.

2.3.3 Culvert Crossings

The following section of the report details the review and subsequent modifications made (if required) to the MIKE11 culvert information.

Lacey Road Crossing

The Lacey Road Culvert was upgraded as part of the Somerset Estate development. The MIKE11 culvert information for the Lacey Road structure was updated from the as-built drawing information for this development.

Railway Crossing

At the railway crossing, the model was updated to incorporate the widening of the railway embankment, which included the new hydraulic structure. The location of the cross-section immediately downstream of the structure was adjusted accordingly. There were some slight adjustments made to the weir representing the vertical geometry of the railway, based on 2002 ALS data.

Access Road Crossing

The Ø900 mm piped culvert underneath the access road to the Bill Brown Sports field was incorporated into the MIKE11, as the original model did not include this minor crossing.

Gympie Road Crossing

There were no changes made to the Gympie Road Culvert, however it was noted that the as-built configuration of the culvert and approach channel is hydraulically very inefficient and not ideal. At its current location, there is a sharp bend required from the main channel to get to the culvert inlet.

3.0 Modelling of Ultimate Conditions

3.1 General

The Ultimate condition modelling was undertaken for the 2, 5, 10, 20, 50 and 100-yr ARI events to determine the corresponding flood levels. The following assumptions were made in the modelling of the Ultimate conditions as per best practice guidelines:

- The hydraulic roughness was increased if it was deemed that there was potential for the hydraulic roughness of the channel to increase through means such as natural vegetation growth.
- The degree of development and hence amount of impervious area was taken as what was considered the ultimate level of development.
- The topography of the channel and floodplain areas was taken as that at the time of modelling, apart from upstream of Gympie Road where a waterway corridor was introduced.
- The Minimum Riparian Corridor (MRC) has been modelled to consider that potentially over time, revegetation can occur on the channel banks. The MRC is assumed to extend 15m on either side of the channel banks where a Manning's 'n' hydraulic roughness parameter value of 0.15 is applied.

The simulations were run for the 60-minute, 120-minute and 180-minute duration storm events and the results presented represent the envelope of the highest values.

3.2 Design Hydrology

To determine the discharge hydrographs for the Ultimate conditions, the RAFTS model was updated to what was considered the ultimate level of development as per Brisbane City Plan. **Table 3.1** indicates the impervious area percentages used for each respective sub-catchment. These values are generally the same as used in the original modelling and allow for a fully urbanised catchment. Where the impervious area percentage has changed from the original model, the original value is shown in brackets.

Table 3.1 Sub-catchment Impervious Percentages - Ultimate Conditions

Sub-catchment	Percentage Impervious	Sub-catchment	Percentage Impervious
1	45 % (30%)	19	45 %
2	45 % (42%)	20	60 % (45 %)
3	75 % (45%)	21	45 %
4	75 % (27%)	22	45 %
5	75 % (45%)	23	45 %
6	75 % (45%)	24	45 %
7	45 %	25	45 %
8	45 %	26	45 % (26 %)
9	45 %	27	45 %
10	45 %	28	45 %
11	45 %	29	45 % (31 %)
12	45 %	30	♦ 45 %
13	45 %	31	45 %
14	45 %	32	45 %
15	45 %	33	45 %
16	45 %	34	45 %
17	45 %	40	45 %
18	45 %		

⁽⁾ previous value for Existing conditions

3.3 Tailwater Conditions

The adopted downstream boundary tailwater conditions were sourced from the original study. These values represent the flood level in Cabbage Tree Creek and are indicated in **Table 3.2**.

Table 3.2 Tailwater Conditions

ARI	Flood Level (m AHD)
2-yr	4.45
5-yr	4.84
10-yr	4.99
20-yr	5.13
50-yr	5.32
100-yr	5.52

3.4 Model Refinements

Upstream of Gympie Road, a waterway corridor was introduced to provide a buffer for potential development adjacent to the channel. The extents of the waterway corridor were as per the current version of City Plan. The effective weir length of Gympie Road was altered to account for the reduced flow width, which would occur as a result of introducing the waterway corridor upstream.

Within the Gympie Road Channel, the Manning's n roughness values were increased from existing values of approximately 0.03/0.04 to a value of 0.08 to allow for some natural revegetation of the channel. Similarly, the Manning's 'n' hydraulic roughness values within the section of the Carseldine Channel between Lacey Road and the Railway were also increased to a value of 0.08 to allow for some natural revegetation.

3.5 Modelling Results

The tabulated results of the MIKE11 modelling of the Ultimate conditions are presented in **Appendix B** and the flood profile / inundation plots in **Appendix C**. The results are presented in the following format:

- Tabulated flood level results for the 2, 5, 10, 20, 50 and 100-yr ARI events Appendix A
- Tabulated discharge results for the 2, 5, 10, 20, 50 and 100-yr ARI events Appendix A
- Flood profile plots for the 2, 5, 10, 20, 50 and 100-yr ARI events Appendix B
- Flood Inundation Maps for the 2, 5, 10, 20, 50 and 100-yr ARI events Appendix C

At the upstream end of the Bill Brown Sports Field there is a similar magnitude discharge in both the Carseldine Channel and the Telegraph Road Channel. **Table 3.3** indicates the discharge in both channels for the full range of ARI events modelled.

Table 3.3 Flow Distribution at Bill Brown Sports Oval - Ultimate Conditions

ADI	Discharge (m³/s)								
ARI	Telegraph Rd Channel	Carseldine Channel							
2-yr	14.3	14.4							
5-yr	17.9	18.1							
10-yr	20.1	21.2							
20-yr	22.0	24.3							
50-yr	24.8	29.0							
100-yr	27.2	32.9							

3.5.1 Hydraulic Structures

Table 3.4 presents the hydraulic head loss and design flood immunities of the modelled hydraulic structures.

Table 3.4 Hydraulic Structure Results - Ultimate Conditions

54-4	Structur	e Headloss	Approx. Flood
Structure	2-yr ARI	100-yr ARI	Immunity
Gympie Road Culvert	1.36	1.49	2-5-yr ARI
Lacey Road Culvert	0.36	0.96	> 100-yr ARI
North Coast Railway Culverts	0.60	1.50	> 100-yr ARI

In the 2-yr ARI event there is some flooding of Telegraph Road in the vicinity of the detention basin. The maximum depth of inundation over this length is approximately 0.4 m and occurs approximately 240 m east of the Norris Road intersection. In the 100-yr ARI event Telegraph Road is inundated from the intersection of Norris Road for a distance of approximately 600 m in an easterly direction. The maximum depth of inundation over this length is approximately 0.8 m. The Bill Brown Sports Field has flood immunity greater than 100-yr ARI, however the access road is inundated in the 2-yr ARI event.

Between the Bill Brown Sports Field and the confluence with Cabbage Tree Creek, the flooding extents are effectively confined to within the vicinity of the main channel and there is no flooding of Telegraph Road in all events up the 100-yr ARI.



4.0 Comparison with Previous Work

4.1 General

This section compares the results for the 100-yr ARI event of the current modelling with the previous work undertaken by consultants.

Figures 4.1 to 4.4 indicate a comparison of the 100-yr ARI flood levels for the Upper Carseldine, Gympie Road, Carseldine and Telegraph Road channels. The 100-yr ARI flood levels are presented for the BCC Ultimate Conditions, WBM 1997 Ultimate Conditions, BCC 1997 Upgrade M and JWP Option A. The tabulated flood levels are presented in Appendix D, for which the values shown in italics represent those which have been interpolated. Some interpolation was required of the previous consultants flood levels to coincide with the location of new cross-sections of this study. Sections 5.1.2 to 5.1.4 describe the major differences between the flood profiles within the four major channels.

4.2 Gympie Road Channel

The BCC Ultimate profile is generally lower than the three other profiles. This is most likely because the constructed dimensions of the re-aligned channel are slightly larger than those proposed in Upgrade M / Option A.

4.3 Upper Carseldine Channel

Immediately upstream of Gympie Road, the 100-yr ARI flood level is highest for the BCC Ultimate profile than for the other four profiles. This is predominantly because of a combination of a higher discharge (due to a higher degree of development assumed) and the effects of the waterway corridor. Between Gympie and Lacey Roads, the results are quite similar for all five profiles apart from immediately upstream of Lacey Road where the profiles which contain the upgraded culvert details are noticeable less.

4.4 Carseldine Channel

Between Lacey Road and the Railway the BCC Ultimate and JWP Option A profiles are considerably lower than the two WBM profiles. This is predominantly because of the additional flood storage created by the major channel works undertaken in conjunction with the Somerset Estate development.

Between the Railway and the upstream end of the Bill Brown Sports Field, the BCC Ultimate and JWP Option A profiles are considerably lower than the two WBM profiles. This is because the three former profiles incorporate the major channel work between Lacey Road and the Railway, which has the effect of attenuating the flow and reducing the discharge and hence flood levels downstream of the Railway.

Downstream of the Bill Brown Sports Field, both the WBM Upgrade M and JWP Option A flood profiles are substantially lower than the other three profiles. This is because these two options assumed major channel works within this area.

4.5 Telegraph Road Channel

Downstream of the Access Road, both the WBM Upgrade M and JWP Option A flood profiles are substantially lower than the other two profiles. This is because of the effects of the assumed major channel works to the Carseldine Channel downstream of the Bill Brown Sports Field.

Immediately upstream of the Access Road, the BCC Ultimate profile is higher than the other three profiles. This is because the current modelling incorporates the Access Road crossing and the previous modelling did not. Also, the discharge in the Telegraph Road Channel is higher in the current modelling because of the link channel, allowing flow distribution between the Carseldine Channel and the Telegraph Road Channel.



Comparison of 100yr ARI Flood Levels - Upper Carseldine Channel

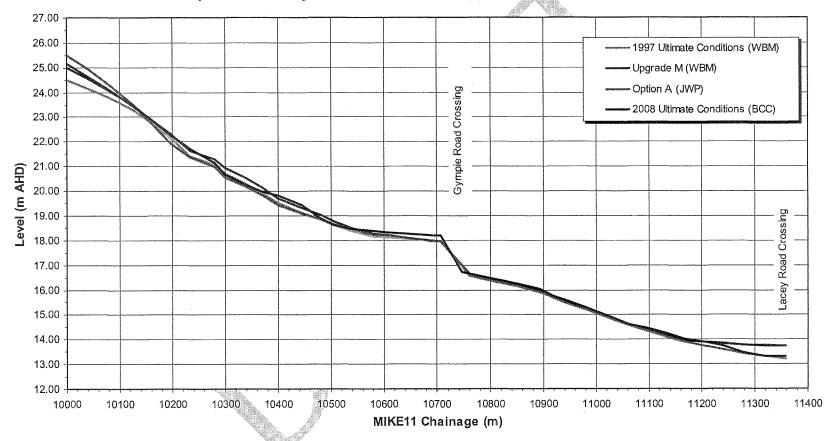


Figure 4.1 Comparison of 100yr ARI Flood Levels - Upper Carseldine Channel



Comparison of 100yr ARI Flood Levels - Gympie Road Channel

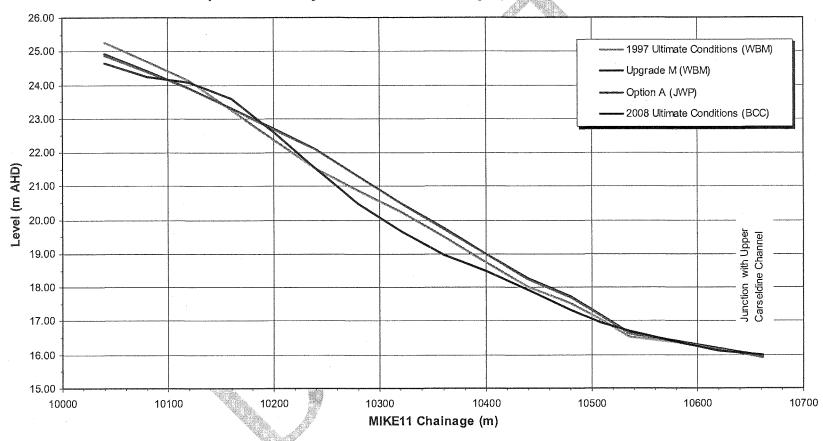


Figure 4.2 Comparison of 100yr ARI Flood Levels - Gympie Road Channel



Comparison of 100yr ARI Flood Levels - Carseldine Channel

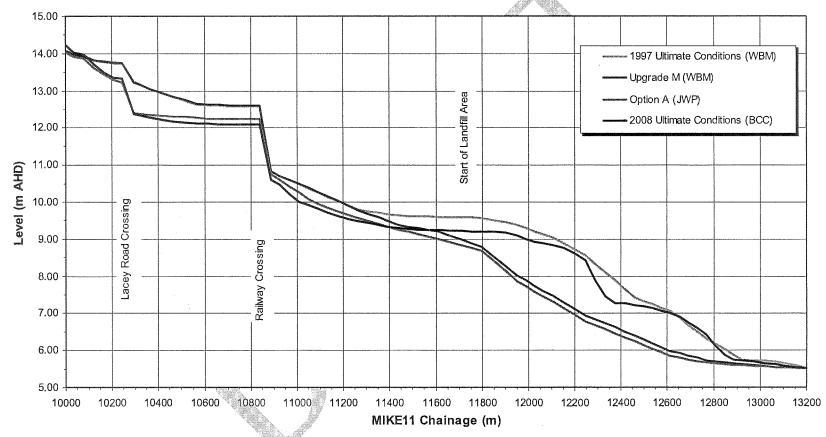


Figure 4.3 Comparison of 100yr ARI Flood Levels - Carseldine Channel



Comparison of 100yr ARI Flood Levels - Telegraph Road Channel

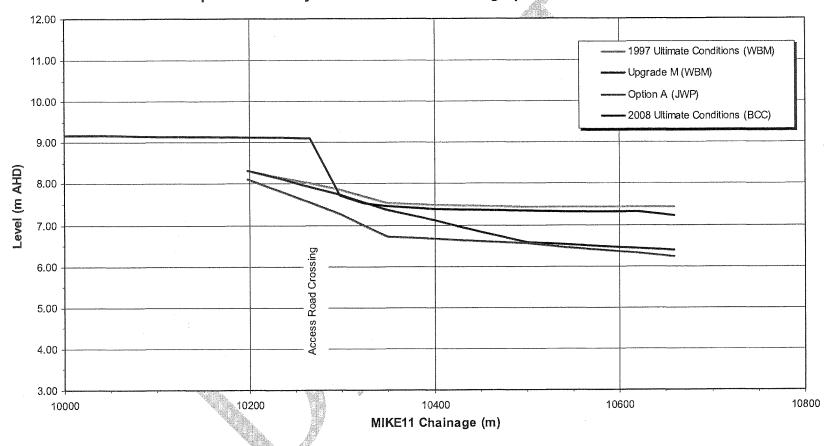


Figure 4.4 Comparison of 100yr ARI Flood Levels - Telegraph Road Channel



5.0 Delineation of Waterway Corridor

5.1 Existing Waterway Corridor

The existing waterway corridor for the Carseldine channel, as given in City Plan, is completely unsuitable having been based on default corridor requirements of 30 m either side of the waterway centre-line with no consideration being given to the hydraulic characteristics of the waterway and adjacent floodplains. As an ephemeral stream and lacking a well-defined low flow channel there is no continuous waterway centre line through the catchment and as a consequence, the waterway corridor is also non-contiguous.

5.2 Proposed Waterway Corridor

A proposed waterway corridor for the Carseldine Channel and associated tributaries is presented in Figure 6.1. The location of the waterway corridor is a conglomeration of previous agreements; logical limits created by the existing development conditions as at the commencement of this study in 2005 and estimated flood inundation extents from the modelling conducted as part of this study. The justification for the various segments of proposed corridor is as follows.

5.2.1 Beams to Gympie Road

An existing development to the east of the defined drainage channel effectively limits the waterway corridor to 30m on that side. On the opposite bank the waterway corridor is defined by the expected 100 year inundation line. Approaching Gympie Road and downstream of the development, the waterway corridor is also limited to the 100 year inundation line.

5.2.2 Gympie Road to Lacey Road

The Brisbane City Council had previously negotiated with land owners/developers for the contribution of a sizeable tract of land between Gympie Road and Lacey Road. This corridor takes into consideration the flooding characteristics and environmental values of the site. A separate, narrower corridor running parallel with Gympie Road provides a drainage path for overflows from the south to enter the main waterway.

5.2.3 Lacey Road to Railway

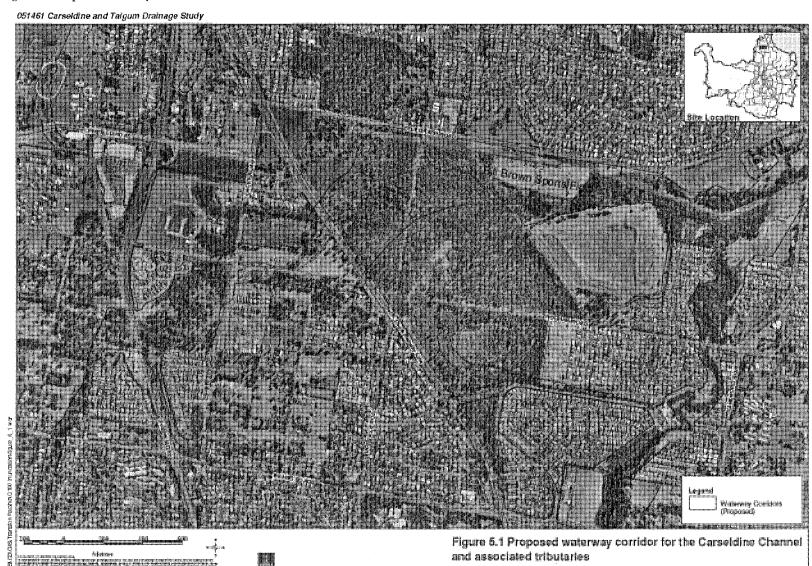
A significant amount of negotiation and hydraulic investigation was undertaken by the City Council in 2003 in relation to the delineation of a waterway corridor through this reach. To achieve a sustainable outcome in terms of flooding and the environment the developer was required to excavate a new channel and complete a controlled revegetation strategy.

5.2.4 Railway to Confluence with Cabbage Tree Creek

In keeping with the original intent of the outcomes of the Master Drainage Plan, the waterway corridor through the ULDA land and Council controlled land is broadly based on the 100 year inundation line. It is expected that this waterway corridor will be amended in the future in accordance with the ULDA land development and accompanying waterway modifications.



Figure 5.1 Proposed waterway corridor for the Carseldine Channel and associated tributaries





6.0 Conclusion

The flood modelling prepared for the Master Drainage Plan for the Carseldine and Taigum Catchments (WBM 1997) was updated to reflect the developments which have occurred in the vicinity of the Carseldine Channel at the time of the commencement of this study in 2005. The most notable developments which have occurred since the original study are Bridgeman Country Club Estate (upstream of Gympie Road); Tallowood Grove (downstream of Gympie Road); North Park Estate (between Gympie Road and Lacey Road) and Somerset Estate (between Lacey Road and North Coast Railway).

This study was conducted using RAFTS 2000 Version 6.5 and MIKE11 Version 2005 SP4. The RAFTS model was adjusted to allow for the changed overland flow conditions as a result of developments adjacent to the Landfill Channel and the catchment boundary was extended further south of Roghan Road to reflect new reality.

Where required, the outdated MIKE11 cross-sections were replaced / adjusted using as-built drawing information as well as BCC ALS data. The culvert crossings at Lacey Road and the North Coast Railway were updated to the current arrangements. A culvert / weir was added to Telegraph Road Channel to represent the Access Road to the Bill Brown Sports Field.

Modelling was undertaken for the Ultimate conditions with design flooding events ranging from the 2-yr ARI to the 100-yr ARI were simulated of which the results are presented in **Appendix A**. The simulations were run for the 60-minute, 120-minute and 180-minute storm events

Between Lacey Road the Northern Railway Line, the substantial earthworks undertaken as part of the Somerset Estate development result in significant attenuation in the mid to large ARI events. At the upstream end of the Bill Brown Sports Field there is a similar magnitude discharge in both the Carseldine Channel and the Telegraph Road Channel.

The flood immunity of the main transport crossings for Ultimate Conditions are:

- Gympie Road is less than 5-yr ARI
- Lacey Road is approximately 100-yr ARI
- North Coast Railway is greater than 100-yr ARI.

The ultimate design flood levels and flows are provided in **Appendix A**. The ultimate flood levels are based on the waterway corridor produced as **Figure 5.1**. The hydrological modelling was undertaken in line with best practice methodology, which included the latest available topographical and structural data available at the commencement of this project in 2005. The ultimate flood levels upstream of the North Coast Railway are considered to be representative of the existing catchment conditions, and are appropriate for adoption as design flood levels.

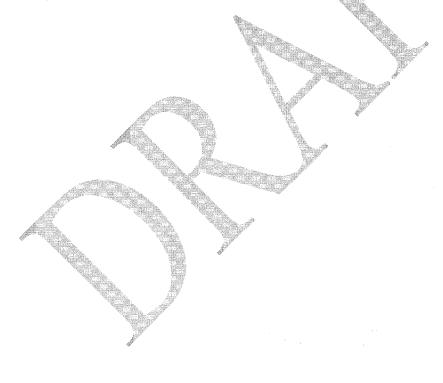
Recently completed development projects downstream of the North Coast Railway have not been modelled within the scope of this project. The flood modelling completed as part of this investigation should be further reviewed to ensure the reliability of design flood levels prior to adoption for the reach downstream of the North Coast Railway.

The major flooding problem areas identified as a result of this study are:

- Flood affected properties in the upstream section of the Upper Carseldine Channel, within the Bridgeman Country Club development
- Flood affected properties immediately upstream at Gympie Road
- Low flooding immunity of Gympie Road
- Low flooding immunity of Telegraph Road.

Recommendations for further work arising from this study are:

- Investigate options for upgrading the Gympie Road Culvert
- Investigate options for increasing the flood immunity of Telegraph Road
- Update MIKE11 cross-sections with new field survey when it is available; in particular, those which currently comprise as-built drawing and ALS data
- Update ALS information to include the recent developments to allow more accurate flood mapping.
- Update this study to account for the recent development downstream of the North Coast Railway line (when complete) which began after the commencement of this study.



APPENDIX A: Ultimate Conditions Results

	Chainage	AMTD		Flood	Level – Ultim	ate Condition	(m AHD)	
Reach	(m)	(m)	2-yr ARI	5-yr ARI	10-yr ARI	20-yr ARI	50-yr ARI	100-yr ARI
Upper Cars	10000	4343	24.32	24.55	24.66	24.79	24.90	25.00
Upper Cars	10126	4217	23.07	23.25	23.30	23.35	23.41	23.47
Upper Cars	10233	4110	21.47	21.55	21.59	21.63	21.67	21.72
Upper Cars	10280	4084	20.75	20.86	20.92	20.99	21.06	21.12
Upper Cars	10300	4064	20.09	20.26	20.35	20.46	20.56	20.66
Upper Cars	10340	4024	19.68	19.85	19.93	20.04	20.13	20.22
Upper Cars	10400	3964	19.26	19.43	19.51	19,62	19.72	19.81
Upper Cars	10444	3920	18.91	19.08	19.16	19.26	19.35	19.44
Upper Cars	10480	3884	18.46	18.59	18.66	18.74	18.81	18.89
Upper Cars	10504	3860	18.18	18.33	18.40	18.47	18.55	18.61
Upper Cars	10540	3824	17.99	18.18	18.25	18.33	18.41	18.47
Upper Cars	10580	3784	17.90	18.10	18.18	18.26	18.33	18.39
Upper Cars	10640	3724	17.85	18.01	18.08	18.15	18.21	18.27
Upper Cars	10692	3672	17.82	17.96	18.02	18.08	18.14	18.19
Upper Cars	10707	3657	17.81	17.96	18.02	18.08	18.14	18.19
* *	pie Road Cul			ANAMAN				A STATE OF THE STA
Upper Cars	10747	3617	16.45	16.54	16.58	16.63	16.67	16.70
Upper Cars	10761	3596	16.39	16.48	16.52	16.57	16.61	16.64
Upper Cars	10893	3464	15.80	15.86	15.90	15.94	15.97	16.01
Upper Cars	10946	3411	15.32	15.38	15.42	15.46	15.49	15.53
Upper Cars	11064	3293	14.39	14.46	14.49	14.53	14.57	14.61
Upper Cars	11167	3190	13.68	13.79	13.84	13.90	13.95	13.99
Upper Cars	11278	3079	13.08	13.18	13.25	13.33	13.41	13.49
Upper Cars	11359	2998	12.17	12.51	12.70	12.92	13.14	13.33
Opper Cars	44.07	2220		374 Salin Sala				
Gympie Rd	10040	596	24.41	24.47	24.51	24.56	24.59	24.63
Gympie Rd	10080	556	23.90	23.99	24.04	24.11	24.17	24.24
Gympie Rd	10120	516	23.69	23.81	23.87	23.95	24.01	24.08
Gympie Rd	10160	477	23.29	23.37	23.42	23.48	23.53	23.58
Gympie Rd	10200	437	22.28	22.37	22.42	22.48	22.53	22.59
Gympie Rd	10240	397	21.20	21.30	21.34	21.40	21.46	21.51
Gympie Rd	10280	356	20.13	20.23	20.28	20.35	20.41	20.47
Gympie Rd	10320	320	19.35	19.45	19.50	19.57	19.63	19.69
Gympie Rd	10360	279	18.59	18.71	18.77	18.85	18.90	18.96
Gympie Rd	10400	241	18.17	18.26	18.32	18.38	18.44	18.49
Gympie Rd	10440	200	17.63	17.72	17.76	17.82	17.87	17.92
Gympie Rd Gympie Rd	10480	156	17.14	17.20	17.23	17.27	17.30	17.33
Gympie Rd Gympie Rd	10536	110	16.52	16.57	16.60	16.63	16.66	16.69
Gympie Rd	10662	0	15.80	15.86	15.90	15.94	15.97	16.01
Sympic Rd	10002							
T'graph Rd	10000	N/A	8.63	8.82	8.88	8.95	9.03	9.09
T'graph Rd	10198	N/A	8.55	8.75	8.82	8.89	8.98	9.04
T'graph Rd	10198	N/A	8.52	8.73	8.80	8.88	8.96	9.03
	ess Road Cross		5.52			1 2.00		
T'graph Rd	10298	N/A	7.19	7.36	7.41	7.48	7.55	7.61
T'graph Rd	10258	N/A	6.83	7.03	7.13	7.16	7.38	7.45
ı grapır Ku	10330	TA/\[\frac{1}{2}\]	0.03	1.05	1 /.12	L	1 7.50	1

Reach	Chainage	AMTD		Flood	Level – Ultim	ate Condition	(m AHD)	
Reacii	(m)	(m)	2-yr ARI	5-yr ARI	10-yr ARI	20-yr ARI	50-yr ARI	100-yr ARI
T'graph Rd	10500	N/A	6.59	6.80	6.90	7.03	7.16	7.25
T'graph Rd	10659	N/A	6.46	6.66	6.75	6.87	6.99	7.08
Landfill	10000	N/A	8.56	8.65	8.70	8.77	8.81	8.84
Landfill	10165	N/A	8.53	8.63	8.69	8.76	8.80	8.83
Landfill	10245	N/A	8.36	8.45	8.50	8.55	8.60	8.64
Landfill	10445	N/A	8.00	8.07	8.10	8.14	8.19	8.24
Landfill	10625	N/A	7.27	7.39	7.45	7.54	7.62	7.70
Landfill	10680	N/A	6.95	7.03	7.07	7.13	7.19	7.25
Landfill	10770	N/A	6.26	6.30	6.33	6.36	6.40	6.44
Landfill	10820	N/A	4.88	5.12	5.24	5.37	5.54	5.70
			Harrista (Maria)					
Lacey	0	N/A	14.39	14.46	14.49	14.53	14.57	14.61
Link 1	100	N/A	13.88	14.00	14.06	14.12	14.18	14.22
Lacey	0	N/A	13.68	13.79	13.84	13.90	13.95	13.99
Link 2	100	N/A	13.67	13.78	13.83	13.88	13.93	13.97
Lacey	0	N/A	13.08	13.18	13.25	13.33	13.41	13.49
Link 3	100	N/A	12.98	13.17	13.24	13.32	13.40	13.48
Carseldine	10000	N/A	13.88	14.00	14.06	14.12	14.18	14.22
Carseldine	10078	N/A	13.67	13.78	13.83	13.88	13.93	13.97
Carseldine	10172	N/A	12.98	13.17	13.24	13.32	13.40	13.48
Carseldine	10243	2945	12.17	12.51	12.70	12.92	13.14	13.33
Lac	ey Road Culv	ert						
Carseldine	10293	2895	11.81	11.98	12.07	12.18	12.29	12.37
Carseldine	10364	2846	11.74	11.90	11.99	12.10	12.20	12.28
Carseldine	10414	2796	11.65	11.82	11.90	12.01	12.11	12.21
Carseldine	10464	2746	11.59	11.76	11.84	11.95	12.05	12.17
Carseldine	10514	2696	11.53	11.69	11.77	11.86	11.99	12.14
Carseldine	10564	2646	11.39	11.53	11.61	11.76	11.96	12.12
Carseldine	10654	2556	11.24	11.41	11.54	11.72	11.93	12.10
Carseldine	10705	2505	11.16	11.39	11.53	11.71	11.93	12.09
Carseldine	10768	2442	11.10	11.36	11.51	11.70	11.92	12.09
Carseldine	10837	2373	11.08	11.36	11.51	11.69	11.92	12.09
Nort	h Coast Railv	vay						
Carseldine	10889	2321	10.48	10.52	10.53	10.56	10.58	10.59
Carseldine	10924	2286	10.33	10.36	10.38	10.40	10.44	10.46
Carseldine	11091	2119	9.70	9.74	9.76	9.78	9.80	9.82
Carseldine	11267	1943	9.33	9.37	9.39	9.42	9.45	9.47
Carseldine	11438	1772	9.03	9.08	9.11	9.15	9.21	9.25
Carseldine	11609	1601	8.89	8.96	9.00	9.05	9.12	9.17
Carseldine	11799	1411	8.83	8.90	8.94	9.00	9.07	9.13
Carseldine	11949	1261	8.75	8.81	8.85	8.90	8.97	9.02
Carseldine	12103	1107	8.54	8.60	8.64	8.68	8.74	8.79
Carseldine	12245	965	8.20	8.23	8.25	8.29	8.33	8.37
Carseldine	12460	750	6.46	6.66	6.75	6.87	6.99	7.08
Carseldine	12611	599	6.27	6.46	6.55	6.66	6.77	6.84
Carseldine	12769	441	5.74	5.91	5.99	6.10	6.20	6.28

Reach	Chainage	AMTD	Flood Level – Ultimate Condition (m AHD)							
	(m)	(m)	2-yr ARI	5-yr ARI	10-yr ARI	20-yr ARI	50-yr ARI	100-yr ARI		
Carseldine	12922	288	4.88	5.12	5.24	5.37	5.54	5.70		
Carseldine	13066	144	4.58	4.93	5.08	5.22	5.41	5.60		
Carseldine	13200	10	4.45	4.84	4.99	5.13	5.32	5.52		
Landfill	0	N/A	8.83	8.90	8.94	9.00	9.07	9.13		
Link	100	N/A	8.63	8.82	8.88	8.95	9.03	9.09		





Reach	Chainage		Disc	charge – Ultin	nate Condition	(m^3/s)	
Reacn	(m)	2-yr ARI	5-yr ARI	10-yr ARI	20-yr ARI	50-yr ARI	100-yr ARI
Upper Cars	10021	12.7	17.8	20.8	24.8	28.7	33.1
Upper Cars	10063	12.7	17.8	20.7	24.7	28.7	33.0
Upper Cars	10105	12.7	17.8	20.7	24.8	28.7	33.0
Upper Cars	10144	12.7	17.8	20.7	24.7	28.5	32.9
Upper Cars	10180	12.7	17.8	20.7	24.7	28.5	32.9
Upper Cars	10215	12.7	17.7	20.7	24.6	28.5	32.8
Upper Cars	10257	12.7	17.7	20.7	24.6	28.4	32.8
Upper Cars	10290	12.7	17.7	20.6	24.6	28.4	32.8
Upper Cars	10320	12.6	17.7	20.6	24.6	28.4	32.8
Upper Cars	10355	12.7	17.7	20.7	24.6	28.4	32.8
Upper Cars	10385	12.7	17.7	20.6	24.6	28.4	32.7
Upper Cars	10422	12.6	17.7	20.6	24.5	28.3	32.6
Upper Cars	10462	12.6	17.7	20.6	24.5	28.3	32.6
Upper Cars	10492	12.6	17.7	20.6	24.5	28.3	32.6
Upper Cars	10522	12.6	17.7	20.7	24.6	28.4	32.7
Upper Cars	10560	12.7	17.9	20.9	24.8	28.6	33.0
Upper Cars	10595	24.0	32.6	38.2	45.4	51.8	59.0
Upper Cars	10625	23.3	32.3	38.1	45.1	51.9	58.7
Upper Cars	10653	22.0	32.3	38.2	45.0	52.0	58.7
Upper Cars	10679	20.7	32.3	38.3	45.1	52.1	58.9
Upper Cars	10700	23.6	37.7	44.6	53.3	61.3	70.0
Upper Cars	10727	23.5	37.5	44.6	53.3	61.3	70.0
Upper Cars	10754	23.5	37.3	44.3	52.9	61.1	69.5
Upper Cars	10783	23.3	36.9	43.9	52.5	60.7	69.1
Upper Cars	10827	23.1	36.2	43.3	51.8	60.0	68.2
Upper Cars	10871	22.9	35.7	42.7	51.2	59.6	67.8
Upper Cars	10906	30.4	45.1	53.6	64.3	75.5	86.4
Upper Cars	10933	30.3	45.1	53.5	64.2	75.4	86.2
Upper Cars	10966	30.3	44.9	53.3	64.0	75.2	86.1
Upper Cars	11005	30.2	44.7	53.1	63.8	75.0	85.9
Upper Cars	11044	30.1	44.5	52.9	63.5	74.7	85.7
Upper Cars	11081	17.8	28.7	35.2	43.6	52.5	61.2
Upper Cars	11116	17.6	28.5	34.9	43.4	52.3	61.1
Upper Cars	11150	17.5	28.1	34.6	43.1	52.1	60.9
Upper Cars	11186	5.5	12.2	16.5	22.6	29.2	35.8
Upper Cars	11223	5.4	12.0	16.2	22.1	28.7	35.3
Upper Cars	11260	5.4	11.9	16.1	21.7	28.5	35.1
Upper Cars	11298	1.1	4.7	8.7	13.8	19.9	27.9
Upper Cars	11339	1.1	4.6	8.3	13.0	18.7	26.0
y a department							
Gympie Rd	10060	6.5	8.8	10.3	12.3	14.1	16.1
Gympie Rd	10100	6.2	8.5	9.8	11.8	13.6	15.6
Gympie Rd	10140	6.1	8.3	9.7	11.7	13.5	15.5
Gympie Rd	10180	6.1	8.3	9.7	11.7	13.5	15.4
Gympie Rd	10220	6.0	8.3	9.7	11.6	13.4	15.4
Gympie Rd	10260	6.0	8.2	9.6	11.5	13.3	15.3
Gympie Rd	10300	6.0	8.2	9.6	11.5	13.3	15.2

n i	Chainage		Disc	charge – Ultin	nate Condition	(m ³ /s)	
Reach	(m)	2-yr ARI	5-yr ARI	10-yr ARI	20-yr ARI	50-yr ARI	100-yr ARI
Gympie Rd	10340	5.9	8.1	9.5	11.4	13.2	15.1
Gympie Rd	10380	5.9	8.1	9.5	11.4	13.2	15.1
Gympie Rd	10420	5.8	8.0	9.4	11.3	13.1	15.0
Gympie Rd	10460	5.8	8.0	9.3	11.2	13.0	14.9
Gympie Rd	10494	5.7	7.9	9.3	11.1	13.0	14.8
Gympie Rd	10522	5.7	7.8	9.2	11.1	12.9	14.8
Gympie Rd	10557	5.5	7.6	9.0	10.9	12.7	14.6
Gympie Rd	10599	5.3	7.5	8.8	10.7	12.5	14.4
Gympie Rd	10641	5.2	7.4	8.7	10.6	12.5	14.4
T'graph Rd	10025	11.3	16.3	17.8	19.6	22.2	24.2
T'graph Rd	10074	11.2	16.1	17.4	19.5	22.1	24.1
T'graph Rd	10124	11.1	15.9	17.4	19.5	22.1	24.0
T'graph Rd	10173	11.0	15.7	17.3	19.4	22.0	23.9
T'graph Rd	10215	10.9	15.6	17.3	19.4	22.0	23.9
T'graph Rd	10249	10.9	15.6	17.2	19.4	22.0	23.9
T'graph Rd	10282	10.9	15.6	17.2	19,4	22.0	23.9
T'graph Rd	10311	10.9	15.6	17.2	19.4	22.0	23.9
T'graph Rd	10337	10.9	15.6	17.2	19.4	22.0	23.9
T'graph Rd	10375	21.2	27.1	30.7	35.6	40.2	43.1
T'graph Rd	10425	21.1	27.1	30.7	35,6	40.2	43.1
T'graph Rd	10475	21.0	27.0	30.6	35.5	40.1	43.1
T'graph Rd	10520	20.9	27.0	30.6	35.5	40.1	43.1
T'graph Rd	10560	20.8	27.0	30.6	35.5	40.1	43.1
T'graph Rd	10599	20.7	26.9	30.6	35.5	40.0	43.1
T'graph Rd	10639	20.6	26.9	30.6	35.5	40.1	43.1
Tally States							
Landfill	10021	0.1	0.1	0.1	0.1	0.1	0.1
Landfill	10062	0.1	0.2	0.2	0.3	0.3	0.3
Landfill	10103	0.2	0.3	0.4	0.5	0.5	0.6
Landfill	10144	0.3	0.5	0.6	0.7	0.8	0.9
Landfill	10185	1.9	2.5	2.8	3.3	4.1	5.0
Landfill	10225	1.9	2.4	2.8	3.2	4.1	4.9
Landfill	10270	1.8	2.3	2.7	3.2	4.0	4.7
Landfill	10320	1.7	2.3	2.6	3.1	3.9	4.5
Landfill	10370	1.7	2.2	2.6	3.1	3.8	4.3
Landfill	10420	1.7	2.2	2.6	3.0	3.7	4.3
Landfill	10468	1.7	2.2	2.6	3.0	3.7	4.3
Landfill	10513	1.7	2.2	2.5	3.0	3.7	4.3
Landfill	10558	1.7	2.2	2.6	3.1	3.8	4.4
Landfill	10603	1.8	2.4	2.7	3.3	4.0	4.7
Landfill	10639	3.1	4.2	4.7	5.7	6.7	7.7
Landfill	10666	3.1	4.2	4.7	5.6	6.7	7.7
Landfill	10703	3.1	4.2	4.7	5.6	6.7	7.7
Landfill	10748	3.1	4.2	4.7	5.6	6.7	7.7
Landfill	10748	3.1	4.2	4.7	5.6	6.7	7.7
Landfill	10/93	3.1	1 4.2	4./	٥.٥	0.7	1.1

	Chainage		Dise	charge – Ultin	nate Condition	(m ³ /s)	
Reach	(m)	2-yr ARI	5-yr ARI	10-yr ARI	20-yr ARI	50-yr ARI	100-yr ARI
Lacey Link 1	50	12.2	15.6	17.5	19.7	22.1	24.3
Lacey Link 2	50	11.9	15.8	17.9	20.3	22.6	24.8
Lacey Link 3	50	8.2	12.8	14.1	16.2	18.9	20.4
Carseldine	10020	12.2	15.6	17.5	19.7	22.1	24.2
Carseldine	10059	12.1	15.5	17.4	19.6	22.0	24.1
Carseldine	10102	24.0	31.1	35.1	39.7	44.4	48.8
Carseldine	10149	23.9	31.1	35.0	39.7	44.4	48.7
Carseldine	10190	32.1	43.7	48.8	55.5	62.9	68.6
Carseldine	10225	32.0	43.5	48.5	\$ 54.5	61.1	65.0
Carseldine	10268	32.9	47.6	56.4	67.1	77.5	86.7
Carseldine	10311	32.4	46.8	55.4	66.3	76.9	86.2
Carseldine	10346	32.2	46.3	54.8	65.7	76.6	85.9
Carseldine	10389	34.1	49.2	√ 58.3	70.1	82.0	92.0
Carseldine	10439	33.8	48.6	57.7	69.5	81.5	91.4
Carseldine	10489	36.8	53.2	63.1	76.1	89.7	100.6
Carseldine	10539	36.6	53.0	62.8	75.8	88.9	99.2
Carseldine	10587	36.5	52.7	62.4	75.0	87.3	96.7
Carseldine	10632	36.3	52.2	61.7	73.4	84.4	92.5
Carseldine	10680	36.2	51.5	60,3	70.7	79.9	86.6
Carseldine	10721	37.5	52.5	60.9	70.7	79.7	86.3
Carseldine	10752	36.2	49.3	56.6	65.0	72.8	78.5
Carseldine	10785	33.7	44.6	50.6	57.5	64.1	68.9
Carseldine	10820	30.2	38.4	43.0	48.6	54.9	60.3
Carseldine	10871	27.6	34.4	38.3	43.5	49.8	54.9
Carseldine	10907	27.6	34.4	38.3	43.5	49.8	54.9
Carseldine	10945	27.6	34.4	38.3	43.4	49.8	54.8
Carseldine	10987	27.6	34.4	38.3	43.4	49.8	54.8
Carseldine	11028	27.5	34.4	38.3	43.4	49.7	54.8
Carseldine	11070	27.5	34.4	38.3	43.3	49.7	54.7
Carseldine	11113	27.5	34.3	38.2	43.3	49.7	54.7
Carseldine	11157	27.5	34.3	38.1	43.2	49.6	54.6
Carseldine	11201	27.4	34.2	38.0	43.2	49.4	54.4
Carseldine	11245	27.3	34.1	37.9	43.0	49.2	54.2
Carseldine	11288	27.2	33.9	37.7	42.8	49.0	53.8
Carseldine	11331	27.0	33.8	37.6	42.6	48.7	53.5
Carseldine	11374	27.0	33.7	37.4	42.4	48.4	53.1
Carseldine	11417	26.9	33.5	37.2	42.1	48.0	52.6
Carseldine	11459	26.7	33.2	36.8	41.7	47.3	51.8
Carseldine	11502	26.2	32.7	36.2	40.9	46.4	50.8
Carseldine	11545	25.6	32.0	35.5	40.0	45.4	49.8
Carseldine	11588	24.9	31.4	34.9	39.1	44.5	49.0
Carseldine	11633	25.3	32.3	36.0	40.5	46.5	51.5
Carseldine	11680	24.9	32.0	35.4	39.9	46.0	51.0
Carseldine	11728	24.6	31.7	34.9	39.5	45.8	50.8

Reach	Chainage	Discharge – Ultimate Condition (m³/s)					
	(m)	2-yr ARI	5-yr ARI	10-yr ARI	20-yr ARI	50-yr ARI	100-yr ARI
Carseldine	11775	24.5	31.6	34.7	39.2	45.7	50.6
Carseldine	11824	14.1	16.7	18.6	21.4	25.7	29.0
Carseldine	11874	14.0	16.6	18.5	21.3	25.6	29.0
Carseldine	11924	14.0	16.6	18.5	21.3	25.7	29.1
Carseldine	11968	15.3	18.4	20.7	24.0	28.9	32.7
Carseldine	12007	15.3	18.4	20.7	24.0	28.9	32.7
Carseldine	12045	15.2	18.4	20.7	24.0	28.8	32.7
Carseldine	12084	15.2	18.4	20.6	24.0	28.8	32.7
Carseldine	12127	15.1	18.4	20.6	23.9	28.8	32.6
Carseldine	12174	15.1	18.3	20.6	23.9	28.8	32.6
Carseldine	12221	15.1	18.3	20.6	23.9	28.8	32.6
Carseldine	12267	15.3	18.6	20.9	24.2	29.1	33.0
Carseldine	12310	15.3	18.6	20.9	24.2	29.1	33.0
Carseldine	12353	15.3	18.6	20.9	24.2	29.1	33.0
Carseldine	12396	15.3	18.6	20.9	24.3	29.2	33.1
Carseldine	12439	15.2	18.6	20.9	24.3	29.2	33.1
Carseldine	12479	29.5	38.4	43.7	50.9	58.4	63.9
Carseldine	12517	29.5	38.4	43.7	50.9	58.4	63.9
Carseldine	12554	29.4	38.4	43.7	50.9	58.4	63.9
Carseldine	12592	29.4	38.4	43.7	50.9	58.4	63.9
Carseldine	12631	29.6	38.7	44.1	51.3	58.9	64.6
Carseldine	12670	29.6	38.7	44.0	51.3	58.9	64.6
Carseldine	12710	29.6	38.7	44.0	51.3	58.9	64.6
Carseldine	12749	29.6	38.7	44.0	51.3	58.9	64.6
Carseldine	12788	29.6	38.7	44.0	51.3	59.0	64.6
Carseldine	12826	29.6	38.7	44.1	51.3	59.0	64.6
Carseldine	12865	29.6	38.7	44.1	51.3	59.0	64.6
Carseldine	12903	29.5	38.7	44.1	51.4	59.0	64.7
Carseldine	12946	34.4	44.8	50.9	59.5	69.1	76.6
Carseldine	12994	34.4	44.8	51.0	59.5	69.2	76.6
Carseldine	13042	34.4	44.8	51.0	59.5	69.2	76.7
Carseldine	13088	35.5	46.4	52.8	61.7	72.0	80.0
Carseldine	13133	35.6	46.4	52.8	61.7	72.0	80.0
Carseldine	13178	35.6	46.4	52.8	61.7	72.0	80.0
Landfill Link	50	10.4	14.9	15.9	17.7	20.0	21.6